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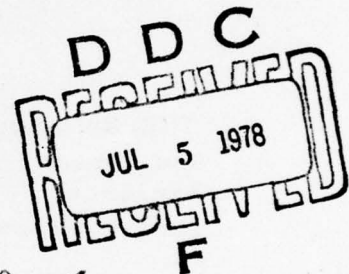
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GENERAL AVIATION AIRPLANE
STRUCTURAL CRASHWORTHINESS USER'S MANUAL

VOLUME I
PROGRAM "KRASH" THEORY

Max A. Gamon



February 1978

Final Report

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16. Abstract This document provides a comprehensive description of program KRASH, as modified under Contract DOT-FA75-WA-3707. Included in this User's Manual are the following sections: 1. Program KRASH (Description and Theory), 2. Program Controls, and Listing. The User's Manual is part one of a three-volume document. The second volume describes modeling techniques applicable to program KRASH to assist in the development of improved structural crashworthiness designs, as well as the detailed input requirements and output capabilities of KRASH. Volume III contains general background data regarding structural crashworthiness design. Each volume has been established in such a manner that they can readily be updated as more data becomes available. The subject matter contained within each section can be expanded or revised, as necessary, without affecting the other sections. Each section contains its own numbering system which facilitates the task of updating the document.		
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METRIC CONVERSION FACTORS

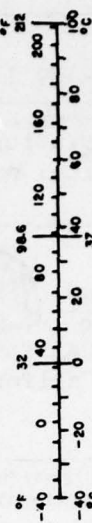
Approximate Conversions to Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
LENGTH				
in	inches	2.5	centimeters	cm
ft	feet	30	centimeters	cm
yd	yards	0.9	meters	m
mi	miles	1.6	kilometers	km
AREA				
m ²	square inches	6.5	square centimeters	cm ²
ft ²	square feet	0.09	square meters	m ²
yd ²	square yards	0.8	square meters	m ²
mi ²	square miles	2.6	square kilometers	km ²
	acres	0.4	hectares	ha
MASS (weight)				
oz	ounces	28	grams	g
lb	pounds	0.45	kilograms	kg
	short tons (2000 lb)	0.9	tonnes	t
VOLUME				
teaspoon	teaspoons	5	milliliters	ml
Tablespoon	tablespoons	15	milliliters	ml
fl oz	fluid ounces	30	milliliters	ml
c	cups	0.24	liters	l
pt	pints	0.47	liters	l
qt	quarts	0.95	liters	l
gal	gallons	3.8	liters	l
ft ³	cubic feet	0.03	cubic meters	m ³
yd ³	cubic yards	0.76	cubic meters	m ³
TEMPERATURE (exact)				
°F	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	°C

*1 in = 2.54 (exactly). For other exact conversions and more detailed tables, see NBS Misc. Publ. 286, Units of Weights and Measures, Price \$2.25. SO 332-10-101-0-286.

Approximate Conversions from Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
LENGTH				
mm	millimeters	0.04	inches	in
cm	centimeters	0.4	inches	in
m	meters	3.3	feet	ft
m	meters	1.1	yards	yd
km	kilometers	0.6	miles	mi
AREA				
cm ²	square centimeters	0.16	square inches	in ²
m ²	square meters	1.2	square yards	yd ²
km ²	square kilometers	0.4	square miles	mi ²
ha	hectares (10,000 m ²)	2.5	acres	
MASS (weight)				
g	grams	0.035	ounces	oz
kg	kilograms	2.2	pounds	lb
t	tonnes (1000 kg)	1.1	short tons	
VOLUME				
ml	milliliters	0.03	fluid ounces	fl oz
l	liters	2.1	pints	pt
l	liters	1.06	quarts	qt
l	liters	0.26	gallons	gal
m ³	cubic meters	35	cubic feet	ft ³
m ³	cubic meters	1.3	cubic yards	yd ³
TEMPERATURE (exact)				
°C	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature	°F



FOREWORD

This report was prepared by the Lockheed-California Company under contract DOT-FA75-WA-3707. The report contains a partial description of the effort performed as Task II of a three task effort. The Task II report covers the period from July 1976 to December 1977. The work was administrated under the direction of the Federal Aviation Administration with H. Spicer acting as Technical Monitor.

The project leader was Gil Wittlin of the Lockheed-California Company. Important contributions were made to the program by the Cessna Aircraft Company under the direction of D.J. Ahrens and W.B. Bloedel. M.A. Gamon and W. L. LaBarge participated in the development of the User's Manual. The Lockheed effort was supervised by J.E. Wignot (Dynamics Loads Group) and R.F. O'Connell (Aeromechanics Department).

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SUMMARY

This document provides a comprehensive description of program KRASH, as modified under Contract DOT-FA75-WA-3707. Included in this User's Manual are the following sections:

1. Program KRASH; Description and Theory
2. Program Controls and Listing

The User's Manual is part one of a three-volume document. The second volume describes modeling techniques applicable to program KRASH to assist in the development of improved structural crashworthiness designs, as well as the detailed input requirements and output capabilities of KRASH. Volume III contains general background data regarding structural crashworthiness design. Each volume has been established in such a manner that they can readily be updated as more data becomes available. The subject matter contained within each section can be expanded or revised, as necessary, without affecting the other sections. Each section contains its own numbering system which facilitates the task of updating the document.

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LIST OF SYMBOLS

$[A_\beta]$	Rotation transformation matrix from ground axes to slope axes
A_i, B_i, C_i	Terms used in Euler's Equations of motion (1-112)
$[A_i]$	Rotation transformation matrix from body axes to ground axes
$[\bar{A}_i]$	Matrix relating $(\dot{\phi}, \dot{\theta}_i, \dot{\psi}_i)$ to (p_i, q_i, r_i) in Equation (1-153)
$[\dot{A}_i]$	Time derivative of $[A_i]$
$[A''_i]$	Rotation transformation matrix from ith body axes to cg axes
A_{ij}	Cross-sectional area for beam ij
$[A_{ij}]$	Rotation transformation matrix from beam ij axes to ground axes
$[A']$	Rotation transformation matrix from cg axes to ground axes
$[AIJTAI]$	Rotation transformation matrix from mass i axes to beam axes
$[AIJTAJ]$	Rotation transformation matrix from mass j axes to beam y axes
$(ax, ay, az)_i$	Translational acceleration components of mass m_i , body axes
CE	External spring crushing energy
\bar{C}_{ij}	Damping ratio for beam ij (actual damping/critical damping)
C_{ik}	End point of kth spring of ith mass
C'_{ik}	Ground contact point of kth spring on ith mass

C_k	Damping contact $2\xi_{ij}/\omega_k$
$(d_1, \dots, d_6)_{ij}$	Incremental relative beam deflections and rotations (j - i)
$(d_7, d_8, d_9)_{ij}$	Incremental beam rotation sums (j + i)
$[D']$	Derivative matrix used in Equation (1-149)
DE	Damping energy
$DELG_{iKM}$	Ground deflection beneath spring iKM
$\{dF_i\}$	$(dFx, dFy, dFz, dM\phi, dM\theta, dM\psi)_i$
$\{dF'_i\}$	Incremental nonlinear strain forces and moments at beam end i
$(dFx, dFy, dFz)_i$	Incremental linear strain forces at beam end i
$[D_i]$	Derivative matrix used in Equation (1-3)
$(dM\phi, dM\theta, dM\psi)_i$	Incremental linear strain moments at beam end i
$(dpin, dqin, drin)_i$	Incremental rotation of mass m_i , body axes
DRI	Dynamic Response Index
dvc_{ijk}	Ground axes components of vector from m_i to C_{ik}
dvc'_{ijk}	Ground axes components of vector from C'_{ik} to C_{ik}
$dvcsl_{ijk}$	Slope axes components of vector from m_i to C_{ik}
$dvcsl'_{ijk}$	Slope axes components of vector from C'_{ik} to C_{ik}
$\{dv_i\}$	$(dx, dy, dz, d\phi, d\theta, d\psi)_i$
$(dx, dy, dz)_i$	Incremental changes (over time) of ground coordinate of mass m_i . Also used as incremental beam deflections of beam end i, beam axes.
$(dxmod, dymod, dzmod)_i$	Incremental changes (over time) of ground coordinates of i end of beam i,j
$(dxup, dyup, dzup)_{iM}$	Incremental changes (over time) of ground coordinates of node point iM
$(dx', dy', dz')_i$	Incremental deflections of mass m_i , body axes

$(d\phi, d\theta, d\psi)_i$	Incremental rotations of beam end i, beam axes
E_{ij}	Modulus of elasticity for beam ij
E_{TOT}	Total system energy
$\{FD_i\}$	Damping forces and moments at beam end i
FE	Friction energy
$f_{g_{ikM}}$	Ground flexibility for spring ikM
$\{F'_i\}$	Total (over time) nonlinear strain forces and moments at beam end i
$F_{plow_{ik}}$	Plowing force for external spring ik
$\{FS_i\}$	Total strain plus damping forces and moments at beam end i, beam axes
$\{FS'_i\}$	Total strain plus damping forces acting on mass m_i , mass axes
FSP_{ijk}	Body i axes components of spring force at ground contact point C'_{ik}
$FSPO_{ik}$	Axial compressive force in kth spring on ith mass
\overline{FSPO}_{ik}	Value of $FSPO_{ik}$ at time of loading reversal
$FSPOI_{ik}$	Value of $FSPO_{ik}$ in first nonlinear region
$FSPOF_{ik}$	Value of $FSPO_{ik}$ in second nonlinear region
G	Center-of-gravity of total vehicle
G_{ij}	Modulus of rigidity for beam ij
H	Origin of airplane coordinate system (F.S.O, B.L.O, W.L.O)
$He_{xi}, He_{yi}, He_{zi}$	Angular momenta of m_i due to rotation of masses internal to m_i
$[I_i]$	Inertia matrix for mass m_i
$(inp, inq, inr)_i$	Time integral of $(p, q, r)_i$, angular velocity components of m_i

I_{xi}, I_{yi}, I_{zi}	Moments of inertia of lumped mass m_i , about ith body fixed axes
$I_{xyi}, I_{yzi}, I_{zxi}$	Products of inertia of lumped mass m_i , about ith body fixed axes
I_{yij}, I_{zij}	Area moments of inertia for beam ij
J_{ij}	Torsional stiffness factor for beam ij
KE	Kinetic energy
$k_{e_{ik}}$	Linear bottoming stiffness for external spring ik
$[K_{ij}]$	Linear stiffness matrix for beam ij
$[KR_{ij}]$	Six by six diagonal stiffness reduction matrix for beam ij
$(k_x, k_y, k_z, k_\phi, k_\theta, k_\psi)_{ij}$	Diagonal elements of stiffness matrix for beam ij
$(k_{y\psi}, k_{z\theta})_{ij}$	Coupled bending elements of stiffness matrix for beam ij
l_{ci}	Aerodynamic lift constant
LIFT _i	Aerodynamic lift on m_i , positive up, in ground axes
l_{ij}	Length of beam ij
l_{ik}	Length of vector from m_i to ground contact point C'_{ik}
$\bar{l}_{xi}, \bar{l}_{yi}, \bar{l}_{zi} (\bar{l}_{ik})$	Free length of kth spring on ith mass
m_i	ith lumped mass
μ_{ik}	Ground-spring friction coefficient for kth spring on ith mass
N, NM	Total number of lumped masses
\bar{n}_{ik}	Unit vector triad fixed in ith body coordinate system
$\bar{n}_x, \bar{n}_y, \bar{n}_z$	Unit vector triad fixed in ground coordinate system
O	Origin of ground coordinate system

p', q', r'	c.g. axes components of initial ($t=0$) vehicle angular velocity vector
PE	Potential energy
p_i, q_i, r_i	i th body axes components of absolute angular velocity vector of mass i
Q	Beam sectional shape factor relating torsional shear stress to applied moment
r_{xi}, r_{yi}, r_{zi} $(r_x, r_y, r_z)_{iM}$	Distances from airplane cg to m_i , airplane axes Body axes components of vector from mass m_i to node point iM
SE	Strain energy
SI, SA, SB, SF	Input constants defining transition points in external spring load-deflection curve for spring ikM
SIFL, SAFL, SBFL, SFFL	Constants defining transition points in external spring load deflections curve for spring ikM , including ground flexibility
s_{ik}	External spring axial compression, k th spring on i th mass
\dot{s}_{ik}	External spring axial velocity
\bar{s}_{ik} , SBAR	Value of s_{ik} at time of loading reversal
t	Time
$T(\omega)$	Filter transfer function
TERM _{ij}	Term in expression for external spring crushing energy, Equation (1-169)
$[TR_{iM}]$	Transformation matrix used in Equation (1-60)
u_i, v_i, w_i	Body i axes components of absolute translation velocity vector of mass m_i
$(u_{mod}, v_{mod}, w_{mod})_i$	Body axes components of velocity of i end of beam ij
$(unp, vnp, wnp)_{iM}$	Node point velocity, body axes

$\{v\}_{ij}$	$(vx, vu, vz, v\phi, v\theta, v\psi)_{ij}$
$m_i \vec{v}^{C'}$	Velocity vector of C'_{ik} with respect to m_i
$0 \vec{v}^{C'}$	Velocity of point fixed in m_i , instantaneously coinciding with point C' , with respect to ground
$0 \vec{v}^{C'}$	Velocity vector of C'_{ik} with respect to ground
$0 \vec{v}^{m_i}$	Velocity vector of m_i with respect to ground
va_{ij}	x_i, y_i, z_i
\bar{v}_{bijl}	Value of v_{ijl} at time of loading reversal
vc_{ijk}	Ground coordinates of point C_{ik}
$\dot{v}_{cp_{ijk}}$	Ground axes components of absolute velocity of ground contact point C'_{ik}
$\dot{v}_{cps}^{\ell}_{ijk}$	Slope axes components of velocity of C'_{ik}
vcs^{ℓ}_{ijk}	Slope coordinates at point C_{ik}
$(vel_1, \dots, vel_6)_{ij}$	Relative beam end velocities ($j - i$)
$(vel_7, vel_8, vel_9)_{ij}$	Beam end velocity sums ($j + i$)
\bar{v}_{ik}	Magnitude of ground plane contact point velocity for spring ik
$\overline{vs}^{\ell}_{ik}$	Magnitude of slope contact point velocity of C'_{ik}
$(vx, vy, vz)_i$	Translational velocity components of beam end i , beam axes
$(vx, vy, vz)_{ij}$	Total (over time) relative beam deflections ($j - i$)
$(v\phi, v\theta, v\psi)_i$	Rotational velocity components of beam end i , beam axes
$(v\phi, v\theta, v\psi)_{ij}$	Total (over time) relative beam rotations ($j - i$)
W_i	Weight of i th lumped mass
W_{TOT}	Total vehicle weight
X_{Ai}, Y_{Ai}, Z_{Ai}	Aerodynamic forces, body i axes

$$\dot{x}_{AP}, \dot{y}_{AP}, \dot{z}_{AP}$$

Ground axes components of airplane cg velocity vector

$$\begin{pmatrix} X_{C_i}, Y_{C_i}, Z_{C_i} \\ L_{C_i}, M_{C_i}, N_{C_i} \end{pmatrix}$$

Crash (external) forces and moments, body i axes

$$(X_{C_{iM}}, \dots, N_{C_{iM}})$$

External spring crash forces due to all springs attached to node point iM

$$x_G, y_G, z_G (vg_j)$$

Ground coordinates of initial (t = 0) cg position

$$\dot{x}_G, \dot{y}_G, \dot{z}_G$$

Ground axes components of initial (t = 0) cg velocity vector

$$x''_G, y''_G, z''_G (vgpp_{ij})$$

Airplane axes coordinates of vehicle cg (point G)

$$X_{Gi}, Y_{Gi}, Z_{Gi}$$

Gravity forces, body i axes

$$x_i, y_i, z_i (va_{ij})$$

Ground coordinates of m_i

$$\begin{pmatrix} X_i, Y_i, Z_i \\ L_i, M_i, N_i \end{pmatrix}$$

Total forces and moments on mass i, in ith body axes

$$x'_i, y'_i, z'_i (vip_{ij})$$

Coordinates of m_i in center-of-gravity coordinate system

$$x''_i, y''_i, z''_i (vipp_{ij})$$

Coordinates of m_i in airplane coordinate system

$$\begin{pmatrix} X_{Ii}, Y_{Ii}, Z_{Ii} \\ L_{Ii}, M_{Ii}, N_{Ii} \end{pmatrix}$$

Internal (strain + damping) forces and moments, body i axes

$$x_{ij}, y_{ij}, z_{ij}$$

Ground coordinates of vector from point i to point j

$$(x_{mod}, y_{mod}, z_{mod})_i$$

Ground coordinates of i end of beam ij

$$\begin{pmatrix} \bar{x}_n, \bar{y}_n, \bar{z}_n \\ \bar{x}_p, \bar{y}_p, \bar{z}_p \end{pmatrix}$$

Mass penetration control volume dimensions

$(x_{np}, y_{np}, z_{np})_{iM}$	Ground coordinates of node point iM
$(\dot{x}_{np}, \dot{y}_{np}, \dot{z}_{np})_{iM}$	Node point velocity, ground axes
x_{pi}, y_{pi}, z_{pi}	pth body axes components of vector from m_p to m_i
$XVOC_{ijk}$	Ground axes components of spring force at ground contact point C'_{ik}
$XVOC_{SL}_{ijk}$	Slope axes components of spring force at C'_{ik}
z^c_{MAX}	Vertical distance from cg to lowest C'_{ik}
z_{SL}	Slope axes coordinate of initial airplane cg position
Δ_i	Determinate expression used in Equation (1-112)
$\Delta t, dt$	Numerical integration time interval
$\vec{\omega}_{m_i}$	Angular velocity of m_i with respect to ground
ω_c	Filter cutoff frequency
ω_{ij}	Natural frequency of beam ij
ϕ', θ', ψ'	Euler angles from ground axes to cg axes (constant); initial ($t = 0$) attitude of vehicle
ϕ_i, θ_i, ψ_i	Euler angles from ground axes to body axes (time varying)
$\phi''_i, \theta''_i, \psi''_i$	Euler angles from cg axes to ith body axes (constant)
$\phi_{ij}, \theta_{ij}, \psi_{ij}$	Euler angles from ground axes to beam ij axes (time varying)
σ_s	Beam element shear stress
σ_{shear}	Allowable shear stress
$\sigma_{s_{max}}$	Beam element maximum shear stress
σ_x	Beam element axial stress
σ_{yield}	Beam element yield stress
σ_1, σ_2	Beam element principal stresses
ξ_{ij}	Damping ratio for beam ij

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SECTION 1

PROGRAM KRASH

1.1 INTRODUCTION

This section presents a comprehensive description of the crash analysis digital computer program called KRASH. Section 1.2 gives an outline of the general features and capabilities of the KRASH program. Section 1.3 presents in detail all the theoretical development of the equations contained in KRASH. Section 2 outlines the input-output control parameters in KRASH, and presents a simplified program flow diagram. A complete program listing is included in Appendix A.

1.2 PROGRAM KRASH DESCRIPTION

Digital computer program KRASH predicts the response of vehicles to multi-directional crash environments. The program computes the time histories of N interconnected masses, each allowed six degrees of freedom defined by inertial coordinates x_i, y_i, z_i and Eulerian angles ϕ_i, θ_i, ψ_i , where $i = 1, 2 \dots N$. Euler's equations of motion are written for each mass. The equations of motion are integrated numerically to obtain velocities, displacements, and rotations. Gravitational forces, internal forces and moments, and external forces are computed. For small deflections a linear analysis is obtained, and for large deflections, general plastic deformation is allowed. The program provides for unloading and subsequent reloading along a linear elastic line.

Program KRASH describes the interaction between a series of massless interconnecting structural elements and concentrated rigid body masses to which the structural elements are attached at their ends with the appropriate end fixity (pinned, fixed). The structural elements can be connected between "node points" which are offset from and rigidly attached to selected mass points. The interconnecting elements represent the stiffness characteristics of the structure between the masses. The masses can translate and

rotate in all directions under the influence of the external forces (i.e., gravity, aerodynamic, impact), as well as the constraining internal element forces. The movement of the masses results in changes in the relative distortion of the structural elements and, in turn, results in a new set of element forces acting throughout the system.

Computer Program KRASH has the capability to:

1. Define the response of six degrees of freedom (DOF) at each representative location, including three translations and three rotations
2. Determine mass accelerations, velocities, and displacements and internal member loads and deformations at each time interval
3. Provide for general nonlinear stiffness properties in the plastic regime, including different types of load-limiting devices, and determine the amount of permanent deformation
4. Determine how and when rupture of an element takes place and redistribute the loading over the structural elements involved
5. Define mass penetration into an occupiable volume
6. Define the volume change due to structural deformations of the occupiable volume
7. Provide for ground contact by external structure including sliding friction and a nonrigid ground surface
8. Include internal structural damping
9. Include a measure of injury potential to the occupants; for instance, the probability of spinal injury indicated by the Dynamic Response Index (DRI)
10. Determine the distribution of kinetic and potential energy by mass item, the distribution of strain and damping energy by element, and the crushing and sliding friction energy associated with each external spring
11. Determine the vehicle response to an initial condition that includes linear and angular velocity about three axes and any arbitrary vehicle attitude

12. Provide a measure of the airplane cg velocity by means of translational momentum relationships.
13. Analyze an impact into a horizontal ground and/or an inclined slope.
14. Provide a measure of the internal stress state of internal beam elements
15. Analyze a mathematical model containing up to 80 masses and 100 internal beam elements

1.3 THEORY

1.3.1 Mathematical Model of Airplane

The airplane is modeled as a series of interconnected lumped masses. Each mass is allowed six degrees of freedom, three translations and three rotations. The masses are connected internally by nonlinear beam elements. Each mass is allowed up to three external nonlinear springs, which radiate outward from the mass and contact the ground, providing external crash forces. A typical airplane model is shown in Figure 1-1.

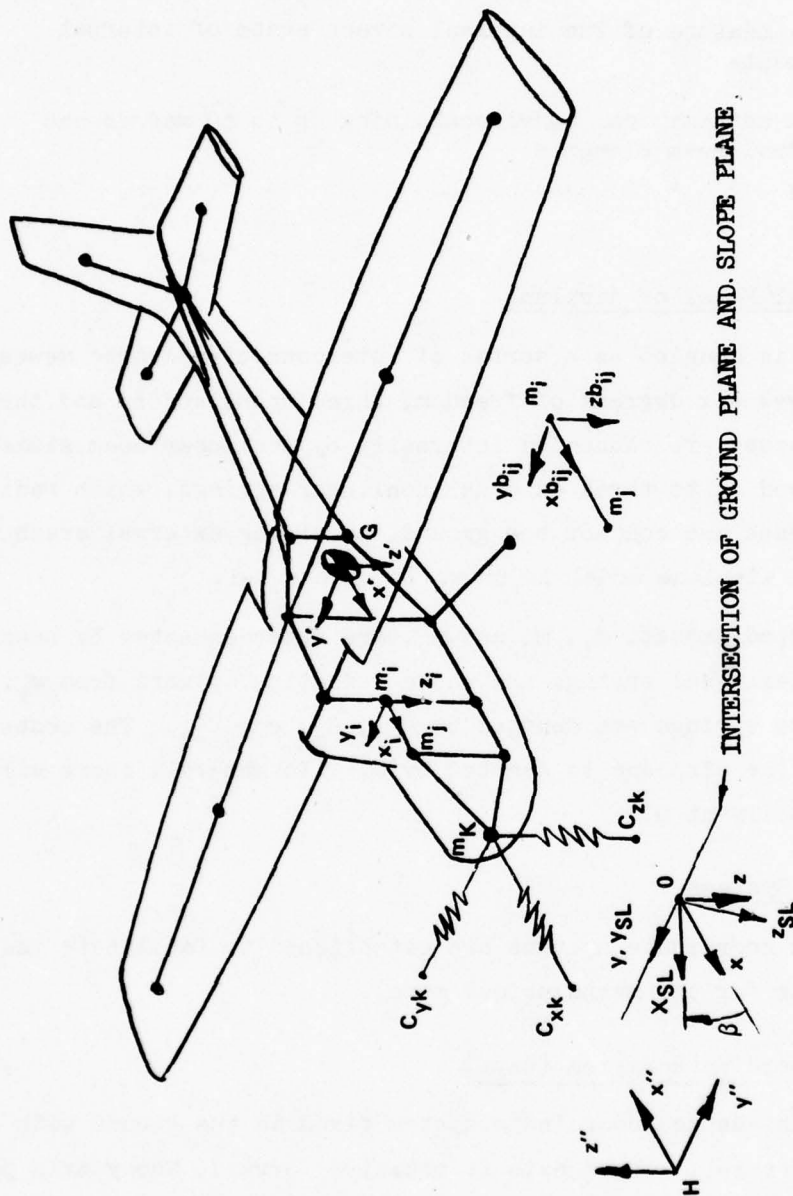
The three lumped masses, m_i , m_j and m_k , are interconnected by beams ij and jk . Three external springs are shown radiating outward from m_k . The end points of these springs are denoted by C_{xk} , C_{yk} and C_{zk} . The center-of-gravity of the entire airplane is denoted by G . (In general, there will be no lumped mass exactly at G .)

1.3.2 Coordinate Systems

The following coordinate systems are established to facilitate the derivation of equations for the mathematical model.

1.3.2.1 Ground Coordinate System (Oxyz)

This is a right-handed coordinate system fixed in the ground with origin at point O in Figure 1-1. The x axis is positive forward, the y axis positive to the right, and the z axis positive downward. The xy plane ($z = 0$) corresponds to the ground surface. The ground coordinate system is considered an inertial coordinate system for writing the dynamic equations of motion.



INTERSECTION OF GROUND PLANE AND SLOPE PLANE

Figure 1-1. Mathematical Model of Airplane

1.3.2.2 Slope Coordinate System ($Ox_{SL}y_{SL}z_{SL}$)

This is a right handed coordinate system fixed in the ground with origin at point O as shown in Figure 1-1. The x_{SL} axis is positive forward up the slope, the y_{SL} axis is positive to the right, and the z_{SL} axis is positive perpendicular to the slope, going into the slope. This coordinate system is the same as the ground coordinate system, rotated through an angle β positive clockwise about the Oy ground axis. The $Ox_{SL}y_{SL}$ plane represents a plane inclined at an angle β with respect to the horizontal ground plane. β is a constant input angle that can lie in the range from zero to ninety degrees.

1.3.2.3 Airplane Coordinate System ($Hx''y''z''$)

This is a left-handed coordinate system fixed in the airplane with origin at point H in Figure 1-1. The x'' axis is positive aft, y'' is positive left, and z'' is positive upward. The origin, point H, corresponds to F.S.O, B.L.O, W.L.O. This coordinate system is used only to input the coordinates of the lumped mass points, since the coordinates of the points are usually available in terms of F.S., B.L. and W.L.

1.3.2.4 Center-of-Gravity Coordinate System ($Gx'y'z'$)

This is a right-handed system fixed in the airplane with the origin at the vehicle cg (Point G). The x' axis is positive forward, y' positive right, and z' positive downward. These axes are parallel to the $Hx''y''z''$ axes.

1.3.2.5 Body Coordinate System ($m_i x_i y_i z_i$)

Each lumped mass has its own right-handed coordinate system fixed in the mass. The initial orientation of each of these coordinate systems is arbitrary, and it is specified by means of three input Euler angles for each mass, relating its initial orientation to the $Gx'y'z'$ center-of-gravity coordinate system. Normally the body coordinate system is taken as initially parallel to the center-of-gravity coordinate system (and hence, the three input Euler angles are set = 0), since the inertia data is generally available about these axes.

The body coordinate system is the system used in writing Euler's equations of motion for each lumped mass m_i .

1.3.2.6 Beam Coordinate System ($m_i, x_{b_{ij}}, y_{b_{ij}}, z_{b_{ij}}$)

This is a right-handed coordinate system with the $x_{b_{ij}}$ axis along a straight line from m_i to m_j . As the masses move, the coordinate system changes orientation so that $x_{b_{ij}}$ is always pointing from m_i to m_j . If the beam connects node points which are offset from the mass points, then $x_{b_{ij}}$ always points from the node point rigidly attached to mass m_i to the node point rigidly attached to mass m_j .

The direction of $y_{b_{ij}}$ and $z_{b_{ij}}$ (they are mutually perpendicular) is arbitrary, and is defined internally within the program. Each beam ij has a beam coordinate system, used to compute the beam forces and moments.

1.3.3 Relations Between Coordinate Systems

Any quantity which can be expressed as a vector in one coordinate system (forces, moments, displacements, velocities, accelerations, but not large rotations) can be, likewise, specified in another coordinate system by use of an Eulerian transformation matrix relating the two coordinate systems. Thus, for example, if we have a force vector at m_i expressed in its body axes components as (X_i, Y_i, Z_i) , this can be expressed in ground axes as simply

$$\begin{Bmatrix} X_{oi} \\ Y_{oi} \\ Z_{oi} \end{Bmatrix} = [A_i] \begin{Bmatrix} X_i \\ Y_i \\ Z_i \end{Bmatrix} \quad (1-1)$$

where $\{X_{oi}, Y_{oi}, Z_{oi}\}$ are the ground axes components of the force vector and $[A_i]$ is a 3 x 3 Eulerian transformation matrix. The form of $[A_i]$ depends on the sequence in which rotations from one axis system to the other are performed. In this program, the following sequence is employed:

1. Starting with the Oxyz coordinate system, perform a clockwise (right-hand rule) rotation about the Oz axis, through an angle ψ_i .

2. Next, perform a clockwise rotation about the new Oy axis, through an angle θ_1 .
3. Finally, perform a clockwise rotation about the final Ox axis, through an angle ϕ_1 .

The resulting transformation matrix is then inverted to obtain a transformation from body axes to ground axes. The resulting transformation matrix is given by

$$A_1 = \begin{bmatrix} \cos\theta_1 \cos\psi_1 & -\cos\phi_1 \sin\psi_1 + \sin\phi_1 \sin\theta_1 \cos\psi_1 & \sin\phi_1 \sin\psi_1 + \cos\phi_1 \sin\theta_1 \cos\psi_1 \\ \cos\theta_1 \sin\psi_1 & \cos\phi_1 \cos\psi_1 + \sin\phi_1 \sin\theta_1 \sin\psi_1 & -\sin\phi_1 \cos\psi_1 + \cos\phi_1 \sin\theta_1 \sin\psi_1 \\ -\sin\theta_1 & \sin\phi_1 \cos\theta_1 & \cos\phi_1 \cos\theta_1 \end{bmatrix} \quad (1-2)$$

Similar transformation matrices are formed to relate various other coordinate systems. These are summarized in Table 1-1.

TABLE 1-1. TRANSFORMATION MATRICES

Matrix	Transforms From	To	Using Angles	Angles Constant or Varying
$[A_i]$	ith body axes	ground axes	ϕ_i, θ_i, ψ_i	varying
$[A_{ij}]$	beam ij axes	ground axes	$\phi_{ij}, \theta_{ij}, \psi_{ij}$	varying
$[A''_i]$	ith body axes	cg axes	$\phi''_i, \theta''_i, \psi''_i$	constant
$[A']$	cg axes	ground axes	ϕ', θ', ψ'	constant
$[A_\beta]$	ground axes	slope axes	$0, \beta, 0$	constant

All the above matrices utilize equation (1-1) with the appropriate angles from Table 1-1. $[A''_i]$ and $[A']$ are used only in initial conditions determination, so that their Euler angles are indicated as constant. These "constants" are really the time zero values of the angles which actually vary but are not used in the time history computations. ϕ' , θ' , ψ' are input constants defining the initial attitude of the overall vehicle.

We also will require the time derivative of the $[A_i]$ matrix, denoted $[\dot{A}_i]$. It can be shown that this is given by postmultiplying $[A_i]$ by a matrix $[D_i]$ so that

$$[\dot{A}_i] = [A_i] [D_i] \quad (1-3)$$

where $[D_i]$ is the following skew-symmetric matrix:

$$[D_i] = \begin{bmatrix} 0 & -r_i & q_i \\ r_i & 0 & -p_i \\ -q_i & p_i & 0 \end{bmatrix} \quad (1-4)$$

p_i , q_i , r_i are the body axis components of the angular velocity of mass m_i .

1.3.4 Sign Conventions

The basic sign convention used for all displacements, rotations, velocities, accelerations, forces and moments is that all quantities are positive in the positive direction of the axes shown in Figure 1-1. Rotation and moments utilize a right-hand rule to define the positive direction. The few exceptions to this rule are indicated in the theoretical development.

1.3.5 Forces Acting on Each Mass

The following forces and moments act on each lumped mass:

- Gravity forces
- Aerodynamic forces
- Internal forces and moments - Strain and Damping
- External forces and moments

All forces and moments are positive when they act in the positive direction of the $m_i x_i y_i z_i$ axes.

1.3.5.1 Gravity Forces

The gravity force for the i th lumped mass is just the weight W_i acting along the ground fixed Oz axis. Transforming this force into body axes gives the gravity forces as

$$\begin{pmatrix} X_{G_i} \\ Y_{G_i} \\ Z_{G_i} \end{pmatrix} = [A_i]^T \begin{pmatrix} 0 \\ 0 \\ W_i \end{pmatrix} \quad (1-5)$$

where $[A_i]^T$ indicates the transpose of $[A_i]$. Note that the transpose rather than the inverse is used, since for rotation transformation matrices the two are equal.

1.3.5.2 Aerodynamic Forces

The only aerodynamic forces considered are a constant lift force, in ground axes, positive upward, acting on each lumped mass. This lift force is expressed as a constant fraction of the total vehicle weight, times the vehicle weight:

$$LIFT_i = l_{c_i} W_{TOT} \quad (1-6)$$

where

$$W_{TOT} = \sum_{i=1}^N W_i \quad (1-7)$$

and N is the total number of lumped masses. Transforming this lift into ith body axes gives the desired aerodynamic forces as

$$\begin{Bmatrix} x_{A_i} \\ y_{A_i} \\ z_{A_i} \end{Bmatrix} = [A_i]^T \begin{Bmatrix} 0 \\ 0 \\ -LIFT_i \end{Bmatrix} \quad (1-8)$$

where the minus sign is necessary because the lift is positive upward (in the negative direction of the Oz ground axis).

1.3.5.3 Internal Forces and Moments - Strain and Damping

These forces and moments result from the deformations of the inter-connecting beams as the lumped masses move. First, for beam ij, the deflections, rotations and velocities of beam end points j and i are computed in beam ij axes. These are then used to calculate the three forces and three moments at point j, utilizing equations based upon the 12 x 12 stiffness matrix relating the loads to the deformations. Nonlinear effects are also included in computing the loads. The loads at point i in beam axes are computed from static equilibrium equations (the beams are assumed massless). Then the loads at i and j are transformed into ith and jth mass body axes, respectively.

Finally, for each mass the contributions from the various beams that attach to that mass are summed to obtain the total internal forces for the mass. All the internal strain force calculations are performed on an incremental basis, i.e., incremental deflections are used to compute incremental forces, since a tangent modulus is utilized for computing nonlinear effects. The damping forces are total, not incremental, based on current beam end point velocities.

1.3.5.3.1 Beam Deformations and Velocities

The first step in determining the internal beam strain and damping loads is to calculate the deflections and rotations of the end points of the beam, as well as the velocities of these points. Figure 1-2 illustrates a typical beam whose position in space is defined by the ground coordinates of the end points of the beam. This figure illustrates the most general case in which the beam connects two node points which are, in turn, rigidly connected to mass points i and j . Beams can also connect directly to the mass points. The purpose of the node points is to allow a finite size for the mass points so that beam end connections can be offset from the lumped mass center of gravity.

Masses i and j are located at (x_i, y_i, z_i) and (x_j, y_j, z_j) respectively, where these are the ground axes coordinates of m_i and m_j . These are time-varying quantities obtained from numerical integration of the equations of motion for m_i and m_j . Node points iM and jN are located at $(xnp_{iM}, ynp_{iM}, znp_{iM})$ and $(xnp_{jN}, ynp_{jN}, znp_{jN})$, respectively. These coordinates are calculated as follows

$$\begin{pmatrix} xnp \\ ynp \\ znp \end{pmatrix}_{iM} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}_i + [A_i] \begin{pmatrix} rx \\ ry \\ rz \end{pmatrix}_{iM} \quad (1-9)$$

$[A_i]$ is given by Equation (1-2) and is a time varying quantity dependent upon the Euler angles ϕ_i , θ_i , and ψ_i that define the orientation of mass m_i with respect to ground. The vector $(rx, ry, rz)_{iM}$ is a constant defining the

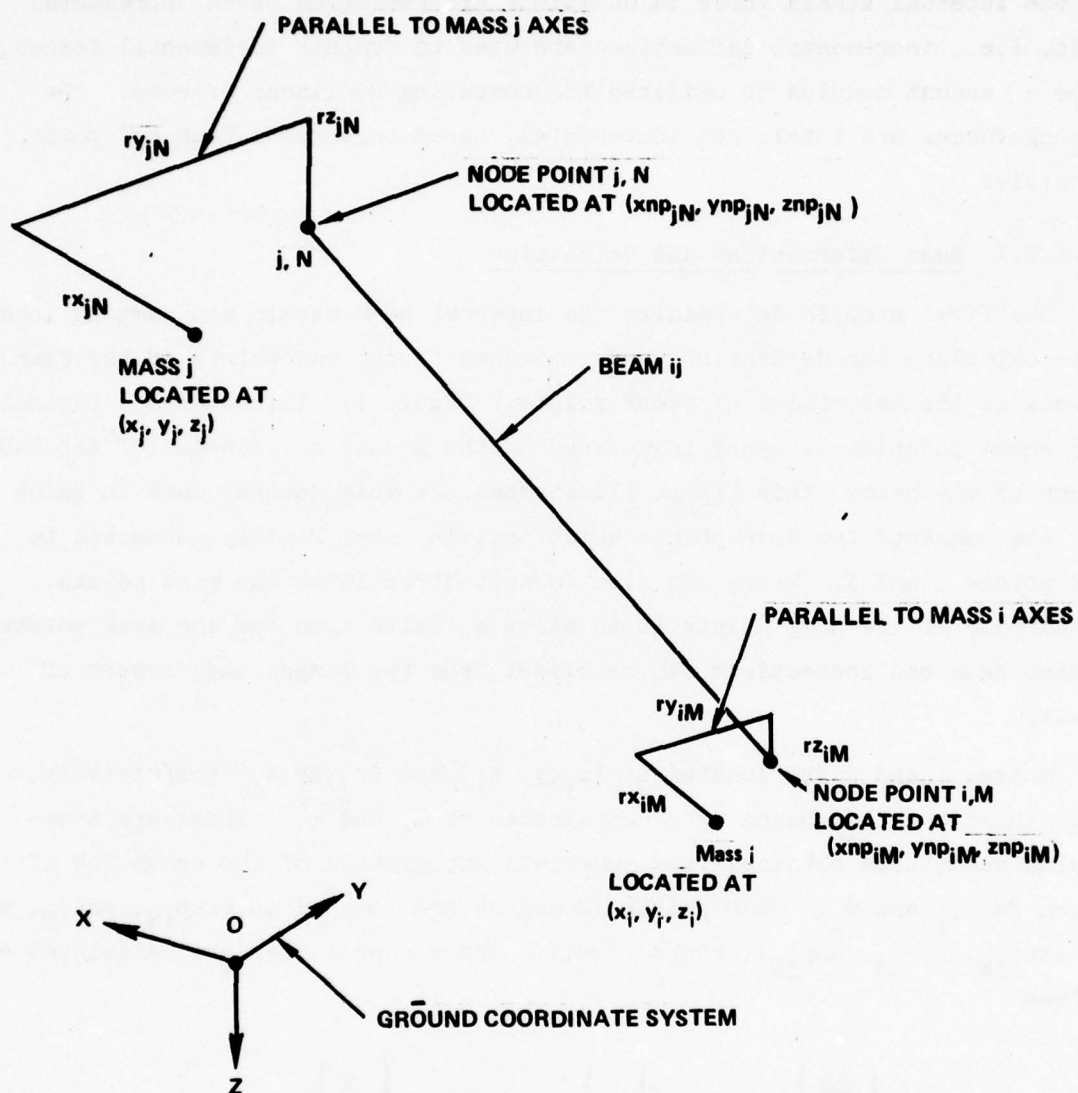


Figure 1-2. Beam End Point Locations

offset of node point iM with respect to mass m_i ; these vector components are in mass-fixed axes.

Taking the time derivative of both sides of Equation (1-9) yields

$$\begin{pmatrix} \dot{x}_{np} \\ \dot{y}_{np} \\ \dot{z}_{np} \end{pmatrix}_{iM} = \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix}_i + \begin{bmatrix} A_i \end{bmatrix} \begin{bmatrix} D_i \end{bmatrix} \begin{pmatrix} rx \\ ry \\ rz \end{pmatrix}_{iM} \quad (1-9)$$

where Equation (1-3) has been used for $\begin{bmatrix} A_i \end{bmatrix}$. Multiplying through by the transpose of $\begin{bmatrix} A_i \end{bmatrix}$ to convert from ground axes back to mass axes yields

$$\begin{pmatrix} u_{np} \\ v_{np} \\ w_{np} \end{pmatrix}_{iM} = \begin{pmatrix} u \\ v \\ w \end{pmatrix}_i + \begin{bmatrix} D_i \end{bmatrix} \begin{pmatrix} rx \\ ry \\ rz \end{pmatrix}_{iM} \quad (1-10)$$

The $(u,v,w)_i$ and $(u_{np},v_{np},w_{np})_{iM}$ are the body axes components of the velocity vectors for mass i and node point iM, respectively. The former is obtained from integration of the equations of motion.

Since the strain forces are calculated on an incremental basis, what is required are the incremental deflections of the end points of the beam. These are calculated directly as the differences between the current coordinates and the values at the previous time point.

$$\begin{pmatrix} dx \\ dy \\ dz \end{pmatrix}_i = \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{i \text{ current}} - \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{i \text{ previous}} \quad (1-11a)$$

$$\begin{pmatrix} dx_{np} \\ dy_{np} \\ dz_{np} \end{pmatrix}_{iM} = \begin{pmatrix} x_{np} \\ y_{np} \\ z_{np} \end{pmatrix}_{iM \text{ current}} - \begin{pmatrix} x_{np} \\ y_{np} \\ z_{np} \end{pmatrix}_{iM \text{ previous}} \quad (1-11b)$$

The incremental rotations are also treated as vectors. Although large rotations are not vector quantities, the incremental rotations from one time step to the next are sufficiently small to be treated as vectors. The angular velocity components of m_i are defined as $(p, q, r)_i$ in mass fixed axes. These are obtained from integration of the angular accelerations $(\dot{p}, \dot{q}, \dot{r})_i$. The incremental rotations are calculated as the differences (current-previous) in the integrals of the angular velocities.

$$\begin{pmatrix} \text{dpin} \\ \text{dqin} \\ \text{drin} \end{pmatrix}_i = \begin{pmatrix} \text{inp} \\ \text{inq} \\ \text{inr} \end{pmatrix}_{\text{current } i} - \begin{pmatrix} \text{inp} \\ \text{inq} \\ \text{inr} \end{pmatrix}_{\text{previous } i} \quad (1-12)$$

where

$$\begin{pmatrix} \text{inp} \\ \text{inq} \\ \text{inr} \end{pmatrix}_i = \int_0^t \begin{pmatrix} p \\ q \\ r \end{pmatrix}_i dt \quad (1-13)$$

The incremental rotations in Equation (1-12) are in mass-fixed axes and follow the right hand rule.

In the actual computer program KRASH, the internal beam strain and damping forces are calculated in a DO loop ranging over all the beams in the model being analyzed. For each beam, the end points are defined by mass numbers i and j and node point numbers M and N . If M or N is zero, the beam connects directly to the mass point at that end. The appropriate equations are then used to calculate the end point positions, velocities and incremental changes in position. For the remaining equations, the following terminology is employed:

$$\begin{pmatrix} \text{xmod} \\ \text{ymod} \\ \text{zmod} \end{pmatrix}_i = \begin{pmatrix} x \\ y \\ z \end{pmatrix}_i \quad \text{or} \quad \begin{pmatrix} \text{xnp} \\ \text{ynp} \\ \text{znp} \end{pmatrix}_{iM} \quad (1-14a)$$

$$\begin{pmatrix} dx_{mod} \\ dy_{mod} \\ dz_{mod} \end{pmatrix}_i = \begin{pmatrix} dx \\ dy \\ dz \end{pmatrix}_i \quad \text{or} \quad \begin{pmatrix} dx_{np} \\ dy_{np} \\ dz_{np} \end{pmatrix}_{iM} \quad (1-14b)$$

$$\begin{pmatrix} u_{mod} \\ v_{mod} \\ w_{mod} \end{pmatrix}_i = \begin{pmatrix} u \\ v \\ w \end{pmatrix}_i \quad \text{or} \quad \begin{pmatrix} u_{np} \\ v_{np} \\ w_{np} \end{pmatrix}_{iM} \quad (1-14c)$$

In each case, the first terms are used if there is no node point ($M = 0$ for the current beam), and the second terms are used if there is a node point ($M \neq 0$). For the angular velocities $(p, q, r)_i$ and the incremental rotations $(dpin, dqin, drin)_i$, the quantities are the same whether or not there is a node point, since the node point iM is rigidly connected to mass i . Beam end j or jN is treated in the same fashion.

Once the quantities in Equations (1-14) have been calculated, the beam orientation with respect to ground is known so that the current $[A_{ij}]$ matrix may be determined. Figure 1-3 illustrates a typical beam ij , showing its spatial orientation with respect to the ground fixed coordinate system and identifying the beam Euler angles θ_{ij} and ψ_{ij} . From Figure 1-3, it can be seen that

$$\begin{pmatrix} x_{ij} \\ y_{ij} \\ z_{ij} \end{pmatrix} = \begin{pmatrix} x_{mod} \\ y_{mod} \\ z_{mod} \end{pmatrix}_j - \begin{pmatrix} x_{mod} \\ y_{mod} \\ z_{mod} \end{pmatrix}_i \quad (1-15)$$

$$\psi_{ij} = \tan^{-1} (y_{ij}/x_{ij}) \quad (1-16a)$$

$$\theta_{ij} = -\tan^{-1} (z_{ij}/\sqrt{x_{ij}^2 + y_{ij}^2}) \quad (1-16b)$$

The remaining Euler angle ϕ_{ij} , defining the "roll" orientation of the beam axes, is initially set to zero and thereafter calculated as

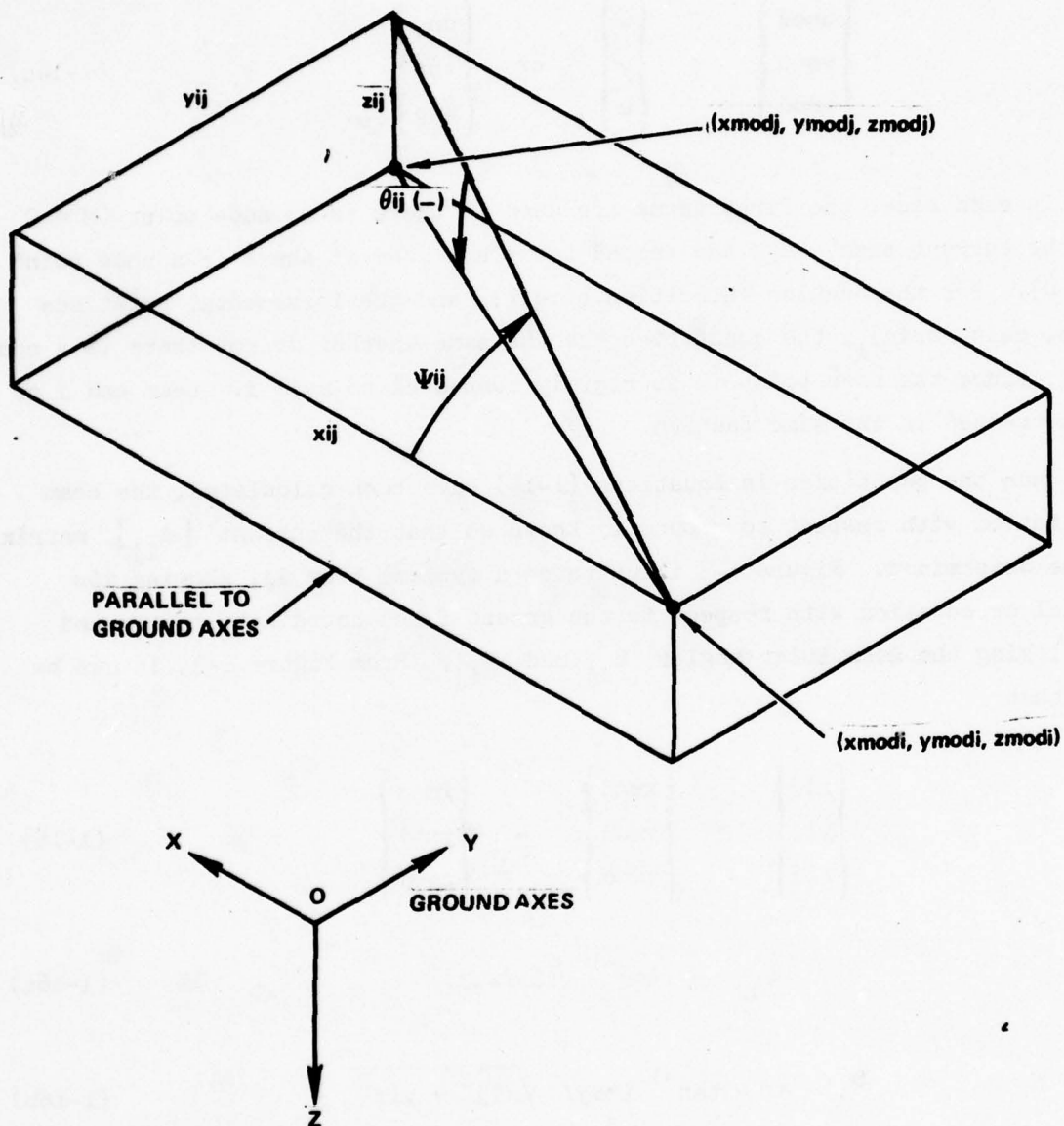


Figure 1-3. Spatial Orientation of Beam ij

$$\begin{array}{ccc} \phi_{ij} & = & \phi_{ij} + d\phi_{ij} \\ \text{current} & & \text{previous} \end{array} \quad (1-16c)$$

where $d\phi_{ij}$ is the average incremental rotation of masses i and j resolved into the current beam x axis. This term is derived later, and is given by Equation (1-33). The current beam length is calculated as

$$l_{ij} = \sqrt{x_{ij}^2 + y_{ij}^2 + z_{ij}^2} \quad (1-17)$$

In order to transform vector quantities directly from mass fixed axes to beam axes, the following transformation matrices are calculated

$$[AIJTAI] = [A_{ij}]^T [A_i] \quad (1-18a)$$

$$[AIJTAJ] = [A_{ij}]^T [A_j] \quad (1-18b)$$

In Equations (1-18), the second matrix transforms from mass fixed axes (either i or j) to ground axes, and the first matrix transforms from ground axes to beam ij axes.

The incremental beam deflections at i and j , in beam ij axes, are given by

$$\begin{pmatrix} dx \\ dy \\ dz \end{pmatrix}_{i,j} = [A_{ij}]^T \begin{pmatrix} dx_{mod} \\ dy_{mod} \\ dz_{mod} \end{pmatrix}_{i,j} \quad (1-19)$$

The beam end translational velocities are simply

$$\begin{pmatrix} vx \\ vy \\ vz \end{pmatrix}_i = [AIJTAI] \begin{pmatrix} u_{mod} \\ v_{mod} \\ w_{mod} \end{pmatrix}_i \quad (1-20a)$$

$$\begin{pmatrix} vx \\ vy \\ vz \end{pmatrix}_j = [AIJTAJ] \begin{pmatrix} umod \\ vmod \\ wmod \end{pmatrix}_j \quad (1-20b)$$

The incremental rotations of the beam ends are calculated as

$$\begin{pmatrix} d\phi \\ d\theta \\ d\psi \end{pmatrix}_i = [AIJTAI] \begin{pmatrix} dpin \\ dqin \\ drin \end{pmatrix}_i \quad (1-21a)$$

$$\begin{pmatrix} d\phi \\ d\theta \\ d\psi \end{pmatrix}_j = [AIJTAJ] \begin{pmatrix} dpin \\ dqin \\ drin \end{pmatrix}_j \quad (1-21b)$$

The beam end rotational velocities are

$$\begin{pmatrix} v\phi \\ v\theta \\ v\psi \end{pmatrix}_i = [AIJTAI] \begin{pmatrix} p \\ q \\ r \end{pmatrix}_i \quad (1-22a)$$

$$\begin{pmatrix} v\phi \\ v\theta \\ v\psi \end{pmatrix}_j = [AIJTAJ] \begin{pmatrix} p \\ q \\ r \end{pmatrix}_j \quad (1-22b)$$

1.3.5.3.2 Linear Strain Forces and Moments

The incremental beam strain forces and moments are first calculated on a linear basis and then modified by a stiffness reduction factor KR, which may vary at each time step. The calculation of the KR factors is discussed in subsection 1.3.5.3.4; this section presents the method of calculating the linear (KR=1) strain forces and moments.

The full 12 x 12 stiffness matrix for a beam element with fixed end conditions is given by Equation (1-23) below.

$$[K] = \begin{bmatrix} \frac{AE}{L} & & & & & & -\frac{AE}{L} & & & & & \\ & \frac{12EI_z}{L^3} & & & & \frac{6EI_z}{L^2} & & -\frac{12EI_z}{L^3} & & & & \frac{6EI_z}{L^2} \\ & & \frac{12EI_y}{L^3} & & -\frac{6EI_y}{L^2} & & & & -\frac{12EI_y}{L^3} & & -\frac{6EI_y}{L^2} & \\ & & & \frac{GJ}{L} & & & & & & -\frac{GL}{L} & & \\ & & -\frac{6EI_y}{L^2} & & \frac{4EI_y}{L} & & & & \frac{6EI_y}{L^2} & & \frac{2EI_y}{L} & \\ & \frac{6EI_z}{L^2} & & & & \frac{4EI_z}{L} & & -\frac{6EI_z}{L^2} & & & & \frac{2EI_z}{L} \\ -\frac{AE}{L} & & & & & & \frac{AE}{L} & & & & & \\ & -\frac{12EI_z}{L^3} & & & & -\frac{6EI_z}{L^2} & & \frac{12EI_z}{L^3} & & & & -\frac{6EI_z}{L^2} \\ & & -\frac{12EI_y}{L^3} & & \frac{6EI_y}{L^2} & & & & \frac{12EI_y}{L^3} & & \frac{6EI_y}{L^2} & \\ & & & -\frac{GJ}{L} & & & & & & \frac{GJ}{L} & & \\ & & -\frac{6EI_y}{L^2} & & \frac{2EI_y}{L} & & & & \frac{6EI_y}{L^2} & & \frac{4EI_y}{L} & \\ & \frac{6EI_z}{L^2} & & & & \frac{2EI_z}{L} & & -\frac{6EI_z}{L^2} & & & & \frac{4EI_z}{L} \end{bmatrix}$$

(1-23)

The corresponding incremental force/deflection equation is

$$\begin{Bmatrix} dF_i \\ dF_j \end{Bmatrix} = [K_{ij}] \begin{Bmatrix} dv_i \\ dv_j \end{Bmatrix} \quad (1-24)$$

where

$$\begin{Bmatrix} dv_i \end{Bmatrix} \triangleq \begin{Bmatrix} dx \\ dy \\ dz \\ d\phi \\ d\theta \\ d\psi_i \end{Bmatrix} \quad \text{and} \quad \begin{Bmatrix} dv_j \end{Bmatrix} \triangleq \begin{Bmatrix} dx \\ dy \\ dz \\ d\phi \\ d\theta \\ d\psi_j \end{Bmatrix} \quad (1-25)$$

The terms in Equations (1-25) are given by Equations (1-19) and (1-21). $\{dF_i\}$ and $\{dF_j\}$ are 6 element vectors for the forces and moments at beam ends i and j ; these forces are ordered in the same manner as the deflections, i.e.

$$\begin{Bmatrix} dF_i \end{Bmatrix} \triangleq \begin{Bmatrix} dFx \\ dFy \\ dFz \\ dM\phi \\ dM\theta \\ dM\psi_i \end{Bmatrix} \quad \text{and} \quad \begin{Bmatrix} dF_j \end{Bmatrix} \triangleq \begin{Bmatrix} dFx \\ dFy \\ dFz \\ dM\phi \\ dM\theta \\ dM\psi_j \end{Bmatrix} \quad (1-26)$$

All quantities in these equations are in beam ij axes.

If Equation (1-24) is multiplied out using (1-23), the axial and torsional (x and ϕ) relationships are simply

$$dFx_j = k_x (dx_j - dx_i), \quad dF_{xi} = -dFx_j \quad (1-27a)$$

$$dM\phi_j = k_\phi (d\phi_j - d\phi_i), \quad dM\phi_i = -dM\phi_j \quad (1-27b)$$

$$k_x \triangleq AE/\ell \quad (1-28a)$$

$$k_\phi \triangleq GJ/\ell \quad (1-28b)$$

The other forces and moments consist of two sets of coupled bending equations. Deflections in the z direction and θ rotations are coupled in forming dF_z and dM_θ , and y deflections and ψ rotations are coupled in the equations for dF_y and dM_ψ . The following relationships result from expanding Equation (1-24):

$$\begin{aligned} dF_{z_j} &= k_z(dz_j - dz_i) + k_{z\theta}(d\theta_j + d\theta_i) \\ dM_{\theta_j} &= k_{z\theta}(dz_j - dz_i) + \frac{k_\theta}{4}(d\theta_j - d\theta_i) + \frac{3k_\theta}{4}(d\theta_j + d\theta_i) \end{aligned} \quad (1-29a)$$

$$dF_{z_i} = -dF_{z_j}$$

$$dM_{\theta_i} = -dM_{\theta_j} + \ell dF_{z_j} \quad (1-29b)$$

where

$$\begin{aligned} k_z &= 12EI_y/\ell^3 \\ k_{z\theta} &= 6EI_y/\ell^2 \\ k_\theta &= 4EI_y/\ell \end{aligned} \quad (1-29c)$$

The corresponding equations for the coupled y, ψ motions are

$$dF_{y_j} = k_y(dy_j - dy_i) + k_{y\psi}(d\psi_j + d\psi_i) \quad (1-30a)$$

$$dM_{\psi_j} = k_{y\psi}(dy_j - dy_i) + \frac{k_\psi}{4}(d\psi_j - d\psi_i) + \frac{3k_\psi}{4}(d\psi_j + d\psi_i)$$

$$dF_{y_i} = -dF_{y_j} \quad (1-30b)$$

$$dM_{\psi_i} = -dM_{\psi_j} - \ell dF_{y_j}$$

where

$$k_y = 12EI_z/\ell^3$$

$$k_{y\psi} = -6EI_z/\ell^2$$

$$k_\psi = 4EI_z/\ell \quad (1-30c)$$

In the above equations, E is the modulus of elasticity, G is the modulus of rigidity, ℓ is the current beam length, I_y and I_z are the beam cross-sectional area moments of inertia about the beam y and z axes, respectively, and A is the cross-sectional area. J is the torsional stiffness factor; for circular cross sections this is equal to the polar moment of inertia ($I_y + I_z$), while for non-circular sections J is less than the polar moment of inertia.

In program KRASH, the following incremental deflection sums and differences are defined

$$\begin{pmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{pmatrix}_{i,j} \triangleq \begin{pmatrix} dx \\ dy \\ dz \\ d\phi \\ d\theta \\ d\psi \end{pmatrix}_j - \begin{pmatrix} dx \\ dy \\ dz \\ d\phi \\ d\theta \\ d\psi \end{pmatrix}_i \quad (1-31a)$$

$$\begin{pmatrix} d_7 \\ d_8 \\ d_9 \end{pmatrix}_{i,j} \triangleq \begin{pmatrix} d\phi \\ d\theta \\ d\psi \end{pmatrix}_j + \begin{pmatrix} d\phi \\ d\theta \\ d\psi \end{pmatrix}_i \quad (1-31b)$$

Utilizing these definitions, the incremental force and moment equations become

$$\begin{aligned}
 dF_{x_j} &= k_x d_1 \\
 dF_{y_j} &= k_y d_2 + k_{y\psi} d_9 \\
 dF_{z_j} &= k_z d_3 + k_{z\theta} d_8 \\
 dM_{\phi_j} &= k_{\phi} d_4 \\
 dM_{\theta_j} &= k_{z\theta} d_3 + \frac{k_{\theta}}{4} d_5 + \frac{3}{4} k_{\theta} d_8 \\
 dM_{\psi_j} &= k_{y\psi} d_2 + \frac{k_{\psi}}{4} d_6 + \frac{3}{4} k_{\psi} d_9
 \end{aligned} \tag{1-32a}$$

While the corresponding quantities at the i end of the beam are

$$\begin{aligned}
 dF_{x_i} &= -dF_{x_j} \\
 dF_{y_i} &= -dF_{y_j} \\
 dF_{z_i} &= -dF_{z_j} \\
 dM_{\phi_i} &= -dM_{\phi_j} \\
 dM_{\theta_i} &= -dM_{\theta_j} + l dF_{z_j} \\
 dM_{\psi_i} &= -dM_{\psi_j} - l dF_{y_j}
 \end{aligned} \tag{1-32b}$$

Figure 1-4 illustrates these incremental forces and moments at both ends of beam ij; positive values are shown in the figure.

In Equation (1-31), the d_7 term is used to update the torsional orientation of the beam axis system. Equation (1-16c) indicates that the beam Euler angle ϕ_{ij} is continuously updated by $d\phi_{ij}$. This is taken as the average incremental rotation of the i and j ends of the beam, and is given by

$$d\phi_{ij} = d_7/2 \tag{1-33}$$

where d_7 is given by Equation (1-31) as $(d\phi_j + d\phi_i)$

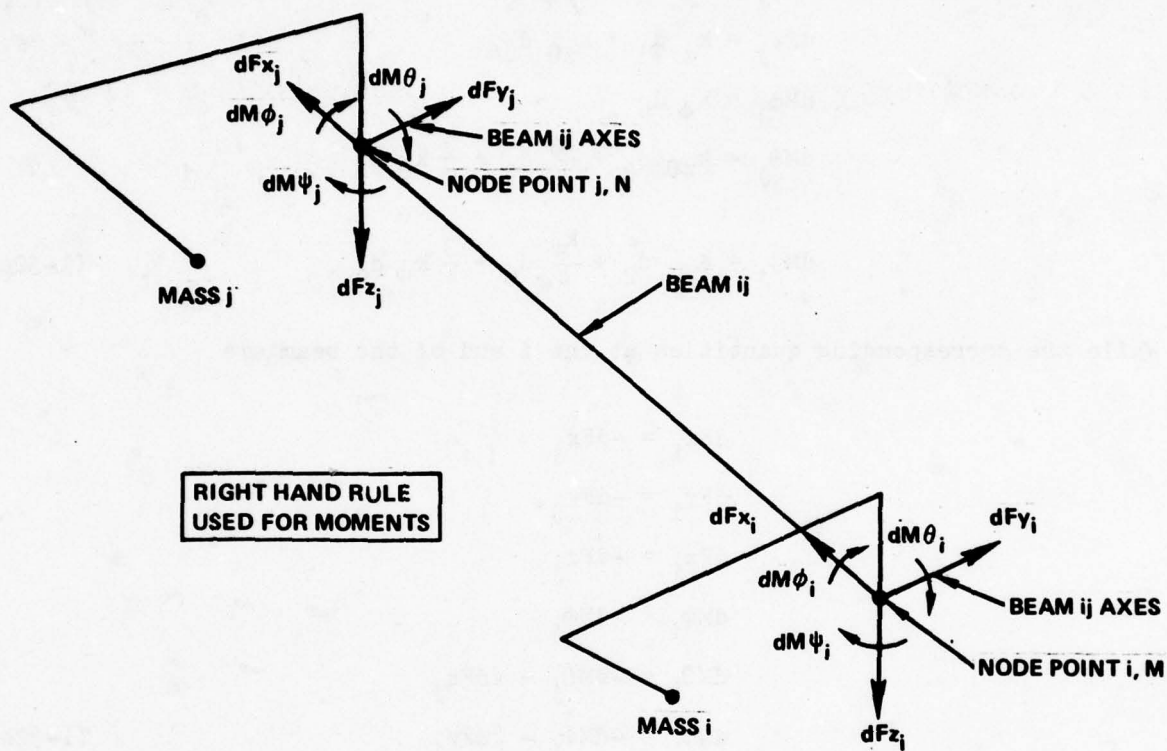


Figure 1-4. Beam Horizontal Strain Forces and Moments

1.3.5.3.3 Pinned End Conditions

Equations (1-32) developed in the preceding section are applicable only for the condition wherein the beam is built in or fixed at both ends. If the beam is pinned at both ends, then both the force and moment at i and j are zero in the plane perpendicular to the pin axis. If the beam is pinned at one end and fixed at the other end, then the equations derived in the preceding section are not applicable.

In order to illustrate the derivation of the force-deflection relationship for a single pinned-end condition, the coupled $z - \theta$ bending equations will be considered. Isolating these terms from Equation (1-23), we have

$$\begin{Bmatrix} dFz_i \\ dM\theta_i \\ dFz_j \\ dM\theta_j \end{Bmatrix} = EI_y \begin{bmatrix} 12/\ell^3 & -6/\ell^2 & -12/\ell^3 & -6/\ell^2 \\ & 4/\ell & 6/\ell^2 & 2/\ell \\ \text{(symmetric)} & & 12/\ell^3 & 6/\ell^2 \\ & & & 4/\ell \end{bmatrix} \begin{Bmatrix} dz_i \\ d\theta_i \\ dz_j \\ d\theta_j \end{Bmatrix} \quad (1-34)$$

If there is a pinned connection at j, then $dM\theta_j$ is zero, and the above equation can be rewritten as

$$\begin{Bmatrix} dF_1 \\ 0 \end{Bmatrix} = EI_y \begin{bmatrix} k_{11} & k_{12} \\ k_{21} & k_{22} \end{bmatrix} \begin{Bmatrix} dv_1 \\ dv_2 \end{Bmatrix} \quad (1-35)$$

$$K_{11} dv_1 + K_{12} dv_2 = dF_1/EI_y$$

$$K_{21} dv_1 + K_{22} dv_2 = 0$$

Solving the second equation for dv_2 and inserting into the first equation yields

$$\left[K_{11} - K_{12} K_{22}^{-1} K_{21} \right] dv_1 = dF_1/EI_y \quad (1-36)$$

Rearranging, we have

$$dF_1 = EI_y [\bar{K}] dv_1 \quad (1-37)$$

where

$$dF_1 \triangleq \begin{Bmatrix} dFz_1 \\ dM\theta_1 \\ dFz_j \end{Bmatrix} \quad dv_1 \triangleq \begin{Bmatrix} dz_1 \\ d\theta_1 \\ dz_j \end{Bmatrix} \quad (1-38a)$$

$$[\bar{K}] \triangleq [K_{11}] - [K_{12}] [K_{22}]^{-1} [K_{21}] \quad (1-38b)$$

$$[K_{11}] = \begin{bmatrix} 12/\ell^3 & -6/\ell^2 & -12/\ell^3 \\ -6/\ell^2 & 4/\ell & 6/\ell^2 \\ -12/\ell^3 & 6/\ell^2 & 12/\ell^3 \end{bmatrix} \quad (3 \times 3 \text{ matrix}) \quad (1-39a)$$

$$[K_{12}] = \begin{Bmatrix} -6/\ell^2 \\ 2/\ell \\ 6/\ell^2 \end{Bmatrix} \quad (3 \times 1 \text{ column matrix}) \quad (1-39b)$$

$$[K_{21}] = [-6/\ell^2 \quad 2/\ell \quad 6/\ell^2] \quad (1 \times 3 \text{ row matrix}) \quad (1-39c)$$

$$[K_{22}] = 4/\ell \quad (1 \times 1 \text{ scalar}) \quad (1-39d)$$

Incorporating (1-39) into (1-38), (1-37) becomes

$$\begin{Bmatrix} dFz_1 \\ dM\theta_1 \\ dFz_j \end{Bmatrix} = 3EI_y \begin{bmatrix} 1/\ell^3 & -1/\ell^2 & -1/\ell^3 \\ -1/\ell^2 & 1/\ell & 1/\ell^2 \\ -1/\ell^3 & 1/\ell^2 & 1/\ell^3 \end{bmatrix} \begin{Bmatrix} dz_1 \\ d\theta_1 \\ dz_j \end{Bmatrix} \quad (1-40)$$

Utilizing the stiffness terms defined by Equation (1-29c) this reduces to

$$\begin{Bmatrix} dFz_i \\ dM\theta_i \\ dFz_j \end{Bmatrix} = \begin{bmatrix} k_z/4 & -k_{z\theta}/2 & -k_z/4 \\ -k_{z\theta}/2 & \frac{3}{4}k_\theta & k_{z\theta}/2 \\ -k_z/4 & k_{z\theta}/2 & k_z/4 \end{bmatrix} \begin{Bmatrix} dz_i \\ d\theta_i \\ dz_j \end{Bmatrix}$$

Multiplying this out and using the definitions of (1-31), we obtain

$$\begin{aligned} dFz_j &= \frac{k_z}{4} dz_i + \frac{k_{z\theta}}{2} d\theta_i \\ dM\theta_j &= 0 \\ dFz_i &= -dFz_j \quad (\text{Pinned at } j) \\ dM\theta_i &= \frac{k_{z\theta}}{2} dz_i + \frac{3}{4}k_\theta d\theta_i \end{aligned} \quad (1-41a)$$

Similar derivations yield the following equations for the situation where the beam is pinned at i and fixed at j.

$$\begin{aligned} dFz_j &= \frac{k_z}{4} dz_j + \frac{k_{z\theta}}{2} d\theta_j \\ dM\theta_j &= \frac{k_{z\theta}}{2} dz_j + \frac{3k_\theta}{4} d\theta_j \quad (\text{Pinned at } i) \\ dFz_i &= -dFz_j \\ dM\theta_i &= 0 \end{aligned} \quad (1-41b)$$

Equations (1-41) are also applicable for the coupled $y - \psi$ bending if subscripts are changed appropriately. The resulting equations are shown for reference:

$$\left. \begin{aligned} dFy_j &= \frac{k_y}{4} d_2 + \frac{k_{y\psi}}{2} d\psi_i \\ dM\psi_j &= 0 \\ dFy_i &= -dFy_j \\ dM\psi_i &= -\frac{k_{y\psi}}{2} d_2 + \frac{3}{4} k_\psi d\psi_i \end{aligned} \right\} \begin{array}{l} \text{(Pinned at j)} \\ \end{array} \quad (1-42a)$$

$$\left. \begin{aligned} dFy_j &= \frac{k_y}{4} d_2 + \frac{k_{y\psi}}{2} d\psi_j \\ dM\psi_j &= \frac{k_{y\psi}}{2} d_2 + \frac{3}{4} k_\psi d\psi_j \\ dFy_i &= -dFy_j \\ dM\psi_i &= 0 \end{aligned} \right\} \begin{array}{l} \text{(Pinned at i)} \\ \end{array} \quad (1-42b)$$

In program KRASH, only the equations for the forces and moments at j are calculated directly from (1-41) and (1-42). The forces and moments at i are calculated using the static balance Equations (1-32b); it can be shown that the results are the same as the i end equations from (1-41) and (1-42).

This concludes the discussion of the linear incremental strain forces and moments; the following section describes the treatment of the nonlinear behavior of the beam elements.

1.3.5.3.4 Nonlinear Strain Forces and Moments

Figure 1-5 illustrates a typical nonlinear load-deflection characteristic curve, in this case the axial load at point j, Fx'_j , versus the axial deflection of j with respect to i, vx . Program KRASH utilizes a piecewise linear representation of the load-deflection curve. At each increment in time, a linear incremental force dFx_j is calculated according to the equations of the previous sections. This incremental force is then multiplied by a stiffness reduction factor, KR_x , to obtain the nonlinear incremental force dF'_x . These increments are then summed over time to form the total force Fx'_j . Figure 1-5 illustrates a typical incremental deflection dv_x , the corresponding linear incremental force dFx_j and the final nonlinear incremental force dF'_x .

The stiffness reduction factor KR_x is an input tabular function of deflection vx . Figure 1-6 shows the KR_x vs vx curve that corresponds to the load-deflection curve in Figure 1-5. Clearly KR_x is just the first derivative of the load-deflection curve with respect to deflection. Any KR curve can be input by the program user to model any general nonlinear behavior. Certain standard curves are available to represent the more common types of nonlinearities. These are discussed in detail in the User's Guide (Volume II).

Separate KR tables are input for each of the 6 directions for which it is desired to model nonlinear behavior, for beam ij . In practice, perhaps only 20% or less of all the beams will be modeled nonlinearly. (If no KR table is input, $KR = 1$ and the beam is linear for the entire run.) In general then, we have

$$\{dF_j'\} = \begin{bmatrix} KR_x & & & & & \\ & KR_y & & & & \\ & & KR_z & & & \\ & & & KR_\phi & & \\ & & & & KR_\theta & \\ & & & & & KR_\psi \end{bmatrix} \{dF_j\} \quad (1-43)$$

where the diagonal $[KR]$ matrix is composed of six stiffness reduction factors, each of which is an input tabular function of the corresponding total beam deflection. The KR 's are functions of the time sums of the first six incremental deflections in Equation (1-31); these are all the $(j - i)$ relative deflections:

$$\begin{Bmatrix} vx \\ vy \\ vz \\ v\phi \\ v\theta \\ v\psi \end{Bmatrix} = \sum_0^t \begin{Bmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{Bmatrix} = \sum_0^t \begin{Bmatrix} dx_j - dx_i \\ dy_j - dy_i \\ dz_j - dz_i \\ d\phi_j - d\phi_i \\ d\theta_j - d\theta_i \\ d\psi_j - d\psi_i \end{Bmatrix} \quad (1-44)$$

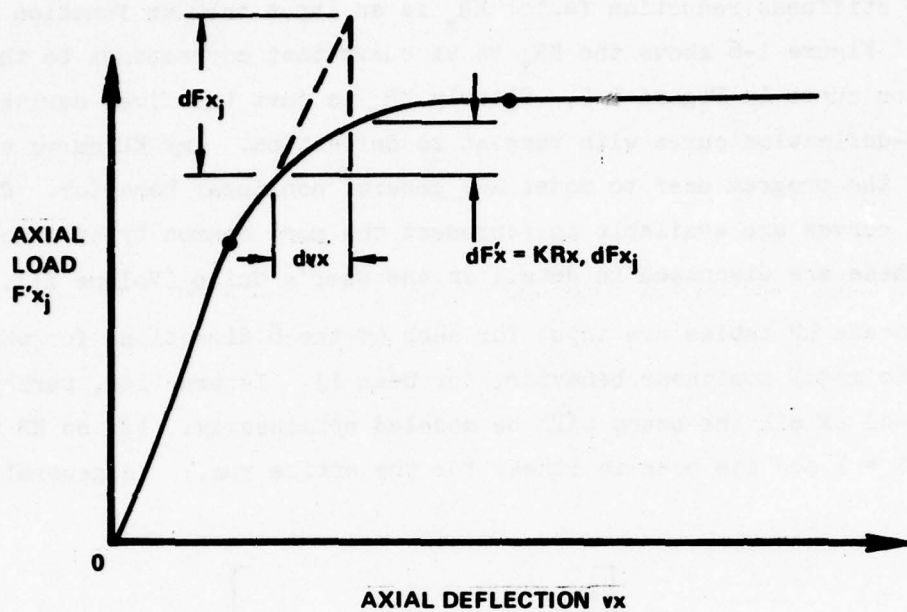


Figure 1-5. Nonlinear Load Deflection Curve

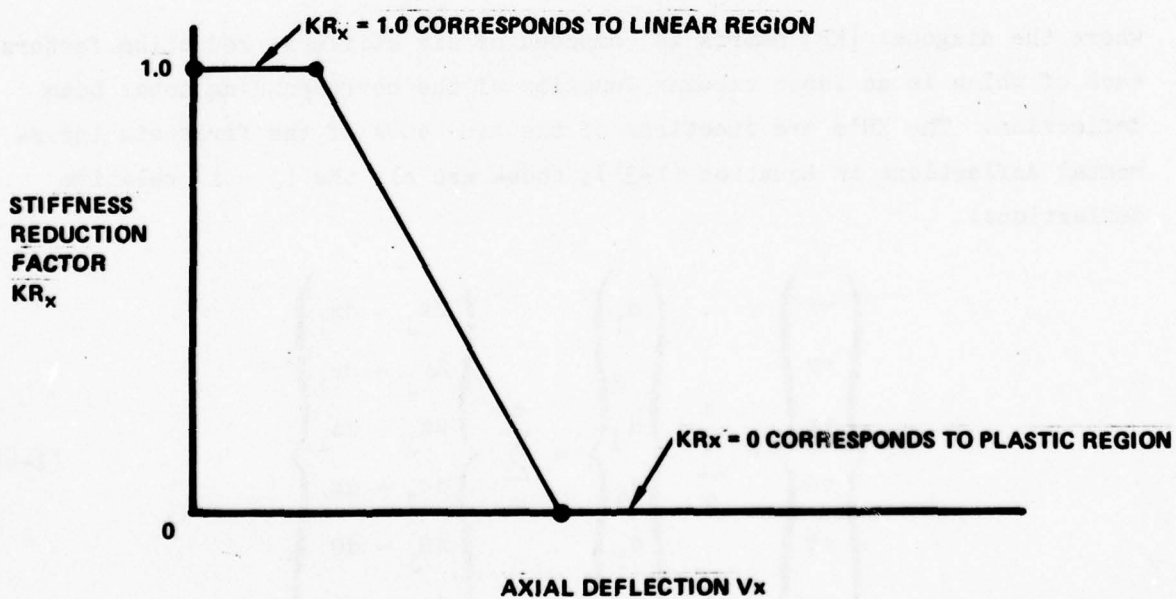


Figure 1-6. Stiffness Reduction Factor Curve

$$\begin{aligned}
KR_x &= f(vx) \\
KR_y &= f(vy) \\
KR_z &= f(vz) \\
KR_\phi &= f(v\phi) \\
KR_\theta &= f(v\theta) \\
KR_\psi &= f(v\psi)
\end{aligned}
\tag{1-45}$$

The total beam forces are calculated as the time sums of the incremental forces from Equation (1-43):

$$\{F_j'\} = \sum_0^t \{dF_j'\} \tag{1-46a}$$

$$\{F_i'\} = \sum_0^t \{dF_i'\} \tag{1-46b}$$

These total strain forces are in beam axes and act at the ends of the beam as shown in Figure 1-4 for the incremental strain forces.

For the uncoupled degrees of freedom (x and ϕ), the force depends only on one relative deflection and the corresponding KR curve. This situation was illustrated previously for the x (axial) direction. For the coupled degrees of freedom, Equation (1-32a) implies that a given force depends on 2 or 3 deflection terms and the one KR curve corresponding to the force. For example, if we combine Equations (1-32a) and (1-43) for the coupled z , θ degrees of freedom, we have

$$\begin{aligned}
dFz_j' &= KR_z(d_3) [k_z d_3 + k_{z\theta} d_\theta] \\
dM\theta_j' &= KR_\theta(d_5) \left[k_{z\theta} d_3 + \frac{k_\theta}{4} d_5 + \frac{3}{4} k_\theta d_\theta \right]
\end{aligned}
\tag{1-47}$$

where the parentheses after the KR terms indicate their functional relationships, not a multiplication.

If the calculations are actually performed in the above manner, the independent behavior of dz and $d\theta$ (and therefore d_3 and d_5) will result in different values for KR_z and KR_θ at any point in time. Since the proportionality of dF_z and dM_θ that always exists in the linear system is lost, this computational scheme has a strong tendency to yield negative strain energy, which a real physical system, even nonlinear, can never do. Furthermore, one would intuitively expect that any failure mechanism in the actual structure which causes yielding or nonlinear behavior in the z direction would also cause similar nonlinear behavior in the coupled θ direction. This reasoning could be extended to include all six independent deflections, so that when any one direction displays nonlinear behavior, this same nonlinearity holds for all 6 directions. However, it is felt that the argument for similar behavior is most persuasive for the coupled degrees of freedom, and that the axial and torsional modes should be treated independently.

In light of the foregoing, the program is coded in the following manner. For the coupled degrees of freedom, the direction which goes nonlinear first determines the nonlinear behavior for both coupled directions. In the above example, this means that if KR_z departs from 1 (linear) before KR_θ does, then KR_z is used for both dF_z' and dM_θ' for the remainder of the run. If KR_θ goes nonlinear first, then it is used in calculating both dF_z' and dM_θ' for the rest of the run. This analytical model preserves the proportionality that exists between dF_z and dM_θ in the linear system, since the linear incremental forces are always multiplied by the same KR factor. The coupled degrees of freedom y and ψ are treated in the same manner. In each case, both deflection and rotation KR curves are input, even though only one will be used, because it is not known in advance which direction will predominate. Axial and torsional deflections are uncoupled and each has its own KR curve, applicable for the entire analysis.

In addition to the nonlinear load capability just described, the program also allows for unloading and subsequent reloading to proceed along an elastic line. This is illustrated in Figure 1-7. The ordinate F_{x_j}' is the total (over time) axial load for beam ij , from Equation (1-46). Similarly, v_x is the corresponding total (over time) axial deflection from Equation (1-44).

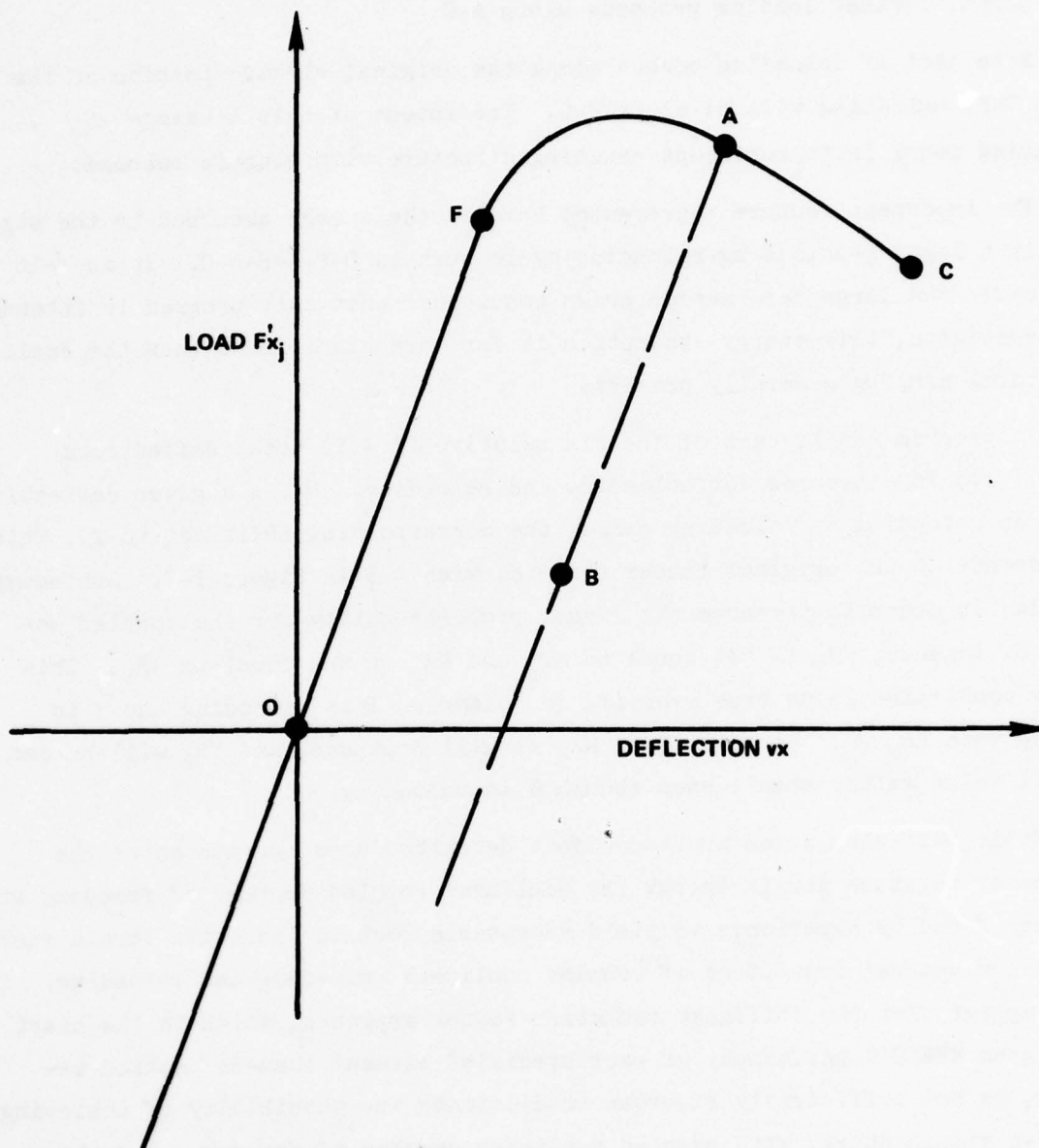


Figure 1-7. Loading - Unloading Model

Loading proceeds along the solid line O-F-A. Unloading then proceeds along dashed line A-B, parallel to the original linear loading line O-F. Subsequent reloading then proceeds along B-A, until point A is reached. At this point, further loading proceeds along A-C.

Note that if unloading occurs along the original elastic portion of the curve O-F, unloading will be along F-O. The intent of this loading-unloading model is to represent crushing structure with elastic rebound.

The important feature represented here is the energy absorbed by the structure in a loading-unloading-reloading cycle such as O-F-A-B-A-C. It is felt that under the large deformation crash conditions that this program is intended to investigate, this energy absorption is far more significant than the small structural damping generally present.

In program KRASH, each of the six relative ($j - i$) total deflections ($v_x \dots v_\psi$) is monitored for unloading and reloading. While a given deflection is in an unloading or reloading phase, the corresponding KR is set to 1. This corresponds to the original linear slope as with A-B in Figure 1-7. Subsequent to this, in order to preserve the linear proportionality for the coupled degrees of freedom, KR_θ is set equal to KR_z and KR_ψ is set equal to KR_y . This latter constraint holds true even if, for example, θ is unloading and z is loading with $KR_z \neq 1$. In this case, $KR_z \neq 1$ will dominate, and KR_θ will be set to this value rather than 1 even though θ is unloading.

While the calculation procedure just described does not guarantee the absence of negative strain energy for nonlinear coupled degrees of freedom, it has been found by experience to yield acceptable results (positive strain energy) except for unusual conditions of coupled nonlinear unloading and reloading. It would appear that the stiffness reduction factor approach, which is the heart of program KRASH's philosophy of user specified element load-deflection behavior, is not sufficiently rigorous to eliminate the possibility of achieving negative strain energy with coupled nonlinear degrees of freedom. A problem formulation based on stress-strain relationships and the compatibility of elemental strains and beam deflections would be required. Such a formulation would involve considerably more computational detail than is used in program KRASH, and would substantially slow down the program execution. In light of

the high degree of success with practical applications of program KRASH, it is felt that the current formulation is quite satisfactory from a practical analysis standpoint, if not from a rigorous analytical viewpoint.

Finally, it should be noted that only the coupled nonlinear degrees of freedom pose potential problems. All linear motion is rigorously correct and never yields negative strain energy, and the uncoupled degrees of freedom (x and ϕ) are well-behaved even with nonlinearities. Since the strain energy of each beam is part of the output, the user will be aware if any beams with negative strain energy exist in the model.

Program KRASH also provides for complete element failure, termed rupture, if any of the six beam relative deflections $\{v\}$ or six total beam forces $\{F_j\}$ exceed specified input values. If any deflection or force exceeds allowable values, that i,j beam element ruptures and all its forces and moments are set to zero for the remainder of the run.

1.3.5.3.5 Unsymmetrical Beam Elements

The beam elements described previously behave symmetrically, meaning that the linear and nonlinear load-deflection characteristics are the same for both positive and negative deflections. Positive deflections yield positive loads, and equal negative deflections result in equal negative loads. For certain modeling situations, it may be desirable to have available beam elements with different characteristics for positive and negative deflections. While providing this capability for the coupled bending degrees of freedom would be unduly complicated for the potential benefits, the uncoupled axial degree of freedom can be treated in a straightforward manner. The axial degree of freedom is also the one wherein unsymmetrical behavior is most common.

Situations calling for unsymmetrical axial load-deflection behavior include "string" type elements such as seat belts or wire braces and diagonal elements representative of shear panel behavior. These applications call for a tension-only element, with zero compression capability. Contact between surfaces not originally touching can be modeled with compression-only elements. An example of this would be an element connecting a landing gear wheel to the

fuselage or wing structure. Until large deformations occur, these surfaces are not in contact. However, after the failure of a landing gear, a wheel may subsequently contact the fuselage or wing. A compression-only element with a deadband could be used to model this type of contact.

Figure 1-8 illustrates the general form of unsymmetrical axial load-deflection characteristic that is allowed in program KRASH. A tension-only element with backlash is illustrated. The load is zero for axial extensions less than DB_{ij} , an input deadband constant for beam ij . Beyond this point, the normal linear/nonlinear beam characteristics are employed, with the following exception. The total (over time) load is never allowed to be negative (for a tension-only element). Therefore, during unloading the path A-B-C is followed, holding Fx_j at zero when a negative value (compression load) would normally occur. Reloading follows C-B-A. The general load-deflection curve for a compression-only element would look like Figure 1-8 except the non-zero loading would be in the lower left quadrant. The input data specifies whether the beam is a tension-only or compression-only element, if it has been identified as an unsymmetrical element.

In order to model a general unsymmetrical element with different non-zero tension and compression properties, two separate beams connecting the same end points are used in the model. One beam is defined as a tension-only element, and the other as a compression only element.

1.3.5.3.6 Damping Forces and Moments

In addition to the nonlinear strain forces and moments derived in the preceding sections, program KRASH also provides for the calculation of damping forces and moments for the internal beams. In order to retain the balance between force and moment for the coupled degrees of freedom inherent in the strain formulation, the damping forces are calculated using the linear stiffness matrix. Naturally, however, these forces are in phase with the velocities rather than the displacements. The resulting model is of the following form.

$$\{FD\} = \frac{2\zeta}{\omega} [K] \{vel\} \quad (1-48)$$

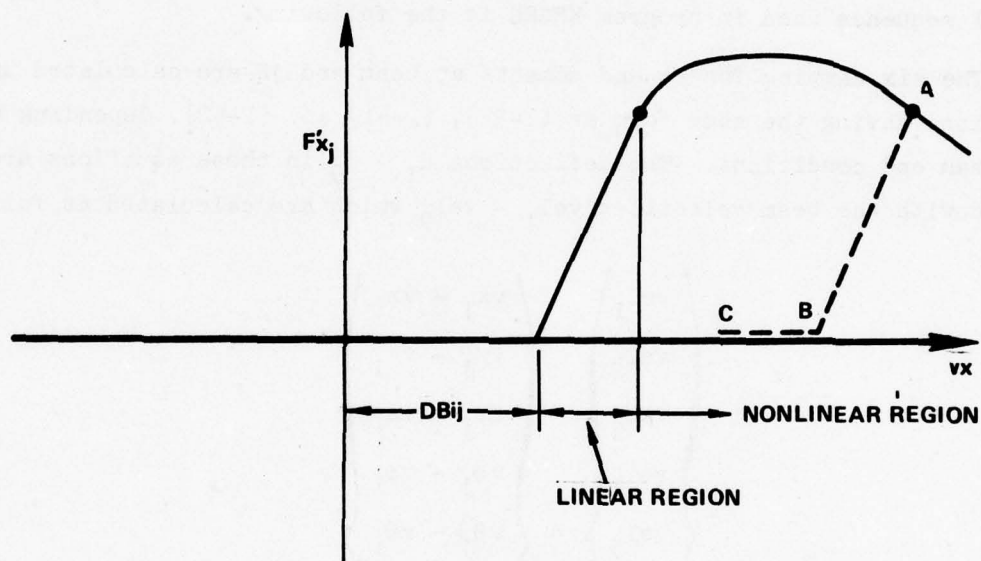


Figure 1-8. Unsymmetrical Axial Load-Deflection Curve

The linear stiffness matrix is multiplied by the beam end point velocity vector. For pure sinusoidal motion, this formulation is the same as conventional structural type damping, in which the damping forces are proportional in magnitude to the strain forces but in phase with the velocity. In such a system, ω would be the response frequency and ζ the damping ratio.

For the actual non-sinusoidal motion of program KRASH, the damping force model could be considered as a pseudo-structural damping model. In this case, the ω in the above equation is taken as the natural frequency of the isolated system consisting of beam ij and the end masses m_i and m_j . The actual computational sequence used in program KRASH is the following.

The six damping forces and moments at beam end jN are calculated using equations having the same form as (1-32), (1-41) and (1-42), depending upon the beam end conditions. The deflections $d_1 - d_9$ in those equations are replaced with the beam velocities $vel_1 - vel_9$ which are calculated as follows

$$\begin{pmatrix} vel_1 \\ vel_2 \\ vel_3 \\ vel_4 \\ vel_5 \\ vel_6 \\ vel_7 \\ vel_8 \\ vel_9 \end{pmatrix} = \begin{pmatrix} vx_j - vx_i \\ vy_j - vy_i \\ vz_j - vz_i \\ v\phi_j - v\phi_i \\ v\theta_j - v\theta_i \\ v\psi_j - v\psi_i \\ v\phi_j + v\phi_i \\ v\theta_j + v\theta_i \\ v\psi_j + v\psi_i \end{pmatrix} \quad (1-49)$$

where the terms on the right are given by Equations (1-20) and (1-22). Similarly, the terms $d\theta_i$, $d\theta_j$, $d\psi_i$, $d\psi_j$ appearing in (1-41) and (1-42) for fixed-pinned end conditions, are replaced by $v\theta_i$, $v\theta_j$, $v\psi_i$ and $v\psi_j$, respectively. The resulting damping forces at jN , in beam axes, are denoted by $\{FD_j\}$, and are shown here for reference.

$$\begin{aligned}
 FDx_j &= k_x \text{ vel}_1 \\
 FDy_j &= k_y \text{ vel}_2 + k_{y\psi} \text{ vel}_9 \\
 FDz_j &= k_z \text{ vel}_3 + k_{z\theta} \text{ vel}_8 \\
 MD\phi_j &= k_\phi \text{ vel}_4 \\
 MD\theta_j &= k_{z\theta} \text{ vel}_3 + \frac{k_\theta}{4} \text{ vel}_5 + \frac{3k_\theta}{4} \text{ vel}_8 \\
 MD\psi_j &= k_{y\psi} \text{ vel}_2 + \frac{k_\psi}{4} \text{ vel}_6 + \frac{3k_\psi}{4} \text{ vel}_9
 \end{aligned}
 \left. \vphantom{\begin{aligned} FDx_j &= k_x \text{ vel}_1 \\ FDy_j &= k_y \text{ vel}_2 + k_{y\psi} \text{ vel}_9 \\ FDz_j &= k_z \text{ vel}_3 + k_{z\theta} \text{ vel}_8 \\ MD\phi_j &= k_\phi \text{ vel}_4 \\ MD\theta_j &= k_{z\theta} \text{ vel}_3 + \frac{k_\theta}{4} \text{ vel}_5 + \frac{3k_\theta}{4} \text{ vel}_8 \\ MD\psi_j &= k_{y\psi} \text{ vel}_2 + \frac{k_\psi}{4} \text{ vel}_6 + \frac{3k_\psi}{4} \text{ vel}_9 \end{aligned}} \right\} \begin{array}{l} \text{(Fixed-Fixed)} \\ (1-50) \end{array}$$

$$\left. \begin{aligned} FDy_j &= \frac{k_y}{4} \text{ vel}_2 + \frac{k_{y\psi}}{2} v\psi_i \\ MD\psi_j &= 0 \end{aligned} \right\} \begin{array}{l} \text{(Pinned at j about y axis)} \\ (1-51a) \end{array}$$

$$\left. \begin{aligned} FDz_j &= \frac{k_z}{4} \text{ vel}_3 + \frac{k_{z\theta}}{2} v\theta_i \\ MD\theta_j &= 0 \end{aligned} \right\} \begin{array}{l} \text{(Pinned at j about z axis)} \\ (1-51b) \end{array}$$

$$\left. \begin{aligned} FDy_j &= \frac{k_y}{4} \text{ vel}_2 + \frac{k_{y\psi}}{2} v\psi_j \\ MD\psi_j &= \frac{k_{y\psi}}{2} \text{ vel}_2 + \frac{3k_\psi}{4} v\psi_j \end{aligned} \right\} \begin{array}{l} \text{(Pinned at i about y axis)} \\ (1-52a) \end{array}$$

$$\left. \begin{aligned} FDz_j &= \frac{k_z}{4} \text{ vel}_3 + \frac{k_{z\theta}}{2} v\theta_j \\ MD\theta_j &= \frac{k_{z\theta}}{2} \text{ vel}_3 + \frac{3k_\theta}{4} v\theta_j \end{aligned} \right\} \begin{array}{l} \text{(Pinned at i about z axis)} \\ (1-52b) \end{array}$$

The result of Equations (1-50), (1-51), and (1-52) is a 6 element force/moment vector $\{FD_j\}$. Each of these elements is next multiplied by a damping coefficient to obtain the actual damping force/moment at the j end of the beam.

$$\{FD_j\} = \begin{bmatrix} c_1 & & & & & \\ & c_2 & & & & \\ & & c_3 & & & \\ & & & c_4 & & \\ & & & & c_5 & \\ & & & & & c_6 \end{bmatrix} \{FD_j\} \quad (1-53)$$

The damping coefficients are calculated as

$$c_K = 2\zeta_{ij}/\omega_k \quad k = 1, \dots, 6 \quad (1-54)$$

where ζ_{ij} is the damping ratio for beam ij which is an input constant. The natural frequency ω_k for each of the 6 beam directions is calculated as

$$\omega_k = \sqrt{\frac{\bar{K}_k(m_i + m_j)}{m_i m_j}} \quad k = 1, 2, 3 \quad (1-55a)$$

$$\omega_{k+3} = \sqrt{\frac{K_{k+3}(I_{ik} + I_{jk})}{I_{ik} I_{jk}}} \quad k = 1, 2, 3 \quad (1-55b)$$

Equations (1-55) are the natural frequency equations for a beam with concentrated inertias at each end. The 6 \bar{K}_k 's used in (1-55) are just the diagonal elements of the stiffness matrix for beam ij .

$$\begin{Bmatrix} \bar{K}_1 \\ \bar{K}_2 \\ \bar{K}_3 \\ \bar{K}_4 \\ \bar{K}_5 \\ \bar{K}_6 \end{Bmatrix} = \begin{Bmatrix} k_x \\ k_y \\ k_z \\ k_\phi \\ k_\theta \\ k_\psi \end{Bmatrix}_{ij} \quad (1-56)$$

These terms were defined in Equations (1-28), (1-29c) and (1-30c). The inertia terms I_{ik} and I_{jk} , $k = 1, 2, 3$, are the inertias of mass i and j , resolved into beam ij axes. These are given by the diagonal elements of the following matrices.

$$[I_i]_{ij \text{ axes}} = [AIJTAI] \underset{\substack{\text{mass} \\ \text{axes}}}{[I_i]} [AIJTAI]^T \quad (1-57a)$$

$$[I_j]_{ij \text{ axes}} = [AIJTAJ] \underset{\substack{\text{mass} \\ \text{axes}}}{[I_j]} [AIJTAJ]^T \quad (1-57b)$$

All quantities in equations (1-54) through (1-57) are constants which do not vary with time. Therefore, these items are calculated just once prior to the main time loop in program KRASH. Equation (1-53) for the damping force vector is, of course, within the time loop. In Equation (1-57), the time zero values of $[AIJTAI]$ and $[AIJTAJ]$ are used, since these are functions of $[A_{ij}]$, $[A_i]$ and $[A_j]$. Although all three of these component matrices are time-varying, their time zero values correspond to an undistorted vehicle and yield the proper transformation from mass to beam axes for the undeformed structure.

1.3.5.3.7 Total Internal Beam Forces and Moments

Equations (1-46a) and (1-53) yield the strain and damping forces and moments at jN . These are denoted $\{F_j'\}$ and $\{FD_j'\}$, respectively. The corresponding quantities at the iM end of the beam are calculated using the static balance Equations (1-32b). These are denoted $\{F_i'\}$ and $\{FD_i'\}$. These four independent sets of forces/moments are used to calculate the internal beam strain and damping energies. These calculations are described in Section 1.3.16. After the energy calculations, we no longer need the strain and damping forces separately. Therefore, the two are now added together to form the total internal beam load.

$$\{FS_i\} = \{F_i'\} + \{FD_i'\} \quad (1-58a)$$

$$\{FS_j\} = \{F_j'\} + \{FD_j'\} \quad (1-58b)$$

These forces are in beam axes with positive directions indicated in Figure 1-4, which shows the forces acting on beam ij. To get the forces acting on masses m_i and m_j , we must reverse the signs and resolve the vectors from beam axes to mass axes.

$$\{FS_i'\} = - [AIJTAI]^T \{FS_i\} \quad (1-59a)$$

$$\{FS_j'\} = - [AIJTAJ]^T \{FS_j\} \quad (1-59b)$$

where the transformation matrices are defined by Equation (1-18). These forces act at beam ends iM and jN in mass axes.

The moments acting on the masses must now be corrected to account for the offset of the node points from the masses. Figure 1-2 shows the offset, where the vector $\{rx, ry, rz\}$ contains the offset components in mass fixed axes. These are not time-varying quantities, since each node point is rigidly attached to a defined mass point. The moments at the mass points are given by

$$\begin{Bmatrix} FS_{i_4}' \\ FS_{i_5}' \\ FS_{i_6}' \end{Bmatrix} = \begin{Bmatrix} FS_{i_4}' \\ FS_{i_5}' \\ FS_{i_6}' \end{Bmatrix} + [TR_{iM}] \begin{Bmatrix} FS_{i_1}' \\ FS_{i_2}' \\ FS_{i_3}' \end{Bmatrix} \quad (1-60a)$$

$$\begin{Bmatrix} FS_{j_4}' \\ FS_{j_5}' \\ FS_{j_6}' \end{Bmatrix} = \begin{Bmatrix} FS_{j_4}' \\ FS_{j_5}' \\ FS_{j_6}' \end{Bmatrix} + [TR_{jN}] \begin{Bmatrix} FS_{j_1}' \\ FS_{j_2}' \\ FS_{j_3}' \end{Bmatrix} \quad (1-60b)$$

(1-59b)

where the first vectors on the right hand side are the three moments from Equation (1-59). These moments act at the node points rather than at the masses. The second vector contains the three forces from (1-59) which act at the node points. The transformation matrices are of the following skew-symmetric form:

$$[TR_{iM}] = \begin{bmatrix} 0 & -rz & ry \\ rz & 0 & -rx \\ -ry & rx & 0 \end{bmatrix}_{iM} \quad (1-61a)$$

$$[TR_{jN}] = \begin{bmatrix} 0 & -rz & ry \\ rz & 0 & -rx \\ -ry & rx & 0 \end{bmatrix}_{jN} \quad (1-61b)$$

These are not time-varying matrices.

Equations (1-59) and (1-60) give the current internal beam forces and moments acting on masses m_i and m_j , due to beam ij , in mass-fixed axes. To obtain the total internal forces and moments acting on each mass, the contributions from each internal beam connecting to a given mass must be accounted for. In program KRASH, this is done within the beam ij loop where $\{FS_i'\}$ and $\{FS_j'\}$ are calculated. These are merely added to the total internal forces and moments for mass i and mass j .

$$\begin{Bmatrix} X_I \\ Y_I \\ Z_I \\ L_I \\ M_I \\ N_I \end{Bmatrix}_i = \begin{Bmatrix} X_I \\ Y_I \\ Z_I \\ L_I \\ M_I \\ N_I \end{Bmatrix}_i + \{FS_i'\} \quad (1-62a)$$

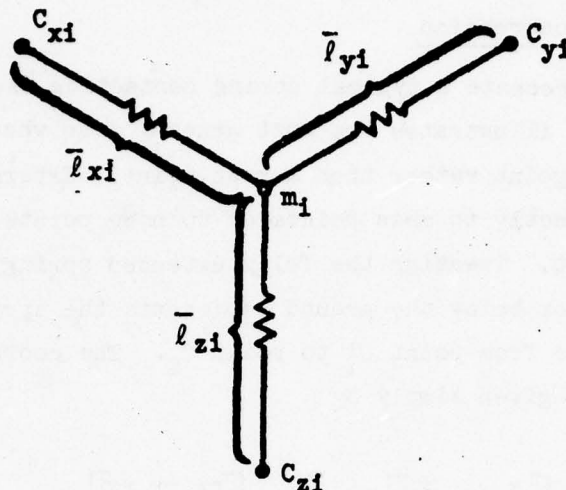
$$\begin{Bmatrix} X_I \\ Y_I \\ Z_I \\ L_I \\ M_I \\ N_I \end{Bmatrix}_j = \begin{Bmatrix} X_I \\ Y_I \\ Z_I \\ L_I \\ M_I \\ N_I \end{Bmatrix}_j + \{FS_j'\} \quad (1-62b)$$

Equations (1-62) should be interpreted as follows. At each time cut, prior to entering the beam loop which calculates the beam forces for all the ij beams in the model, $(X_{I_i} \dots, N_{I_i})$ are all set to zero for all masses i . Equation (1-62) is then employed for each beam in turn, where $\{FS_i'\}$ and $\{FS_j'\}$ are added to the total internal beam forces acting on the proper masses i and j , respectively. Once all the beams have been calculated in the beam loop, $(X_{I_i} \dots, N_{I_i})$ will contain the contributions from all beams connecting to mass m_i , for all the masses in the model.

1.3.5.4 External Forces and Moments

The crash forces result from the compression of external springs radiating from selected mass or node points, when these springs contact either the ground

plane ($z = 0$) or the slope ($z_{s1} = 0$). The following sketch shows the three spring radiating outward from mass i :



The free (uncompressed) lengths of the three springs are denoted \bar{l}_{xi} , \bar{l}_{yi} , and \bar{l}_{zi} . These springs lie along the body axes for the i th mass. \bar{l}_{xi} , \bar{l}_{yi} , and \bar{l}_{zi} are input either positive or negative, depending upon whether the spring radiates outward along the positive or negative body axis. Those shown above are all positive springs. C_{xi} , C_{yi} , and C_{zi} are the end points of the fully extended springs. Only data for those springs desired in the analysis need be input; if no spring is input, its crash forces are set to zero. Typically, only those masses at the extremities of the vehicle likely to contact the ground would have crash springs. The intent of these springs is to represent crushable external structure such as found on the lower fuselage and nose sections.

The first step in the calculation is to determine which of the C_{xi} , C_{yi} , and C_{zi} spring end points are below the ground or slope. Only these springs are further analyzed to determine their crash forces. For these springs, the spring compression along the spring axis is determined, as well as the compression velocity and the ground contact point velocity. Then the spring force along the spring axis is calculated, from which the vertical load in ground axes at the ground contact point is obtained. From this vertical load and an input friction coefficient, the ground drag load is computed. The direction of this load is opposite the ground contact point velocity vector.

Finally, the three forces at the ground contact point are rotated into ith mass body axes, and the resulting forces and moments at mass i are calculated.

1.3.5.4.1 Spring Compression

Figure 1-9 represents a typical spring contacting the ground at an oblique angle. This figure illustrates the most general case where the spring is attached to a node point rather than a mass point. External springs can be attached either directly to mass points or to node points. Point C_i is the ground contact point. Treating the fully extended spring as a vector, that portion of the vector below the ground represents the spring compression. This is the distance from point C_i to point C_i . The coordinates of point C_i , in ground axes, are given simply by

$$\begin{bmatrix} x_{ci} & y_{ci} & z_{ci} \\ y_{ci} & y_{ci} & y_{ci} \\ z_{ci} & z_{ci} & z_{ci} \end{bmatrix} = \begin{bmatrix} x_i & x_i & x_i \\ y_i & y_i & y_i \\ z_i & z_i & z_i \end{bmatrix} + [A_i] \begin{bmatrix} r_x & r_x & r_x \\ r_y & r_y & r_y \\ r_z & r_z & r_z \end{bmatrix} + [A_i] \begin{bmatrix} \bar{\ell}_{xi} \\ \bar{\ell}_{yi} \\ \bar{\ell}_{zi} \end{bmatrix} \quad (1-63)$$

The above equation gives the coordinates of all three C_i for mass i; these points are denoted C_{xi} , C_{yi} , and C_{zi} . Figure 1-9 shows only one of the three springs, so the nomenclature in Figure 1-9 is not subscripted to indicate whether an x, y or z spring is shown. The third term in the above equation is equal to dx_{ci} , dy_{ci} , and dz_{ci} in Figure 1-9:

$$\begin{bmatrix} dx_{ci} & dy_{ci} & dz_{ci} \\ dy_{ci} & dy_{ci} & dy_{ci} \\ dz_{ci} & dz_{ci} & dz_{ci} \end{bmatrix} = [A_i] \begin{bmatrix} \bar{\ell}_{xi} \\ \bar{\ell}_{yi} \\ \bar{\ell}_{zi} \end{bmatrix} \quad (1-64)$$

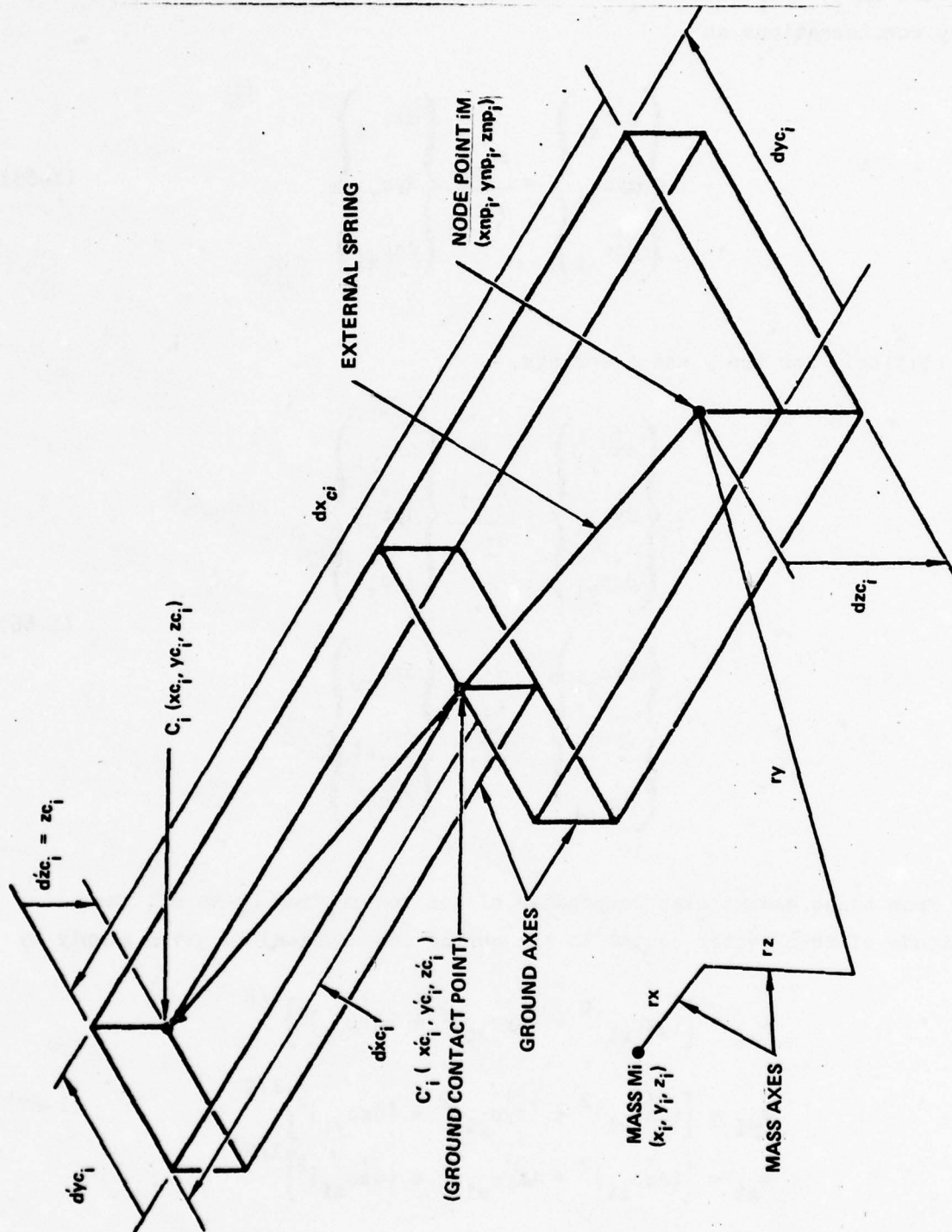


Figure 1-9. External Spring Compression Geometry

The \dot{dxc}_i , \dot{dyc}_i , and \dot{dzc}_i in Figure 1-9 can be determined from proportionality considerations as

$$\begin{Bmatrix} \dot{dxc}_{xi} \\ \dot{dyc}_{xi} \\ \dot{dzc}_{xi} \end{Bmatrix} = \frac{z_{c_{xi}}}{dzc_{xi}} \begin{Bmatrix} dxc_{xi} \\ dyc_{xi} \\ dzc_{xi} \end{Bmatrix} \quad (1-65)$$

and similarly for the y and z springs,

$$\begin{Bmatrix} \dot{dxc}_{yi} \\ \dot{dyc}_{yi} \\ \dot{dzc}_{yi} \end{Bmatrix} = \frac{z_{c_{yi}}}{dzc_{yi}} \begin{Bmatrix} dxc_{yi} \\ dyc_{yi} \\ dzc_{yi} \end{Bmatrix}$$

$$\begin{Bmatrix} \dot{dxc}_{zi} \\ \dot{dyc}_{zi} \\ \dot{dzc}_{zi} \end{Bmatrix} = \frac{z_{c_{zi}}}{dzc_{zi}} \begin{Bmatrix} dxc_{zi} \\ dyc_{zi} \\ dzc_{zi} \end{Bmatrix} \quad (1-66)$$

From these ground axes components of the vector from C'_i to C_i , the magnitude of this vector (equal to the spring compression) is given simply by

$$s_{xi} = \left[(\dot{dxc}_{xi})^2 + (\dot{dyc}_{xi})^2 + (\dot{dzc}_{xi})^2 \right]^{1/2}$$

$$s_{yi} = \left[(\dot{dxc}_{yi})^2 + (\dot{dyc}_{yi})^2 + (\dot{dzc}_{yi})^2 \right]^{1/2}$$

$$s_{zi} = \left[(\dot{dxc}_{zi})^2 + (\dot{dyc}_{zi})^2 + (\dot{dzc}_{zi})^2 \right]^{1/2} \quad (1-67)$$

In order to simplify the notation, the following vectors and matrices are defined ($i = 1, 2, \dots, N$ indicates the mass; $j = 1, 2, 3$ indicates the direction; $k = 1, 2, 3$ indicates which spring):

$$\bar{l}_{ik} \triangleq \begin{Bmatrix} \bar{l}_{xi} \\ \bar{l}_{yi} \\ \bar{l}_{zi} \end{Bmatrix} \quad v_{a_{ij}} \triangleq \begin{Bmatrix} x_i \\ y_i \\ z_i \end{Bmatrix} \quad s_{ik} \triangleq \begin{Bmatrix} s_{xi} \\ s_{yi} \\ s_{zi} \end{Bmatrix}$$

$$dvc_{ijk} \triangleq \sum_j \begin{bmatrix} dxc_{xi} & dxc_{yi} & dxc_{zi} \\ dyc_{xi} & dyc_{yi} & dyc_{zi} \\ dzc_{xi} & dzc_{yi} & dzc_{zi} \end{bmatrix}$$

k

(1-68)

$$vc_{ijk} \triangleq \sum_j \begin{bmatrix} xc_{xi} & xc_{yi} & xc_{zi} \\ yc_{xi} & yc_{yi} & yc_{zi} \\ zc_{xi} & zc_{yi} & zc_{zi} \end{bmatrix}$$

k

$$\dot{dvc}_{ijk} \triangleq \sum_j \begin{bmatrix} \dot{dxc}_{xi} & \dot{dxc}_{yi} & \dot{dxc}_{zi} \\ \dot{dyc}_{xi} & \dot{dyc}_{yi} & \dot{dyc}_{zi} \\ \dot{dzc}_{xi} & \dot{dzc}_{yi} & \dot{dzc}_{zi} \end{bmatrix}$$

k

Using this nomenclature, equations (1-63) through 1-67) become simply

$$vc_{ijk} = v_{a_{ij}} + dvr_{ij} + dvc_{ijk} \quad (1-69)$$

$$\{dvr_i\} = [A_i] \begin{Bmatrix} rx \\ ry \\ rz \end{Bmatrix}_{iM} \quad (1-70)$$

$$\dot{dvc}_{ijk} = A_{ijk} \bar{\ell}_{ik} \quad (1-71)$$

$$\dot{dvc}_{ijk} = \frac{vc_{i3k}}{dvc_{i3k}} \dot{dvc}_{ijk} \quad (1-72)$$

$$s_{ik} = \left[\sum_{j=1}^3 (\dot{dvc}_{ijk})^2 \right]^{1/2} \quad (1-73)$$

The spring compression velocity, \dot{s}_{ik} , is also required. This is given by differentiating Equation (1-73) as

$$\dot{s}_{ik} = \frac{1}{2s_{ik}} \sum_{j=1}^3 2 \dot{dvc}_{ijk} (\dot{dvc}_{ijk}) \quad (1-74)$$

where the last term is obtained from (1-72) as

$$\dot{dvc}_{ijk} = \frac{vc_{i3k}}{dvc_{i3k}} \dot{dvc}_{ijk} + dvc_{ijk} \frac{\dot{dvc}_{i3k} \dot{vc}_{i3k} - vc_{i3k} \dot{dvc}_{i3k}}{(dvc_{i3k})^2} \quad (1-75)$$

The time derivatives in (1-75) are given by

$$\dot{dvc}_{ijk} = \dot{A}_{ijk} \bar{\ell}_{ik} \quad j = 1, 2, 3 \quad (1-76)$$

$$\dot{vc}_{ijk} = \dot{z}_i + \dot{dvr}_{ij} + \dot{dvc}_{ijk} \quad j = 1, 2, 3 \quad (1-77)$$

$$\left\{ \dot{dvr}_i \right\} = [\dot{A}_i] \begin{Bmatrix} rx \\ ry \\ rz \end{Bmatrix}_{iM} \quad (1-78)$$

The above equations are appropriate if the spring intersects the horizontal ground plane. If the spring intersects the sloping ground plane, the following equations are utilized:

$$vcs_{ijk}^l = \sum_{\ell=1}^3 ABETA_{j\ell} v_{i\ell k} \quad (1-79)$$

$$dvcs_{ijk}^l = \sum_{\ell=1}^3 ABETA_{j\ell} dv_{i\ell k} \quad (1-80)$$

$$dvcs'_{ijk} = \frac{vcs_{i3k}^l}{dvcs_{i3k}^l} dvcs_{ijk}^l \quad (1-81)$$

$$s_{ik} = \left[\sum_{j=1}^3 \left(dvcs'_{ijk} \right)^2 \right]^{1/2} \quad (1-82)$$

$$\dot{s}_{ik} = \frac{1}{2s_{ik}} \sum_{j=1}^3 2 dvcs'_{ijk} \left(dvcs'_{ijk} \right) \quad (1-83)$$

$$\begin{aligned} dvcs'_{ijk} &= \frac{vcs_{i3k}^l}{dvcs_{i3k}^l} dvcs_{ijk}^l \\ &+ dvcs_{ijk}^l \frac{dvcs_{i3k}^l vcs_{i3k}^l - vcs_{i3k}^l dvcs_{i3k}^l}{\left(dvcs_{i3k}^l \right)^2} \end{aligned} \quad (1-84)$$

$$dvcs_{ijk}^l = \sum_{\ell=1}^3 ABETA_{j\ell} dv_{i\ell k} \quad (1-85)$$

$$vcs_{13k} = (\sin \beta) \dot{v}_{1lk} + (\cos \beta) \dot{v}_{13k} \quad (1-86)$$

1.3.5.4.2 Ground Contact Point Velocity

The next computation required is to determine the spring contact point velocity in the ground plane (either the horizontal ground plane or the slope plane, whichever the spring is contacting). This is necessary to determine the line of action of the ground plane drag load, which is opposite to the contact point velocity vector. The velocity of point C' with respect to ground is given in vector notation as

$${}^0 \overrightarrow{V}^{C'} = m_i \overrightarrow{V}^{C'} + {}^0 \overrightarrow{V}^{C'} \quad (1-87)$$

where

$${}^0 \overrightarrow{V}^{C'} = \text{velocity of } C' \text{ with respect to ground}$$

$$m_i \overrightarrow{V}^{C'} = \text{velocity of } C' \text{ with respect to } m_i$$

$${}^0 \overrightarrow{V}^{C'} = \text{velocity of point fixed in } m_i, \text{ instantaneously coinciding with point } C', \text{ with respect to ground}$$

This latter term is given by

$${}^0 \overrightarrow{V}^{C'} = {}^0 \overrightarrow{V}^{m_i} + {}^0 \omega_i^{m_i} \times \vec{R}_{iKM} \quad (1-88)$$

where

${}^0 \vec{V}_{m_1}$ = velocity of m_1 with respect to ground

${}^0 \vec{\omega}_{m_1}$ = rotational velocity of m_1 with respect to ground

\vec{R}_{ikM} = vector from m_1 to spring/ground contact point C'

Figure 1-10 illustrates the geometry involved. The vector \vec{R}_{ikM} is given by

$$\begin{Bmatrix} Rx \\ Ry \\ Rz \end{Bmatrix}_{ikM} = \begin{Bmatrix} rx \\ ry \\ rz \end{Bmatrix}_{ikM} + \sum_{k=1} \begin{Bmatrix} \ell_{i1} \\ 0 \\ 0 \end{Bmatrix} \text{ or } \sum_{k=2} \begin{Bmatrix} 0 \\ \ell_{i2} \\ 0 \end{Bmatrix} \text{ or } \sum_{k=3} \begin{Bmatrix} 0 \\ 0 \\ \ell_{i3} \end{Bmatrix} \quad (1-89)$$

The components of (1-87) and (1-88) are given by

$$m_1 \vec{V}_{C'} = -\dot{s}_{ik} \bar{n}_{ik} \quad (\text{body axes}) \quad (1-90)$$

$${}^0 \vec{V}_{m_1} = \dot{x}_i \bar{n}_x + \dot{y}_i \bar{n}_y + \dot{z}_i \bar{n}_z \quad (\text{ground axes}) \quad (1-91)$$

$${}^0 \vec{\omega}_{m_1} \times \vec{R}_{ikM} = \begin{bmatrix} 0 & -r_i & q_i \\ r_i & 0 & -p_i \\ -q_i & p_i & 0 \end{bmatrix} \begin{Bmatrix} Rx \\ Ry \\ Rz \end{Bmatrix}_{ikM} \quad (\text{body axes}) \quad (1-92)$$

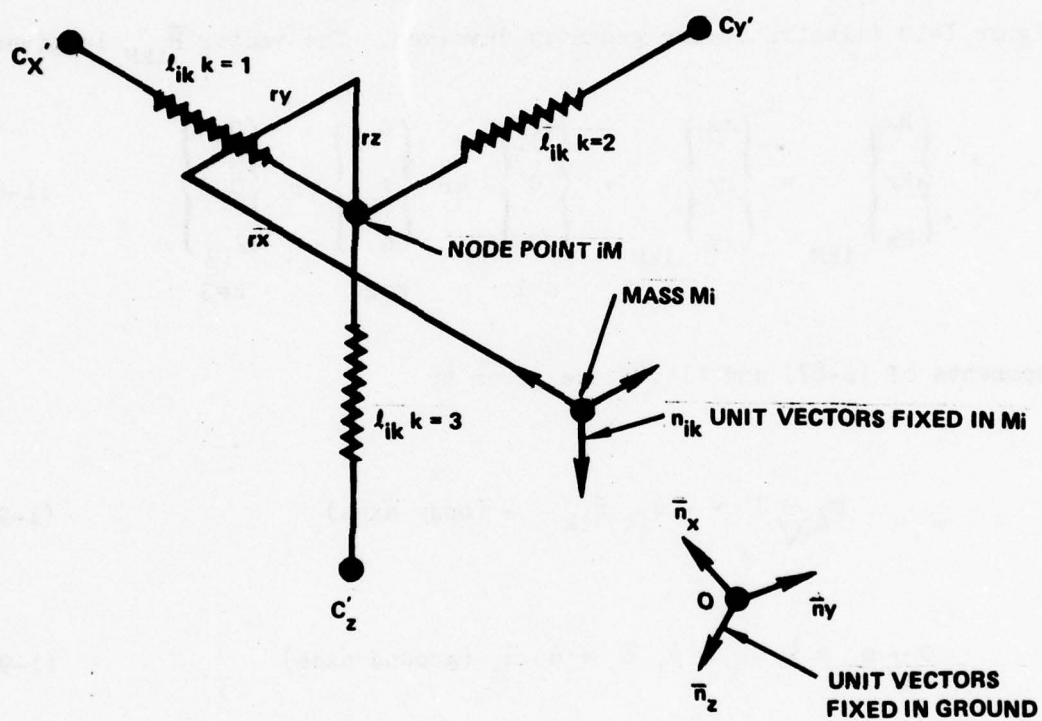


Figure 1-10. External Spring Geometry

Combining the above equations, the ground contact point velocity is given by

$$\begin{aligned}
 \vec{V}_{C'} &\triangleq \{vcp\}_{ikM} = \begin{Bmatrix} \dot{x}_i \\ \dot{y}_i \\ \dot{z}_i \end{Bmatrix} + [A_i] \begin{Bmatrix} -\dot{s}_{i1} \\ 0 \\ 0 \end{Bmatrix} \text{ or } \begin{Bmatrix} 0 \\ -\dot{s}_{i2} \\ 0 \end{Bmatrix} \text{ or } \begin{Bmatrix} 0 \\ 0 \\ -\dot{s}_{i3} \end{Bmatrix} \\
 &+ [A_i] \begin{bmatrix} 0 & -r_i & q_i \\ r_i & 0 & -p_i \\ -q_i & p_i & 0 \end{bmatrix} \begin{Bmatrix} rx \\ ry \\ rz \end{Bmatrix}_{iM} \\
 &+ [A_i] \begin{bmatrix} 0 & -r_i & q_i \\ r_i & 0 & -p_i \\ -q_i & p_i & 0 \end{bmatrix} \begin{Bmatrix} l_{i1} \\ 0 \\ 0 \end{Bmatrix} \text{ or } \begin{Bmatrix} 0 \\ l_{i2} \\ 0 \end{Bmatrix} \text{ or } \begin{Bmatrix} 0 \\ 0 \\ l_{i3} \end{Bmatrix}
 \end{aligned}
 \tag{1-93}$$

where the three options apply to $k = 1, 2$ or 3 in the order shown. In other words, Equation (1-93) represents three equations, applicable to either an x , y or z ($k = 1, 2$ or 3) direction external spring. The time varying spring length l_{ik} in Equation (1-93) is calculated as

$$l_{ikM} = \text{SIGN} \left(\bar{l}_{ikM} \right) \left[\left| \bar{l}_{ikM} \right| - s_{ikM} \right]
 \tag{1-94}$$

This form is used so that l_{ikM} has the same sign as the input \bar{l}_{ikM} , which as mentioned earlier can be negative to allow springs in the negative direction of the body axes. These spring lengths are shown in Figure 1-10; the points C' in this figure are the ground contact points. If an external spring is directly connected to a mass m_i instead of a node point, then (rx, ry, rz) are all zero.

If the spring is contacting the slope rather than the horizontal ground, the above velocities are transformed into slope axes as follows:

$$vcpsl_{ijk} = \sum_{l=1}^3 ABETA_{jl} \dot{vcp}_{ilk} \quad (1-95)$$

1.3.5.4.3 External Spring Axial Force

This section discusses the calculation of the external spring force along the spring axis. The axial force in the spring, denoted $FSPO_{ikM}$, is input as a tabular function of the spring compression s_{ikM} . As with the internal forces, unloading along an elastic line is included. However, unlike the internal forces, an extension load is not allowed; positive $FSPO_{ikM}$ is a compressive load acting at the ground contact point along the axis of spring ikM .

Figure 1-11 illustrates the shape of the input external spring load-deflection curve. SI , SA , SB , SF , $FSPOI$, $FSPOF$ and Ke are all input constants.

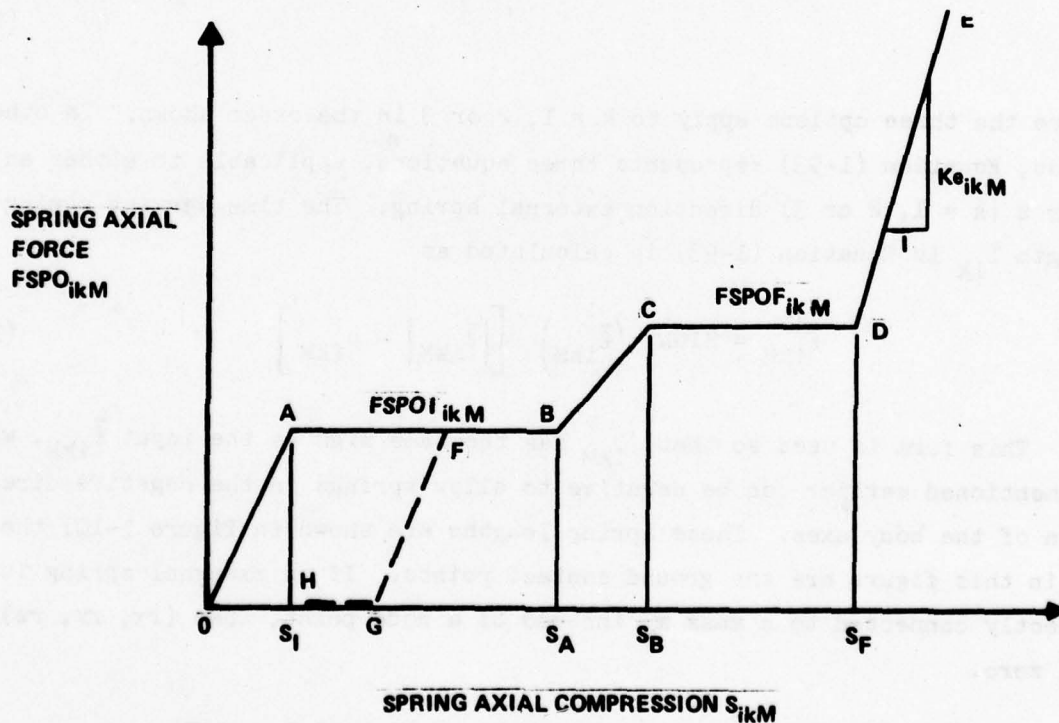


Figure 1-11. External Spring Load-Stroke Curve

Loading proceeds along O-A-B-C-D-E. At any spring compression s_{ikM} less than SA, unloading occurs along a line having the same slope as O-A. At any spring compression between SA and SF, unloading occurs along a line parallel to B-C. (If an extension of this unloading line would cross above O-A-B, resulting in more energy released during unloading than input during loading, then the unloading curve is parallel to O-A rather than B-C.) Once SF is reached, all subsequent loading and unloading follows line D-E and its extension in both directions. In all cases, unloading does not extend beyond $FSP0 = 0$. For example, if unloading begins at F, it proceeds along F-G (parallel to O-A), and then holds at $FSP0 = 0$ from G to H. Subsequent reloading takes place along H-G-F-B-C-D-E. There is no rupture of external spring elements.

A first-order approximation of the effect of ground flexibility is included in the following manner. A ground flexibility constant $f_{g_{ikM}}$ is input for each external spring. The deflection coordinates in Figure 1-11 are modified to include this flexibility.

$$\begin{aligned} SIFL_{ikM} &= SI_{ikM} + FSP0I_{ikM} * f_{g_{ikM}} \\ SAFL_{ikM} &= SA_{ikM} + FSP0I_{ikM} * f_{g_{ikM}} \\ SBFL_{ikM} &= SB_{ikM} + FSP0F_{ikM} * f_{g_{ikM}} \\ SFFL_{ikM} &= SF_{ikM} + FSP0F_{ikM} * f_{g_{ikM}} \end{aligned} \quad (1-96)$$

This has the effect of softening the input load-deflection curve representing the airplane structure to include the flexibility of the ground in series with the structure. The bottoming spring constant is modified as follows:

$$KEFL_{ikM} = \frac{1}{\frac{1}{k_{e_{ikM}}} + f_{g_{ikM}}} \quad (1-97)$$

The ground deflection is calculated for each spring at each time cut as

$$DELG_{ikM} = FSPO_{ikM} * fg_{ikM} \quad (1-98)$$

Furthermore, the ground is never allowed to rebound; the ground deflection always increases or stays constant. This is accomplished by setting $DELG_{ikM}$ at each time step to the maximum of the current value and the previous maximum. The ground deflection must also be accounted for in the calculation of the deflected spring length from Equation (1-94).

$$l_{ikM} = SIGN(\bar{l}_{ikM}) \left[|\bar{l}_{ikM}| - s_{ikM} + DELG_{ikM} \right] \quad (1-99)$$

In effect, the spring compression s_{ikM} is reduced by the amount that is directly attributable to ground deflection, since the spring/ground interface is actually lower than would be calculated for a rigid ground.

The flow diagram for the calculation of the spring-force $FSPO_{ik}$ is shown in Figure 1-12. The calculations are performed within nested i and k loops. Immediately prior to the calculations shown in Figure 1-12, there is a test to see if an external spring exists for the ik pair being considered. If a spring exists, it is checked to see if it is in contact with either the horizontal ground or the slope. If both these tests are satisfied, the algorithm shown in Figure 1-12 is entered, otherwise this block of coding is skipped. In Figure 1-12, SK is the spring compression s_{ik} .

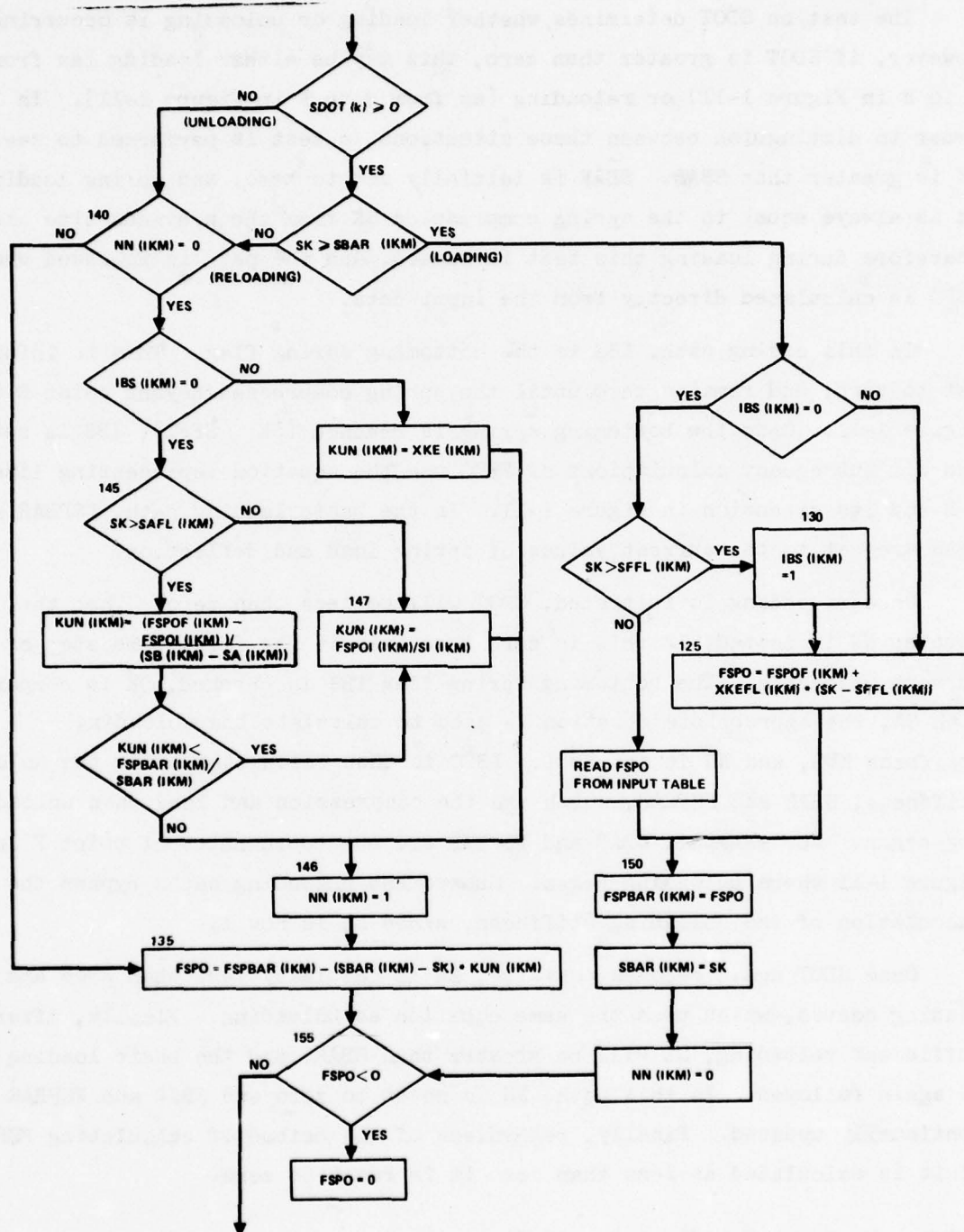


Figure 1-12. External Load Calculation

The test on SDOT determines whether loading or unloading is occurring. However, if SDOT is greater than zero, this may be either loading (as from A to B in Figure 1-11) or reloading (as from G to F in Figure 1-11). In order to distinguish between these situations, a test is performed to see if SK is greater than SBAR. SBAR is initially set to zero, and during loading it is always equal to the spring compression SK from the previous time step. Therefore during loading this test is passed, and the path is followed wherein FSPO is calculated directly from the input data.

In this coding path, IBS is the bottoming spring flag. This is initially set to zero, and remains zero until the spring compresses beyond point D in Figure 1-11. Once the bottoming spring is reached ($SK > SFFL$), IBS is set to 1 and all subsequent calculations of FSPO use the equation representing line D-E and its extension in Figure 1-11. In the basic loading path, FSPBAR and SBAR are set to the current values of spring load and deflection.

Once unloading is initiated, SDOT will be less than zero. Then the counter NN is tested; if this is zero then this is the first time step of the current unloading. The bottoming spring flag IBS is checked, SK is compared with SA, the appropriate equation is used to calculate the unloading stiffness KUN, and NN is set to 1. FSPO is then calculated using the unloading stiffness, SBAR and FSPBAR, which are the compression and load when unloading began. For example, SBAR and FSPBAR are the coordinates of point F in Figure 1-11 where unloading began. Subsequent unloading paths bypass the calculation of the unloading stiffness, since NN is now 1.

Once SDOT again becomes positive, SK is initially less than SBAR and reloading occurs, which uses the same equation as unloading. Finally, after sufficient reloading, SK will be greater than SBAR, and the basic loading path is again followed. In this path, NN is reset to zero and SBAR and FSPBAR are continually updated. Finally, regardless of the method of calculating FSPO, if it is calculated as less than zero it is reset to zero.

1.3.5.4.4 Crash Forces at Ground Contact Point

The three components of the ground interaction force at the ground contact point are denoted by $XVOC_{ijk}$, where, as before, i refers to the ith

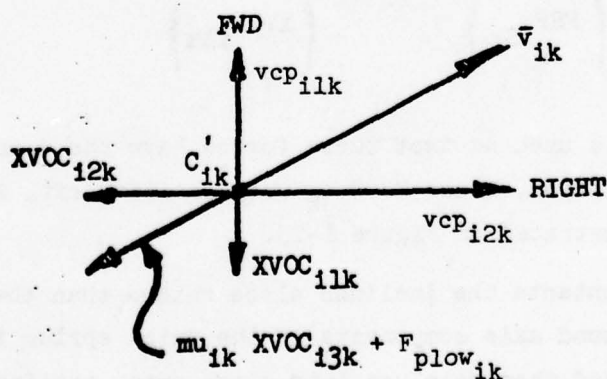
mass, j to the force direction, and k to the k th spring for mass i . First the component of the axial spring force perpendicular to the ground is computed. This is positive upward acting on the spring. This is given simply by resolving $FSPO_{ik}$ into ground axes and retaining only the vertical component.

$$XVOC_{i3k} = A_{i3k} FSPO_{ik} \text{SIGN}(\bar{\ell}_{ik}) \quad k = 1, 2, 3 \quad (1-100)$$

since $FSPO_{ik}$ acts along the k th body axis for mass i . The $\text{SIGN}(\bar{\ell}_{ik})$ term is necessary to retain the convention of $XVOC_{i3k}$ acting positive upward with negative springs. The ground plane components of the axial force $FSPO_{ik}$ are ignored, since these values are next computed on the assumption that they are functions of the ground-spring friction coefficient. The ground plane velocity vector, from Equation (1-93), has the magnitude

$$\bar{v}_{ik} = \left[(\dot{v}_{cp_{i1k}})^2 + (\dot{v}_{cp_{i2k}})^2 \right]^{1/2} \quad (1-101)$$

This is shown in the following sketch, a plan view looking downward at ground contact point C'_{ik} :



The magnitude of the resultant ground plane load is given by $(\mu_{ik} X_{VOC_{i3k}} + F_{plow_{ik}})$, i.e., an input friction coefficient times the vertical load perpendicular to the ground plane, plus a constant plowing force. $F_{plow_{ik}}$ and μ_{ik} are input constants. $F_{plow_{ik}}$ is a constant plowing force that acts from $t = 0$ to $t = PLOWT$, an input constant, and then drops to 0 for the remainder of the run. μ_{ik} and $F_{plow_{ik}}$ together allow the program user to calculate a drag load that is either dependent on the vertical load or is a constant. The direction of the total ground plane load is opposite to the contact point velocity vector \bar{v}_{ik} , as shown in the above sketch. Therefore, the drag and side loads at point C'_{ik} , in ground axes, are given by

$$X_{VOC_{ijk}} = \left[\mu_{ik} X_{VOC_{i3k}} + F_{plow_{ik}} \right] \frac{v_{cp_{ijk}}}{\bar{v}_{ik}} \quad j = 1, 2 \quad (1-102)$$

These are illustrated in the above sketch. These forces are now resolved back into ith mass body axes; these resolved forces are denoted by FSP_{ijk} .

We have

$$\begin{Bmatrix} FSP_{11k} \\ FSP_{12k} \\ FSP_{13k} \end{Bmatrix} = -[A_i]^T \begin{Bmatrix} X_{VOC_{11k}} \\ X_{VOC_{12k}} \\ X_{VOC_{13k}} \end{Bmatrix} \quad k = 1, 2, 3 \quad (1-103)$$

The minus sign is used so that these forces have the same sense as the basic body axis convention, since $X_{VOC_{ijk}}$ were positive aft, left and upward. These forces are illustrated in Figure 1-13.

If the spring contacts the inclined slope rather than the horizontal ground, all three ground axis components of the axial spring force $FSP_{0_{ik}}$ are obtained first, and then resolved into slope axes, retaining only the component normal to the slope. For this situation,

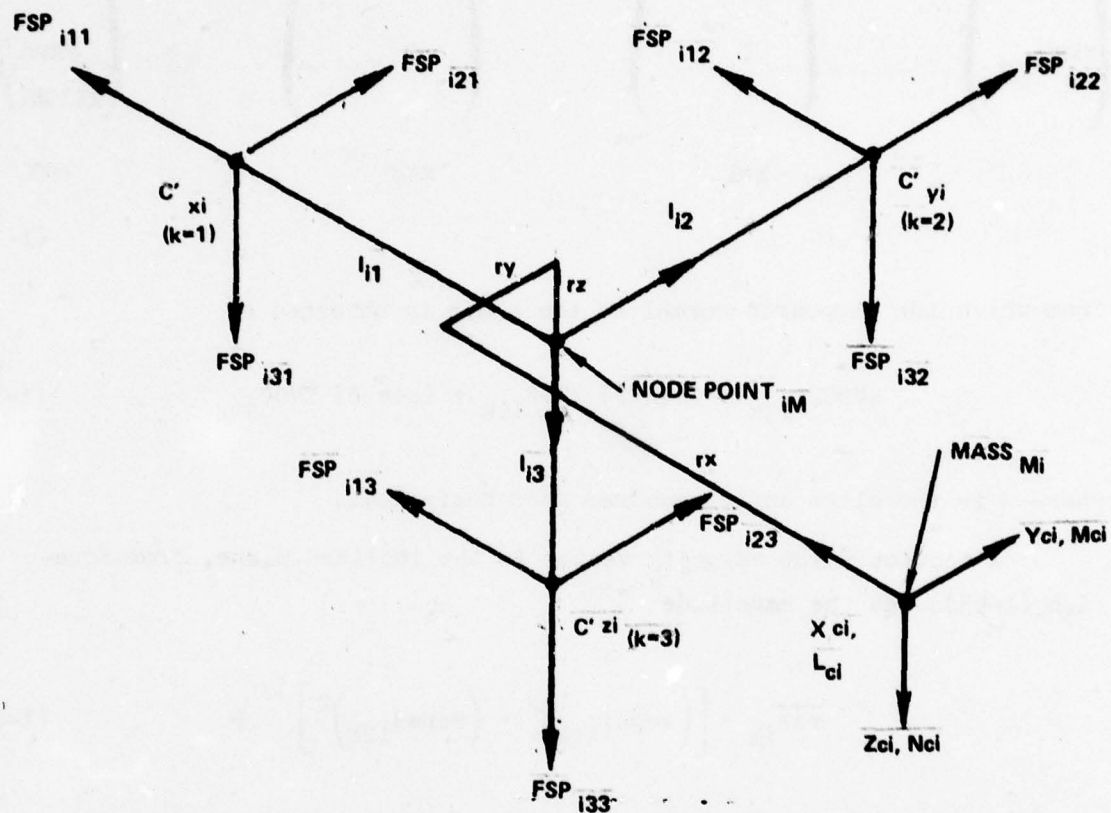


Figure 1-13. Crash Forces and Moments

$$\begin{Bmatrix} \text{XVOC}_{i1k} \\ \text{XVOC}_{i2k} \\ \text{XVOC}_{i3k} \end{Bmatrix} = [A_i] \begin{Bmatrix} \text{FSPO}_{ik} \text{ xSIGN}(\bar{\ell}_{ik}) \\ 0 \\ 0 \end{Bmatrix} \text{ or } [A_i] \begin{Bmatrix} 0 \\ \text{FSPO}_{ik} \text{ xSIGN}(\bar{\ell}_{ik}) \\ 0 \end{Bmatrix} \text{ or } [A_i] \begin{Bmatrix} 0 \\ 0 \\ \text{FSPO}_{ik} \text{ xSIGN}(\bar{\ell}_{ik}) \end{Bmatrix}$$

$k=1 \qquad \qquad \qquad k=2 \qquad \qquad \qquad k=3$

(1-104)

from which the component normal to the slope is obtained as

$$\text{XVOCSL}_{i3k} = (\sin \beta) \text{XVOC}_{i1k} + (\cos \beta) \text{XVOC}_{i3k} \quad (1-105)$$

where β is the slope angle measured from horizontal.

The contact point velocity vector in the inclined plane, from Equation (1-95), has the magnitude

$$\overline{vs\ell}_{ik} = \left[\left(\text{vcps}\ell_{i1k} \right)^2 + \left(\text{vcps}\ell_{i2k} \right)^2 \right]^{1/2} \quad (1-106)$$

The drag and side loads in the plane of the inclined slope are as follows.

$$\text{XVOCSL}_{ijk} = \left[\begin{matrix} \mu_{ik} \text{XVOCSL}_{i3k} \\ + F_{\text{plow}_{ik}} \end{matrix} \right] \frac{\text{vcps}\ell_{ijk}}{\overline{vs\ell}_{ik}} \quad j = 1, 2 \quad (1-107)$$

Finally, the three contact point forces given by Equations (1-105) and (1-107) are resolved into horizontal ground axes and then into ith mass axes to form the FSP_{ijk} illustrated in Figure 1-13.

$$\begin{Bmatrix} FSP_{11k} \\ FSP_{12k} \\ FSP_{13k} \end{Bmatrix} = - [A_i]^T [ABETA] \begin{Bmatrix} XVOCSL_{11k} \\ XVOCSL_{12k} \\ XVOCSL_{13k} \end{Bmatrix} \quad k = 1, 2, 3 \quad (1-108)$$

Now that the spring contact forces are in i th mass axes, there is no further distinction between forces resulting from contact with the horizontal ground (Equation (1-103)) and those resulting from contact with the slope (Equation (1-108)).

1.3.5.4.5 Crash Forces and Moments at Point m_i

Figure 1-13 shows the crash forces and moments acting at m_i , which are just the resultant of the FSP_{ijk} also shown in Figure 1-13; i.e., the FSP_{ijk} are just moved to point m_i and compensating moments at m_i added.

$$\begin{aligned} XC_{iM} &= \sum_{k=1}^3 FSP_{11k} \\ YC_{iM} &= \sum_{k=1}^3 FSP_{12k} \quad i = 1, 2, \dots, N \end{aligned} \quad (1-109a)$$

$$ZC_{iM} = \sum_{k=1}^3 FSP_{13k}$$

$$\begin{aligned} LC_{iM} &= FSP_{132} (ry + l_{i2}) - FSP_{123} (l_{i3} + rz) \\ &\quad + ry (FSP_{131} + FSP_{133}) - rz (FSP_{121} + FSP_{122}) \\ MC_{iM} &= FSP_{113} (rz + l_{i3}) - FSP_{131} (rx + l_{i1}) \\ &\quad + rz (FSP_{111} + FSP_{112}) - rx (FSP_{132} + FSP_{133}) \end{aligned} \quad (1-109b)$$

$$\begin{aligned} NC_{iM} &= FSP_{121} (rx + l_{i1}) - FSP_{112} (ry + l_{i2}) \\ &\quad + rx (FSP_{122} + FSP_{123}) - ry (FSP_{111} + FSP_{113}) \end{aligned}$$

The l_{ik} are from Equation (1-99); recall that they may be plus or minus to allow for springs in the negative direction of the mass body axes. Figure 1-13 shows all l_{ik} positive.

Equations (1-109) yield only the contribution of springs attached to node point iM to the total external spring forces and moments acting on mass m_i . To achieve the desired total forces and moments on m_i , the contributions from all node points attached to m_i and having external springs must be summed.

$$\begin{aligned} \begin{Bmatrix} XC_i \\ YC_i \\ ZC_i \end{Bmatrix} &= \sum_{M=1}^{NNP_i} \begin{Bmatrix} XC_{im} \\ YC_{im} \\ ZC_{im} \end{Bmatrix} \\ \begin{Bmatrix} LC_i \\ MC_i \\ NC_i \end{Bmatrix} &= \sum_{M=1}^{NNP_i} \begin{Bmatrix} LC_{im} \\ MC_{im} \\ NC_{im} \end{Bmatrix} \end{aligned} \quad (1-110)$$

where NNP_i is the number of node points attached to mass m_i and having external springs.

1.3.6 Total Forces and Moments

The total forces and moments at m_i , in i th body axes, are used to drive the six rigid-body degrees of freedom of lumped mass m_i . These total forces and moments are just the sum of the components, i.e., the gravity, aerodynamic, internal beam, and external spring forces and moments. The total loads are given by:

$$X_i = X_{G_i} + X_{A_i} + X_{I_i} + X_{C_i}$$

$$Y_i = Y_{G_i} + Y_{A_i} + Y_{I_i} + Y_{C_i}$$

$$Z_i = Z_{G_i} + Z_{A_i} + Z_{I_i} + Z_{C_i}$$

(1-111)

$$L_i = L_{I_i} + L_{C_i}$$

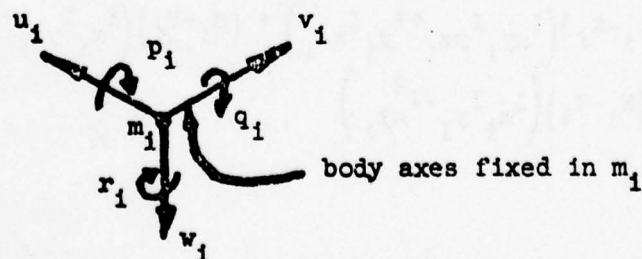
$$M_i = M_{I_i} + M_{C_i}$$

$$N_i = N_{I_i} + N_{C_i}$$

There are no gravity and aerodynamic moments. The terms of Equation (1-111) come from Equations (1-5), (1-8), (1-62) and (1-110).

1.3.7 Rigid-Body Equations of Motion

Having obtained all the forces and moments acting on each mass m_i , the rigid-body equations of motion for mass m_i can be written. Euler's equations of motion are used. These are derived in Reference 1; the derivation is not repeated here. The body axis components of the absolute (relative to ground) translational velocity of mass m_i are denoted by u_i , v_i , and w_i . The corresponding rotational velocities are designated p_i , q_i , and r_i . These velocities are shown in the following sketch:



Euler's equations of motion are six equations for the time derivatives of the six velocities, in terms of the six total forces and moments from the preceding section, the velocities themselves, and the inertia properties of mass m_i . These equations are (from Reference 1):

$$\dot{u}_i = \frac{X_i g}{W_i} - q_i w_i + r_i v_i$$

$$\dot{v}_i = \frac{Y_i g}{W_i} - r_i u_i + p_i w_i$$

$$\dot{w}_i = \frac{Z_i g}{W_i} - p_i v_i + q_i u_i$$

$$\begin{aligned} \dot{p}_i &= \frac{1}{\Delta_i} \left[\begin{aligned} &(L_i - A_i) \left(I_{y_i} I_{z_i} - I_{yz_i}^2 \right) + (M_i - B_i) \left(I_{xy_i} I_{z_i} + I_{yz_i} I_{xz_i} \right) \\ &+ (N_i - C_i) \left(I_{xy_i} I_{yz_i} + I_{y_i} I_{xz_i} \right) \end{aligned} \right] \\ \dot{q}_i &= \frac{1}{\Delta_i} \left[\begin{aligned} &(L_i - A_i) \left(I_{xy_i} I_{z_i} + I_{yz_i} I_{xz_i} \right) + (M_i - B_i) \left(I_{x_i} I_{z_i} - I_{xz_i}^2 \right) \\ &+ (N_i - C_i) \left(I_{x_i} I_{yz_i} + I_{xz_i} I_{xy_i} \right) \end{aligned} \right] \\ \dot{r}_i &= \frac{1}{\Delta_i} \left[\begin{aligned} &(L_i - A_i) \left(I_{xy_i} I_{yz_i} + I_{y_i} I_{xz_i} \right) + (M_i - B_i) \left(I_{x_i} I_{yz_i} + I_{xz_i} I_{xy_i} \right) \\ &+ (N_i - C_i) \left(I_{x_i} I_{y_i} - I_{xy_i}^2 \right) \end{aligned} \right] \end{aligned} \quad (1-112)$$

where

$$\begin{aligned}
 \Delta_i &= I_{x_i} (I_{y_i} I_{z_i} - I_{yz_i}^2) - I_{xy_i} (I_{xy_i} I_{z_i} + I_{xz_i} I_{yz_i}) - I_{xz_i} (I_{xy_i} I_{yz_i} + I_{y_i} I_{xz_i}) \\
 A_i &= q_i (H_{e_{z_i}} - I_{xz_i} p_i - I_{yz_i} q_i + I_{z_i} r_i) - r_i (H_{e_{y_i}} - I_{xy_i} p_i + I_{y_i} q_i - I_{yz_i} r_i) \\
 B_i &= r_i (H_{e_{x_i}} + I_{x_i} p_i - I_{xy_i} q_i - I_{xz_i} r_i) - p_i (H_{e_{z_i}} - I_{xz_i} p_i - I_{yz_i} q_i + I_{z_i} r_i) \\
 C_i &= p_i (H_{e_{y_i}} - I_{xy_i} p_i + I_{y_i} q_i - I_{yz_i} r_i) - q_i (H_{e_{x_i}} + I_{x_i} p_i - I_{xy_i} q_i - I_{xz_i} r_i)
 \end{aligned} \tag{1-113}$$

$X_i, Y_i, Z_i, L_i, M_i,$ and N_i are the total forces and moments from Equation (1-111). $I_{x_i}, I_{y_i},$ and I_{z_i} are the moments of inertia of mass m_i about its body fixed axes. $I_{xy_i}, I_{yz_i},$ and I_{xz_i} are the products of inertia, e.g., $I_{xy_i} = \int x_i y_i dm_i$, etc. $H_{e_{x_i}}, H_{e_{y_i}},$ and $H_{e_{z_i}}$ are the angular momenta of masses m_i , due to rotation of internal masses within m_i , such as propellers, rotors, and engine turbines.

The above equations of motion are integrated numerically to yield $u_i, v_i, w_i,$ and p_i, q_i, r_i . The translational velocities are obtained in ground axes by a simple transformation.

$$\begin{Bmatrix} \dot{x}_i \\ \dot{y}_i \\ \dot{z}_i \end{Bmatrix} = [A_i] \begin{Bmatrix} u_i \\ v_i \\ w_i \end{Bmatrix} \tag{1-114}$$

Similarly, the angular velocities $p_i, q_i,$ and r_i are the body axes components of the instantaneous absolute rotation rate $\vec{\omega}_i$ of mass m_i . These variables do not correspond to any set of coordinates which specify the

orientation of the airplane. Therefore, in order to solve for the orientation, it is necessary to transform the p' , q' , r' to the time derivatives $\dot{\phi}_i$, $\dot{\theta}_i$, $\dot{\psi}_i$ of the Euler angles. By summing the orthogonal projections of $\dot{\phi}_i$, $\dot{\theta}_i$, $\dot{\psi}_i$ onto each of the body fixed axes, the following kinematic relations are obtained (Reference 1):

$$\begin{aligned}\dot{\phi}_i &= p_i + (q_i \sin \phi_i + r_i \cos \phi_i) \tan \theta_i \\ \dot{\theta}_i &= q_i \cos \phi_i - r_i \sin \phi_i \\ \dot{\psi}_i &= (q_i \sin \phi_i + r_i \cos \phi_i) \sec \theta_i\end{aligned}\tag{1-115}$$

Equations (1-114) and (1-115) are integrated numerically to obtain x_i , y_i , z_i and ϕ_i , θ_i , ψ_i . Also, p_i , q_i , and r_i are integrated to obtain the quantities inp_i , inq_i , and inr_i . The incremental changes in these integrals are used in Equation (1-12). They represent the incremental rotations of mass m_i in body fixed axes.

It should be noted that $(\dot{u}_i, \dot{v}_i, \dot{w}_i)$ from Equation (1-112) are not the components of the absolute acceleration of m_i . The expressions for these quantities are:

$$\begin{aligned}ax_i &= \frac{X_i}{W_i} \\ ay_i &= \frac{Y_i}{W_i} \\ az_i &= \frac{Z_i}{W_i}\end{aligned}\tag{1-116}$$

where the accelerations are in g units. These are used only for output data in program KRASH. Comparing Equations (1-112) and (1-116), the relationships between the absolute accelerations and the time derivatives of the body axis components of the absolute velocity are seen to be:

$$\begin{aligned}
 ax_i &= \frac{1}{g} \left[\dot{u}_i + q_i w_i - r_i v_i \right] \\
 ay_i &= \frac{1}{g} \left[\dot{v}_i + r_i u_i - p_i w_i \right] \\
 az_i &= \frac{1}{g} \left[\dot{w}_i + p_i v_i - q_i u_i \right]
 \end{aligned}
 \tag{1-117}$$

These relationships can be independently derived from the time derivative of the absolute velocity, accounting for the time rate of change of the unit vectors fixed in the body.

1.3.8 Filtered Accelerations

Program KRASH has been extensively used in conjunction with full scale crash tests, wherein it is desired to establish the degree of correlation between analytical and test results. The most readily obtainable test results are measured accelerations at various points on the structure. Since crash test accelerometer outputs generally contain a great deal of very high frequency, high amplitude responses, the data is normally filtered prior to its usage or formal presentation. A wide variety of analog and digital filters may be employed, but in general the cutoff frequency is in the area of 100 Hz to 300 Hz.

In order to facilitate comparisons of KRASH analytical results with test results, the calculation of filtered mass accelerations is included in the program. The filter employed in the program is a simple first order lag. The Laplace transform for such a filter is given by:

$$T(\omega) = \frac{1}{1 + j \frac{\omega}{\omega_c}} \tag{1-118}$$

where

$$j = \sqrt{-1}$$

ω = response frequency, rad/sec

ω_c = cutoff frequency of filter, rad/sec

The phase and amplitude response for this filter is shown in Figure 1-14. Although the filters used for test data reduction are generally much steeper, it is felt that the computational effort (and run time) required for a more complex filter is not appropriate for inclusion in the direct time-history solution of program KRASH.

The first order filter is implemented through the following equation in the time domain:

$$p\dot{y} + y = x \quad (1-119)$$

where

x = unfiltered acceleration (input) time history

y = filtered acceleration (output) time history

$$\dot{y} = \frac{d}{dt} y(t) \quad (1-120)$$

$$p = \frac{1}{\omega_c} = \frac{1}{2\pi f_c}$$

The filter cutoff frequency f_c is an input parameter.

Equation (1-119) is solved for \dot{y} :

$$\dot{y} = \frac{x-y}{p} \quad (1-121)$$

This derivative is then integrated directly along with the other integrations performed in the program to yield $y(t)$ which is the desired filtered acceleration. This procedure is employed for all the linear accelerations for all the masses in the model. The unfiltered accelerations used for the input to (1-121) are those from Equation (1-116), which are in g units. Therefore, the filtered accelerations are also in g units.

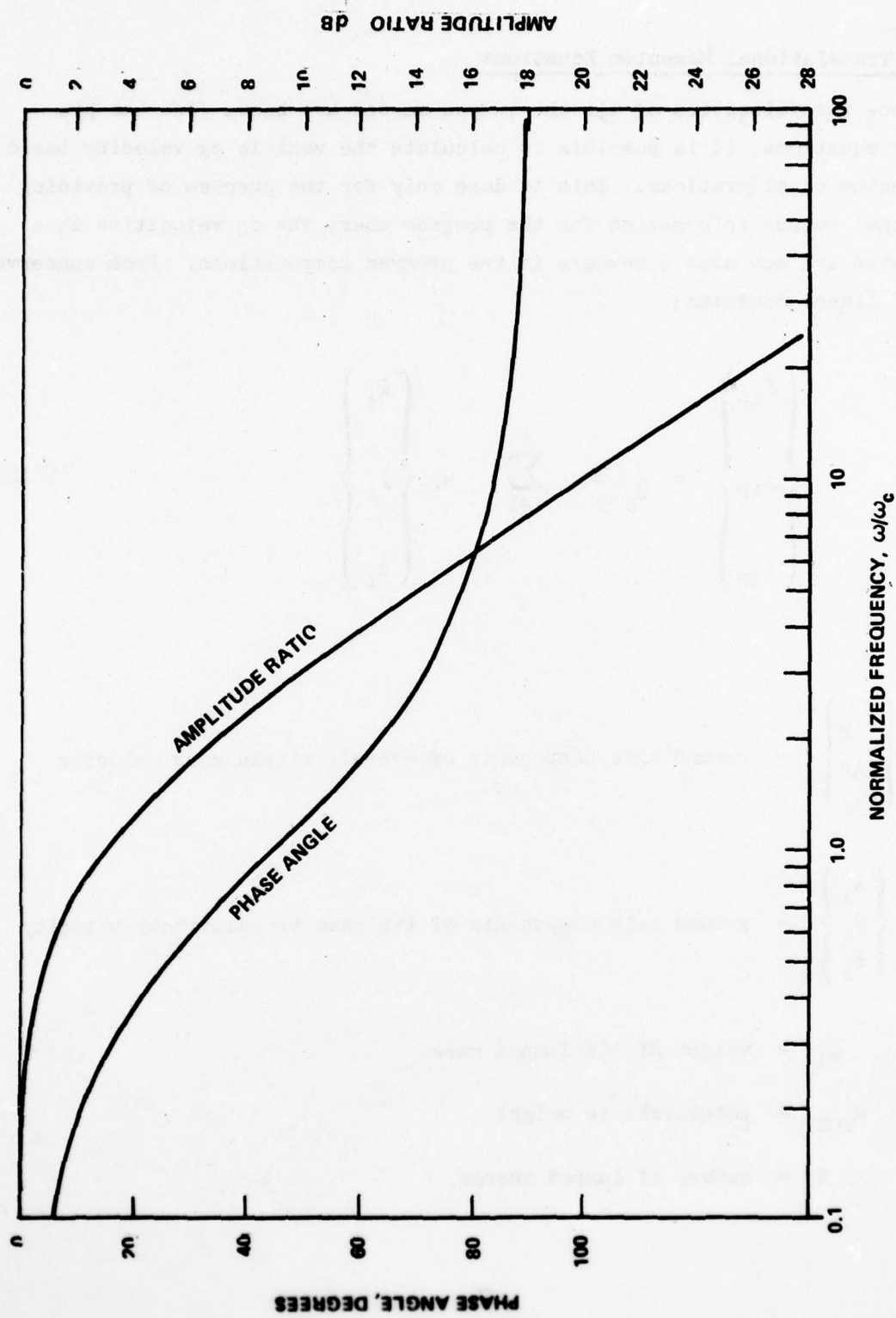


Figure 1-14. First Order Filter Response Characteristics

1.3.9 Translational Momentum Equations

Once the velocities of all the lumped masses are known from the preceding equations, it is possible to calculate the vehicle cg velocity based on momentum considerations. This is done only for the purpose of providing additional output information for the program user; the cg velocities thus calculated are not used elsewhere in the program computations. From conservation of linear momentum:

$$\begin{Bmatrix} \dot{x}_{AP} \\ \dot{y}_{AP} \\ \dot{z}_{AP} \end{Bmatrix} = \frac{1}{w_{TOT}} \sum_{i=1}^N w_i \begin{Bmatrix} \dot{x}_i \\ \dot{y}_i \\ \dot{z}_i \end{Bmatrix} \quad (1-122)$$

where

$$\begin{Bmatrix} \dot{x}_{AP} \\ \dot{y}_{AP} \\ \dot{z}_{AP} \end{Bmatrix} = \text{ground axis components of overall airplane cg velocity}$$

$$\begin{Bmatrix} \dot{x}_i \\ \dot{y}_i \\ \dot{z}_i \end{Bmatrix} = \text{ground axis components of } i\text{th mass translational velocity}$$

$$w_i = \text{weight of } i\text{th lumped mass}$$

$$w_{TOT} = \text{total vehicle weight}$$

$$N = \text{number of lumped masses}$$

The results of Equation (1-122) are printed at every print time interval. This information is useful for giving the program user an indication of the translational velocity state of the vehicle as a whole, which is very difficult to deduce from inspection of the velocities of all the lumped masses.

A similar calculation could be performed for the angular velocity of the vehicle. However, since the angular inertia properties in ground axes are dependent on mass orientation, the moments of inertia for all the lumped masses would have to be continually calculated in ground axes, as would the angular velocities of the masses, since their spatial attitude varies with time. Alternatively, the angular velocities and inertias could all be calculated in some reference frame approximating the overall vehicle attitude. In either case, it is felt that the complexity of the necessary calculations outweighs any potential benefits from the overall airplane angular velocities that could be derived. Therefore, average airplane angular velocities are not calculated.

1.3.10 Control Volume Mass Penetration Calculations

The computer program includes the calculation of whether or not any of the N lumped masses have penetrated into an input control volume. The purpose of these calculations is to determine if a major mass item (such as the engine) has moved into a position where it threatens the vehicle's passengers. Therefore, the control volume input is intended to define the volume of the vehicle in which human occupants are present. The rectangular control volume is located with respect to one of the lumped masses, which is specified in the input. Figure 1-15 shows a typical rectangular control volume defined with respect to mass m_p .

The six walls of the control volume are always perpendicular to the three body axes fixed in mass m_p . Thus, the spatial orientation of the control volume varies as mass m_p rotates. \bar{x}_p , \bar{x}_n , \bar{y}_p , \bar{y}_n , \bar{z}_p , and \bar{z}_n , all positive, are the input constants defining the distances from m_p to the six walls, measured in the positive and negative directions along the body fixed axes of m_p .

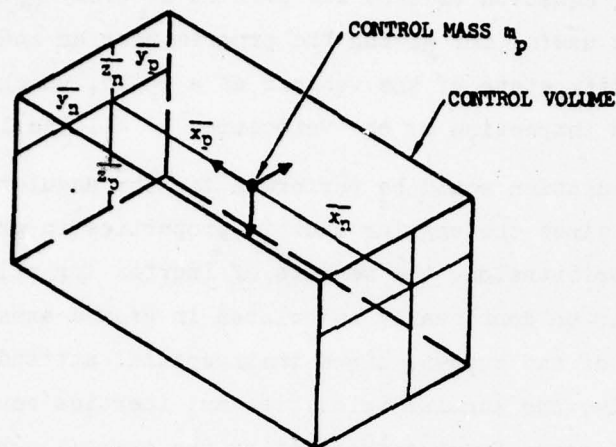


Figure 1-15. Control Volume for Mass Penetration

Mass penetration is determined by merely examining the p th body axes components of a vector from control mass m_p to mass m_i , $i = 1, 2, \dots, N$ ($i \neq p$). These components are given simply by

$$\begin{pmatrix} x_{p_i} \\ y_{p_i} \\ z_{p_i} \end{pmatrix} = [A_p]^T \begin{pmatrix} x_i - x_p \\ y_i - y_p \\ z_i - z_p \end{pmatrix} \quad i = 1, 2, \dots, N (i \neq p) \quad (1-123)$$

where $[A_p]$ is the transformation matrix $[A_i]$ for $i = p$. These vector components are then tested against the control volume dimensions. If all three vector components lie within the corresponding pairs of control volume walls,

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then the i th point has penetrated inside the control volume. Whenever a mass penetration occurs, the program prints out the time and mass that penetrated. These data are repeated in a summary table at the end of the run, showing all the mass penetrations for that run.

1.3.11 Volume Change Calculations

In order to determine the potential for occupant injury in a crash, the program includes the capability to calculate the change in volume of a region defined by eight (8) corner point masses. In practice, the volume specified would represent the region in which human occupants are located. Figure 1-16 illustrates a typical volume specified by defining the mass numbers at the corner points 1-8.

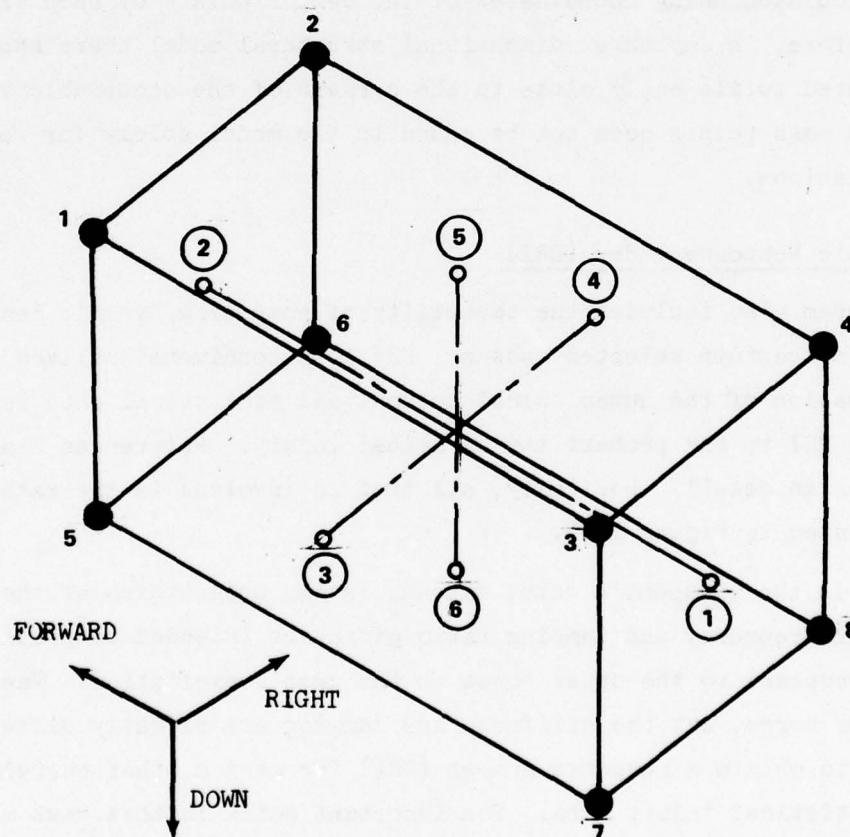


Figure 1-16. Volume Change Geometry

The program calculates the x, y, z ground coordinates of the circled points ① through ⑥ as the average of the coordinates of the appropriate 4 mass points. For example, to calculate the coordinate of ⑤, the coordinates of masses located at 1, 2, 3 and 4 are used. When the ground coordinates of ① through ⑥ are known, the lengths of lines ① - ②, ③ - ④ and ⑤ - ⑥ are computed. These are then multiplied to obtain the volume. Both the volume and the lengths of lines ① - ②, ③ - ④, and ⑤ - ⑥ are printed at each print time interval. The program allows for up to 8 separate volumes to be specified, so that different occupant regions can be separately analyzed.

While Figure 1-16 implies that 8 masses must be located in the model in a perfectly rectangular pattern, sloping planes are acceptable since the volume is calculated using coordinates of the center points of each side plane. Therefore, in any three dimensional structural model there should be 8 masses located sufficiently close to the corners of the occupiable volume, so that extra mass points need not be added to the model solely for volume change calculations.

1.3.12 Dynamic Response Index (DRI)

The program also includes the capability of computing Dynamic Response Index (DRI) for certain selected masses. DRI is a nondimensionalized measure of the compression of the human spinal column, and statistical data is available relating DRI to the probability of spinal injury. References 2 and 3 describe DRI's in detail. Basically, all that is involved is the mathematical model illustrated in Figure 1-17.

Mass m_1 is the occupant's seat; mass m_2 is the upper torso of the occupant. The frequency and damping ratio given are intended to properly model the dynamic response to the upper torso to the seat's excitation. Mass m_3 is also the upper torso, but the stiffness and damping are slightly different. This is done to obtain a response number (DRI) for mass m_3 that correlates well with statistical injury data. The important point is that mass m_3 is driven by mass m_1 , but the interconnecting forces only drive mass m_3 , not

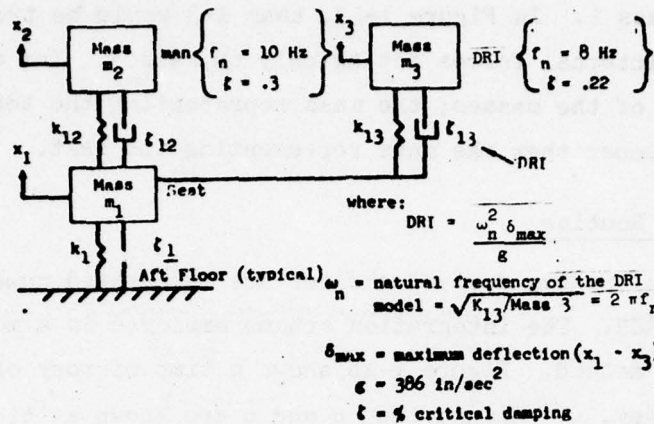


Figure 1-17. DRI Model

mass m_1 . Thus, the coupled systems of m_1 and m_2 determine the response of m_1 , and this response drives m_3 . The Dynamic Response Index is defined in Figure 1-17 by

$$DRI = \frac{\omega_n^2 \delta}{g} \quad (1-124)$$

Substituting the constants, the DRI is:

$$DRI = 6.55\delta \quad (1-125)$$

If the damping were zero, the DRI would be the acceleration of mass m_3 . With damping, it is a nondimensionalized measure of spring compression. In the computer program, δ is taken as $-v_x$ (Equation 1-44) for the ij element corresponding to the beam between mass 1 and 3. The program is coded so that for selected ij pairs (specified by the input), the internal force acts only

on mass j, not on mass i. In Figure 1-17, beam 1-3 would be treated in this way, with its internal forces acting only on mass 3. The only restriction is in the numbering of the masses; the mass representing the torso must be assigned a larger number than the mass representing the seat.

1.3.13 Integration Routine

The equations of motion derived earlier are integrated numerically in computer program KRASH. The integration scheme employed is a modified predictor-corrector method. Figure 1-18 shows a time history of a typical response quantity, say, u . Assume that u and \dot{u} are known at time t and all previous times. The predicted value of u at $t + \Delta t$, $u_{p_{t+\Delta t}}$ is computed as

$$u_{p_{t+\Delta t}} = u_{t-\Delta t} + 2\Delta t \dot{u}_t \quad (1-126)$$

This is shown in the Figure 1-18 by the upper dashed line of slope \dot{u}_t . Using this predicted value of u at $t + \Delta t$, the derivative \dot{u} at $t + \Delta t$ is

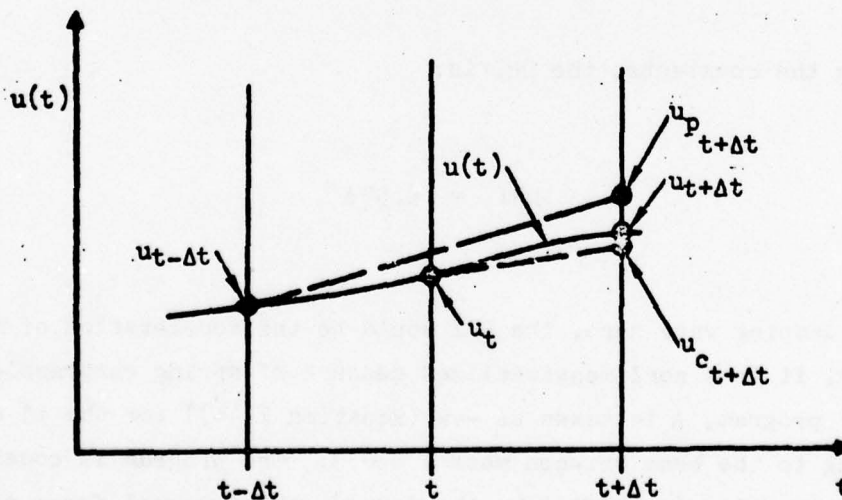


Figure 1-18. Numerical Integration Scheme

computed from the equations derived in the theory. This derivative is then averaged with \dot{u} at t to determine a corrected value of u at $t + \Delta t$:

$$u_{c,t+\Delta t} = u_t + \frac{\Delta t}{2}(\dot{u}_{t+\Delta t} + \dot{u}_t) \quad (1-127)$$

This is shown by the lower dashed line in Figure 1-18. The final value used for $u_{t+\Delta t}$ is a weighted average of the predicted and corrected values. For the present program, the weighting used is 4 to 1 in favor of the corrected value. Hence

$$u_{t+\Delta t} = 0.8u_{c,t+\Delta t} + 0.2u_{p,t+\Delta t} \quad (1-128)$$

A computational flow diagram for this scheme is shown in Figure 1-19. Since the technique is not self-starting (due to the $u_{t-\Delta t}$ term in equation (1-126)), a simple Euler integration is used for the first step. The subroutine DERIV encompasses all the equations derived in the theory, and is used to compute the derivatives of all the variables, knowing the variables themselves.

The iteration shown by the dashed line in Figure 1-19 is often employed with this scheme, the iteration continuing until the predicted and corrected values agree to within a specified tolerance. However, the iteration is not used in the program KRASH. Due to the large number of computations in the subroutine DERIV, it is more efficient to go through DERIV only once per time step, and to choose a sufficiently small time step Δt to obtain the desired accuracy.

The subroutine IC computes all the initial values (at $t = 0$) of the variables necessary for the integration to proceed. Section 1.3.15 discusses the calculations of these initial conditions.

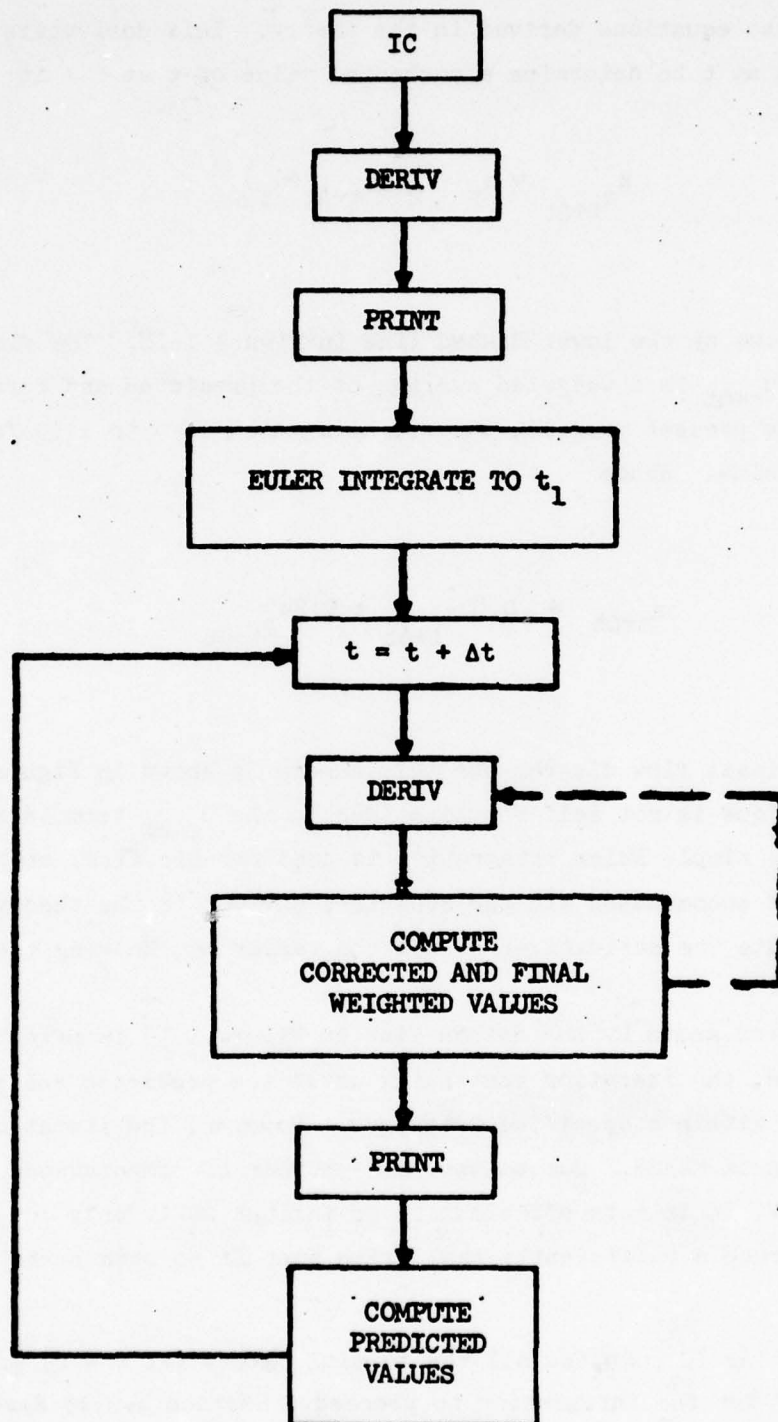


Figure 1-19. Numerical Integration Flow Diagram

1.3.14 Symmetrical Modeling

Program KRASH is coded to allow the analysis of a half-airplane model for symmetrical impact conditions. Figure 1-20 illustrates a very simple model of an airplane, in which masses 1, 2 and 3 represent the fuselage, 4 and 5 side fuselage structure, 6 the landing gear and 7 the wing. If the airplane itself is symmetrical, which is normally the case, then the program user need only input data for masses 1 through 7. Beam data is input for the following ij pairs:

1 - 2
2 - 3
2 - 4
4 - 5
4 - 6
5 - 0
5 - 7

The notation 5-0 means that a beam connects mass 5 to an equal mass on the opposite side of the airplane. (Mass 9 is not input to the model, so beam 5-9 cannot be input.) Program KRASH then analyzes the response of the model consisting of the left hand side of the airplane only, for a symmetrical impact condition. A symmetrical impact is one containing no roll or yaw angles, no lateral cg velocity, and no roll and yaw angular velocities.

For the half-airplane analysis, the "missing" half of the airplane is accounted for in the following manner:

- For traverse beams such as 5-0, the conditions at beam end j are set equal to those at i, with appropriate changes in sign. x, z and θ motions are equal; y, ϕ and ψ motions are opposite.
- The X, Z and M internal beam loads acting on a mass on the plane of symmetry are doubled to account for the presence of opposite side beams that are not explicitly modeled. Prior to this, loads for beams lying entirely in the plane of symmetry (such as 1-2 and 2-3 in Figure 1-20) are halved. This is done so that when the X, Z and M internal loads are doubled on a mass such as 2, the contribution from beams such as 1-2 will not be doubled. Y, L and N loads are set to zero.

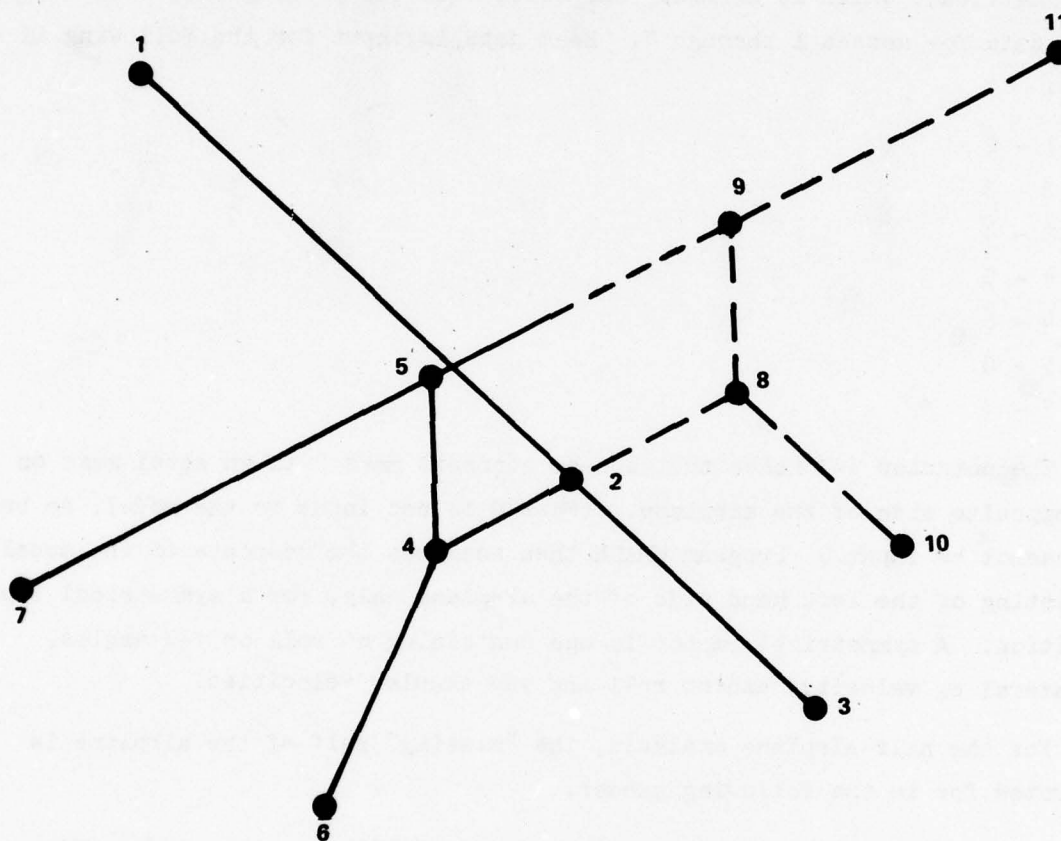


Figure 1-20. Symmetrical Airplane Model

The input data defining the characteristics of beams in the plane of symmetry, such as 1-2, should include the contributions from both the left and right hand sides of the airplane. The same is true for mass data for masses in the plane of symmetry, such as 1, 2 and 3. In other words, "half-airplane" data is not utilized for beams or masses in the plane of symmetry. While this convention differs from that used in certain other standard structural analysis computer programs, it is consistent with the full airplane models used with previous versions of KRASH.

For unsymmetrical impact conditions, the program user can still input a half-airplane model. For this situation, the program internally generates the rest of the model and performs the analysis using a full-airplane model. For example, the program would internally generate the data for masses 8, 9, 10 and 11 in Figure 1-20, as well as beams 2-8, 8-9, 8-10 and 9-11. Therefore, the program user can always work with a reduced size data set representing half an airplane, as long as the airplane itself is symmetrical. Any change made to the half-airplane data set will automatically be included in the opposite mass or beam when the program generates the full-airplane model.

1.3.15 Initial Conditions

Initial values (at $t = 0$) are required for the following quantities:

$$\left. \begin{array}{ll} x_i, y_i, z_i & \phi_i, \theta_i, \psi_i \\ u_i, v_i, w_i & p_i, q_i, r_i \\ \dot{x}_i, \dot{y}_i, \dot{z}_i & \dot{\phi}_i, \dot{\theta}_i, \dot{\psi}_i \end{array} \right\} \quad i = 1, 2, \dots, N \quad (1-129)$$

The initial conditions which are input to the program are the following:

$\dot{x}_g, \dot{y}_g, \dot{z}_g$	vehicle c.g. velocity in ground axes
p', q', r'	vehicle angular velocity in body axes
ϕ', θ', ψ'	vehicle attitude, Euler angles of vehicle relative to ground

First the total vehicle weight is computed from the individual mass weights (input):

$$W_{TOT} = \sum_{i=1}^N W_i \quad (1-130)$$

Next, the location of the overall vehicle c.g., in the Hx"y"z" coordinate system, is determined as follows:

$$\begin{aligned} x_G'' &= \frac{1}{W_{TOT}} \sum_{i=1}^N W_i x_i'' \\ y_G'' &= \frac{1}{W_{TOT}} \sum_{i=1}^N W_i y_i'' \\ z_G'' &= \frac{1}{W_{TOT}} \sum_{i=1}^N W_i z_i'' \end{aligned} \quad (1-131)$$

An expression for the ground coordinates of m_i is written:

$$\begin{pmatrix} x_i \\ y_i \\ z_i \end{pmatrix} = \begin{pmatrix} x_G \\ y_G \\ z_G \end{pmatrix} + [A'] \begin{pmatrix} x_i' \\ y_i' \\ z_i' \end{pmatrix} \quad (1-132)$$

or

$$va_{ij} = vg_j + \sum_{l=1}^3 A'_{jl} vip_{il} \quad j = 1,2,3$$

where x_G , y_G , and z_G are currently unknown, and

$$\begin{pmatrix} x'_i \\ y'_i \\ z'_i \end{pmatrix} = - \begin{pmatrix} x''_i - x''_G \\ y''_i - y''_G \\ z''_i - z''_G \end{pmatrix} \quad (1-133)$$

or

$$vip_{ij} = -(vipp_{ij} - vgpp_{ij}) \quad j = 1,2,3$$

The $vipp_{ij}$ are the input coordinates of the m_i , and the $vgpp_{ij}$ were computed in Equation (1-131), so the $vipp_{ij}$ are known. In Equation (1-132), $[A']$ is known from the input Euler angles ϕ' , θ' , and ψ' . The only unknowns in Equation (1-132) are x_G , y_G , z_G (defined as vg_j). Clearly, the y ground coordinate of the initial c.g. position is arbitrary, so this is set to zero.

It remains to determine the initial c.g. position, both fore-aft and vertically. This position is determined within the program so that the vehicle, in the desired attitude with respect to ground, "fits into" the wedge formed by the ground plane and slope with the lowest springs .001 inch off the ground and slope. This situation is illustrated in Figure 1-21. Point O is the origin of the ground coordinate system, with x positive forward and z positive down. Point O is located at the intersection of the horizontal ground plane and the slope. The vehicle cg is shown in Figure 1-21. The initial coordinates of the c.g. in ground axes, shown as x_G and z_G in Figure 1-21, are desired. Also shown are two typical masses m_i and m_j , with external springs radiating outward.

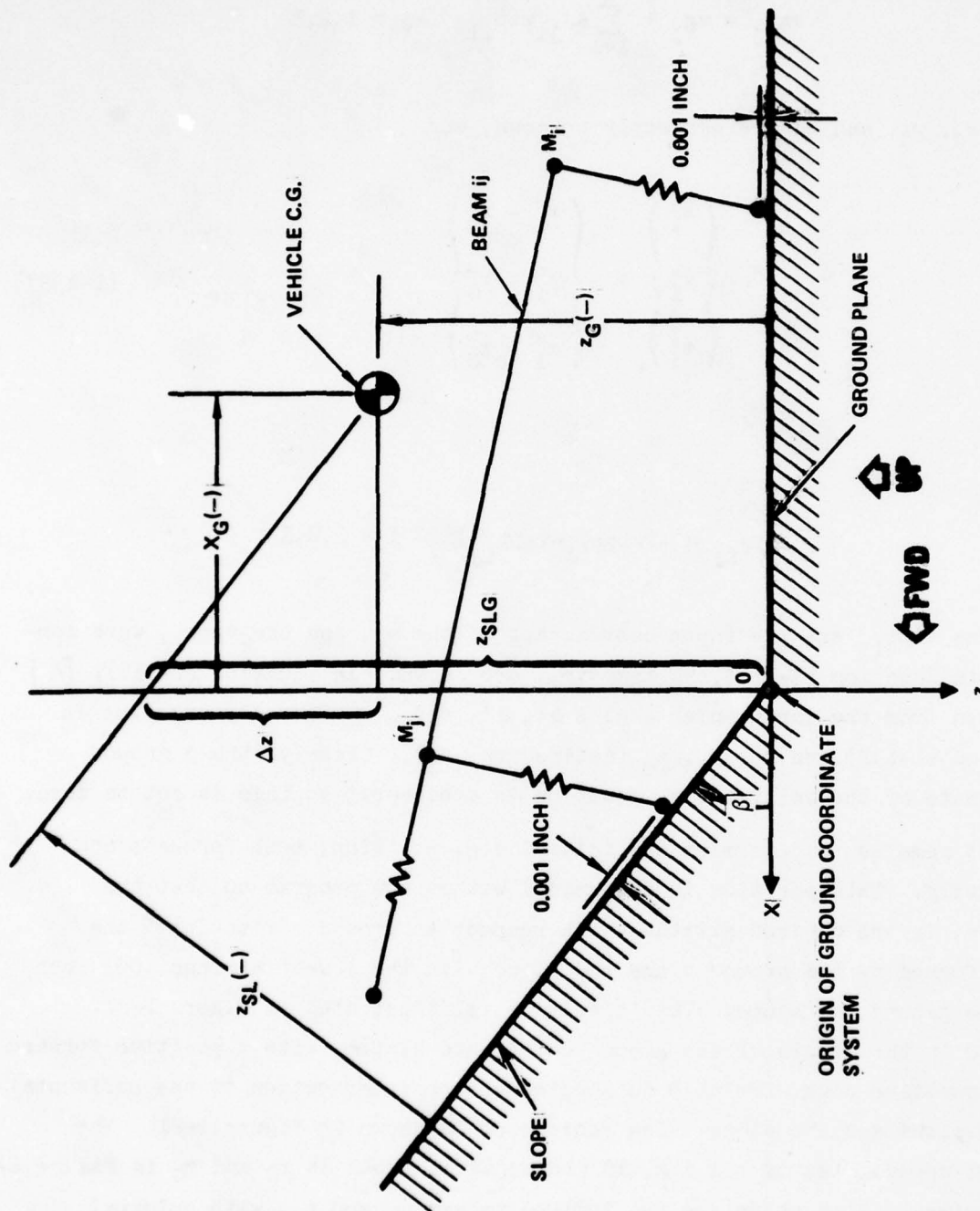


Figure 1-21. Vehicle Initial Position

The procedure for determining x_G and z_G is:

1. Write equations for the ground and slope coordinates of the end points of all the external springs in the model, assuming the vehicle cg is located at point 0.
2. Search for the largest magnitude of these distances, both in ground and slope axes.
3. From this information, calculate z_{SL} and z_G to give .001 inch ground clearance at the spring ends.
4. Finally, calculate x_G .

From Equation (1-69), the z coordinate of the end of spring ik is known as:

$$vc_{i3k} = va_{i3} + dvr_{i3} + dvc_{i3k} \quad (1-134)$$

From Equation (1-132) va_{i3} is:

$$va_{i3} = vg_3 + \sum_{l=1}^3 A'_{3l} vip_{il} \quad (1-135)$$

once $vg_3(z_G)$ is known. Combining (1-134) and (1-135) and utilizing (1-71) for dvc_{ijk} :

$$vc_{i3k} = vg_3 + \sum_{l=1}^3 A'_{3l} vip_{il} + dvr_{i3} + A_{i3k} \bar{l}_{ik} \quad (1-136a)$$

The x coordinates are obtained similarly as

$$vc_{i1k} = vg_1 + \sum_{l=1}^3 A'_{1l} vip_{il} + dvr_{i1} + A_{i1k} \bar{l}_{ik} \quad (1-136b)$$

Now the x and z coordinates of all the spring ends are calculated using Equation (1-136) with $vg_1 = vg_3 = 0$ (vehicle c.g. at point 0). The z_{sl} slope axis coordinate is calculated also for all the spring ends. This is given simply by

$$z_{sl_{ik}} = \sin \beta (vc_{il_k}) + \cos \beta (vc_{i3k}) \quad (1-137)$$

The results of equations (1-136a) and (1-137) are now searched for the maximum magnitudes:

$$\begin{aligned} z_{c_{max}} &= \left| \text{largest} \left| vc_{i3k} \right| \right| \text{ for all ik pairs} \\ z_{SL_{max}} &= \left| \text{largest} \left| z_{sl_{ik}} \right| \right| \text{ for all ik pairs} \end{aligned} \quad (1-138)$$

The calculation of z_G and z_{SL} , shown in Figure 1-21, is now possible. These are given by

$$\begin{aligned} z_G &= -z_{C_{MAX}} \quad -.001 \\ z_{SL} &= -z_{SL_{MAX}} \quad -.001 \end{aligned} \quad (1-139)$$

It still remains to calculate x_G from z_G and z_{SL} . (z_G and z_{SL} uniquely define the vehicle c.g. position, but we want x_G and z_G , not z_{SL} and z_G , for use in equation (1-132).)

Obtain first the projection of z_{SL} on the vertical Oz axis as

$$z_{SLG} = -z_{SL} / \cos \beta \quad (1-140)$$

Then Δz is given by

$$\Delta z = -z_G - z_{SLG} \quad (1-141)$$

Finally x_G is computed as

$$x_G = \Delta z / \tan \beta \quad (1-142)$$

For $\beta = 0$, don't use equations (1-140) through (1-142), but set $x_G = 0$. For $\beta = 90$, set $x_G = z_{SL}$ (both are negative). Finally, modify the calculated values of x_G and z_G by the input values x_{GIN} and z_{GIN} :

$$x_G = x_G - x_{GIN}$$

Equation (1-142)

(1-143)

$$z_G = z_G - z_{GIN}$$

Equation (1-139)

Positive input constants x_{GIN} and z_{GIN} define the distances aft and up in ground axes that the initial c.g. position is relative to the "wedged" position shown in Figure 1-21. Normally these are input as zero, since the "wedged" position is where one usually wants the vehicle. However, for certain special cases it may be desired to drop the vehicle a finite distance or to impact entirely on the slope. It should be noted that the z_G in Equation (1-143) is actually used to calculate Δz in Equation (1-141). This means that if a nonzero z_{GIN} is used, the vehicle will be lifted up from the "wedged" position and then moved forward until almost contacting the slope. Thus one can start any distance up the slope to get clear of the ground plane if so desired. The slope extends indefinitely. With x_G and z_G now known (and y_G set = 0), we can use Equation (1-132) to calculate the initial values for all the mass ground coordinates.

In determining the initial position of the airplane, only the mass points having external springs are checked. The program **assumes** that the user has assigned springs to the masses at the lower **extremities** of the vehicle. If this is not the case, the program may place the vehicle in an initial position wherein some of the masses are below the ground plane ($z = 0$). This will

manifest itself by negative potential energy for any "subterranean" masses. If this occurs, the user should correct the model by adding external springs to the lowest masses.

To perform the preceding calculations, $[A_i]$ is required, which is used in Equations (1-136a, b). From the definitions of the transformation matrices (refer to Table 1-1 earlier):

$$[A_i] = [A'] [A''] \quad i = 1, 2, \dots, N \quad (1-144)$$

\uparrow \uparrow
 ith body axes to c.g. axes
 c.g. axes to ground axes

Equation (1-144) also provides a method for determining the initial values for ϕ_i, θ_i, ψ_i . First θ_i is determined from $A_{i31} = -\sin\theta_i$ as

$$\theta_i = -\sin^{-1} A_{i31} \quad (1-145)$$

Next ϕ_i is found from $A_{i32} = \sin\phi_i \cos\theta_i$, since θ_i is now known:

$$\phi_i = \sin^{-1} \left(\frac{A_{i32}}{\cos\theta_i} \right) \quad (1-146)$$

Finally, ψ_i is obtained from $A_{i21} = \cos\theta_i \sin\psi_i$:

$$\psi_i = \sin^{-1} \left(\frac{A_{i21}}{\cos\theta_i} \right) \quad (1-147)$$

Note that equations (1-145) through (1-147) all involve arc sine, so the difference between a positive and negative angle can be detected.

Next the linear and angular velocities are calculated. Differentiating equation (1-132):

$$\begin{pmatrix} \dot{x}_i \\ \dot{y}_i \\ \dot{z}_i \end{pmatrix} = \begin{pmatrix} \dot{x}_G \\ \dot{y}_G \\ \dot{z}_G \end{pmatrix} + [\dot{A}'] \begin{pmatrix} x'_i \\ y'_i \\ z'_i \end{pmatrix} \quad (1-148)$$

where the first vector is input and the second vector is given by Equation (1-133). $[\dot{A}']$ is treated the same as $[\dot{A}_i]$ was earlier in the theory:

$$[\dot{A}'] = [A'] [D'] \quad (1-149)$$

where

$$[D'] = \begin{bmatrix} 0 & -r' & q' \\ r' & 0 & -p' \\ -q' & p' & 0 \end{bmatrix} \quad (1-150)$$

p' , q' and r' are input constants defining the initial vehicle angular velocity.

Once \dot{x}_i , \dot{y}_i , and \dot{z}_i are known from (1-148), these are simply transformed into body axes to obtain u_i , v_i , and w_i :

$$\begin{pmatrix} u_i \\ v_i \\ w_i \end{pmatrix} = [A_i]^T \begin{pmatrix} \dot{x}_i \\ \dot{y}_i \\ \dot{z}_i \end{pmatrix} \quad (1-151)$$

The angular velocities in body axes (p_i , q_i , and r_i) are equal to the vehicle angular velocity (p' , q' , and r'), transformed from c.g. axes to i th mass axes:

$$\begin{pmatrix} p_i \\ q_i \\ r_i \end{pmatrix} = [A_i'']^T \begin{pmatrix} p' \\ q' \\ r' \end{pmatrix} \quad (1-152)$$

Next we determine $\dot{\phi}_i$, $\dot{\theta}_i$, and $\dot{\psi}_i$ by Equation (1-115).

$$\begin{pmatrix} \dot{\phi}_i \\ \dot{\theta}_i \\ \dot{\psi}_i \end{pmatrix} = [\bar{A}_i] \begin{pmatrix} p_i \\ q_i \\ r_i \end{pmatrix} \quad (1-153)$$

where

$$[\bar{A}_i] = \begin{bmatrix} 1 & \sin\phi_i \tan\theta_i & \cos\phi_i \tan\theta_i \\ 0 & \cos\phi_i & -\sin\phi_i \\ 0 & \sin\phi_i \sec\theta_i & \cos\phi_i \sec\theta_i \end{bmatrix} \quad (1-154)$$

The only remaining initial conditions to be determined are the beam deflections and forces. At present, the program is written so that the initial values for these quantities are zero. This is only true for the case where there are no aerodynamic loads, so that all masses are uniformly accelerating downward at $1g$. Therefore, if aerodynamic loads are used in the program, the initial conditions will not be correct since internal forces would be required to balance the aerodynamic and gravity forces. However, this is not considered a serious limitation since the dynamic impact forces in a crash situation will overshadow any imbalance present due to nonzero aerodynamic forces.

In the IC subroutine, the overall vehicle moments of inertia are calculated from the individual mass inertia data, to inform the user as to how well his model matches the overall inertias of the vehicle being analyzed. The overall inertias are given by

$$\begin{aligned}
 I_x &= \sum_{i=1}^{NM} \left(I_{xi} + m_i r_{xi}^2 \right) \\
 I_y &= \sum_{i=1}^{NM} \left(I_{yi} + m_i r_{yi}^2 \right) \\
 I_z &= \sum_{i=1}^{NM} \left(I_{zi} + m_i r_{zi}^2 \right)
 \end{aligned}
 \tag{1-155}$$

The I_{xi} , I_{yi} , I_{zi} are the individual mass moments of inertia, the m_i are the individual masses, and r_{xi}^2 , r_{yi}^2 , r_{zi}^2 are the squares of the distances from the cg to m_i , measured normal to the Hx"y"z" axes as appropriate.

$$\begin{aligned}
 r_{xi}^2 &= (y_i'' - y_G'')^2 + (z_i'' - z_G'')^2 \\
 r_{yi}^2 &= (x_i'' - x_G'')^2 + (z_i'' - z_G'')^2 \\
 r_{zi}^2 &= (x_i'' - x_G'')^2 + (y_i'' - y_G'')^2
 \end{aligned}
 \tag{1-156}$$

1.3.16 Energy Balance Equations

The primary objective of a crash analysis in the preliminary design phase is to determine how to absorb the initial vehicle kinetic energy while maintaining a livable environment for the occupants. This task is greatly facilitated if information regarding the spatial distribution of the energy flow through the vehicle is available. With this objective in mind, energy balance equations are developed. These equations do not alter the previously described computational procedures; they merely provide additional information to assist in understanding how the initial kinetic energy is absorbed.

The total system energy at any time is given by the following expression:

$$E_{TOT} = KE + PE + SE + DE + CE + FE \quad (1-157)$$

where

E_{TOT} = Total system energy

KE = Total kinetic energy

PE = Total potential energy

SE = Total strain energy absorbed

DE = Total damping energy dissipated

CE = Total crushing (external spring) energy absorbed

FE = Total friction energy dissipated by sliding of
external springs on the ground

The total system energy E_{TOT} remains constant during the analysis. The total kinetic and potential energies result from summing the energies for each mass over the number of masses (NM).

$$KE = \sum_{i=1}^{NM} KE_i \quad PE = \sum_{i=1}^{NM} PE_i \quad (1-158)$$

The total strain and damping energies are obtained by summing the strain and damping energy for each internal beam element (ij pair) over the NB ij pairs.

$$SE = \sum_{ij=1}^{NB} SE_{ij} \quad DE = \sum_{ij=1}^{NB} DE_{ij} \quad (1-159)$$

SE_{ij} results from the elastic-plastic behavior of the beam, and DE_{ij} results from its damping properties. The total crushing and friction energies result from summing the energies for all the individual crash springs (ik pairs) over all the NSP ik pairs.

$$FE = \sum_{ik=1}^{NSP} FE_{ik} \quad CE = \sum_{ik=1}^{NSP} CE_{ik} \quad (1-160)$$

Referring to Equation (1-157), at time zero all energies are zero except KE, PE and E_{TOT} . The potential energy is referenced to the ground plane. After impact with the ground, the kinetic energy decreases, and the potential energy may increase or decrease. Damping, strain, crushing and friction energies all increase to keep E_{TOT} constant.

In Equation (1-159), the summations over the ij pairs exclude those ij pairs that are identified in the input as DRI elements. This is done because these ij beams and their masses are isolated from the rest of the system; the forces in DRI beam ij drive mass j but not mass i. Also, the summations in Equation (1-158) for the kinetic and potential energies exclude mass j in a DRI ij pair, since this mass is isolated from the system. Thus, if ij pairs 6-9 and 11-15 are defined as DRI elements, the summations for SE and DE will exclude these ij pairs and the summations for KE and PE will exclude masses 9 and 15.

The kinetic energy for each mass, including translational and rotational components, is simply

$$KE_i = \frac{1}{2} \{vel_i\}^T [M_i] \{vel_i\} \quad (1-161)$$

where

$$[M_i] = \begin{bmatrix} m_i & & & & & \\ & m_i & & & & \\ & & m_i & & & \\ & & & I_{xi} & I_{xyi} & I_{xzi} \\ & & & I_{xyi} & I_{yi} & I_{yzi} \\ & & & I_{xzi} & I_{yzi} & I_{zi} \end{bmatrix} \quad (1-162)$$

and

$$\{vel_i\} = \begin{pmatrix} u_i \\ v_i \\ w_i \\ p_i \\ q_i \\ r_i \end{pmatrix} \quad (1-163)$$

$[M_i]$ is the 6 x 6 inertia matrix for mass i , and $\{vel_i\}$ is a six-element vector of the linear and angular velocity components of mass i in body-fixed axes.

The i^{th} mass potential energy, referenced to the ground plane, is given by

$$PE_i = -W_i z_i \quad (1-164)$$

Note that z_i is positive downward, measured from the ground plane.

The strain energy in internal beam ij is computed as a continuous summation of the incremental energy contributions from each integration interval.

$$(SE_{ij})_{current} = (SE_{ij})_{previous} + \sum_{l=1}^6 (F'_{il} dv_{il} + F'_{jl} dv_{jl}) \quad (1-165)$$

$F'_{i\ell} dv_{i\ell}$ is the internal beam force (or moment) in the ℓ^{th} direction, multiplied by the incremental beam deflection (or rotation) in the ℓ^{th} direction at beam end iM. The corresponding j subscript terms apply to beam end jN. The sum of these constitute the incremental strain energy for the integration interval being considered. This straightforward formulation automatically accounts for the complexities of nonlinear, coupled deflections and unloading-reloading behavior, since these are considered in the calculation of $F'_{i\ell}$.

The damping energy dissipated in internal beam ij is computed in a similar manner:

$$(DE_{ij})_{\text{current}} = (DE_{ij})_{\text{previous}} + \sum_{\ell=1}^6 (F'_{Di\ell} dv_{i\ell} + F'_{Dj\ell} dv_{j\ell}) \quad (1-166)$$

$F'_{Di\ell}$ is the internal beam damping force (or moment) in the ℓ^{th} direction.

The crushing and friction energies are calculated as a summation of incremental energy changes. These are first expressed in terms of the total external spring forces acting on mass m_i , and the incremental displacements and rotations of m_i . These total forces are then broken down into the components from each individual external spring (ik pair), and further into the components resulting from spring loads normal to the surface (crushing energy) and those loads in the plane of the surface (friction energy).

First we write

$$\begin{Bmatrix} CE_i \\ + \\ FE_i \end{Bmatrix}_{\text{current}} = \begin{Bmatrix} CE_i \\ + \\ FE_i \end{Bmatrix}_{\text{previous}} - \left[XC_i, YC_i, \dots, NC_i \right] \begin{Bmatrix} dx'_i \\ dy'_i \\ dz'_i \\ dpin_i \\ dqin_i \\ drin_i \end{Bmatrix} \quad (1-167)$$

XC_i, YC_i, \dots, NC_i are the six forces and moments acting on mass i in body-fixed axes, resulting from all ik external springs attached to mass i . These are given by Equation (1-110). The vector $\{dx'_i, dy'_i, dz'_i, dpin_i, dqin_i, drin_i\}$ is made up of the six incremental deflections and rotations of mass m_i , in the same body-fixed axes. The first three terms of this vector are given by a simple rotation transformation of the incremental deflections in ground axes, which are obtained directly from numerical integration of the equations of motion.

$$\begin{Bmatrix} dx'_i \\ dy'_i \\ dz'_i \end{Bmatrix} = [A_i]^T \begin{Bmatrix} dx_i \\ dy_i \\ dz_i \end{Bmatrix} \quad (1-168)$$

The last three terms of the incremental displacement vector in Equation (1-167) are the incremental changes in the integrals of the angular velocities of mass m_i , p_i , q_i , r_i . These are the incremental rotations of mass m_i in body-fixed axes for the integration interval being considered, given by Equation (1-12).

The negative sign in Equation (1-167) results from the fact that the forces acting on mass m_i rather than the forces within the ik springs are being considered. A positive deflection of spring ik results in a negative force on mass m_i . The energy calculated in Equation (1-167) includes the energy dissipated by the sliding of spring ik on the ground with a friction coefficient, since the forces in that equation include the ground drag loads due to friction.

Now separate out the contribution of each external spring (ik pair), by substituting Equations (1-109) and (1-110) for the $[XC_i, YC_i, \dots, NC_i]$ in Equation (1-167). This reformulates Equation (1-167) into a function of the individual crash spring forces FSP_{ijk} , where i and k refer to the ik spring and

j refers to the direction of the forces on the ik spring. These forces are shown in Figure 1-13. The resulting equation for the crushing/friction energy associated with each spring ik is the following:

$$\begin{pmatrix} CE_{ik} \\ + \\ FE_{ik} \end{pmatrix}_{\text{current}} = \begin{pmatrix} CE_{ik} \\ + \\ FE_{ik} \end{pmatrix}_{\text{previous}} - \sum_{j=1}^3 FSP_{ijk} d'vc_{ij} + TERM_{ik} \quad (1-169)$$

where

$$\{d'vc_i\} = \begin{Bmatrix} dx'_i \\ dy'_i \\ dz'_i \end{Bmatrix} \quad (1-170)$$

and

$$\begin{aligned} TERM_{ik} &= FSP_{i31} (\ell_{i1} + rx) dqin_i - FSP_{i21} (\ell_{i1} + rx) drin_i \\ &\quad + FSP_{i11} (rydrin_i - rzdqin_i) + FSP_{i21} rzdpin_i - FSP_{i31} rydpin_i \quad k = 1 \\ \\ TERM_{ik} &= - FSP_{i32} (\ell_{i2} + ry) dpin_i + FSP_{i12} (\ell_{i2} + ry) drin_i \\ &\quad - FSP_{i12} rzdqin_i + FSP_{i22} (rzdpin_i - rxdrin_i) + FSP_{i32} rxdqin_i \quad k = 2 \\ \\ TERM_{ik} &= FSP_{i23} (\ell_{i3} + rz) dpin_i - FSP_{i13} (\ell_{i3} + rz) dqin_i \\ &\quad + FSP_{i13} rydrin_i - FSP_{i23} rxdrin_i + FSP_{i33} (rxdqin_i - rydpin_i) \quad k = 3 \end{aligned} \quad (1-171)$$

Finally, Equation (1-169) is further reduced by separating the individual spring forces FSP_{ijk} into the components due to friction and crushing. These are denoted by $FSPF_{ijk}$ and $FSPC_{ijk}$, respectively. These are calculated by using Equations (1-103) and (1-108), with $XVOC_{ijk}$ and $XVOC_{SL,ijk}$ broken down further into crushing and friction components. This results in the following set of equations:

$$\begin{array}{ll}
\text{crushing} & \{XVOCC_{ik}\} = \begin{Bmatrix} 0 \\ 0 \\ XVOCC_{13k} \end{Bmatrix} \\
\text{friction} & \{XVOCF_{ik}\} = \begin{Bmatrix} XVOCC_{11k} \\ XVOCC_{12k} \\ 0 \end{Bmatrix}
\end{array} \left. \vphantom{\begin{array}{l} \text{crushing} \\ \text{friction} \end{array}} \right\} \begin{array}{l} \text{Contact} \\ \text{with} \\ \text{Horizontal} \\ \text{Ground} \end{array}$$

(1-172)

$$\begin{array}{ll}
\text{crushing} & \{XVOCSLC_{ik}\} = \begin{Bmatrix} 0 \\ 0 \\ XVOCSL_{13k} \end{Bmatrix} \\
\text{friction} & \{XVOCSLF_{ik}\} = \begin{Bmatrix} XVOCSL_{11k} \\ XVOCSL_{12k} \\ 0 \end{Bmatrix}
\end{array} \left. \vphantom{\begin{array}{l} \text{crushing} \\ \text{friction} \end{array}} \right\} \begin{array}{l} \text{Contact} \\ \text{with} \\ \text{Inclined} \\ \text{Slope} \end{array}$$

$$\begin{array}{ll}
\text{crushing} & \{FSPC_{ik}\} = - [Ai]^T \{XVOCC_{ik}\} \\
\text{friction} & \{FSPF_{ik}\} = - [Ai]^T \{XVOCF_{ik}\}
\end{array} \left. \vphantom{\begin{array}{l} \text{crushing} \\ \text{friction} \end{array}} \right\} \begin{array}{l} \text{Contact} \\ \text{with} \\ \text{Horizontal} \\ \text{Ground} \end{array}$$

(1-173)

$$\begin{array}{ll}
\text{crushing} & \{FSPC_{ik}\} = - [Ai]^T [ABETA] \{XVOCSLC_{ik}\} \\
\text{friction} & \{FSPF_{ik}\} = - [Ai]^T [ABETA] \{XVOCSLF_{ik}\}
\end{array} \left. \vphantom{\begin{array}{l} \text{crushing} \\ \text{friction} \end{array}} \right\} \begin{array}{l} \text{Contact} \\ \text{with} \\ \text{Inclined} \\ \text{Slope} \end{array}$$

$$\begin{aligned}
(CE_{ik})_{\text{current}} &= (CE_{ik})_{\text{previous}} - \sum_{j=1}^3 FSPC_{ijk} d'_{vc_{ij}} + TERM_{ik} \\
(FE_{ik})_{\text{current}} &= (FE_{ik})_{\text{previous}} - \sum_{j=1}^3 FSPF_{ijk} d'_{vc_{ij}} + TERM_{ik}
\end{aligned}$$

(1-174)

In Equations (1-174), $TERM_{ik}$ and $TERM_{ik}$ are evaluated using Equation (1-171) with the FSP's replaced by FSPC and FSPF as appropriate. Equations (1-174) give the crushing and friction energies for each spring (ik pair) used in equations (1-160) to calculate the total CE and FE.

1.3.17 Stress Equations

The program is coded so that internal beam elements can be analyzed for stresses and checked against two failure criteria. For each beam element, the location of the maximum bending moments in two planes is determined. This occurs at one end of the beam or the other, never in the middle. The program calculates the stress state of four plane elements located at the four sides of the beam; top, bottom, left and right. Axial stresses due to axial load and bending are computed. Shear stresses due to tension and lateral loads are also calculated. For each of the four plane elements of a given beam, the maximum shear stress and two principal stresses are then calculated. These are used to form ratios of actual stress/failure stress using two failure criteria; Maximum Shear Stress Theory and the Theory of Constant Energy of Distortion. The stress calculations in no way alter the scheme for computing internal beam loads discussed in Section 1.3.5.3. They are an additional calculation to provide the program user with a measure of the stress state for the beam elements.

Figure 1-22 illustrates a typical plane element as viewed from the top (for the top and bottom elements) or from the left side (for the left and right side elements).

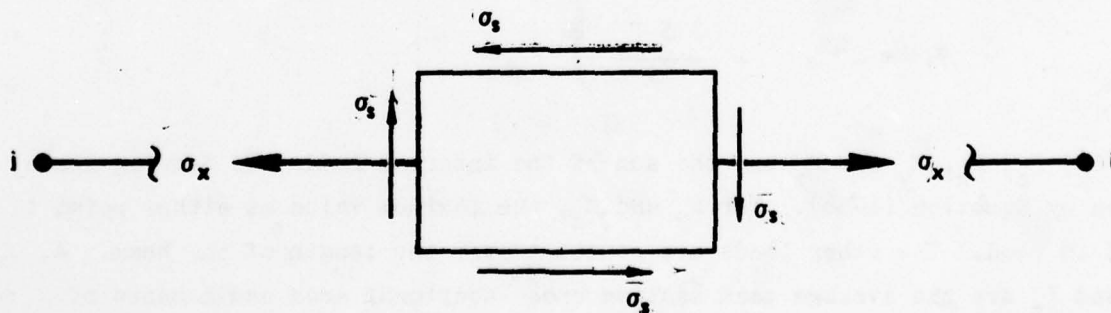


Figure 1-22. Stress Element

For the top and bottom elements, Figure 1-22 is looking in the direction of the positive $z_{b_{ij}}$ beam axis; for the left and right side elements in the direction of the positive $y_{b_{ij}}$ axis. The positive sign conventions for axial stress σ_x and shear stress σ_s are shown.

The axial and shear stresses are calculated as follows:

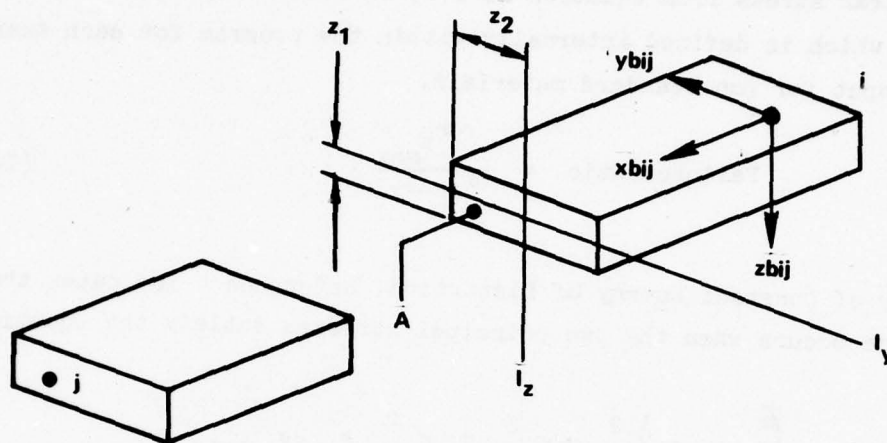
$$\left. \begin{aligned} \sigma_x &= \frac{F_x}{A} - \frac{M_y z_1}{I_y} \\ \sigma_s &= QM_x + \frac{1.5 F_y}{A} \end{aligned} \right\} \begin{array}{l} \text{Top} \\ \\ \end{array} \quad (1-175a)$$

$$\left. \begin{aligned} \sigma_x &= \frac{F_x}{A} + \frac{M_y z_1}{I_y} \\ \sigma_s &= -QM_x + \frac{1.5 F_y}{A} \end{aligned} \right\} \begin{array}{l} \text{Bottom} \\ \\ \end{array} \quad (1-175b)$$

$$\left. \begin{aligned} \sigma_x &= \frac{F_x}{A} + \frac{M_z z_2}{I_z} \\ \sigma_s &= QM_x - \frac{1.5 F_z}{A} \end{aligned} \right\} \begin{array}{l} \text{Left Side} \\ \\ \end{array} \quad (1-175c)$$

$$\left. \begin{aligned} \sigma_x &= \frac{F_x}{A} - \frac{M_z z_2}{I_z} \\ \sigma_s &= -QM_x - \frac{1.5 F_z}{A} \end{aligned} \right\} \begin{array}{l} \text{Right Side} \\ \\ \end{array} \quad (1-175d)$$

F_x , F_y , F_z , M_x , M_y and M_z are the sum of the internal loads and damping loads given by Equation (1-58). For M_y and M_z , the maximum value at either point i or j is used. The other loads are constant over the length of the beam. A , I_y and I_z are the average beam section cross-sectional area and moments of inertia about the $y_{b_{ij}}$ and $z_{b_{ij}}$ axes, respectively. z_1 and z_2 are the distances from the neutral axes to the extreme fibres in the $z_{b_{ij}}$ and $y_{b_{ij}}$ directions, respectively. These are illustrated in the following sketch:



Q is a sectional shape factor relating the torsional shear stress to the applied moment. Reference 4, Table IX contains formulae for $1/Q$ for a variety of commonly encountered structural cross sections. The 1.5 factor for the direct shear contributions in Equations (1-175) results from the non-uniform distribution of the shear stress across the section. The peak value at the center is used.

After the axial stress σ_x and shear stress σ_s are calculated for each of the four locations, the maximum shear stress $\sigma_{s_{max}}$ and the principal stresses σ_1 and σ_2 are calculated. Reference 4, Table II, gives the following equations:

$$\sigma_{s_{max}} = \sqrt{\left(\frac{1}{2} \sigma_x\right)^2 + \sigma_s^2} \quad (1-176a)$$

$$\sigma_1, \sigma_2 = \frac{1}{2} \sigma_x \pm \sigma_{s_{max}} \quad (1-176b)$$

These stresses are used to calculate "failure ratios," which are the ratios of the current stress to the failures stress, for each of the four locations. The failure ratios are calculated for two failure theories; Maximum Shear Stress Theory and Theory of Constant Energy of Distortion. For the former, the maximum shear stress from equation (1-176) is divided by the allowable shear stress, which is defined internally within the program for each standard material or input for non-standard materials.

$$\text{Failure Ratio} = \frac{\sigma_{s \max}}{\sigma_{\text{shear}}} \quad (1-177)$$

For the Theory of Constant Energy of Distortion, Reference 4 indicates that elastic failure occurs when the two principal stresses satisfy the equation

$$(\sigma_1 - \sigma_2)^2 + \sigma_2^2 + \sigma_1^2 = 2\sigma_{\text{yield}}^2$$

This reduces to

$$\sigma_1^2 - \sigma_1 \sigma_2 + \sigma_2^2 = \sigma_{\text{yield}}^2 \quad (1-178)$$

The program calculates a reference principal stress defined as

$$\sigma_p = \sqrt{\sigma_1^2 - \sigma_1 \sigma_2 + \sigma_2^2}$$

This is then divided by σ_{yield} to form a Failure Ratio for the Theory of Constant Energy Distortion:

$$\text{Failure Ratio} = \frac{\sigma_p}{\sigma_{\text{yield}}} \quad (1-179)$$

Both Failure Ratios from equations (1-177) and (1-179) are printed out at each print time interval, for each of the four plane element locations for each internal beam.

SECTION 2

PROGRAM CONTROLS

2.1 GENERAL

This section contains a brief description of

- The symbols which control the input-output capabilities of KRASH,
- the program subroutines,
- a comprehensive program listing

A User's Guide which completely defines the input-output requirements is provided in Volume 2, Section 2.

2.2 CONTROL PARAMETERS

Tables 2-1 through 2-4 list the various input/output control parameters which are used extensively in KRASH. Table 2-1 presents the program sizing constants, and shows the maximum allowable sizes for the different types of data. Table 2-2 defines the program execution modes. Tables 2-3 and 2-4 define the print output and plot output options, respectively. Table 2-5 and Figure 2-1 list the subroutines used in KRASH and provide a brief outline of the program flow. A Programmer's Manual (Reference 7) contains detailed programming data.

TABLE 2-1. PROGRAM SIZING CONSTANTS

CONSTANT	MAXIMUM VALUE	DESCRIPTION
NM	80	Number of masses
NSP	40	Number of external springs
NB	100	Number of internal beams
NLB	120	Number of nonlinear beam-direction combinations (KR Tables)
NHI	80	Number of masses having non-zero $H_{e_{x_i}}$, $H_{e_{y_i}}$, $H_{e_{z_i}}$, I_{xy_i} , I_{yz_i} , or ℓ_{c_i}
MVP	-	Reference mass number for volume penetration calculations
NVCH	5	Number of volumes for occupiable volume change calculations
NDRI	100	Number of DRI beam elements
NMTL	5	Number of non-standard beam materials
NACC	50	Number of input acceleration time-history tables
NVBM	100	Number of internal beams having non-standard maximum deflections for beam rupture. Standard Value = 100 (inches of deflection and radians of rotation)
NFBM	100	Number of internal beams having non-standard maximum forces for beam rupture. Standard Value = 1E10
NPH	80	Number of masses having non-zero Euler angles ϕ_i ", θ_i ", ψ_i "
ND	100	Number of internal beams having damping ratios different from that specified on card 0900
NKM	100	Number of internal beams for which the full 6 x 6 stiffness matrix is directly input
NPIN	100	Number of internal beams having other than fixed-fixed end conditions
NNP	50	Number of node points
NUB	100	Number of unsymmetrical beams

TABLE 2-2. PROGRAM EXECUTION MODES

RUNMOD	INPUT DATA SET	DATA SET ANALYZED	AIRPLANE MODEL	IMPACT CONDITIONS
0	Full Airplane	Full Airplane	Unsymmetrical	Unsymmetrical
1	Half Airplane	Half Airplane	Symmetrical	Symmetrical
2	Half Airplane	Full Airplane	Symmetrical	Unsymmetrical

TABLE 2-3. PRINT OUTPUT OPTIONS

INPUT CONSTANT	CORRESPONDING PRINT DATA
NSF	Beam strain forces
NTF	Beam total forces (strain and damping)
NDE	Beam deflections
NSPD	External spring loads and deflections
NED	Energy breakdown by mass, beam and spring
NS	Beam stresses
NRP	Mass displacement, velocity and acceleration data

TABLE 2-4. PLOT OUTPUT PARAMETERS

INPUT CONSTANT	CORRESPONDING PLOT CONTROL
NMEP	Number of mass points to be plotted
NNEP	Number of node points to be plotted
NBFP	Number of beams having force/moment plots
NBDP	Number of beams having deflection/rotation plots
NSTP	Number of beams having stress plots
NSEP	Number of masses having external spring force/deflection plots
NDRP	Number of DRI masses for plotting

TABLE 2-5. PROGRAM KRASH SUBROUTINES

SUBROUTINE NAME	FUNCTION
MAIN	Controls overall program execution, numerical integration
ECHO	Prints out listing of input data cards
INPUT	Reads input data
GENMOD	Generates full airplane input data set from half airplane input data
INPRNT	Prints out input data
IC	Calculates initial conditions
DOAIJ	Calculates internal beam frequencies and damping constants
DERIV	Calculates accelerations of masses
CFORCE	Calculates external spring forces
PRINT	Prints output data and stores data for plots
RC	Initial conditions used with restart case
RSIN	Reads initial conditions off tape from previous case for restart case
RSOUT	Writes current conditions onto tape for future restart usage
PREPLT	Reads and orders plot data
PLOTT	Prints data in special plot format
DATIN	Performs actual tape read, called from RSIN
DATOUT	Performs actual tape write, called from RSOUT
ACCELT	Calculates specified mass accelerations from input data
INTERP	Interpolation subroutine used in ACCELT
EULER	Calculates 3 x 3 rotation transformation on matrix given 3 Euler angles
MATMUL	Multiplies two 3 x 3 matrices
MATVEC	Multiplies a 3 x 3 matrix times a 3 x 1 vector

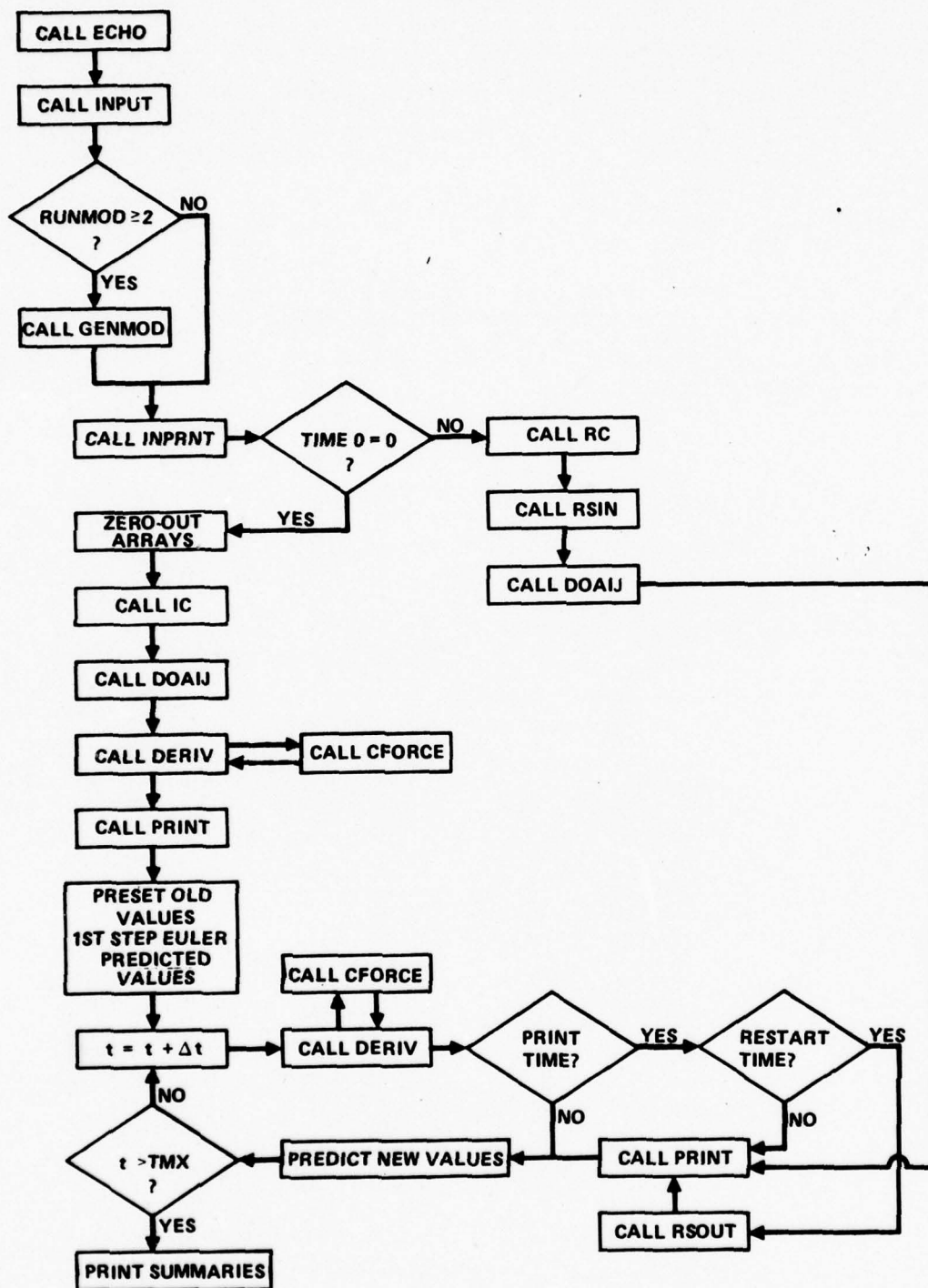


Figure 2-1. KRASH Flow Chart

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ERRATA SHEET

Report No. FAA-RD-77-189, I

PROGRAM "KRASH" THEORY

1. Delete complete Appendix A, Program Listing, and replace with enclosed Appendix A (Revised), Program Listing, pages A-2 through A-202.
2. The enclosed change (yellow sheet) to the listing, Subroutine 'INPUT', is necessary if it is desired to model more than one oleo strut. Refer to Page A-130.

Released September 28, 1979


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7 PHOLD(80),THEOLD(80),PSTOLD(80),
8 XACFO(80),YACFO(80),ZACFO(80),XAFOLD(80),YAFOLD(80),ZAFOLD(80),
9 XNPFD(50),YNPFD(50),ZNPFD(50),XANPFO(50),YANPFO(50),ZANPFO(50),
A TKR(200),TPEN(80),DTHALF,
B KRBEAH(4,200),KRFLAG(900),IPEN(80),KPEN,KRCNT
COMMON/CORNEW/ DAMPC,RUNMOD,PUNMOD
COMMON/MCFIII/ SYMFG
COMMON/CORALL/ C(6,150),PI(60),Q(60),R(80),UI(80),VI(80),W(80),X(81),
1 Y(81),ZI(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),
2 YI(80),ZI(80),XYI(80),XZI(80),YZI(80),AIJ(9),BIJ(720),
3 DROT(150),OAT(720),VEE(900),NGT(80),PHI(80),THETA(80),PSI(80),
4 POOT(60),PDOT(80),RDOT(80),UDOT(80),VDOT(80),MDOT(80),XDOT(80),
5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTA,T,
6 XACC(80),YACC(80),ZACC(80),AIDOT(9),
7 PHIIJ(150),THEIJ(150),PSIIJ(150),SUHDF(6,150),TITLE,
8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9 OPINI(81),DQIN(81),DRINI(81),SEIJJ(150),DEIJJ(150),CEIK(40),
A CEIKF(40),
B SBARI(40),KUNI(40),MAXNM,MXIGS,MXTBL,
C NM,NB,I,J,IG(150),JG(150),
D NI(900),NI(40),IJPR(150)
COMMON/OTPLT/ NNEP,NNEP,NBFP,NSEP,NDRP,NSTP,NENP,
* *
NHESS,NODE,NBMF,JBDH,JBSR,JENG,JDRJ,
NHEM,NHEM,NBFM,NDSM,NSEW,NDRM,NSTM,NEM,NPRINT
COMMON /RESTR/ CASEIN,RUNIN,MSECIN,CASOUT,RUNOUT,MSCOUT(5)
COMMON /VARINT/ MINDT,DT2,TPRINT,EL,EU,RATHIN,RATHAX,IPC,IVAR
EQUIVALENCE INI(I),N3(I),VEE(I),VEE2(I))
DATA STOP,'END ','
MAXNM = 80
IPC = 0
MXIGS = 150
MXTBL = 180
CALL ECHO
CALL ECHO
1 CALL INPUT
IF(TITLE(1).EQ.STOP) GO TO 1000
IF(DELTAT.LE.0.) GO TO 1000
IF(INM.LE.0) GO TO 1000

C THE INPUT PARAMETER RUNMOD CONTROLS THE TYPE OF CASE TO BE RUN
C ACCORDING TO THE FOLLOWING OPTIONS:
C
C
C RUNMOD DESCRIPTION
C
C 0. INPUT FULL AIRPLANE DATA SET, STANDARD EXECUTION
C
C 1. INPUT 1/2 AIRPLANE DATA SET, SYMMETRICAL IMPACT
C
C 2. INPUT 1/2 AIRPLANE DATA SET AND THE PROGRAM WILL
C GENERATE AND PRINT THE FULL SYMMETRICAL DATA SET
C
C 3. SAME AS 2 WITH COMPLETE DATA SET PUNCH
C

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C      4.      SAME AS 2 ONLY INCLUDE SYMMETRICAL CONSTRAINTS IN DE.
C
C      REMIND NECESSARY UNITS IF PLOTS ARE REQUESTED
C
      IF(NMEP .GT. 0) REMIND 1
      IF(NNEP .GT. 0) REMIND 2
      IF(NBFP .GT. 0) REMIND 3
      IF(NBDP .GT. 0) REMIND 4
      IF(NSEP .GT. 0) REMIND 8
      IF(NORP .GT. 0) REMIND 9
      IF(NENP.GT.0) REMIND 11
      REMIND 10
      IF(NSTP .GT. 0) REMIND 13
C
C      SET PLOT COUNTERS TO ZERO
C
      NMEW = 0
      NNEW = 0
      NBFW = 0
      NBDW = 0
      NSEW = 0
      NDRW = 0
      NSTW = 0
      NENW = 0
      NPRINT = 0
C
C      SET ENERGY ERROR MESSAGE INDICES TO ZERO
C
      IEER=0
      IETOT=0
      IESE=0
      IEPSE=0
      IEDE=0
      IEPDE=0
      IECE=0
      IEPCE=0
      IEFE=0
      IEPFE=0
      IEDEV=0
      SYMFLG = 0.
      PUNMOD = 0.
      IF(RUNMOD.EQ.1.) SYMFLG = 1.
      IF(RUNMOD.EQ.3.) PUNMOD = 1.
      IF(RUNMOD.EQ.4.) SYMFLG = 2.
      IF(RUNMOD.EQ.2.) CALL GENMOD
      CALL INPRINT
      DT2 = 2.0*DELTAT
      DTHALF = .5*DELTAT
      DO 130 I = 1,NH
        XI(I) = YI(I)*ZII(I)-YZI(I)*YZII(I)
        XI2(I) = XYI(I)*ZII(I)+XZI(I)*YZII(I)

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ISN 0044
ISN 0046
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ISN 0096

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ISN 0097      XI3(I) = XYI(I)*YZI(I)+YI(I)*XZI(I)
ISN 0098      XI4(I) = XI(I)*YZI(I)+XZI(I)*YI(I)
ISN 0099      XI5(I) = XI(I)*ZI(I)-XZI(I)*XZI(I)
ISN 0100      XI6(I) = XI(I)*YI(I)-YI(I)*XZI(I)
ISN 0101      DELI(I) = 1.0/(XI(I)*XI(I)-YI(I)*XZI(I)+XZI(I)*XZI(I))
ISN 0102      DO 154 I=1,200
C              COUNTERS FOR RUPTURE AND YIELD SUMMARY ARE SET TO ZERO
ISN 0103      TKRI(I)=0.
ISN 0104      DO 154 J=1,4
ISN 0105      KRBEAM(J,I)=0.
ISN 0106      154 CONTINUE
ISN 0107      DO 155 I=1,200
ISN 0108      TSP(I)=0.
ISN 0109      DO 155 J=1,5
ISN 0110      EXSP(J,I)=0.
ISN 0111      KXSP(J,I)=0.
ISN 0112      155 CONTINUE
ISN 0113      IF (RUNIN .EQ. 0) GO TO 5
ISN 0114      CALL RC
ISN 0115      CALL RSINICASEIN,RUNIN,MSECIN)
ISN 0116      PRINT 5000,CASEIN,RUNIN,MSECIN
ISN 0117      CALL DOAIJ
ISN 0118      INGOLD = INGSCCT
ISN 0119      GO TO 270
ISN 0120      5 CONTINUE
ISN 0121      5000 FORMAT(1H0,2X,'***DATA MANAGEMENT RESTART ROUTINES INVOKED***'
ISN 0122      1 / 10X,'REQUESTED CASE TITLE - ',A8
ISN 0123      2 / 10X,'REQUESTED RUN NUMBER - ',I10
ISN 0124      3 / 10X,'REQUESTED RESTART TIME - ',I10 / 1H0)
ISN 0125      INGSCCT = 0
ISN 0126      INGOLD = 0
ISN 0127      KRCONT = 0
ISN 0128      KPEN=0
ISN 0129      KKONT=0
ISN 0130      KPL=0
C (26)
C ZERO ARRAYS
ISN 0131      TIME = 0.0
ISN 0132      NM9 = 9*NM
ISN 0133      DO 140 I = 1,NM9
ISN 0134      BIJ(I) = 0.0
ISN 0135      DO 150 I = 1,NM
ISN 0136      DX(I) = 0.0
ISN 0137      DY(I) = 0.0
ISN 0138      DZ(I) = 0.0
ISN 0139      XX(I) = 0.0
ISN 0140      XY(I) = 0.0
ISN 0141      XZ(I) = 0.0
ISN 0142      XL(I) = 0.0
ISN 0143      XH(I) = 0.0
ISN 0144      XN(I) = 0.0
ISN 0145      XIMP(I)=0.
ISN 0146      YIMP(I)=0.

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ISN 0145      ZIMP(I)=0.
ISN 0146      DPX(I) = 0.0
ISN 0147      DRY(I) = 0.0
ISN 0148      DPZ(I) = 0.0
ISN 0149      DPL(I) = 0.0
ISN 0150      DPH(I) = 0.0
ISN 0151      DPN(I) = 0.0
ISN 0152      DPN(I) = 0.0
ISN 0153      DQINI(I) = 0.0
ISN 0154      DRIN(I) = 0.0
ISN 0155      XACC(I)=0.0
ISN 0156      YACC(I)=0.0
ISN 0157      ZACC(I)=0.0
ISN 0158      150 CONTINUE
ISN 0159      DO 156 I=1,600
ISN 0160      KRFLAG(I)=0
ISN 0161      156 CONTINUE
ISN 0162      DO 157 I=1,NNP
ISN 0163      XIMNP(I)=0.
ISN 0164      YIMNP(I)=0.
ISN 0165      ZIMNP(I)=0.
ISN 0166      802 FORMAT(/IX,'MAIN',4E15.6)
ISN 0167      157 CONTINUE
ISN 0168      DO 152 IKM=1,NSP
ISN 0169      IBS(IKM) = 0
ISN 0170      NN(IKM) = 0
ISN 0171      SC(IKM) = 0.0
ISN 0172      CEIK(IKM) = 0.0
ISN 0173      CEIKF(IKM) = 0.
ISN 0174      SBAR(IKM) = 0.
ISN 0175      KUN(IKM) = 0.
ISN 0176      FSPBAR(IKM) = 0.0
ISN 0177      C      EXTERNAL SPRING SUPPLY TERMS 3/79
ISN 0178      FSPOP(IKM)=0.
ISN 0179      SCP(IKM)=0.
ISN 0180      JBS(IKM)=0
ISN 0181      STEMP1(IKM)=0.
ISN 0182      STEMP2(IKM)=0.
ISN 0183      STEMP3(IKM)=0.
ISN 0184      STEMP4(IKM)=0.
ISN 0185      STEMP5(IKM)=0.
ISN 0186      152 CONTINUE
ISN 0187      DO 160 IJ = 1,NB
ISN 0188      SEIJ(IJ) = 0.0
ISN 0189      DEIJ(IJ) = 0.0
ISN 0190      KFL35(IJ) = 0
ISN 0191      FL26(IJ)=0
ISN 0192      FL26J(IJ)=0
ISN 0193      FL35I(IJ)=0
ISN 0194      FL35J(IJ)=0
ISN 0195      DO 160 L = 1,6
ISN 0196      SUMDF(L,IJ) = 0.0
00001990
00002000
00002010
00002020
00002030
00002040
00002050
00002060
00002070
00002080
00002090
00002100
00002110
00002120
00002130
00002140
00002150
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00002200
00002210
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00002450
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00002490
00002500
00002510

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ISN 0197      N3(IJ,L) = 0
ISN 0198      160 VEE2(L,IJ) = 0.0
ISN 0199      DO 165 J = 1,3
ISN 0200      DO 165 K = 1,3
ISN 0201      165 VEEDOT(J,K) = 0.0
ISN 0202      C DO INITIAL CONDITIONS
ISN 0203      CALL IC
ISN 0204      C DO ALL THE (AIJ) INTO DIJ
ISN 0205      CALL DOAIJ
ISN 0206      CALL DERIV
ISN 0207      CALL PRINT
ISN 0208      NPRINT = 1
ISN 0209      IPC = 0
ISN 0210      DO 200 I = 1,NH
ISN 0211      C PRESET OLD VALUES
ISN 0212      PHINO(I) = 0.0
ISN 0213      QINO(I) = 0.0
ISN 0214      RINO(I) = 0.0
ISN 0215      XOLD(I) = X(I)
ISN 0216      YOLD(I) = Y(I)
ISN 0217      ZOLD(I) = Z(I)
ISN 0218      PHIOLD(I) = PHI(I)
ISN 0219      THEOLD(I) = THETA(I)
ISN 0220      PSIOLD(I) = PSI(I)
ISN 0221      POLD(I) = P(I)
ISN 0222      QOLD(I) = Q(I)
ISN 0223      ROLD(I) = R(I)
ISN 0224      UOLD(I) = U(I)
ISN 0225      VOLD(I) = V(I)
ISN 0226      WOLD(I) = W(I)
ISN 0227      XAFOLD(I) = XACF(I)
ISN 0228      YAFOLD(I) = YACF(I)
ISN 0229      ZAFOLD(I) = ZACF(I)
ISN 0230      XIMPOLD(I) = XIMP(I)
ISN 0231      YIMPOLD(I) = YIMP(I)
ISN 0232      ZIMPOLD(I) = ZIMP(I)
ISN 0233      C DO 1ST STEP EULER
ISN 0234      OPIN(I) = DELTAT*P(I)
ISN 0235      OQIN(I) = DELTAT*Q(I)
ISN 0236      ORIN(I) = DELTAT*R(I)
ISN 0237      PIN(I) = OPIN(I)
ISN 0238      QIN(I) = OQIN(I)
ISN 0239      RIN(I) = ORIN(I)
ISN 0240      P(I) = P(I)+DELTAT*POOT(I)
ISN 0241      Q(I) = Q(I)+DELTAT*QOOT(I)
ISN 0242      R(I) = R(I)+DELTAT*ROOT(I)
ISN 0243      U(I) = U(I)+DELTAT*UOOT(I)
ISN 0244      V(I) = V(I)+DELTAT*VOOT(I)
ISN 0245      W(I) = W(I)+DELTAT*WOOT(I)
ISN 0246      XACF(I) = XACF(I)+DELTAT*XACFD(I)
ISN 0247      YACF(I) = YACF(I)+DELTAT*YACFD(I)
ISN 0248      ZACF(I) = ZACF(I)+DELTAT*ZACFD(I)
ISN 0249      XIMP(I) = XIMP(I)+DELTAT*XACF(I)
ISN 0250      00002520
ISN 0251      00002530
ISN 0252      00002540
ISN 0253      00002550
ISN 0254      00002560
ISN 0255      00002570
ISN 0256      00002580
ISN 0257      00002590
ISN 0258      00002600
ISN 0259      00002610
ISN 0260      00002620
ISN 0261      00002630
ISN 0262      00002640
ISN 0263      00002650
ISN 0264      00002660
ISN 0265      00002670
ISN 0266      00002680
ISN 0267      00002690
ISN 0268      00002700
ISN 0269      00002710
ISN 0270      00002720
ISN 0271      00002730
ISN 0272      00002740
ISN 0273      00002750
ISN 0274      00002760
ISN 0275      00002770
ISN 0276      00002780
ISN 0277      00002790
ISN 0278      00002800
ISN 0279      00002810
ISN 0280      00002820
ISN 0281      00002830
ISN 0282      00002840
ISN 0283      00002850
ISN 0284      00002860
ISN 0285      00002870
ISN 0286      00002880
ISN 0287      00002890
ISN 0288      00002900
ISN 0289      00002910
ISN 0290      00002920
ISN 0291      00002930
ISN 0292      00002940
ISN 0293      00002950
ISN 0294      00002960
ISN 0295      00002970
ISN 0296      00002980
ISN 0297      00002990
ISN 0298      00003000
ISN 0299      00003010
ISN 0300      00003020
ISN 0301      00003030
ISN 0302      00003040

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ISN 0246 YIMP(I)=YIMP(I)+DELTAT*YACF(I)
ISN 0247 ZIMP(I)=ZIMP(I)+DELTAT*ZACF(I)
ISN 0248 DX(I) = DELTAT*XDOT(I)
ISN 0249 X(I) = X(I)+DX(I)
ISN 0250 DY(I) = DELTAT*YDOT(I)
ISN 0251 Y(I) = Y(I)+DY(I)
ISN 0252 DZ(I) = DELTAT*ZDOT(I)
ISN 0253 Z(I) = Z(I)+DZ(I)
ISN 0254 PHI(I) = PHI(I) + DELTAT*PHIDOT(I)
ISN 0255 THETA(I) = THETA(I) + DELTAT*THETADOT(I)
ISN 0256 PSI(I) = PSI(I) + DELTAT*PSIDOT(I)
ISN 0257
200 CONTINUE
IF(NNP.EQ.0) GO TO 190
DO 210 J=1,NNP
  XANPFO(J)=XACNPF(J)
  YANPFO(J)=YACNPF(J)
  ZANPFO(J)=ZACNPF(J)
  XINPPL(J)=XIMPNP(J)
  YINPPL(J)=YIMPNP(J)
  ZINPPL(J)=ZIMPNP(J)
  XACNPF(J)=XACNPF(J)+DELTAT*XNPF(J)
  YACNPF(J)=YACNPF(J)+DELTAT*YNPF(J)
  ZACNPF(J)=ZACNPF(J)+DELTAT*ZNPF(J)
  XIMPNP(J)=XIMPNP(J)+DELTAT*XACNPF(J)
  YIMPNP(J)=YIMPNP(J)+DELTAT*YACNPF(J)
  ZIMPNP(J)=ZIMPNP(J)+DELTAT*ZACNPF(J)
210 CONTINUE
190 TIME = TIME+DT2-DELTAT
IPC = IPC+1
CAL_ DERIV
IF(IPC-IPRINT) 310,260,260
260 ITIME = TIME*1000 + .5
IF (MSCOUT(1).LE.0 .OR. MSCOUT(1).GT.ITIME) GO TO 270
CALL RSOUT(CASOUT, RUNOUT, ITIME)
PRINT 4000, MSCOUT(1), ITIME, TIME, CASOUT, RUNOUT
DO 265 II=1,4
265 MSCOUT(II) = MSCOUT(II+1)
MSCOUT(5) = 0
4000 FORMAT(1H0,2X,'***DATA MANAGEMENT CHECKPOINT ROUTINES INVOKED***'
1 / 10X,'REQUESTED TIME - ',I10 / 10X,' ACTUAL TIME - ',I1000003440
2 / 10X,' REAL TIME - ',1PE10.4 / 10X,' CASE TITLE - ',A8
3 / 10X,' RUN NO. - ',I10 / 1H0)
270 CALL PRINT
NPRINT = 1
IPC = 0
310 CONTINUE
C PREDICT, MOVE DOWN, AND DO DELTA'S
280 DO 300 I = 1,NNP
  T = PINO(I)+DT2*PI(I)
  PINO(I) = PIN(I)
  PINI(I) = T
  DPIN(I) = PINI(I)-PINO(I)
  T = QINO(I)+DT2*Q(I)
ISN 0287
ISN 0288
ISN 0289
ISN 0290
ISN 0291
ISN 0292
ISN 0293
ISN 0294
ISN 0295
ISN 0296
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00003570

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ISN 0297 QINO(I) = QIN(I)
ISN 0298 QINI(I) = T
ISN 0299 QINI(I) = QINI(I)-QINO(I)
ISN 0300 T = RINO(I)+DT2*R(I)
ISN 0301 RINO(I) = RINI(I)
ISN 0302 RINI(I) = T
ISN 0303 ORINI(I) = RINI(I)-RINO(I)
ISN 0304 T = XOLD(I)+DT2*XDOT(I)
ISN 0305 XOLD(I) = X(I)
ISN 0306 X(I) = T
ISN 0307 DX(I) = X(I)-XOLD(I)
ISN 0308 T = YOLD(I)+DT2*YDOT(I)
ISN 0309 YOLD(I) = Y(I)
ISN 0310 Y(I) = T
ISN 0311 DY(I) = Y(I)-YOLD(I)
ISN 0312 T = ZOLD(I)+DT2*ZDOT(I)
ISN 0313 ZOLD(I) = Z(I)
ISN 0314 Z(I) = T
ISN 0315 OZ(I) = Z(I)-ZOLD(I)
ISN 0316 T = PHIOLD(I)+DT2*PHIDOT(I)
ISN 0317 PHIOLD(I) = PHI(I)
ISN 0318 PHI(I) = T
ISN 0319 T = THEOLD(I)+DT2*THEDOT(I)
ISN 0320 THEOLD(I) = THETA(I)
ISN 0321 THETA(I) = T
ISN 0322 T = PSIOOLD(I)+DT2*PSIDOT(I)
ISN 0323 PSIOOLD(I) = PSI(I)
ISN 0324 PSI(I) = T
ISN 0325 T = POLD(I)+DT2*PODOT(I)
ISN 0326 POLD(I) = P(I)
ISN 0327 P(I) = T
ISN 0328 T = QOLD(I)+DT2*QDOT(I)
ISN 0329 QOLD(I) = Q(I)
ISN 0330 Q(I) = T
ISN 0331 T = ROLD(I)+DT2*RDOT(I)
ISN 0332 ROLD(I) = R(I)
ISN 0333 R(I) = T
ISN 0334 T = UOLD(I)+DT2*UDOT(I)
ISN 0335 UOLD(I) = U(I)
ISN 0336 U(I) = T
ISN 0337 T = VOLD(I)+DT2*VDOT(I)
ISN 0338 VOLD(I) = V(I)
ISN 0339 V(I) = T
ISN 0340 T = WOLD(I)+DT2*WDOT(I)
ISN 0341 WOLD(I) = W(I)
ISN 0342 W(I) = T
ISN 0343 T=XAFOLD(I)+DT2*XACFD(I)
ISN 0344 XAFOLD(I)=XACF(I)
ISN 0345 XACF(I)=T
ISN 0346 T=XIMPOL(I)+DT2*XACF(I)
ISN 0347 XIMPOL(I)=XIMP(I)
ISN 0348 XIMP(I)=T
ISN 0349 T=YAFOLD(I)+DT2*YACFD(I)

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00003960
00003970
00003980
00003990
00004000
00004010
00004020
00004030
00004040
00004050
00004060
00004070
00004080
00004090
00004100

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ISN 0350 YAFOLD(I)=YACF(I)
ISN 0351 YACF(I)=T
ISN 0352 T=YIMPOL(I)+DT2*YACF(I)
ISN 0353 YIMPOL(I)=YIMP(I)
ISN 0354 YIMP(I)=T
ISN 0355 T=ZAFOLD(I)+DT2*ZACFD(I)
ISN 0356 ZAFOLD(I)=ZACF(I)
ISN 0357 ZACF(I)=T
ISN 0358 T=ZIMPOL(I)+DT2*ZACF(I)
ISN 0359 ZIMPOL(I)=ZIMP(I)
ISN 0360 ZIMP(I)=T
ISN 0361
ISN 0362 800 FORMAT(/'MAIN',2X,'I=',I5,2X,'ZAFOLD=',E15.6,2X,'ZACFD=',E15.6,
1 2X,'ZACF=',E15.6,2X,'ZIMP=',E15.6,2X,'ZIMPOL=',E15.6/)
801 FORMAT(/6X,'J=',I5,2X,'ZANPFO=',E15.6,2X,'ZNPFD=',E15.6,2X,
1 'ZACNPF=',E15.6,2X,'ZIMPNP=',E15.6,2X,'ZIMPPL=',E15.6/)
300 CONTINUE
IF(INP.EQ.0) GO TO 400
DO 410 J=1,NIP
T=XANPFO(J)+DT2*XNPFD(J)
XANPFO(J)=XACNPF(J)
XACNPF(J)=T
T=XIMPPL(J)+DT2*XACNPF(J)
XIMPPL(J)=XIMPNP(J)
XIMPNP(J)=T
T=YANPFO(J)+DT2*YNPFD(J)
YANPFO(J)=YACNPF(J)
YACNPF(J)=T
T=YIMPPL(J)+DT2*YACNPF(J)
YIMPPL(J)=YIMPNP(J)
YIMPNP(J)=T
T=ZANPFO(J)+DT2*ZNPFD(J)
ZANPFO(J)=ZACNPF(J)
ZACNPF(J)=T
T=ZIMPPL(J)+DT2*ZACNPF(J)
ZIMPPL(J)=ZIMPNP(J)
ZIMPNP(J)=T
410 CONTINUE
400 CONTINUE
IF(IEER.NE.1) GO TO 420
PRINT 7100
7100 FORMAT(1H1 // 1X,'TERMINATION DUE TO ENERGY ERROR MESSAGE')
7201 IF(IESE.NE.1) GO TO 7202
PRINT 7301
7301 FORMAT(/ 1X,'26. IESE=1 TOTAL STRAIN ENERGY IS NEGATIVE')
7202 IF(IEPSE.NE.1) GO TO 7203
PRINT 7302
7302 FORMAT(/ 1X,'27. IEPSE=1 ELEMENT STRAIN ENERGY EXCEEDS NTOL2',
* ' VALUE')
7203 IF(IEDE.NE.1) GO TO 7204
PRINT 7303
7303 FORMAT(/ 1X,'28. IEDE=1 TOTAL DAMPING ENERGY IS NEGATIVE')
7204 IF(IEPDE.NE.1) GO TO 7205
PRINT 7304
ISN 0350 00004110
ISN 0351 00004120
ISN 0352 00004130
ISN 0353 00004140
ISN 0354 00004150
ISN 0355 00004160
ISN 0356 00004170
ISN 0357 00004180
ISN 0358 00004190
ISN 0359 00004200
ISN 0360 00004210
ISN 0361 00004220
ISN 0362 00004230
ISN 0363 00004240
ISN 0364 00004250
ISN 0365 00004260
ISN 0366 00004270
ISN 0367 00004280
ISN 0368 00004290
ISN 0369 00004300
ISN 0370 00004310
ISN 0371 00004320
ISN 0372 00004330
ISN 0373 00004340
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ISN 0375 00004360
ISN 0376 00004370
ISN 0377 00004380
ISN 0378 00004390
ISN 0379 00004400
ISN 0380 00004410
ISN 0381 00004420
ISN 0382 00004430
ISN 0383 00004440
ISN 0384 00004450
ISN 0385 00004460
ISN 0386 00004470
ISN 0387 00004480
ISN 0388 00004490
ISN 0389 00004500
ISN 0390 00004510
ISN 0391 00004520
ISN 0392 00004530
ISN 0393 00004540
ISN 0394 00004550
ISN 0395 00004560
ISN 0396 00004570
ISN 0397 00004580
ISN 0398 00004590
ISN 0399 00004600
ISN 0400 00004610
ISN 0401 00004620
ISN 0402 00004630

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ISN 0406 7304 FORMAT( / 1X, '29. IEPFE=1 ELEMENT DAMPING ENERGY EXCEEDS NTOL2',
* , VALUE',
ISN 0407 7205 IF(IECE.NE.1) GO TO 7206
ISN 0409 PRINT 7305
ISN 0410 7305 FORMAT( / 1X, '30. IECE=1 TOTAL CRUSHING ENERGY IS NEGATIVE')
ISN 0411 7206 IF(IEPCE.NE.1) GO TO 7207
ISN 0413 PRINT 7306
ISN 0414 7306 FORMAT( / 1X, '31. IEPCE=1 MASS CRUSHING ENERGY EXCEEDS NTOL2',
* , VALUE',
ISN 0415 7207 IF(IEFE.NE.1) GO TO 7208
ISN 0417 PRINT 7307
ISN 0418 7307 FORMAT( / 1X, '32. IEFE=1 TOTAL FRICTION ENERGY IS NEGATIVE')
ISN 0419 7208 IF(IEPFE.NE.1) GO TO 7209
ISN 0421 PRINT 7308
ISN 0422 7308 FORMAT( / 1X, '33. IEPFE=1 MASS FRICTION ENERGY EXCEEDS NTOL2',
* , VALUE',
ISN 0423 7209 IF(IEDEV.NE.1) GO TO 7210
ISN 0425 PRINT 7309
ISN 0426 7309 FORMAT( / 1X, '34. IEDEV=1 MASS DEVIATION EXCEEDS NTOL3 VALUE')
ISN 0427 7210 IF(IETOT.NE.1) GO TO 7211
ISN 0429 PRINT 7310
ISN 0430 7310 FORMAT( / 1X, '35. IETOT=1 TOTAL ENERGY CHANGE EXCEEDS NTOL1',
* , VALUE',
ISN 0431 7211 GO TO 500
ISN 0432 420 IF(TIME-TMAX) 190,190,500
ISN 0433 500 IF(KRCNT.LE.0) GO TO 4500
ISN 0435 PRINT 2000
ISN 0436 2000 FORMAT(1H1 // 1X, 'SUMMARY OF INTERNAL BEAM YIELDING',
1 'AND RUPTURE' / 18X, 'BEAM', 13X, 'BEAM DIRECTION FOR', 2X,
2 'TENSION(+) OR', 6X, 'TIME', 6X, 'I', 3X, 'J', 3X, 'M', 3X, 'N',
3 3X, 'YIELD', 6X, 'RUPTURE', 2X, 'COMPRESSION(-)') /
DO 3500 JJ=1,KRCNT
IJ = KRBEAM(1,JJ)
PRINT 3000,TKR(IJJ),KRBEAM(1,JJ),IG(IJJ),JG(IJJ),MG(IJJ),NG(IJJ),
1 KRBEAM(2,JJ),KRBEAM(3,JJ),KRBEAM(4,JJ)
3500 CONTINUE
ISN 0437 3000 FORMAT(1X,F9.6,3X,I3,4(2X,I2),5X,I1,11X,I1,10X,I2)
ISN 0438 4500 IF(KKONT.LE.0) GO TO 5600
ISN 0439 PRINT 2500
ISN 0440 2500 FORMAT(1H1//6X, 'SUMMARY OF EXTERNAL SPRING LOADING AND UNLOADING',
1 // 10X, 'TYPES;1=INITIAL LOADING 2=MAX.LOADING 3=UNLOAD TO ZERO
2 FORCE 4=INITIATION OF RELOAD'//10X, 'NOTE:SPRING RELOADS AT ZERO
3 FORCE(SEQ.1,2,3,4) OR AT FINITE FORCE VALUE(SEQ.1,2,4).
4 // 10X, 'NOTE:INITIAL DEFLECTION IS FIRST IMPACT IF NYPE=1,
5 OTHERWISE IT IS POINT AT WHICH RELOADING OCCUR FOR NYPE=4'
6 //1X, 'TIME(SEC)', 2X, 'MASS', 3X, 'NODE', 2X, 'DIRECTION',
7 2X, 'TYPE', 3X, 'INITIAL', 9X, 'MAXIMUM', 15X, 'UNLOADED',
8 / 13X, 'NO.', 4X, 'NO.', 3X, 'L=1,2,3,4X, 'NO.', 2X,
9 'DEFLECTION', 3X, 'FORCE', 1X, 4/ OR', 1X, 'DEFLECT', 1X, 'DEFLECT',
A 2X, 'I', 1X, 'FORCE')
DO 3600 JJ=1,KKONT
PRINT 3100,TSPI(JJ),KKSP(1,JJ),KKSP(2,JJ),KKSP(3,JJ),KKSP(4,JJ),
1 EXSP(1,JJ),EXSP(2,JJ),EXSP(3,JJ),EXSP(4,JJ),EXSP(5,JJ)

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ISN 0448 3600 CONTINUE
ISN 0449 3100 FORMAT(1X,F9.6,3X,3(12,5X),2X,12,3X,F8.4,2X,E10.2,2(2X,F8.4),2X,
1 E10.2)

C
C SUMMARY TABLE FOR PLASTIC HINGE
C
ISN 0450 5600 IF(KPL.LE.0) GO TO 5500
ISN 0452 5610 PRINT 5610
ISN 0453 5610 FORMAT(//,1X,'SUMMARY OF PLASTIC HINGE FORMATIONS')
ISN 0454 PRINT 5620
ISN 0455 5620 FORMAT(/,17X,'BEAM',9X,'BEAM END',4X,'TIME',5X,
1 'I J I J M N',3X,'MASS NO. DIRECTION')
ISN 0456 DO 5630 K=1,KPL
ISN 0457 TIMEPL=TPL(K)
ISN 0458 IJ=BPL(K,1)
ISN 0459 I=IG(IJ)
ISN 0460 J=JG(IJ)
ISN 0461 M=MG(IJ)
ISN 0462 N=NG(IJ)
ISN 0463 MNUB=BPL(K,3)
ISN 0464 NDIR=BP(K,2)
ISN 0465 PRINT 5640,TIMEPL,IJ,I,J,M,N,MNUB,NDIR
ISN 0466 5640 FORMAT(1X,F9.6,2X,513,5X,13,9X,12)
ISN 0467 5630 CONTINUE
ISN 0468 5500 IF (KPL.LE.0) GO TO 6000
ISN 0470 PRINT 5501
ISN 0471 5501 FORMAT(1H,7X,'CONTROL VOLUME PENETRATIONS' //)
ISN 0472 PRINT 5502
ISN 0473 5502 FORMAT(1H,13X,'TIME',10X,'MASS' //)
ISN 0474 PRINT 5503,(TPEN(K),IPEN(K),K=1,KPEN)
ISN 0475 5503 FORMAT(1H,10X,F10.5,110)
C*****PRINT ENERGY SUMMARY
ISN 0476 6000 PRINT 9
ISN 0477 9 FORMAT(1H1 // 1X,'SUMMARY OF ENERGY DISTRIBUTION' ///)
ISN 0478 PRINT 10
ISN 0479 10 FORMAT(10X,'PERCENT',2X,'TOTAL',5(11X,'PERCENT'),10X,'PERCENT' /
1 10X,'MAXIMUM',3X,'TOTAL',14X,'OF',4(16X,'OF'),15X,'OF',11X,
2 'ENERGY',2X,'SYSTEM',3X,'KINETIC',2X,'CURRENT',1X,
3 'POTENTIAL',1X,'CURRENT',2X,'STRAIN',3X,'CURRENT',2X,
4 'DAMPING',2X,'CURRENT',1X,'CRUSHING',2X,'CURRENT',1X,
5 'FRICTION',1X,'CURRENT' / 2X,'TIME',3X,'DEVIATION',1X,'ENERGY',
6 5(3X,'ENERGY',4X,'TOTAL'),3X,'ENERGY',3X,'TOTAL' /)
C
C DTP = IPRINT*DELTA
C TIME = -DTP
C INGO = INGOLD + 1
C DO 20 I = INGO,INGSC
C TIME = TIME+DTP
C ITIME = TIME*1000 + .5
C IF (ITIME .LT. MSECIN) GO TO 20
C ETOT = 0.0
C DO 30 J = 1,6
C ETOT = ETOT+ENGSHY(J,1)
C 30 PCIT0 = ETOT/ETOT0
ISN 0480
ISN 0481
ISN 0482
ISN 0483
ISN 0484
ISN 0485

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DO 40 J = 1,6
40 PERCNT(J) = ENGSHY(J,I)/ETOT
PRINT 60, ETIME(I),DEV(I),PCTT0,(ENGSHY(J,I),PERCNT(J),J=1,6)
60 FORMAT(1X,F6.5,2X,F9.6,2PF7.2,6(1PE11.3,2PF7.2))
20 CONTINUE
      TNAX=TIME
      CALL PREPLT(TPRINT,NM,NNP,NB,NSP,NORI,MSECIN)
      GO TO 1
1000 CONTINUE
      STOP
      END

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ISN 0486
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ISN 0488
ISN 0489
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ISN 0492
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ISN 0495
ISN 0496

PAGE 002

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6113 ZC = ACOUT
GO TO 6107
6114 A1 = ACOUT
GO TO 6107
6115 A2 = ACOUT
GO TO 6107
6116 A3 = ACOUT
6107 IF(IISAV.61.NACC) RETURN
GO TO 6105
END

ISN 0042
ISN 0043
ISN 0044
ISN 0045
ISN 0046
ISN 0047
ISN 0048
ISN 0049
ISN 0051
ISN 0052

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
 SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
 C DATA SET D2334CFORC AT LEVEL 004 AS OF 06/25/79
 C DATA SET D2332VCF AT LEVEL 001 AS OF 01/27/78
 C DATA SET D2332VCFOR AT LEVEL 001 AS OF 09/06/77
 C DATA SET D2332CF AT LEVEL 009 AS OF 09/02/77
 C SUBROUTINE CFORCE

ISN 0002	C	IMPLICIT REAL*8 (A-H,O-Z)	00000010
ISN 0003		REAL*8 KUN	00000020
ISN 0004		INTEGER*4 TITLE(40)	00000030
ISN 0005		INTEGER*2 NI,NN,IBS,JBS	00000040
ISN 0006		INTEGER*2 MTEMP(40)	00000050
ISN 0007		INTEGER*2 IJPR,IG,JG	00000060
ISN 0008		INTEGER*2 II(40),KK(40),MM(40),NNP(50),MG(150),NG(150)	00000070
ISN 0009		DIMENSION VA(3),VADOT(3),PBAR(3),XLENGTH(3),IISPI(3),XXLBAR(3),	00000080
ISN 0010		1 FSP(3,3),XVOC(3,3),C4(3),C5(3),S(3),SDOT(3),PL(3,3)	00000090
ISN 0011		DIMENSION DPGRIIN(4),DXYZI(3),DXYZPRI(3),TERM(6)	00000100
ISN 0012		DIMENSION XVOCSL(3,3),DVC3(3)	00000110
ISN 0013		DIMENSION FSPB(3,3),FSPF(3,3),XVOCB(3,3),XVOCF(3,3),TERMF(6)	00000120
ISN 0014		DIMENSION DVC(3),DVC1(3),DVC2(3),DVC3(3),VCINT(3),	00000130
ISN 0015		1 VEEDT(3),VEEC3(3),VEEC33(3)	00000140
ISN 0016		DIMENSION TT(3),XXC(6),RTERH(6)	00000150
ISN 0017		DIMENSION RX(50),RY(50),RZ(50),XNPDP(50),YNPDP(50),ZNPDP(50)	00000160
ISN 0018		DIMENSION LSTEST(3)	00000170
ISN 0019		DIMENSION ETERM(3),ETB(3),ETF(3)	00000180
ISN 0020		COMMON/CFIC/ SINBET,COSBET,ABETA(9)	00000190
ISN 0021		COMMON/CFIR/ SIFL(40),SAFL(40),SBFL(40),SFFL(40),XKEFL(40)	00000200
ISN 0022		COMMON/CFPR/ FSPRG(40,8),DELGI(40)	00000210
ISN 0023		COMMON/INCF/ SA(40),SB(40),SF(40),SI(40),XMI(40),XKE(40),	00000220
ISN 0024		1 XMAX(40),FSPOF(40),FSPOI(40),GFLEX(40),CDAMP(40),PLOWT	00000230
ISN 0025		COMMON/INPR/ NDRI,NSP	00000240
ISN 0026		COMMON/INCFIC/ BETA	00000250
ISN 0027		COMMON/INIDCP/ YDP(80)	00000260
ISN 0028		COMMON/MACF/IBS(40),FSPOF(40),SCPI(40),JBS(40),	00000270
ISN 0029		1 KXSPI(5,200),EXSPI(5,200),TSP(200),STEMP1(40),STEMP2(40),	00000280
ISN 0030		2 STEMP3(40),STEMP4(40),STEMP5(40),KKONT	00000290
ISN 0031		COMMON/MACFIN/ THAX,IPRINT	00000300
ISN 0032		COMMON/MCFIIL/ SYHFLG	00000310
		COMMON/NP00I2/ MG,NG,INP,PNP	00000320
		COMMON/NP01I2/ II,KK,MM	00000330
		COMMON/NP00I4/ NNP	00000340
		COMMON/NP00R8/ RX,RY,RZ	00000350
			00000360
			00000370
			00000380
			00000390
			00000400


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C      NOM DO ALL CFORCE CALCULATIONS INSIDE AN M LOOP FROM 1
C      TO KOUNT.
C
C      DO 20 IN=1,KOUNT
C      M = MTEMP(IN)
C
C      DETERMINE WHICH K'S HAVE SPRINGS FOR CURRENT I AND M,
C      AND SET IISP(K).
C
C      DO 14 K=1,3
C      IISP(K) = 0
C      DO 16 IKH=1,NSP
C      IF(I.EQ.II(IKM).AND.M.EQ.MM(IKM).AND.K.EQ.KK(IKM)) IISP(K)=1
C      16 CONTINUE
C      14 CONTINUE
C
C      DETERMINE COMPONENTS OF RADIUS VECTOR FROM MASS POINT
C      TO NODE POINT.
C
C      IF(M.NE.0) GO TO 18
C      RRX = 0.
C      RRY = 0.
C      RRZ = 0.
C      GO TO 19
C      18 DO 17 JJ=1,NNP
C      IF(I.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 15
C      17 CONTINUE
C      PRINT 9,I,M
C      9 FORMAT('2. NO SUCH NODE POINT I,M',2I5)
C      STOP
C      15 RRX = RX(JJ)
C      RRY = RY(JJ)
C      RRZ = RZ(JJ)
C      19 CONTINUE
C      INITIALIZE SOME MORE
C      DO 910 K = 1,3
C      DO 22 IKH=1,NSP
C      IF(I.EQ.II(IKM).AND.K.EQ.KK(IKM).AND.M.EQ.MM(IKM)) GO TO 24
C      22 CONTINUE
C      24 XLNGTH(K) = XLBAR(IKM)
C      XXLBAR(K) = XLBAR(IKM)
C      VCINT(K) = 0.
C      SDOT(K) = 0.
C      DO 915 JJ = 1,3
C      FSP(JJ,K) = 0.0
C      FSPB(JJ,K) = 0.
C      FSPF(JJ,K) = 0.
C      XVCSL(JJ,K) = 0.
C      XVOCB(JJ,K) = 0.
C      XVOCF(JJ,K) = 0.
C      915 XVOC(JJ,K) = 0.0
C      DO 911 K2=1,7
C      FSPRG(IKM,K2) = 0.

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ISN 0114 911 CONTINUE
ISN 0115 910 CONTINUE
C LOOP 6
C CALCULATE VC3, C4, C5 IN GROUND AND SLOPE AXES
DVR1 = AI(1)*RRX+AI(4)*RRY+AI(7)*RRZ
DVR3 = AI(3)*RRX+AI(6)*RRY+AI(9)*RRZ
DVRD1 = AIDOT(1)*RRX+AIDOT(4)*RRY+AIDOT(7)*RRZ
DVRD3 = AIDOT(3)*RRX+AIDOT(6)*RRY+AIDOT(9)*RRZ
DO 920 K = 1,3
IF (IISP(K)) 925,920,925
925 ISUB1 = 3*K-2
DVC1(K) = AI(ISUB1) * XXLBAR(K)
ISUB3 = 3*K
DVC3(K) = AI(ISUB3) * XXLBAR(K)
DVC3L3 = SINBET * DVC1(K) + COSBET * DVC3(K)
VC1 = VA(1) + DVC1(K)*DVR1
VC3 = VA(3) + DVC3(K)*DVR3
VC3L3 = SINBET * VC1 + COSBET * VC3
DVC1D1 = AIDOT(ISUB1) * XXLBAR(K)
DVC3D3 = AIDOT(ISUB3) * XXLBAR(K)
DVCSD3 = SINBET * DVC1D1 + COSBET * DVC3D3
VCD1 = VADOT(1) + DVC1D1*DVRD1
VCD3 = VADOT(3) + DVC3D3*DVRD3
VCDSD3 = SINBET * VCD1 + COSBET * VCD3
VEEC3(K) = VC3
VEEC3L3(K) = VC3L3
IF (DVC3(K)) 927,926,927
926 C4(K) = 0.
C5(K) = 0.
GO TO 928
927 C4(K) = VC3/DVC3(K)
C5(K) = (DVC3(K) * VCD3 - VC3 * DVC3D3)/(DVC3(K) * DVC3L3)
928 IF (DVC3L3) 930,929,930
929 C4SL(K) = 0.
C5SL(K) = 0.
GO TO 920
930 C4SL(K) = VC3L3/DVC3L3
C5SL(K) = (DVC3L3 * VCDSD3 - VC3SD3 * DVC3D3)/(DVC3L3 * DVC3L3)
920 CONTINUE
C LOOP H
C CALCULATE X COORD OF SPRING INTERSECTION PT TO SEE IF LEVEL OR
C SLOPE IS USED.
DO 30 K = 1,3
IF (IISP(K)) 35,30,35
35 IF (VEEC3(K)) 36,36,40
36 IF (VEEC3L3(K)) 30,30,40
40 VCINT(K) = VA(1) + DVC1(K) * (1-C4(K))*DVR1
IF(DVC3(K).LE.0.) VCINT(K) = 1000.D0
THIS TAKES CARE OF HORIZONTAL AND UPWARD POINTING SPRINGS
ISUB = 3*(K-1)
BARL = XXLBAR(K)
SUM = 0.0
SUMD = 0.0

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ISN 0116
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ISN 0162      C LOOP J1  CALCULATE ALL DVC & DVCDOOT IN GROUND SYSTEM
ISN 0163      DO 50 J=1,3
ISN 0164      JSUB = JSUB + 1
ISN 0165      DVC(J) = AI(JSUB) * BAPL
ISN 0166      DVCDOOT(J) = AIDOT(JSUB) * BAPL
ISN 0167      50 CONTINUE
ISN 0168      C LOOP J2  CALCULATE DVC & DVCDOOT IN SLOPE AXES IF APPROPRIATE. FORM
ISN 0169      C
ISN 0170      SUM & SUMD FOR SK & SKDOOT.
ISN 0171      DO 52 J=1,3
ISN 0172      IF (BETA) 54,56,54
ISN 0173      54 IF (VCINT(K)) 56,56,58
ISN 0174      56 SUM1 = 0.
ISN 0175      SUM2 = 0.
ISN 0176      JSUB = 3*(J-1)
ISN 0177      DO 53 L=1,3
ISN 0178      JSUB = JSUB + 1
ISN 0179      SUM1 = SUM1 + ABETA(JSUB) * DVC(L)
ISN 0180      SUM2 = SUM2 + ABETA(JSUB) * DVCDOOT(L)
ISN 0181      53 CONTINUE
ISN 0182      DVEEC = SUM1
ISN 0183      DVEECDOOT = SUM2
ISN 0184      C4BAR = C4SL(K)
ISN 0185      C5BAR = C5SL(K)
ISN 0186      LSTEST(K) = 1.
ISN 0187      60 TO 59
ISN 0188      56 DVEEC = DVC(J)
ISN 0189      DVEECDOOT = DVCDOOT(J)
ISN 0190      C4BAR = C4(K)
ISN 0191      C5BAR = C5(K)
ISN 0192      LSTEST(K) = 0
ISN 0193      DVP = C4BAR * DVEEC
ISN 0194      DOP = C4BAR * DVEECDOOT + C5BAR * DVEEC
ISN 0195      SUM = SUM + DVP * DVP
ISN 0196      SUMD = SUMD + DVP * DOP
ISN 0197      SK = SORT(SUM)
ISN 0198      S(K) = SK
ISN 0199      SKOOT(K) = SUMD/SK
ISN 0200      C GET LENGTH
ISN 0201      DO 822 IKH=1,NSP
ISN 0202      IF(I.EQ.II(IKH),AND,K.EQ.KK(IKH),AND,M.EQ.MM(IKH)) 60 TO 824
ISN 0203      822 CONTINUE
ISN 0204      824 SC(IKH) = SK
ISN 0205      IF(BAPL) 55,60,60
ISN 0206      55 T = -BAPL-SK*DELG(IKH)
ISN 0207      T = -T
ISN 0208      60 TO 65
ISN 0209      60 T = BAPL-SK*DELG(IKH)
ISN 0210      65 XLNGTH(K) = T
ISN 0211      30 CONTINUE
ISN 0212      PL(1,1) = -SKOOT(1)*SIGN(ONE,XXLBAP(1))
ISN 0213      PL(2,2) = -SKOOT(2)*SIGN(ONE,XXLBAP(2))
ISN 0214      PL(3,3) = -SKOOT(3)*SIGN(ONE,XXLBAP(3))

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ISM 0212      PL(1,1) = 0.
ISM 0213      PL(2,2) = 0.
ISM 0214      PL(3,3) = 0.
ISM 0215      PL(2,1) = PPAR(3)*XLNGTH(1)
ISM 0216      PL(3,1) = -PPAR(2)*XLNGTH(1)
ISM 0217      PL(1,2) = -PPAR(3)*XLNGTH(2)
ISM 0218      PL(3,2) = PPAR(1)*XLNGTH(2)
ISM 0219      PL(1,3) = PPAR(2)*XLNGTH(3)
ISM 0220      PL(2,3) = -PPAR(1)*XLNGTH(3)
ISM 0221      IF(M.EQ.0) GO TO 76
ISM 0222      TT(1) = -PPAR(3)*PPR+PPAR(2)*RRZ
ISM 0223      TT(2) = PPAR(3)*PRX-PPAR(1)*RRZ
ISM 0224      TT(3) = -PPAR(2)*RRX+PPAR(1)*RRY
ISM 0225      DO 77 K=1,3
ISM 0226      DO 77 K=1,3
ISM 0227      DO 78 JJ=1,3
ISM 0228      PL(JJ,K) = PL(JJ,K)+TT(JJ)
ISM 0229      77 CONTINUE
ISM 0230      78 CONTINUE
C LOOP K
76 DO 75 JJ = 1,3
  ISUB = JJ-3
  VAD = VADOT(JJ)
C LOOP L
DO 80 K = 1,3
  IF(IISP(K)) 85,80,85
  85 IF(VEEC3(K)) 81,81,90
  81 IF(VEEC3(K)) 80,80,90
  90 SUM = 0.0
C LOOP N
DO 95 L = 1,3
  ISUB = ISUB+3
  95 SUM = SUM+AI(ISUB)*PL(L,K)
  VEEDOT(JJ,K) = VAD+SUM
  80 CONTINUE
  75 CONTINUE
C CALCULATE CONTACT POINT VELOCITIES ON SLOPE.
98 DO 101 K=1,3
  IF (VCINT(K)) 101,101,94
  94 DO 97 J=1,3
    SUM = 0.
    JSUB = 3*(J-1)
    DO 99 L=1,3
      JSUB = JSUB + 1
    SUM = SUM + ABETA(JSUB) * VEEDOT(L,K)
  99 CONTINUE
  VEEDT(J) = SUM
  97 CONTINUE
  DO 102 JJ=1,3
    VEEDOT(JJ,K) = VEEDT(JJ)
  102 CONTINUE
  101 CONTINUE
C LOOP N

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ISN 0261      % 00 105 K = 1.3
ISN 0262      IF(IISPI(K)) 110,105,110
ISN 0263      110 IF(VEEC3(K)) 111,111,115
ISN 0264      111 IF(VEEC3(K)) 105,105,115
ISN 0265      115 SK = SIK)
C
C      GET SPRING NUMBER TO USE INPUT DATA SUBSCRIPTED BY IKM.
C
ISN 0266      DO 1002 IKH=1,NSP
ISN 0267      IF(I.EQ.II(IKM).AND.K.EQ.KK(IKM).AND.M.EQ.MM(IKM)) GO TO 1003
ISN 0269      1002 CONTINUE
ISN 0270      1003 SC(IKM) = SK
C
C      CALCULATION OF FSPO.
C
ISN 0271      IF(SDOT(K).LT.0.) GO TO 140
ISN 0273      IF(SK.LT.SBAR(IKM)) GO TO 140
C
C      LOADING PATH.
C
ISN 0275      IF(IBS(IKM).NE.0) GO TO 125
ISN 0277      IF(SK.GT.SFFL(IKM)) GO TO 130
C
C      NORMAL FSPO CALCULATIONS FOR LOADING CASE.
C
ISN 0279      FSPO = FSPOF(IKM)
ISN 0280      IF(SK.GE.SBFL(IKM)) GO TO 150
ISN 0282      IF(SK.GE.SAFL(IKM)) GO TO 148
ISN 0284      FSPO = FSPOI(IKM)
ISN 0285      IF(SK.GE.SIFL(IKM)) GO TO 150
ISN 0287      FSPO = FSPO*SK/SIFL(IKM)
ISN 0288      GO TO 150
ISN 0289      148 FSPO = FSPOI(IKM)*(SK-SAFL(IKM))*(FSPO-FSPOI(IKM))/
          1 (SBFL(IKM)-SAFL(IKM))
          GO TO 150
ISN 0290      C
C
C      FSPO CALCULATIONS ON BOTTOMING SPRING.
C
ISN 0291      130 IBS(IKM) = 1
ISN 0292      125 FSPO = FSPOF(IKM)+XKEFL(IKM)*(SK-SFFL(IKM))
ISN 0293      150 FSPBAR(IKM) = FSPO
ISN 0294      SBAR(IKM) = SK
ISN 0295      NH(IKM) = 0
ISN 0296      GO TO 155
C
C      UNLOADING AND RELOADING PATHS.
C
ISN 0297      140 IF(NH(IKM).NE.0) GO TO 135
ISN 0299      IF(IBS(IKM).EQ.0) GO TO 145
C
C      UNLOADING AND RELOADING ON BOTTOMING SPRING.
C
ISN 0301      KUN(IKM) = XKE(IKM)

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ISN 0302      GO TO 146
C
C  NORMAL UNLOADING AND RELOADING.
C
145 IF(SK.LE.SAFL(IKM)) GO TO 147
KUN(IKM) = (FSPOF(IKM)-FSPOI(IKM))/(SB(IKM)-SA(IKM))
IF(KUN(IKM).LT.(FSPBAR(IKM)/SBAR(IKM))) GO TO 147
GO TO 146
147 KUN(IKM) = FSPOI(IKM)/SI(IKM)
146 NK(IKM) = 1
135 FSPO = FSPBAR(IKM)-(SBAR(IKM)-SK)*KUN(IKM)
155 FSPO=CDAMP(IKM)*SDOT(K)
IF(SDOT(K).LT. 0) FSPO=0.
FSPO=FSPO+FSPO
C
C  NOW IF FSPO IS NEGATIVE, SET IT EQUAL TO ZERO
IF(FSPO.LT.0.) FSPO=0.
FSPOF5=10.*ANAXI(FSPOF(IKM),FSPOI(IKM))
CUTOFF FORCE=10*MAX OF FSPOF,FSPOI
IF(FSPO.GT.FSPOF5) FSPO=FSPOF5
IF(SDOT(K).LT.0.) GO TO 1020
JBS=1 INITIAL LOADING OCCURS
JBS=2 MAX. LOAD AND/OR DEFLECTION OCCUR
JBS=3 UNLOAD TO ZERO FORCE
JBS=4 RELOAD OCCURS
JBS=5 MAX. LOAD DUE TO DAMPING OCCURS
IF(JBS(IKM).EQ.5) GO TO 1040
INITIAL LOADING SUMMARY
IF(JBS(IKM).EQ.2) GO TO 1030
IF(SCP(IKM).GT.0.0 .AND.FSPD.NE.0.) GO TO 1012
IF(SCP(IKM).GT.0.) GO TO 1030
IF(SC(IKM).LE.0.) GO TO 1030
IF(JBS(IKM).GT.0) GO TO 1009
KKONT=KKONT+1
TSPI(KKONT)=TIME
EXSPI1, KKONT)=SK
STEP1(IKM)=SK
KKSP1(1, KKONT)=II(IKM)
KKSP2(2, KKONT)=III(IKM)
KKSP3(3, KKONT)=KK(IKM)
KKSP4(4, KKONT)=1
1009 IF(JBS(IKM).GT.3) GO TO 1008
JBS(IKM)=1
GO TO 1040
1008 IF(FSPO.GT.0.0 .AND.SK.GT.SCP(IKM)) GO TO 1031
GO TO 1040
C  MAXIMUM LOADING SUMMARY
1012 IF(JBS(IKM).EQ.3) GO TO 1030
IF(FSPOP(IKM).LT.FSPO) GO TO 1040
IF(JBS(IKM).EQ.4) JBS(IKM)=5
IF(JBS(IKM).EQ.1) JBS(IKM)=5
1010 IF(JBS(IKM).EQ.2) GO TO 1040
KKONT=KKONT+1
TSPI(KKONT)=TIME

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ISN 0303
ISN 0305
ISN 0306
ISN 0308
ISN 0309
ISN 0310
ISN 0311
ISN 0312
ISN 0313
ISN 0315
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ISN 0318
ISN 0319
ISN 0321
ISN 0323
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ISN 0331
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ISN 0338
ISN 0339
ISN 0340
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ISN 0360
ISN 0361

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ISN 0362      EXSP(1,KKONT)=STEMP1(IKM)
ISN 0363      EXSP(2,KKONT)=FSPOP(IKM)
ISN 0364      EXSP(3,KKONT)=SCP(IKM)
ISN 0365      EXSP(4,KKONT)=STEMP3(IKM)
ISN 0366      EXSP(5,KKONT)=STEMP2(IKM)
ISN 0367      STEMP4(IKM)=FSPOP(IKM)
ISN 0368      STEMP5(IKM)=SCP(IKM)
ISN 0369      KKSP(1,KKONT)=II(IKM)
ISN 0370      KKSP(2,KKONT)=MM(IKM)
ISN 0371      KKSP(3,KKONT)=KK(IKM)
ISN 0372      KKSP(4,KKONT)=2
ISN 0373      IF(FSPO.EQ.0.) GO TO 1013
ISN 0375      IF(JBS(IKM).NE.5) GO TO 1013
ISN 0376      GO TO 1040
ISN 0377      1013 JBS(IKM)=2
ISN 0378      GO TO 1040
ISN 0379      GO TO 1040

C      UNLOADING SUMMARY
1020 IF(FSPOP(IKM).GT.FSPO .AND.FSPO.NE.0.0 .AND.SK.LT.SCP(IKM))
      1 GO TO 1010
ISN 0380      IF(FSPO.NE.0.) GO TO 1040
ISN 0382      IF(FSPOP(IKM).LT.FSPO) GO TO 1040
ISN 0384      IF(JBS(IKM).EQ.3) GO TO 1040
ISN 0386      KKONT=KKONT+1
ISN 0388      TSPI(KKONT)=TIME
ISN 0389      EXSP(1,KKONT)=STEMP1(IKM)
ISN 0390      EXSP(2,KKONT)=STEMP4(IKM)
ISN 0391      EXSP(3,KKONT)=STEMP5(IKM)
ISN 0392      EXSP(4,KKONT)=SK
ISN 0393      EXSP(5,KKONT)=FSPO
ISN 0394      STEMP2(IKM)=FSPO
ISN 0395      STEMP3(IKM)=SK
ISN 0396      KKSP(1,KKONT)=II(IKM)
ISN 0397      KKSP(2,KKONT)=MM(IKM)
ISN 0398      KKSP(3,KKONT)=KK(IKM)
ISN 0399      KKSP(4,KKONT)=3
ISN 0400      JBS(IKM)=3
ISN 0401      GO TO 1040
ISN 0402      GO TO 1040

C      RELOADING SUMMARY
1030 IF(JBS(IKM).EQ.2 .AND.FSPOP(IKM).NE.0.0 .AND.FSPO.GT.FSPOP(IKM))
      1 GO TO 1031
ISN 0403      IF(JBS(IKM).EQ.1) GO TO 1040
ISN 0405      IF(JBS(IKM).EQ.4) GO TO 1040
ISN 0407      IF(SK.LT.STEMP3(IKM)) GO TO 1040
ISN 0409      IF(FSPOP(IKM).NE.0.0 .AND.FSPO.LE.FSPOP(IKM)) GO TO 1040
ISN 0411      KKONT=KKONT+1
ISN 0413      TSPI(KKONT)=TIME
ISN 0414      EXSP(1,KKONT)=SK
ISN 0415      EXSP(2,KKONT)=STEMP4(IKM)
ISN 0416      EXSP(3,KKONT)=STEMP5(IKM)
ISN 0417      IF(JBS(IKM).EQ.2) GO TO 1032
ISN 0418      EXSP(4,KKONT)=STEMP3(IKM)
ISN 0420      EXSP(5,KKONT)=STEMP2(IKM)
ISN 0421      GO TO 1033
ISN 0422      GO TO 1033

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1032 EXSPI(4,KKONT)=SK
    EXSPI(5,KKONT)=FSPO
    STEMP2(IKH)=FSPO
    STEMP3(IKH)=SK
1033 STEMP1(IKH)=SK
    KKSP1(1,KKONT)=II(IKH)
    KKSP2(2,KKONT)=MM(IKH)
    KKSP3(3,KKONT)=KK(IKH)
    KKSP4(4,KKONT)=4
    JBS(IKH)=4
1040 SCP(IKH)=SK
    FSOPI(IKH)=FSPO
    OLDELG = DELG(IKH)
    DELG(IKH) = FSPO*GFLEX(IKH)
    DELG(IKH) = AMAX1(OLDELG,DELG(IKH))
    FSPRING(IKH,1) = FSPO
    FSPRING(IKH,8)=FSPO
    CALCULATE FPLON(TIME)
    FPLON = XMAX(IKH)
    IF(TIME.GE.PLOMT) FPLON=0.
    CHECK TO SEE IF SPRING IS ON SLOPE OR BETA = 0.
    IF(VICNT(I)) 191,191,180
180 IF(BETA.EQ.0.) GO TO 191
    GET 3 COMPONENTS OF FSPO IN GROUND AXES
    XVOC(1,K) = AI(3*K-2)*FSPO
    XVOC(2,K) = AI(3*K-1)*FSPO
    XVOC(3,K) = AI(3*K)*FSPO
    XVOC(1,K) = XVOC(1,K)*SIGNONE,XXLBAR(K))
    XVOC(2,K) = XVOC(2,K)*SIGNONE,XXLBAR(K))
    XVOC(3,K) = XVOC(3,K)*SIGNONE,XXLBAR(K))
    CONVERT TO SLOPE AXES,GETTING Z COMPONENT ONLY
    XVOCSL(3,K) = SINBET*XVOC(1,K)+COSBET*XVOC(3,K)
    CALCULATE X AND Y COMPONENTS IN SLOPE AXES FROM GROUND FRICTION
    AND VELOCITY DIRECTION
    V1 = VEEDOT(1,K)
    V2 = VEEDOT(2,K)
    VBB = SQRT(V1*V1+V2*V2)
    IF(VBB) 183,183,182
183 VX=0.
    GO TO 184
182 VX = X*V1(IKH)*XVOCSL(3,K)/VBB+FPLON/VBB
184 XVOCSL(1,K) = VX*VEEDOT(1,K)
    XVOCSL(2,K) = VX*VEEDOT(2,K)
    IF(STHFLG.NE.0.AND.YDPI(I).EQ.0.) XVOCSL(2,K) = 0.
    FSPRING(IKH,2) = XVOCSL(1,K)
    FSPRING(IKH,3) = XVOCSL(2,K)
    FSPRING(IKH,4) = XVOCSL(3,K)
    NOM TRANSFORM BACK TO GROUND AXES TO REJOIN BASIC CODING
    FROM HERE ON SEPARATE LOADS NORMAL TO SURFACE AND FRICTION LOADS
    TO CALCULATE CRUSHING ENERGY AND FRICTION ENERGY
181 XVOCB(1,K) = SINBET*XVOCSL(3,K)
    XVOCB(2,K) = 0.
    XVOCB(3,K) = COSBET*XVOCSL(3,K)

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10004660
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10004690
10004700
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10005100
10005110
10005120
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10005140
10005150
10005160
10005170

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ISN 0470      XVOCF(1,K) = COSBET*XVOCSL(1,K)
ISN 0471      XVOCF(2,K) = XVOCSL(2,K)
ISN 0472      XVOCF(3,K) = -SINBET*XVOCSL(1,K)
ISN 0473      GO TO 210

C (15A)
ISN 0474      191 VX = AI(3,K)*FSP0
ISN 0475      VX = VX*SIGNONE,XXLBAR(K)
ISN 0476      XVOC(3,K) = VX
ISN 0477      V1 = VEEDOT(1,K)
ISN 0478      V2 = VEEDOT(2,K)
ISN 0479      VBB = SQRT(V1*V1+V2*V2)
ISN 0480      IF(VBB) 201,201,200
ISN 0481      201 VX=0.
ISN 0482      GO TO 202
ISN 0483      200 VX = XMU(IKM)*VX/VBB+FLOW/VBB
ISN 0484      202 XVOCB(1,K) = 0.
ISN 0485      XVOCB(2,K) = 0.
ISN 0486      XVOCB(3,K) = XVOC(3,K)
ISN 0487      XVOCF(3,K) = 0.
ISN 0488      XVOCF(1,K) = VX*VEEDOT(1,K)
ISN 0489      XVOCF(2,K) = VX*VEEDOT(2,K)
ISN 0490      IF(SYMF LG.NE.0.AND.YDPI(1).EQ.0.) XVOCF(2,K) = 0.
ISN 0491      FSPRNG(IKM,2) = XVOCF(1,K)
ISN 0492      FSPRNG(IKM,3) = XVOCF(2,K)
ISN 0493      FSPRNG(IKM,4) = XVOCB(3,K)
ISN 0494      210 IF(BARL) 355,360,360
ISN 0495      355 T = -BARL-SK*DELG(IKM)
ISN 0496      T = -T
ISN 0497      GO TO 365
ISN 0498      360 T = BARL-SK*DELG(IKM)
ISN 0499      365 XLNGTH(K) = T
ISN 0500      IS = 0
ISN 0501      C LOOP Q

ISN 0502      DO 220 J = 1,3
ISN 0503      SUMB = 0.
ISN 0504      SUMF = 0.

C LOOP R
ISN 0505      DO 230 L = 1,3
ISN 0506      IS = IS+1
ISN 0507      SUMB = SUMB-AI(IS)*XVOCB(L,K)
ISN 0508      230 SUMF = SUMF-AI(IS)*XVOCF(L,K)
ISN 0509      FSPB(J,K) = SUMB
ISN 0510      FSPF(J,K) = SUMF
ISN 0511      FSP(J,K) = SUMB+SUMF
ISN 0512      FSPRNG(IKM,(J+4)) = FSP(J,K)
ISN 0513      220 CONTINUE

C END OF LOOP N
ISN 0514      105 CONTINUE

C CRASH FORCES
ISN 0515      DO 240 J = 1,3
ISN 0516      SUM = 0.0
ISN 0517      DO 250 K = 1,3
ISN 0518      250 SUM = SUM+FSP(J,K)

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00005180
00005190
00005200
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00005230
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00005640
00005650
00005660
00005670
00005680
00005690
00005700

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ISN 0519      XXC(J) = SUM
ISN 0520      240 CONTINUE
C             DXZ(1) = DX(I)
C             DXZ(2) = DY(I)
C             DXZ(3) = DZ(I)
ISN 0521      DXZ(1) = VADOT(1)*DELTA
ISN 0522      DXZ(2) = VADOT(2)*DELTA
ISN 0523      DXZ(3) = VADOT(3)*DELTA
C             DPQRIN(1) = DQIN(I)
C             DPQRIN(2) = DRIN(I)
C             DPQRIN(3) = DPIN(I)
C             DPQRIN(4) = DQIN(I)
C             DPQRIN(1) = PSAR(2)*DELTA
ISN 0524      DPQRIN(2) = PSAR(3)*DELTA
ISN 0525      DPQRIN(3) = PSAR(1)*DELTA
ISN 0526      DPQRIN(4) = PSAR(2)*DELTA
ISN 0527      TERM(1) = FSPB(3,1)*(XLNGTH(1)+RRX)
ISN 0528      TERM(2) = FSPB(1,2)*(XLNGTH(2)+RRY)
ISN 0529      TERM(3) = FSPB(2,3)*(XLNGTH(3)+RRZ)
ISN 0530      TERM(4) = FSPB(2,1)*(XLNGTH(1)+RRX)
ISN 0531      TERM(5) = FSPB(3,2)*(XLNGTH(2)+RRY)
ISN 0532      TERM(6) = FSPB(1,3)*(XLNGTH(3)+RRZ)
ISN 0533      TERM(1) = FSPF(3,1)*(XLNGTH(1)+RRX)
ISN 0534      TERM(2) = FSPF(1,2)*(XLNGTH(2)+RRY)
ISN 0535      TERM(3) = FSPF(2,3)*(XLNGTH(3)+RRZ)
ISN 0536      TERM(4) = FSPF(2,1)*(XLNGTH(1)+RRX)
ISN 0537      TERM(5) = FSPF(3,2)*(XLNGTH(2)+RRY)
ISN 0538      TERM(6) = FSPF(1,3)*(XLNGTH(3)+RRZ)
ISN 0539      C CRASH MOMENTS
ISN 0540      XXC(4) = TERM(5)+TERM(6)-TERM(3)-TERM(1)
ISN 0541      XXC(5) = TERM(6)+TERM(4)-TERM(1)-TERM(2)
ISN 0542      XXC(6) = TERM(4)+TERM(5)-TERM(2)-TERM(3)
ISN 0543      IF(N.EQ.0) GO TO 2001
C             IF WE ARE AT A NODE POINT, WE MUST CALCULATE ADDITIONAL
C             MOMENT CONTRIBUTIONS TO XXC(4-6).
C             RTERM(1) = RRX*(FSPB(3,2)+FSPB(3,3))
C             RTERM(2) = RRY*(FSPB(1,1)+FSPB(1,3))
C             RTERM(3) = RRZ*(FSPB(2,1)+FSPB(2,2))
C             RTERM(4) = RRX*(FSPB(2,2)+FSPB(2,3))
C             RTERM(5) = RRY*(FSPB(3,1)+FSPB(3,3))
C             RTERM(6) = RRZ*(FSPB(1,1)+FSPB(1,2))
C             RTERM(1) = RRX*(FSPF(3,2)+FSPF(3,3))
C             RTERM(2) = RRY*(FSPF(1,1)+FSPF(1,3))
C             RTERM(3) = RRZ*(FSPF(2,1)+FSPF(2,2))
C             RTERM(4) = RRX*(FSPF(2,2)+FSPF(2,3))
C             RTERM(5) = RRY*(FSPF(3,1)+FSPF(3,3))
C             RTERM(6) = RRZ*(FSPF(1,1)+FSPF(1,2))
C             XXC(4) = XXC(4)+RTERM(5)+RTERM(6)-RTERM(1)-RTERM(3)
C             XXC(5) = XXC(5)+RTERM(4)+RTERM(6)-RTERM(1)-RTERM(2)
C             XXC(6) = XXC(6)+RTERM(4)+RTERM(5)-RTERM(2)-RTERM(3)
C             ETERM(1) = RRY*DPQRIN(2)-RRZ*DPQRIN(1)
ISN 0545      00005710
ISN 0546      00005720
ISN 0547      00005730
ISN 0548      00005740
ISN 0549      00005750
ISN 0550      00005760
ISN 0551      00005770
ISN 0552      00005780
ISN 0553      00005790
ISN 0554      00005800
ISN 0555      00005810
ISN 0556      00005820
ISN 0557      00005830
ISN 0558      00005840
ISN 0559      00005850
ISN 0560      00005860
ISN 0561      00005870
ISN 0562      00005880
ISN 0563      00005890
ISN 0564      00005900
ISN 0565      00005910
ISN 0566      00005920
ISN 0567      00005930
ISN 0568      00005940
ISN 0569      00005950
ISN 0570      00005960
ISN 0571      00005970
ISN 0572      00005980
ISN 0573      00005990
ISN 0574      00006000
ISN 0575      00006010
ISN 0576      00006020
ISN 0577      00006030
ISN 0578      00006040
ISN 0579      00006050
ISN 0580      00006060
ISN 0581      00006070
ISN 0582      00006080
ISN 0583      00006090
ISN 0584      00006100
ISN 0585      00006110
ISN 0586      00006120
ISN 0587      00006130
ISN 0588      00006140
ISN 0589      00006150
ISN 0590      00006160
ISN 0591      00006170
ISN 0592      00006180
ISN 0593      00006190
ISN 0594      00006200
ISN 0595      00006210
ISN 0596      00006220
ISN 0597      00006230

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ISN 0561      ETERM(2) = RRZ*DPQRIN(3)-RRX*DPQRIN(2)
ISN 0562      ETERM(3) = RRX*DPQRIN(1)-RRY*DPQRIN(3)
ISN 0563      ETB(1) = DPQRIN(3)*(RRY*FSPB(3,1)-RRZ*FSPB(2,1))
ISN 0564      ETB(2) = DPQRIN(1)*(RRZ*FSPB(1,2)-RRX*FSPB(3,2))
ISN 0565      ETB(3) = DPQRIN(2)*(RRX*FSPB(2,3)-RRY*FSPB(1,3))
ISN 0566      ETF(1) = DPQRIN(3)*(RRY*FSPF(3,1)-RRZ*FSPF(2,1))
ISN 0567      ETF(2) = DPQRIN(1)*(RRZ*FSPF(1,2)-RRX*FSPF(3,2))
ISN 0568      ETF(3) = DPQRIN(2)*(RRX*FSPF(2,3)-RRY*FSPF(1,3))

C
C   FOR SYMMETRICAL CASE,CENTERLINE MASSES,FORCE Y,L,N LOADS TO ZERO
C
C
C   2001 IF(SYMFLEQ.EQ.0.OR.YDP(I).NE.0.) GO TO 2010
C       XXC(2) = 0.
C       XXC(4) = 0.
C       XXC(6) = 0.
C       IF(M.EQ.0.OR.SYMFLEQ.EQ.2.) GO TO 2010
C       DO 2002 JJ=1,NP
C         IF(I.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 2004
C       2002 CONTINUE
C       2004 IF(INP(JJ).EQ.0.) GO TO 2010
C
C   C   IF WE HAVE A SYMMETRIC CASE,CL MASS,AND NON-CL NODE POINT,
C       C   WE MUST DOUBLE X,Z AND M LOADS ON MASS I DUE TO THE EXTERNAL
C       C   SPRING ON THE OPPOSITE SIDE NODE POINT.
C
C       XXC(1) = 2.*XXC(1)
C       XXC(3) = 2.*XXC(3)
C       XXC(5) = 2.*XXC(5)
C
C   C   WE ARE STILL IN AN M (NODE POINT) LOOP. NOW SUM UP ALL THE
C       C   EXTERNAL SPRING FORCES AND MOMENTS ACTING AT MASS I DUE TO
C       C   EACH OF THE KOUNT NODE POINTS M.
C
C   2010 DO 2020 J=1,6
C       XC(J) = XC(J)+XXC(J)
C   2020 CONTINUE
C       CALL MATVEC(AI,XYZ,DXYZPR,1)
C       DO 260 K = 1,3
C         IF(IISP(K).EQ.0) GO TO 260
C         SUM = 0.
C         SUMF = 0.
C         DO 270 J = 1,3
C           SUM = SUM+FSPB(J,K)*DXYZPR(J)
C           SUMF = SUMF-FSPF(J,K)*DXYZPR(J)
C       270 CONTINUE
C       SUM1 = TERM(K)*DPQRIN(K)-TERM(K+3)*DPQRIN(K+1)
C       SUMF1 = TERM(K)*DPQRIN(K)-TERM(K+3)*DPQRIN(K+1)
C       DO 2050 IKH=1,NSP
C         IF(I.EQ.II(IKH).AND.K.EQ.KK(IKH).AND.M.EQ.MM(IKH)) GO TO 2060
C       2050 CONTINUE
C       2060 IF(M.EQ.0) GO TO 2030
C       SUM1 = SUM1+FSPB(K,K)*ETERM(K)-ETB(K)
C       SUMF1 = SUMF1+FSPF(K,K)*ETERM(K)-ETF(K)

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ISN 0561
ISN 0562
ISN 0563
ISN 0564
ISN 0565
ISN 0566
ISN 0567
ISN 0568

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ISN 0582
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2030 CEIK(IKM) = CEIK(IKM)+SUM+SUM1
      CEIKF(IKM) = CEIKF(IKM)+SUMF+SUMF1
C
C   FOR A SYMMETRICAL MODEL WE MUST ADD CE AND FE CONTRIBUTIONS
C   FROM THE OPPOSITE SPRINGS THAT ARE NOT INPUT EXPLICITLY.
C
      IF(SYMF1G.NE.1.) GO TO 260
      IF(M.EQ.0.AND.YOP(I).EQ.0.) GO TO 260
      IF(M.EQ.0) GO TO 3000
      IF(YOP(I).EQ.0.AND.YNPDPL(JJ).EQ.0.) GO TO 260
3000 CEIK(IKM) = CEIK(IKM)+SUM+SUM1
      CEIKF(IKM) = CEIKF(IKM)+SUMF+SUMF1
260 CONTINUE
20 RETURN
END

```

ISN 0608
ISN 0609

ISN 0610
ISN 0612
ISN 0614
ISN 0616
ISN 0618
ISN 0619
ISN 0620
ISN 0621
ISN 0622
ISN 0623


```
IF (DUMMY .NE. END) GO TO 30
PRINT 1000,NAME
JWDS = JWDS - 3
ERROR = 25
RETURN
```

```
C 30 IF (NAME.EQ. BLANK) NAME = DUMMY
C
C ...GET VALUES...
```

```

40 NREC = TEMP(3)
   NSTORE = NREC
   IF (NREC .GT. NMDS) NSTORE = NMDS
   IF (NAME .NE. DUMMY) NSTORE = 0
   IF (NREC .LE. 0) GO TO 70
   DO 60 I=1,NREC
     IF (JMDS .LT. LRECL) GO TO 50
     READ (UNIT,END=99) RECORD

```

```

50      JNDS = JNDS + 1
      IF ( I .LE. NSTORE ) X(I) = RECORD(JNDS)
60      CONTINUE
70      ERROR = -NSTORE
      RETURN
99      ERROR = 20
      PRINT 3000, NAME
      RETURN

```

...READ HEADER...

```
ENTRY OPIN(HEADER,NMDS,UNIT,ERROR)
INTEGER HEADER(1)
ERROR = 0
```

```

JND5 = 3
100 READ (UNIT,END=199) RECORD
    TEMP(1) = RECORD(1)
    TEMP(2) = RECORD(2)
    IF (DUMMY.NE. START) GO TO 100
    NREC = RECORD(3)
    IF (NREC.LT. 1) RETURN
    DO 120 I = 1, NREC

```

C

ISN 0050
ISN 0051
ISN 0052
ISN 0053
ISN 0054
ISN 0055
ISN 0056
ISN 0057
ISN 0059
ISN 0060
ISN 0062
ISN 0063
ISN 0064
ISN 0066
ISN 0067
ISN 0068
ISN 0069
ISN 0070
ISN 0071

0000000410
0000000420
0000000430
0000000440
0000000450
0000000460
0000000470
0000000480
0000000490
0000000500
0000000510
0000000520
0000000530
0000000540
0000000550
0000000560
0000000570
0000000580
0000000590
0000000600
0000000610
0000000620
0000000630
0000000640
0000000650
0000000660
0000000670
0000000680
0000000690
0000000700
0000000710
0000000720
0000000730
0000000740
0000000750
0000000760
0000000770
0000000780
0000000790
0000000800
0000000810
0000000820
0000000830
0000000840
0000000850
0000000860
0000000870
0000000880
0000000890
0000000900
0000000910
0000000920
0000000930

```

ISN 0072 C      ...POSITION TO END OF DATA SET...
ISN 0073 C
ISN 0074 C
ISN 0075 C      ENTRY CLSIN(UNIT,ERROR)
ISN 0076 C      JADS = -1
ISN 0077 C      ERROR = 0
ISN 0078 C      200 IF (RECORD(LRECL) .EQ. ENDI) RETURN
ISN 0079 C      READ (UNIT,END=299) RECORD
ISN 0080 C      GO TO 200
ISN 0081 C      299 CONTINUE
ISN 0082 C      ERROR = 30
C      PRINT 5000
C      RETURN
C      ...FORMATS...
C      1000 FORMAT(1H0,10X,'11. ****ERROR - END OF DATA REACHED AT',
C          1 VARIABLE 'A8,****')
C      3000 FORMAT(1H0,10X,'12. ****ERROR - END OF FILE REACHED AT',
C          1 VARIABLE 'A8,****')
C      4000 FORMAT(1H0,10X,'13. ****ERROR - END OF FILE REACHED TRYING TO',
C          1 OPEN DATA SET FOR READING****')
C      5000 FORMAT(1H0,10X,'14. ****ERROR - EOF TRYING TO CLOSE DATA SET',
C          1 AFTER READING****')
C      6000 FORMAT(1H0,10X,'15. ****ERROR - CANNOT READ DATA WITHOUT',
C          1 FIRST OPENING DESIRED DATA SET****')
C      END
ISN 0083
ISN 0084
ISN 0085
ISN 0086
ISN 0087
ISN 0088

```

```

00000940
00000950
00000960
00000970
00000980
00000990
00001000
00001010
00001020
00001030
00001040
00001050
00001060
00001070
00001080
00001090
00001100
00001110
00001120
00001130
00001140
00001150
00001160
00001170
00001180
00001190
00001200
00001210

```



```

ISN 0069      210  RECORD(I) = HEAD(3)
ISN 0070      WRITE (UNIT) RECORD
C
C      TAPE FILE IS ENDED, THEN BACKSPACED TWICE TO POSITION
C      TAPE HEAD TO BEGINNING OF LAST RECORD. THAT RECORD IS
C      THEN READ, AND NEXT READ WILL ENCOUNTER EOF.
C
      END FILE UNIT
      DO 215 J=1,2
      BACKSPACE UNIT
215 CONTINUE
      READ(21) RECORD
      JNDS = -1
      RETURN
ISN 0071      1000 FORMAT(IH0,10X,'16. ****ERROR - MUST OPEN DATA SET BEFORE',
ISN 0072      'WRITING DATA OUT****')
ISN 0073      2000 FORMAT(IH0,10X,'17. **WARNING - REQUESTED STORING ',I9,
ISN 0074      ' VALUES. STORE FAILED**')
ISN 0075      1
ISN 0076      1
ISN 0077      1
ISN 0078      END
ISN 0079
ISN 0080

```

```

00094
00095
00096
00097
00098
00099
00100
00101
00102
00103
00104
00105
00106
00107
00108
00109
00110
00111
00112

```


1 XLB(150),ZL(150),Z2(150),MC(150),XJ(150),SF26(150),SF35(150),
 2 SF26J(150),SF35J(150),PY,PZ,PTJ,PZJ,NSC,NPIN
 COMMON/ENERGY/ XPC(80),XETOT(80),XETOTO(80),XSE(80),XDE(80),
 1 XCE(80),XFE(80),KEI(80),PEI(80),XETOTL,KETOIL,
 2 PETOTL,SETOTL,DETOIL,CETOTL,FETOTL
 COMMON/MADE/KFL26(150),KFL35(150),FL26J,FL35J,FL35J,
 1 TPL(100),BPL,KPL
 COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),EE(20),GG(20),
 1 FIN(6,150),VOL(5),VZERO(5),KNATRI(6,4),NVCH,INBUFF(5,8)
 COMMON/INDEAC/ NACC
 COMMON/INDICP/ YDP(80)
 COMMON/INPR/ NDRI,NSP
 COMMON
 1 XN(80),DPX(80),DPY(80),DPZ(80),DPL(80),DPH(80),DPN(80),PIN(80),
 2 QIN(80),RIN(80),XII(80),XIZ(80),XIS(80),XI4(80),XI5(80),XI6(80),
 5 DELI(80),POLDI(80),QOLD(80),ROLD(80),UOLD(80),VOLD(80),
 6 MOLD(80),XOLD(80),YOLD(80),ZOLD(80),PIND(80),QIND(80),RIND(80),
 7 PHOLD(80),THEOLD(80),PSIOLD(80),
 8 XACFDI(80),YACFDI(80),ZACFDI(80),XAFOLD(80),YAFOLD(80),ZAFOLD(80),
 9 XNPFDI(80),YNPFDI(80),ZNPFDI(80),XANPFOI(80),YANPFOI(80),ZANPFOI(80),
 A TKR(200),TPEN(80),DTHALF,
 B KBEAM(4,200),KRFLAG(900),IPEN(80),KPEN,KRCONT
 COMMON/MCFIII/ SYHFLG
 COMMON/NP0012/ MG,NG,INP,INP
 COMMON/NP0012/ II,KK,MM
 COMMON/NP0014/ NNP
 COMMON/NP0018/ RX,RY,RZ
 COMMON/NP01R8/ XNP,YNP,ZNP,UNP,VNP,WNP,XDNP,YDNP,ZDNP,
 1 XACNP,YACNP,P,ZACNP,SBUCKR(150),PCR(150)
 COMMON/DEIC/ MTOT,CLTEST(150)
 COMMON/OLEO/OLEOI(20),FAO(20),FAA(20),EXPOL(20),YMAX(20),
 1 YOLEOI(20),BOLEOI(20),BROLEOI(20),XKEXT(20),XKCOMPI(20),FCOUL(20),
 2 ALPHAP,IGOLEOI(20),JGOLEOI(20),NGOLEOI(20),NGOLEOI(20),NOLEO
 COMMON/PRMA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50),
 1 ZACNPF(50),XIMP(80),YIMP(80),ZIMP(80),XIMPNP(50),YIMPNP(50),
 2 ZIMPNP(50),XIMPOL(80),YIMPOL(80),ZIMPOL(80),XIMPPL(50),
 3 YIMPPL(50),ZIMPPL(50)
 COMMON/IRDE/ PFIL
 COMMON/UB/ DB(150),IJB(150),NUB
 COMMON/COMALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),
 1 Y(81),Z(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),
 2 YI(80),ZI(80),YI(80),XZI(80),YZI(80),AIJ(9),BIJ(720),
 3 DRI(150),QAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80),
 4 POOT(80),QOOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),
 5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
 6 XACC(80),YACC(80),ZACC(80),AIDOT(9),
 7 PHIJ(150),THEIJ(150),PSIIJ(150),SUMOF(6,150),TITLE,
 8 XIBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
 9 DFIN(81),DQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),
 A CEIKF(40),
 B SBAR(40),KUN(40),MAXNM,MAXIGS,MAXTBL,
 C NM,NB,I,J,IG(150),JG(150),
 D NI(900),NN(40),IJPR(150)

```

ISN 0050      COMMON /MAX/ IRUPSM(150),IPENSH(80),VEEBAR(900),ZINIT(80),
ISN 0051      1 DPHIJ(150),FUB(150)
ISN 0052      COMMON /VARINT/ MINDT,DT2,TPRINT,EL,EU,RATMIN,RATHAX,IPC,IVAR
ISN 0053      COMMON /MACFIN/ THAX,IPRINT
ISN 0054      EQUIVALENCE (S1,SINCOS(1)),(C1,SINCOS(2)),(S2,SINCOS(3)),
ISN 0055      (C2,SINCOS(4)),(S3,SINCOS(5)),(C3,SINCOS(6))
ISN 0056      SQRT(X) = DSQRT(X)
ISN 0057      SIN(X) = DSIN(X)
ISN 0058      COS(X) = DCOS(X)
ISN 0059      SIGN(X1,X2) = DSIGN(X1,X2)
ISN 0060      ABS(X) = DABS(X)
ISN 0061      AMAX1(X,Y) = DMAX1(X,Y)
ISN 0062      ATAN2(Y,X) = DATAN2(Y,X)
ISN 0063      TANH(X)=DTANH(X)
ISN 0064      ONE = 1.
ISN 0065      TT = .2
ISN 0066      ET = .8
ISN 0067      S = DELTAT
ISN 0068      P12 = 3.141592653589793240/2.
ISN 0069      ERR = 0.
ISN 0070      IF(TIME.NE.0.0) GO TO 60
ISN 0071      DO 70 IJ = 1,NB
ISN 0072      PHIJ(IJ) = 0.
ISN 0073      VEEN(1,IJ) = 0.
ISN 0074      VEEN(2,IJ) = 0.
ISN 0075      DO 71 K=1,6
ISN 0076      71 SUMDFI(K,IJ) = 0.
ISN 0077      70 IRUPSM(IJ) = 0
ISN 0078      XSE(I) = 0.
ISN 0079      XDE(I) = 0.
ISN 0080      72 IPENSM(I)=0
ISN 0081      NB9 = 9*NB
ISN 0082      DO 74 I = 1,NB9
ISN 0083      VEEBAR(I) = 0.
ISN 0084      74 CONTINUE
ISN 0085      C DO ALL THE (AJ)((AJ))
ISN 0086      60 DO 10 I = 1,NH
ISN 0087      ARG = PHI(I)
ISN 0088      S1 = SIN(ARG)
ISN 0089      C1 = COS(ARG)
ISN 0090      ARG = THETA(I)
ISN 0091      S2 = SIN(ARG)
ISN 0092      C2 = COS(ARG)
ISN 0093      ARG = PSI(I)
ISN 0094      S3 = SIN(ARG)
ISN 0095      C3 = COS(ARG)
ISN 0096      DO 40 J = 1,6
ISN 0097      T = SINCOS(J)
ISN 0098      IF(T) 45,40,50
ISN 0099      45 T = -T
ISN 0100      50 IF(T-1.E-10) 55,40,40

```

```

ISN 0101 55 SINCOS(J) = 0.0
ISN 0102 40 CONTINUE
ISN 0103 C
ISN 0104 J = 9*(I-1)
ISN 0105 DO 4 J1 = 1,9
ISN 0106 4 OAI(J+J1) = BIJ(J+J1)
ISN 0107 S1S2 = S1*S2
ISN 0108 C1S2 = C1*S2
ISN 0109 AI(1) = C2*C3
ISN 0110 BIJ(J+1) = AI(1)
ISN 0111 AI(2) = C2*S3
ISN 0112 BIJ(J+2) = AI(2)
ISN 0113 AI(3) = -S2
ISN 0114 BIJ(J+3) = AI(3)
ISN 0115 AI(4) = -C1*S3+S1S2*C3
ISN 0116 BIJ(J+4) = AI(4)
ISN 0117 AI(5) = C1*C3+S1S2*S3
ISN 0118 BIJ(J+5) = AI(5)
ISN 0119 AI(6) = S1*C2
ISN 0120 BIJ(J+6) = AI(6)
ISN 0121 AI(7) = S1*S3+C1S2*C3
ISN 0122 BIJ(J+7) = AI(7)
ISN 0123 AI(8) = -S1*C3+C1S2*S3
ISN 0124 BIJ(J+8) = AI(8)
ISN 0125 AI(9) = C1*C2
ISN 0126 BIJ(J+9) = AI(9)
ISN 0127 C (27)
ISN 0128 PP = P(I)
ISN 0129 QQ = Q(I)
ISN 0130 RR = R(I)
ISN 0131 UU = U(I)
ISN 0132 VV = V(I)
ISN 0133 WW = W(I)
ISN 0134 XDOT(I) = AI(1)*UU+AI(4)*VV+AI(7)*WW
ISN 0135 YDOT(I) = AI(2)*UU+AI(5)*VV+AI(8)*WW
ISN 0136 ZDOT(I) = AI(3)*UU+AI(6)*VV+AI(9)*WW
ISN 0137 C (28), (29)
ISN 0138 CS = S1/C2
ISN 0139 CC = C1/C2
ISN 0140 PHIDOT(I) = PP+QQ*CS*S2+RR*CC*S2
ISN 0141 THEDOT(I) = QQ*C1-RR*S1
ISN 0142 PSIDOT(I) = QQ*CS+RR*CC
ISN 0143 C DO AIDOT NOW
ISN 0144 T = PSIDOT(I)*C2
ISN 0145 T1 = THEDOT(I)*S1-T*C1
ISN 0146 T2 = THEDOT(I)*C1-T*S1
ISN 0147 T3 = PHIDOT(I)-PSIDOT(I)*S2
ISN 0148 CIJ(J+1) = -BIJ(J+4)*T1-BIJ(J+7)*T2
ISN 0149 CIJ(J+4) = BIJ(J+1)*T1+BIJ(J+7)*T3
ISN 0150 CIJ(J+7) = BIJ(J+1)*T2-BIJ(J+4)*T3
ISN 0151 CIJ(J+2) = -BIJ(J+5)*T1-BIJ(J+8)*T2
ISN 0152 CIJ(J+5) = BIJ(J+2)*T1+BIJ(J+8)*T3

```

```

00001470
00001480
00001490
00001500
00001510
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00001890
00001900
00001910
00001920
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00001950
00001960
00001970
00001980
00001990

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```

ISN 0149      CIJ(J+8)= BIJ(J+2)*T2-BIJ(J+5)*T3
ISN 0150      CIJ(J+3)= -BIJ(J+6)*T1-BIJ(J+9)*T2
ISN 0151      CIJ(J+6)= BIJ(J+3)*T1-BIJ(J+9)*T3
ISN 0152      CIJ(J+9)= BIJ(J+3)*T2-BIJ(J+6)*T3
ISN 0153      10 CONTINUE

C
C      THE FOLLOWING CODING GETS THE VEHICLE C.G. TRANSLATIONAL
C      VELOCITY IN GROUND AXES BY EQUATING THE VEHICLE LINEAR
C      MOMENTUM WITH THE SUM OF THE MOMENTA OF ALL THE INDIVIDUAL
C      LUMPED MASSES.
C
      SUMMXD = 0.
      SUMMYD = 0.
      SUMMZD = 0.
      SUMW = 0.
      DO 12 I=1,NM
        SUMW = SUMW+WGT(I)
        SUMMXD = SUMMXD+WGT(I)*XDOT(I)
        SUMMYD = SUMMYD+WGT(I)*YDOT(I)
        SUMMZD = SUMMZD+WGT(I)*ZDOT(I)
      12 CONTINUE

C      FOR A SYMMETRICAL MODEL WE MUST ADD THE MOMENTUM CONTRIBUTIONS
C      FROM THE OPPOSITE MASSES THAT ARE NOT INPUT EXPLICITLY.
C
      IF(SYHFLG.NE.1.OR.YDP(I).EQ.0.) GO TO 12
      SUMW = SUMW+WGT(I)
      SUMMXD = SUMMXD+WGT(I)*XDOT(I)
      SUMMYD = SUMMYD+WGT(I)*YDOT(I)
      SUMMZD = SUMMZD+WGT(I)*ZDOT(I)
      12 CONTINUE
      XDOTAP = SUMMXD/SUMW
      YDOTAP = SUMMYD/SUMW
      ZDOTAP = SUMMZD/SUMW

C
C      FOR THE MAIN INTERNAL BEAM LOOP (DO 1000), WE NEED XNP(J),
C      DXNP(J), AND UNP(J) FOR THE NODE POINTS.
C
      IF(NNP.EQ.0) GO TO 16
      DO 14 J=1,NNP
        XNPOLD(J) = XNP(J)
        YNPOLD(J) = YNP(J)
        ZNPOLD(J) = ZNP(J)
        I = INP(J)
        IS = 9*(I-1)
        DO 15 KS=1,9
          IS = IS+1
          AI(KS) = BIJ(IS)
        15 CONTINUE
        TX = AI(1)*RX(J)+AI(4)*RY(J)+AI(7)*RZ(J)
        TY = AI(2)*RX(J)+AI(5)*RY(J)+AI(8)*RZ(J)
        TZ = AI(3)*RX(J)+AI(6)*RY(J)+AI(9)*RZ(J)
        XNP(J) = X(I)+TX
        YNP(J) = Y(I)+TY
      14 CONTINUE
      16 CONTINUE

```

ISN 0149
ISN 0150
ISN 0151
ISN 0152
ISN 0153

ISN 0154
ISN 0155
ISN 0156
ISN 0157
ISN 0158
ISN 0159
ISN 0160
ISN 0161
ISN 0162

ISN 0163
ISN 0165
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ISN 0186
ISN 0187
ISN 0188
ISN 0189


```

ISN 0190      ZNP(J) = Z(I)+YZ
ISN 0191      DXNP(J) = XNP(J)-XNPOLD(J)
ISN 0192      DYNP(J) = YNP(J)-YNPOLD(J)
ISN 0193      DZNP(J) = ZNP(J)-ZNPOLD(J)
ISN 0194      OTCRX = -R(I)*RY(J)+Q(I)*RZ(J)
ISN 0195      OTCRY = R(I)*RX(J)-P(I)*RZ(J)
ISN 0196      OTCRZ = -Q(I)*RX(J)+P(I)*RY(J)
ISN 0197      UNP(J) = U(I)+OTCRX
ISN 0198      VNP(J) = V(I)+OTCRY
ISN 0199      WNP(J) = W(I)+OTCRZ
ISN 0200      IF(TIME.NE.0.) GO TO 14
ISN 0201      DXNP(J) = 0.
ISN 0202      DYNP(J) = 0.
ISN 0203      DZNP(J) = 0.
ISN 0204      14 CONTINUE
ISN 0205      C
C
C      C ZERO OUT BEAM FORCES ON MASSES.
C
C      16 DO 16 I=1,NM
ISN 0206      XX(I) = 0.
ISN 0207      XY(I) = 0.
ISN 0208      XZ(I) = 0.
ISN 0209      XL(I) = 0.
ISN 0210      XH(I) = 0.
ISN 0211      XN(I) = 0.
ISN 0212      18 CONTINUE
ISN 0213      ILAST = 0
ISN 0214      C
C
C      C DO 1000 IS MAIN DO LOOP TO GET TOTAL INTERNAL FORCES AND MOMENTS
C
C      DO 1000 IJ = 1,NB
ISN 0215      IJK = 6*(IJ-1)
ISN 0216      IF(IRUPSM(IJ).NE.0) GO TO 1000
ISN 0217      I = IG(IJ)
ISN 0218      J = JG(IJ)
ISN 0219      M = MG(IJ)
ISN 0220      N = NG(IJ)
ISN 0221      C
ISN 0222      C IF WE GET TO A NEW I WE MUST MOVE (AI) INTO AI.
ISN 0223      IF(I-ILAST) 20,30,20
ISN 0224      20 ILAST = I
ISN 0225      IS = 9*(I-1)
ISN 0226      DO 320 KS = 1,9
ISN 0227      IS = IS+1
ISN 0228      AIDOT(KS) = CIJ(IS)
ISN 0229      320 AI(KS) = BIJ(IS)
C
C      NOW GET AJ.
C
C      30 IS = 9*(J-1)
ISN 0230      DO 3201 KS=1,9
ISN 0231      IS = IS+1
ISN 0232      IF(J.EQ.0) GO TO 3202
ISN 0233      AJ(KS) = BIJ(IS)
ISN 0234
ISN 0235
00002530
00002540
00002550
00002560
00002570
00002580
00002590
00002600
00002610
00002620
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00002800
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ISN 0236      GO TO 3201
ISN 0237      3202 AJ(KS) = AI(KS)
ISN 0238      IF(KS.EQ.2.OR.KS.EQ.4.OR.KS.EQ.6.OR.KS.EQ.8) AJ(KS) = -AJ(KS)
ISN 0240      3201 CONTINUE
C
C IF J.EQ.0, WE HAVE A SYMMETRICAL MODEL IN WHICH BEAM IJ
C CONNECTS NODE POINT (I,M) TO AN IMAGINARY POINT (J,N=0)
C LOCATED SYMMETRICALLY ACROSS THE AIRPLANE PLANE OF SYMMETRY
C (X-Z PLANE). FOR THESE TRANSVERSE BEAMS, THE CONDITIONS AT (J,N)
C ARE DEDUCED FROM THE STATE AT (I,M). J IS CHANGED TO 81 BECAUSE
C THE IBM 360-91 WILL NOT ACCEPT A ZERO SUBSCRIPTED VECTOR.
C
ISN 0241      IF(J.NE.0) GO TO 3300
ISN 0243      J = 81
ISN 0244      IF(M.NE.0) GO TO 3301
C
C IF M.EQ.0, THERE IS NO NODE POINT AT I.
C
C
C 3302 DXMODI = DX(I)
C      DYMODI = DY(I)
C      DZMODI = DZ(I)
C      XMODI = X(I)
C      YMODI = Y(I)
C      ZMODI = Z(I)
C      UMODI = U(I)
C      VMODI = V(I)
C      WMODI = W(I)
C      PI = P(I)
C      QI = Q(I)
C      RI = R(I)
C      GO TO 3303
C
C THIS LOOP GETS NODE POINT NUMBER JI KNOWING I AND M.
C
C 3301 DO 3305 JI=1,NNP
C      IF(I.EQ.INPI(JI).AND.M.EQ.MNPI(JI)) GO TO 3306
C 3305 CONTINUE
C 3306 DXMODI = DXNP(JI)
C      DYMODI = DYNP(JI)
C      DZMODI = DZNP(JI)
C      XMODI = XNP(JI)
C      YMODI = YNP(JI)
C      ZMODI = ZNP(JI)
C      UMODI = UNPI(JI)
C      VMODI = VNPI(JI)
C      WMODI = WNPI(JI)
C      PI = P(I)
C      QI = Q(I)
C      RI = R(I)
C 3303 IF(J.NE.81) GO TO 3310
C
C IF J.EQ.81, WE HAVE A SYMMETRICAL MODEL. NOW CALCULATE
C CONDITIONS AT J,N BASED ON KNOWLEDGE OF STATE AT I,M.
C

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0003560
0003570
0003580

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C
ISN 0277 DXMOOJ = DXMOOI
ISN 0278 DYMOOJ = -DYMOOI
ISN 0279 DZMOOJ = DZMOOI
ISN 0280 XMOOJ = XMOOI
ISN 0281 YMOOJ = -YMOOI
ISN 0282 ZMOOJ = ZMOOI
ISN 0283 OPIN(J) = -OPIN(I)
ISN 0284 DQIN(J) = DQIN(I)
ISN 0285 DRIN(J) = -DRIN(I)
ISN 0286 UMOOJ = UMOOI
ISN 0287 VMOOJ = -VMOOI
ISN 0288 WMOOJ = WMOOI
ISN 0289 PJ = PI
ISN 0290 QJ = QI
ISN 0291 RJ = RI
ISN 0292 GO TO 3320
ISN 0293 3300 IF(N.EQ.0) GO TO 3302
ISN 0295 GO TO 3301
ISN 0296 3310 IF(N.NE.0) GO TO 3311
C
C IF N.EQ.0, THERE IS NO NODE POINT AT J.
C
C
DXMOOJ = DX(J)
DYMOOJ = DY(J)
DZMOOJ = DZ(J)
XMOOJ = X(J)
YMOOJ = Y(J)
ZMOOJ = Z(J)
UMOJ = U(J)
VMOOJ = V(J)
WMOOJ = W(J)
PJ = PI(J)
QJ = Q(J)
RJ = R(J)
GO TO 3320
C
C THIS LOOP GETS NODE POINT NUMBER JJ KNOWING J AND N.
C
3311 DO 3312 JJ=1,NNP
IF(J.EQ.INP(JJ).AND.N.EQ.WNP(JJ)) GO TO 3313
3312 CONTINUE
3313 DXMOOJ = DXNP(JJ)
DYMOOJ = DYNP(JJ)
DZMOOJ = DZNP(JJ)
XMOOJ = XNP(JJ)
YMOOJ = YNP(JJ)
ZMOOJ = ZNP(JJ)
UMOJ = UNP(JJ)
VMOOJ = VNP(JJ)
WMOOJ = WNP(JJ)
PJ = PI(J)
QJ = Q(J)
ISN 0311 ISN 0312 ISN 0314 ISN 0315 ISN 0316 ISN 0317 ISN 0318 ISN 0319 ISN 0320 ISN 0321 ISN 0322 ISN 0323 ISN 0324 ISN 0325

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ISN 0326      RJ = R(IJ)
C
C
C      ALL OF THE ABOVE PATHS LEAD TO HERE. WE NOW HAVE POSITIONS
C      (XMOD,ETC.) AND INCREMENTAL CHANGES IN POSITIONS (DXMOD,ETC.)
C      FOR BOTH ENDS OF BEAM IJ.
C
3320 XIJ = XMODJ-XMODI
ISN 0327      YIJ = YMODJ-YMODI
ISN 0328      ZIJ = ZMODJ-ZMODI
ISN 0329
C
C CALCULATE AIJ. FIRST UPDATE PHI(IJ), THE(IJ), PSI(IJ).
C
C      PHI(IJ) = PHI(IJ) + DPHI(IJ)
C      IF(XIJ.EQ.0.AND.YIJ.EQ.0.) GO TO 3330
C      PSI(IJ) = ATAN2(YIJ,XIJ)
C      GO TO 3340
3330 PSI(IJ) = 0.
3340 THE(IJ) = -ATAN2(ZIJ,SQRT(XIJ*XIJ+YIJ*YIJ))
C
C ZERO OUT VERY SMALL SIN AND COS TERMS.
C
C      ARG = PHI(IJ)
C      S1 = SIN(ARG)
C      C1 = COS(ARG)
C      ARG = THE(IJ)
C      S2 = SIN(ARG)
C      C2 = COS(ARG)
C      ARG = PSI(IJ)
C      S3 = SIN(ARG)
C      C3 = COS(ARG)
C      DO 3392 J1 = 1,6
C      T = SIN(COS(J1))
C      IF(T) 3394,3392,3398
3394 T = -T
3398 IF(T-1.E-10) 3396,3392,3392
ISN 0330      3396 SIN(COS(J1)) = 0.0
ISN 0331      3392 CONTINUE
ISN 0332      S1S2 = S1*S2
ISN 0333      C1S2 = C1*S2
ISN 0334      AIJ(1) = C2*C3
ISN 0335      AIJ(2) = C2*S3
ISN 0336      AIJ(3) = -S2
ISN 0337      AIJ(4) = -C1*S3 + S1S2*C3
ISN 0338      AIJ(5) = C1*C3 + S1S2*S3
ISN 0339      AIJ(6) = S1*C2
ISN 0340      AIJ(7) = S1*S3 + C1S2*C3
ISN 0341      AIJ(8) = -S1*C3 + C1S2*S3
ISN 0342      AIJ(9) = C1*C2
ISN 0343
C
C CALCULATE CURRENT BEAM LENGTH XXLB.
C
C      XXLB = SQRT(XIJ*XIJ+YIJ*YIJ+ZIJ*ZIJ)
C

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C CALCULATE AIJTAJ AND AIJTAI. FILL TEMP WITH EITHER AJ OR AI.

ISN 0365
ISN 0366
ISN 0367
ISN 0369
ISN 0370
ISN 0371
ISN 0372
ISN 0373
ISN 0374
ISN 0375
ISN 0376
ISN 0377
ISN 0378
ISN 0379
ISN 0380
ISN 0381
ISN 0383
ISN 0384
ISN 0385
ISN 0386
ISN 0387
ISN 0388

DO 6000 I3=1,2
DO 6010 I4=1,9
IF(I3.EQ.2) GO TO 6020
TEMP(I4) = AJ(I4)
GO TO 6010
6020 TEMP(I4) = AI(I4)
6010 CONTINUE
L2 = 0
DO 6030 K2=1,3
DO 6040 J2=1,3
L2 = L2+1
SUMH(L2) = 0.
DO 6050 I2=1,3
SUMH(L2) = SUMH(L2) + AIJ(3*(J2-1)+I2)*TEMP(3*(K2-1)+I2)
6050 CONTINUE
IF(I3.EQ.2) GO TO 6060
AIJTAJ(L2) = SUMH(L2)
GO TO 6040
6060 AIJTAI(L2) = SUMH(L2)
6040 CONTINUE
6030 CONTINUE
6000 CONTINUE

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00004660
00004670
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00005000
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C CALCULATE VELOCITIES AND INCREMENTAL DEFLECTIONS AT J-N
C AND I-M IN BEAM AXES.

ISN 0389
ISN 0390
ISN 0391
ISN 0392
ISN 0393
ISN 0394
ISN 0395
ISN 0396
ISN 0397
ISN 0398
ISN 0399
ISN 0400
ISN 0401
ISN 0402
ISN 0403
ISN 0404
ISN 0405
ISN 0406
ISN 0407
ISN 0408
ISN 0409
ISN 0410
ISN 0411
ISN 0412

VJ(1) = AIJTAJ(1)*UMODJ+AIJTAJ(4)*VMODJ+AIJTAJ(7)*MMODJ
VJ(2) = AIJTAJ(2)*UMODJ+AIJTAJ(5)*VMODJ+AIJTAJ(8)*MMODJ
VJ(3) = AIJTAJ(3)*UMODJ+AIJTAJ(6)*VMODJ+AIJTAJ(9)*MMODJ
VJ(4) = AIJTAJ(1)*PJ+AIJTAJ(4)*QJ+AIJTAJ(7)*RJ
VJ(5) = AIJTAJ(2)*PJ+AIJTAJ(5)*QJ+AIJTAJ(8)*RJ
VJ(6) = AIJTAJ(3)*PJ+AIJTAJ(6)*QJ+AIJTAJ(9)*RJ
VI(1) = AIJTAI(1)*UMODI+AIJTAI(4)*VMODI+AIJTAI(7)*MMODI
VI(2) = AIJTAI(2)*UMODI+AIJTAI(5)*VMODI+AIJTAI(8)*MMODI
VI(3) = AIJTAI(3)*UMODI+AIJTAI(6)*VMODI+AIJTAI(9)*MMODI
VI(4) = AIJTAI(1)*PI+AIJTAI(4)*QI+AIJTAI(7)*RI
VI(5) = AIJTAI(2)*PI+AIJTAI(5)*QI+AIJTAI(8)*RI
VI(6) = AIJTAI(3)*PI+AIJTAI(6)*QI+AIJTAI(9)*RI
DJ(1) = AIJ(1)*DXMODJ + AIJ(2)*DYMODJ + AIJ(3)*DZMODJ
DJ(2) = AIJ(4)*DXMODJ + AIJ(5)*DYMODJ + AIJ(6)*DZMODJ
DJ(3) = AIJ(7)*DXMODJ + AIJ(8)*DYMODJ + AIJ(9)*DZMODJ
DI(1) = AIJ(1)*DXMODI + AIJ(2)*DYMODI + AIJ(3)*DZMODI
DI(2) = AIJ(4)*DXMODI + AIJ(5)*DYMODI + AIJ(6)*DZMODI
DI(3) = AIJ(7)*DXMODI + AIJ(8)*DYMODI + AIJ(9)*DZMODI
DJ(4) = AIJTAJ(1)*DPINI(J)+AIJTAJ(4)*DQINI(J)+AIJTAJ(7)*DRINI(J)
DJ(5) = AIJTAJ(2)*DPINI(J)+AIJTAJ(5)*DQINI(J)+AIJTAJ(8)*DRINI(J)
DJ(6) = AIJTAJ(3)*DPINI(J)+AIJTAJ(6)*DQINI(J)+AIJTAJ(9)*DRINI(J)
DI(4) = AIJTAI(1)*DPINI(I)+AIJTAI(4)*DQINI(I)+AIJTAI(7)*DRINI(I)
DI(5) = AIJTAI(2)*DPINI(I)+AIJTAI(5)*DQINI(I)+AIJTAI(8)*DRINI(I)
DI(6) = AIJTAI(3)*DPINI(I)+AIJTAI(6)*DQINI(I)+AIJTAI(9)*DRINI(I)

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C C CALCULATE VELOCITIES AND RELATIVE INCREMENTAL DEFLECTIONS (J-I) AND
C C SUMS (J+I) FOR INTERNAL FORCE CALCULATIONS. VEEN(I AND 2) ARE
C C USED FOR OUTPUT ONLY.
C
ISN 0413 DO 6100 J2=1,9
ISN 0414 IF(J2.GT.6) GO TO 6110
ISN 0416 DI(J2) = DJ(J2) - DI(J2)
ISN 0417 VEL(J2) = VJ(J2) - VI(J2)
ISN 0418 GO TO 6100
ISN 0419
ISN 0420 6110 DI(J2) = DJ(J2-3) + DI(J2-3)
ISN 0422 IF(J2.NE.7) VEEN(J2-7,IJ) = VEEN(J2-7,IJ)+DI(J2)
ISN 0423 VEL(J2) = VJ(J2-3) + VI(J2-3)
ISN 0424 6100 CONTINUE
C
C DPHIJ(IJ) = D(7)/2.
C
C MARCH 1977 INTERNAL FORCE CODING
C
C DO 150 K = 1,6
C IJK = IJK+1
C
C NOW LETS GET A KR IF A TABLE EXISTS
C FIRST DETERMINE WHICH TABLE WE WANT
C
ISN 0427 ITN = NLSFLG(IJK)
ISN 0428 IF(ITN.EQ.0) GO TO 144
ISN 0430 IF(K.EQ.1.OR.K.EQ.4) GO TO 191
ISN 0432 IF(K.EQ.2.OR.K.EQ.6) GO TO 192
ISN 0434 IF(KFL35(IJ).EQ.0) GO TO 191
ISN 0436 KPR = KFL35(IJ)
ISN 0437 GO TO 193
ISN 0438 192 IF(KFL26(IJ).EQ.0) GO TO 191
ISN 0440 KPR = KFL26(IJ)
ISN 0441 GO TO 193
ISN 0442 191 KPR = K
C
C 193 MYSUB = IJK-K+KPR
C
ISN 0443 ITN = NLSFLG(MYSUB)
ISN 0445 IF(K.NE.1.OR.IJUB(IJ).EQ.0) GO TO 200
ISN 0447 AXK=ABS(VEE(MYSUB))-DB(IJ)
ISN 0448 IF(AXK.LT.0.) AXK=0.
ISN 0450 IF((VEE(MYSUB).LT.0.AND.IJUB(IJ).GT.0).OR.
1 (VEE(MYSUB).GT.0.AND.IJUB(IJ).LT.0)) AXK=0.
GO TO 201
ISN 0452 200 AXK = ABS(VEE(MYSUB))
ISN 0453 201 PTR = CHUG(ITN)
ISN 0454 IF(AXK.LT.XKR(PTR)) GO TO 110
ISN 0455 IF(AXK.GT.XKR(PTR+1)) GO TO 120
ISN 0457 140 KR(K) = XKS(PTR)+AXK+XKI(PTR)
ISN 0459
C
C CALCULATE STUFF FOR YIELDING AND RUPTURE SUMMARY TABLES,
C (YIELDING ONLY HERE).
C
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00005690
00005700

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ISN 0460      C      IF(KRFLAG(IJK).NE.0) GO TO 141
ISN 0462      IF(KR(K).EQ.1.) GO TO 141
ISN 0464      KRCONT = KRCONT+1
ISN 0465      TKR(KRCONT) = TIME
ISN 0466      KRBEAM(1,KRCONT) = IJ
ISN 0467      KRBEAM(2,KRCONT) = K
ISN 0468      KRFLAG(IJK) = 1
ISN 0469      GO TO 141

C*****CHUG DOWN
ISN 0470      110 PTR = PTR-1
ISN 0471      IF(AXK.L..XKR(PTR)) GO TO 110
ISN 0473      130 CHUG(IIN) = PTR
ISN 0474      GO TO 140

C*****CHUG UP
ISN 0475      120 PTR = PTR+1
ISN 0476      IF(AXK.GT.XKR(PTR+1)) GO TO 120
ISN 0478      GO TO 130
ISN 0479      144 KR(K) = 1
ISN 0480      GO TO 150

C      C      AFTER ALL THIS CHUGGING,140 CALCULATES KR.
C      C      NOTE THAT 130 SAVED LOCATION IN TABLE NO. ITN FOR THE
C      C      STARTING POINT AT THE NEXT TIME CUT.
C      C
ISN 0481      141 IF(K.EQ.1.OR.K.EQ.4) GO TO 150
ISN 0483      IF(K.EQ.2.OR.K.EQ.6) GO TO 142
ISN 0485      IF(KR(K).NE.1.AND.KFL35(IJ).EQ.0) KFL35(IJ) = K
ISN 0487      GO TO 150
ISN 0488      142 IF(KR(K).NE.1.AND.KFL26(IJ).EQ.0) KFL26(IJ) = K

C      C      THIS LOOP SETS KFL35 TO EITHER 3 OR 5,WHICHEVER KR TABLE
C      C      GOES NONLINEAR FIRST. FROM THEN ON,KR WILL BE READ FROM
C      C      THAT TABLE WHETHER K=3 OR 5. THE SAME GOES FOR KFL26.
C      C
ISN 0490      150 CONTINUE

C      C      SET KR=1. FOR UNLOADING AND RELOADING.
C      C
ISN 0491      IJL = 6*(IJ-1)
ISN 0492      DO 7000 L = 1,6
ISN 0493      IJL = IJL + 1
ISN 0494      A = D(L)

C      C      CORRECT Y AND Z DEFLECTIONS BY REMOVING ROTATION COMPONENT.
C      C      SEE ALSO LABEL 632.
C      C
ISN 0495      IF(L.EQ.2) A=A-XXLB*D(9)/2.
ISN 0497      IF(L.EQ.3) A=A+XXLB*D(8)/2.
ISN 0499      B = A + VEE(IJL)
ISN 0500      IF(A.GE.0.0.AND.B.GE.0.0.OR.A.LT.0.0.AND.B.LT.0.0) GO TO 7010

C      C      SIGNS ARE NOT THE SAME (UNLOADING)
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0006680
0006690
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0006740
0006750
0006760

C
IF(NI(IJL).NE.0) GO TO 7020
NI(IJL) = 1
VEEBAR(IJL) = ABS(VEE(IJL))
GO TO 7020
7010 IF(ABS(VEE(IJL)).LT.VEEBAR(IJL)) GO TO 7020
C
C LOADING PATH, USE KR FROM ABOVE.
C
NI(IJL) = 0
GO TO 7000
7020 KR(L) = 1.
7000 CONTINUE
IF(KR(5).NE.KR(3)) KR(5) = KR(3)
IF(KR(6).NE.KR(2)) KR(6) = KR(2)
C
C LETS GET THE STIFFNESSES.
C
ISTART = 36*(IJ-1)
XX11 = XK(ISTART + 1)
XX22 = XK(ISTART + 8)
XX26 = XK(ISTART + 12)
XX33 = XK(ISTART + 15)
XX35 = XK(ISTART + 17)
XX44 = XK(ISTART + 22)
XX55 = XK(ISTART + 29)
XX66 = XK(ISTART + 36)
C
C CORRECT STIFFNESSES FOR CURRENT BEAN LENGTH.
C
C XXLB IS CURRENT LENGTH, XLB(IJ) IS ORIGINAL LENGTH.
C
XLRAT1 = XLB(IJ)/XXLB
XLRAT2 = XLRAT1*XLRAT1
XLRAT3 = XLRAT1*XLRAT2
XX11SR=XX11
XX44SR=XX44
XX55SR=XX55
XX66SR=XX66
XX22SR=XX22
XX33SR=XX33
XX26SR=XX26
XX35SR=XX35
IF(MOLEQ.EQ.0) GO TO 4080
DO 4081 JJ=1,MOLEQ
IF(MOLEQ(IJ).EQ.IG(IJ).AND. JGOLEO(IJ).EQ.JG(IJ).AND.MGOLEO(JJ)
1.EQ.MG(IJ).AND.NGOLEO(JJ).EQ.NG(IJ)) GO TO 4083
4081 CONTINUE
GO TO 4080
4083 XX55SR=XX55*SQRT(XLRAT1)
XX66SR=XX66*SQRT(XLRAT1)
XX22SR=XX22*SQRT(XLRAT3)
XX33SR=XX33*SQRT(XLRAT3)
XX26SR=XX26*SQRT(XLRAT2)
ISN 0502
ISN 0503
ISN 0504
ISN 0505
ISN 0506
ISN 0507
ISN 0508
ISN 0509
ISN 0510
ISN 0511
ISN 0512
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ISN 0518
ISN 0519
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ISN 0547
ISN 0548

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ISN 0549      XK35SR=XK35*SQRT(XLRAT2)
ISN 0550      XK55=XK55*XLRAT1
ISN 0551      XK66=XK66*XLRAT1
ISN 0552      XK22=XK22*XLRAT3
ISN 0553      XK33=XK33*XLRAT3
ISN 0554      XK26=XK26*XLRAT2
ISN 0555      XK35=XK35*XLRAT2
ISN 0556      4080 CONTINUE

C
C  C  CALCULATE INCREMENTAL STRAIN FORCES DFJ AND DAMPING FORCES FDJ
C  C  AT J,N IN BEAM AXES.
C
      DFJ(1) = XK11*D(1)
      FDJ(1) = XK11SR*VEL(1)
      IF(IJUB(IJ).EQ.0) GO TO 202
      FDJ(1) = 0.
      IJ1 = 6*(IJ-1)+1
      IF(ABS(VEE(IJ1)+D(1)).GE.DB(IJ)) GO TO 202
      DFJ(1) = 0.
      202 DFJ(4) = XK44*D(4)
      FDJ(4) = XK44SR*VEL(4)

C
C  C  CALCULATE 2.6 LOADS.
C
      IF(PZ(IJ).EQ.0.AND.PZJ(IJ).EQ.0) GO TO 204
      IJPIN=0
      IF(PZ(IJ).NE.0.AND.ABS(SUMDF(6,IJ)).GE.PLM26(IJ)) GO TO 810
      IF(PZJ(IJ).NE.0.AND.ABS(SUMDF(6,IJ)).GE.PLM26J(IJ)) GO TO 812
      GO TO 204
      810 IF(PLM26(IJ).EQ.0.OR.FL26(IJ).NE.0) GO TO 814
      816 IJPIN=1
      812 IF(PLM26J(IJ).EQ.0.OR.FL26J(IJ).NE.0) GO TO 818

C
C  C  FIRST TIME THRU FOR PLASTIC HINGE FORMATION SAVE DATA
C  C  FOR SUMMARY TABLE. I END OF BEAM,6 DIRECTION
C
      FL26(IJ)=1
      KPL=KPL+1
      TPL(KPL)=TIME
      BPL(KPL,1)=IJ
      BPL(KPL,2)=6
      IF(SUMDF(6,IJ).LT.0.) BPL(KPL,2)=-6
      BPL(KPL,3)=IG(IJ)
      814 IF(PZJ(IJ).NE.0.AND.ABS(SUMDF(6,IJ)).GE.PLM26J(IJ)) GO TO 816
      816 IJPIN=1
      812 IF(PLM26J(IJ).EQ.0.OR.FL26J(IJ).NE.0) GO TO 818

C
C  C  FIRST TIME THRU FOR PLASTIC HINGE FORMATION.
C  C  SAVE DATA FOR SUMMARY TABLE. J END OF BEAM,6 DIRECTION
C
      FL26J(IJ)=1
      KPL=KPL+1
      TPL(KPL)=TIME
      BPL(KPL,1)=IJ

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ISN 0596      BPL(KPL,2)=6
ISN 0597      IF(SUMDF(6,IJ).LT.0.) BPL(KPL,2)=-6
ISN 0599      BPL(KPL,3)=JG(IJ)
ISN 0600      818 IF(IJPIN.EQ.1) GO TO 206
C
C PINNED AT J ONLY.
C
ISN 0602      DFJ(2) = XK22/4*D(2)+XK26/2*DI(6)
ISN 0603      FDJ(2) = XK22SR/4*VEL(2)+XK26SR/2*VI(6)
ISN 0604      DFJ(6) = 0.
ISN 0605      FDJ(6) = 0.
ISN 0606      GO TO 210
C
C PINNED AT I ONLY.
C
ISN 0607      208 DFJ(2) = XK22/4*D(2) + XK26/2*D(6)
ISN 0608      FDJ(2) = XK22SR/4*VEL(2) + XK26SR/2*VJ(6)
ISN 0609      DFJ(6) = XK26/2*D(2) + XK66*3/4*D(6)
ISN 0610      FDJ(6) = XK26SR/2*VEL(2) + XK66SR*3/4*VJ(6)
ISN 0611      GO TO 210
C
C PINNED AT I AND J.
C
ISN 0612      206 DFJ(2) = 0.
ISN 0613      FDJ(2) = 0.
ISN 0614      DFJ(6) = 0.
ISN 0615      FDJ(6) = 0.
ISN 0616      GO TO 210
C
C FIXED AT I AND J. (NORMAL CASE)
C
ISN 0617      204 DFJ(2) = XK22*D(2) + XK26*D(9)
ISN 0618      FDJ(2) = XK22SR*VEL(2) + XK26SR*VEL(9)
ISN 0619      DFJ(6) = XK66*(D(6)+3.*D(9))/4. + XK26*D(2)
ISN 0620      FDJ(6) = XK66SR*(VEL(6)+3.*VEL(9))/4. + XK26SR*VEL(2)
C
C CALCULATE 3,5 LOADS.
C
ISN 0621      210 IF(PY(IJ).EQ.0.AND.PYJ(IJ).EQ.0) GO TO 214
ISN 0623      IJPIN=0
ISN 0624      IF(PY(IJ).NE.0.AND.ABS(SUMDF(5,IJ)).GE.PLM35(IJ)) GO TO 820
ISN 0626      IF(PYJ(IJ).NE.0.AND.ABS(SUMDF(5,IJ)).GE.PLM35(IJ)) GO TO 822
ISN 0628      GO TO 214
ISN 0629      820 IF(PLM35(IJ).EQ.0.OR.FL35I(IJ).NE.0) GO TO 824
C
C FIRST TIME THRU FOR PLASTIC HINGE FORMATION.SAVE DATA
C FOR SUMMARY TABLE. I END OF BEAM,5 DIRECTION
C
ISN 0631      FL35I(IJ)=1
ISN 0632      KPL=KPL+1
ISN 0633      TPL(KPL)=TIME
ISN 0634      BPL(KPL,1)=IJ
ISN 0635      BPL(KPL,2)=5

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ISN 0636 IF(SUMDF(I,5,IJ),LT.0.) BPL(KPL,2)=-5
ISN 0638 BPL(KPL,3)=IG(IJ)
ISN 0639 824 IF(PYJ(IJ),NE.0.AND.ABS(SUMDF(5,IJ)).GE.PLM35J(IJ)) GO TO 826
ISN 0641 GO TO 218
ISN 0642 826 IJPIN=1
ISN 0643 822 IF(PLM35J(IJ),EQ.0.OR.FL35J(IJ),NE.0) GO TO 828

C FIRST TIME THRU FOR PLASTIC HINGE FORMATION.
C SAVE DATA FOR SUMMARY TABLE. J END OF BEAH,5 DIRECTION
C
ISN 0645 FL35J(IJ)=1
ISN 0646 KPL=KPL+1
ISN 0647 TPL(KPL)=TIME
ISN 0648 BPL(KPL,1)=IJ
ISN 0649 BPL(KPL,2)=5
ISN 0650 IF(SUMDF(5,IJ),LT.0) BPL(KPL,2)=-5
ISN 0651 BPL(KPL,3)=JG(IJ)
ISN 0652 828 IF(IJPIN.EQ.1) GO TO 216
ISN 0653 C PINNED AT J ONLY.
C
ISN 0655 DFJ(3) = XK33/4*D(3)+XK35/2*DI(5)
ISN 0656 FDJ(3) = XK33SR/4*VEL(3)+XK35SR/2*VI(5)
ISN 0657 DFJ(5) = 0.
ISN 0658 FDJ(5) = 0.
ISN 0659 GO TO 220

C PINNED AT I ONLY.
C
ISN 0660 218 DFJ(3) = XK33/4*D(3) + XK35/2*DJ(5)
ISN 0661 FDJ(3) = XK33SR/4*VEL(3) + XK35SR/2*VJ(5)
ISN 0662 DFJ(5) = XK35/2*D(3) + XK55*3/4*DJ(5)
ISN 0663 FDJ(5) = XK35SR/2*VEL(3) + XK55SR*3/4*VJ(5)
ISN 0664 GO TO 220

C PINNED AT I AND J.
C
ISN 0665 216 DFJ(3) = 0.
ISN 0666 FDJ(3) = 0.
ISN 0667 DFJ(5) = 0.
ISN 0668 FDJ(5) = 0.
ISN 0669 GO TO 220

C FIXED AT I AND J. (NORMAL CASE)
C
ISN 0670 214 DFJ(3) = XK33*D(3) + XK35*D(8)
ISN 0671 FDJ(3) = XK33SR*VEL(3) + XK35SR*VEL(8)
ISN 0672 DFJ(5) = XK55*(D(5)+3.*D(8))/4. + XK35*D(3)
ISN 0673 FDJ(5) = XK55SR*(VEL(5)+3.*VEL(8))/4. + XK35SR*VEL(3)

C MULTIPLY DFJ'S BY KP'S.
C
ISN 0674 220 DO 7030 J2=1,6

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ISN 0675      DFJ(J2) = KR(J2)*DFJ(J2)
ISN 0676      7030 CONTINUE
C
C      MULTIPLY FDJ'S BY DAMPING CONSTANTS.
C
      222 DO 6130 J2=1,6
          IF(J2.EQ.1.OR.J2.EQ.4) GO TO 6132
          IF(J2.EQ.2.OR.J2.EQ.6) GO TO 6134
          CON = 0.5*(C(3,IJ)+C(5,IJ))
          GO TO 6136
      6134 CON = 0.5*(C(2,IJ)+C(6,IJ))
      6136 FDJ(J2) = CON*FDJ(J2)
          FDJ(J2)=KR(J2)*FDJ(J2)
          GO TO 6130
      6132 FDJ(J2) = C(J2,IJ)*FDJ(J2)
          FDJ(J2)=KR(J2)*FDJ(J2)
      6130 CONTINUE
C
C      CALCULATE INCREMENTAL FORCES AT I,M USING
C      STATIC BALANCE EQUATIONS. DAMPING FORCES ARE TOTAL.
C
      DO 6120 J2=1,6
          DFI(J2) = -DFJ(J2)
          FDI(J2) = -FDJ(J2)
      6120 CONTINUE
          DFI(5) = DFI(5) + XXLB*DFJ(3)
          DFI(6) = DFI(6) - XXLB*DFJ(2)
          FDI(5) = FDI(5) + XXLB*FDJ(3)
          FDI(6) = FDI(6) - XXLB*FDJ(2)
C
C      NOW SUM OVER TIME TO GET CURRENT TOTAL
C      FORCES AT I,M AND J,N. STILL IN BEAM AXES.
C
          IJK1 = 6*(IJ-1) + 1
          DO 630 K=1,6
C
C      CHECK FOR UNSYMMETRICAL BEAMS.
C
          IF(K.NE.1.OR.IJUB(IJ).EQ.0) GO TO 602
          IF(IME.EQ.0.) FUB(IJ) = 0.
          FUB(IJ) = FUB(IJ) + DFJK
C
C      FUB(IJ) IS THE TOTAL AXIAL LOAD FOR UNSYMMETRICAL BEAMS
C      WITHOUT ANY RESTRICTIONS ON + OR -. NOW ZERO OUT SUMDF
C      IF REQUIRED. SUMDF IS USED IN SUBSEQUENT CALC'S AND PRINT.
C
          A = D(K)
          B = VEE(IJK1) + A
          IF((B.LT.0.AND.IJUB(IJ).GT.0).OR.
      1 (B.GT.0.AND.IJUB(IJ).LT.0)) GO TO 606
          IF((FUB(IJ).LE.0.AND.IJUB(IJ).LT.0).OR.
      1 (FUB(IJ).GE.0.AND.IJUB(IJ).GT.0)) GO TO 604
      606 SUMDF(K,IJ) = 0.

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ISN 0677
ISN 0678
ISN 0680
ISN 0682
ISN 0683
ISN 0684
ISN 0685
ISN 0686
ISN 0687
ISN 0688
ISN 0689
ISN 0690

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ISN 0691
ISN 0692
ISN 0693
ISN 0694
ISN 0695
ISN 0696
ISN 0697
ISN 0698

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ISN 0699
ISN 0700

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ISN 0701
ISN 0703
ISN 0705

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ISN 0706
ISN 0707
ISN 0708
ISN 0710
ISN 0712

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ISM 0713 SUMDFI(K,IJ) = 0.
ISM 0714 GO TO 600
ISM 0715 604 SUMDF(K,IJ) = FUB(IJ)
ISM 0716 SUMDFI(K,IJ) = -FUB(IJ)
ISM 0717 GO TO 600
ISM 0718 602 SUMDF(K,IJ) = SUMDF(K,IJ) + DFJ(K)
ISM 0719 SUMDFI(K,IJ) = SUMDFI(K,IJ) + DFI(K)
ISM 0720 600 FSJ(K) = SUMDF(K,IJ)
ISM 0721 FSI(K) = SUMDFI(K,IJ)
ISM 0722 FINT(K,IJ) = FSJ(K) + FDJ(K)
ISM 0723 FINTI(K,IJ) = FSI(K) + FDI(K)

C
C REDO AXIAL LOAD CALCULATIONS FOR LANDING GEAR OLEO MODULES
C STRAIN FORCES ARE DUE TO AIR CURVE, DAMPING FORCES ARE DUE
C TO HYDRAULIC DAMPING & FRICTION
C

IF(NOLEO.EQ.0 .OR. K.NE.1) GO TO 630
DO 700 JJ=1,NOLEO
  IF(I.EQ.IGOLEO(JJ).AND. J.EQ.JGOLEO(JJ).AND. M.EQ.MGOLEO(JJ)
    1 .AND. N.EQ.NGOLEO(JJ)) GO TO 702
  700 CONTINUE
  GO TO 630
  702 YOLEO(JJ)=YOLEO(JJ)-D(1)
  YDOLEO=-VEL(1)
  FA=FAO(JJ)*(EOLEO(JJ)/(EOLEO(JJ)-YOLEO(JJ)))*EXPLOE(JJ)-FAA(JJ)
  BDAMP=BOLEO(JJ)
  IF(YOLEO.LT.0) BDAMP=BOLEO(JJ)
  FH=BDAMP*YDOLEO*ABS(YDOLEO)
  ARGU=YDOLEO/ALPHAP
  FC=FCOUL(JJ)*TANH(ARGU)
  FCOMP=(YOLEO(JJ)-YMAX(JJ))*KCOMP(JJ)
  IF(FCOMP.LT.0.) FCOMP=0.
  FEXT=YOLEO(JJ)*KEXT(JJ)
  IF(FEXT.GT.0.) FEXT=0.
  FOLEO=FA+FH+FC+FEXT+FCOMP
  SUMDF(K,IJ)=FA+FCOMP+FEXT
  SUMDF(K,IJ)=SUMDF(K,IJ)
  FSJ(K)=SUMDF(K,IJ)
  FSI(K)=SUMDFI(K,IJ)
  FDI(K)=FH+FC
  FDJ(K)=-FDI(K)
  FINT(K,IJ)=FSJ(K)+FDJ(K)
  FINTI(K,IJ)=FSI(K)+FDI(K)
  630 CONTINUE

C
C STRESS CALCULATIONS
C
IF(NSC.EQ.0) GO TO 633
Z1,Z2,XIQ AND SYIELD DATA STORED IN SMALL ARRAYS, REFERENCED BY
NJ, WHICH VARIES FROM 1 TO NS. OTHER DATA STORED IN LARGE ARRAYS
FOR BEAM DATA, REFERENCED BY IJ, WHICH VARIES FROM 1 TO NB.
C

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ISM 0724
ISM 0726
ISM 0727
ISM 0729
ISM 0730
ISM 0731
ISM 0732
ISM 0733
ISM 0734
ISM 0735
ISM 0737
ISM 0738
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ISM 0740
ISM 0741
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ISM 0748
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ISM 0750
ISM 0751
ISM 0752
ISM 0753
ISM 0754
ISM 0755

ISM 0756

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C C C C C
C DETERMINE MAXIMUM BENDING MOMENTS ABOUT Y AND Z AXES.
C THESE COULD OCCUR AT EITHER END OF BEAM (I OR J).
C SHEAR FORCES AND AXIAL LOAD AND TORSION ARE CONSTANT ALONG BEAM.
C
501 FX = FINT(1,IJ)
FY = FINT(2,IJ)
FZ = FINT(3,IJ)
MX = FINT(4,IJ)
MYJ = FINT(5,IJ)
MZJ = FINT(6,IJ)
MYI = MYJ-XXLB*FZ
MZI = MZJ+XXLB*FY
MY = MYJ
MZ = MZJ
IF(PCR(IJ).NE.0.) GO TO 510
SBUCKR(IJ) = 0.
GO TO 512
510 SBUCKR(IJ)=FINT(1,IJ)/PCR(IJ)
512 IF(ABS(MYI).GT.ABS(MYJ)) MY = MYI
IF(ABS(MZI).GT.ABS(MZJ)) MZ = MZI
C C C C C
C CALCULATE AXIAL STRESSES (SX) AND SHEAR STRESSES (SS)
C FOR PLANE ELEMENTS LOCATED AT TOP,BOTTOM,RIGHT AND LEFT
C SIDES OF BEAM.
C
C IF YY(IJ),ZZ(IJ)=0 SXMY,SXMZ BLOW UP CODE TO BYPASS
C IF (YY(IJ).NE.0.) GO TO 502
SXY = 0.0
GO TO 507
502 SXMY = MY*Z1(IJ)/YY(IJ)
507 IF(ZZ(IJ).NE.0.) GO TO 503
SXMZ = 0.0
GO TO 504
503 SXMZ = MZ*Z2(IJ)/ZZ(IJ)
504 SSMX = MX*XI(IJ)
IF (AA(IJ).NE.0.) GO TO 505
SSFY = 0.0
SSFZ = 0.0
SXFY = 0.0
GO TO 506
505 SSFY = FY/AA(IJ)*1.5
SSFZ = FZ/AA(IJ)*1.5
SAFX = FX/AA(IJ)
C C C
C TOP (1)
C
506 SAX(1) = SXFX-SXMY
SS(1) = SSMX+SSFY
C C C
C BOTTOM (2)
C
SAX(2) = SXFX+SXMY

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ISN 0758
ISN 0759
ISN 0760
ISN 0761
ISN 0762
ISN 0763
ISN 0764
ISN 0765
ISN 0766
ISN 0767
ISN 0768
ISN 0770
ISN 0771
ISN 0772
ISN 0773
ISN 0775

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ISN 0777
ISN 0779
ISN 0780
ISN 0781
ISN 0782
ISN 0784
ISN 0785
ISN 0786
ISN 0787
ISN 0788
ISN 0790
ISN 0791
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ISN 0794
ISN 0795
ISN 0796

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ISN 0797
ISN 0798

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ISN 0799

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00009950
00009960
00009970
00009980
00009990
00010000
00010010
00010020
00010030
00010040
00010050
00010060
00010070
00010080
00010090
00010100
00010110
00010120
00010130
00010140
00010150
00010160
00010170
00010180
00010190
00010200
00010210
00010220
00010230
00010240
00010250
00010260
00010270
00010280
00010290
00010300
00010310
00010320
00010330
00010340
00010350
00010360
00010370
00010380
00010390
00010400
00010410
00010420
00010430
00010440
00010450
00010460
00010470

SS(2) = -SSHX+SSFY
C
C
LEFT (3)
C
SAX(3) = SXFX+XHZ
SS(3) = SSX-SSFZ
C
C
RIGHT (4)
C
C
SAX(4) = SXFX-XHZ
SS(4) = -SSX-SSFZ
C
C
NON,FOR EACH OF THE FOUR LOCATIONS,CALCULATE MAXIMUM SHEAR
C STRESS (SSH) AND PRINCIPAL STRESSES (S1,S2). USE THESE TO
C FORM RATIOS OF ACTUAL STRESS/FAILURE STRESS FOR TWO FAILURE
C CRITERIA.THE TWO CRITERIA USED ARE MAXIMUM SHEAR THEORY AND
C THEORY OF CONSTANT ENERGY OF DISTORTION. REFER TO ROARK,P.94,29.
C
DO 653 IS=1,4
SYIELD = STENS(MC(IJ))
IF(SAX(IS).LT.0.) SYIELD=SCOMP(MC(IJ))
SSM = SQRT(.25*SAX(IS)*SAX(IS)+SS(IS)*SS(IS))
S1 = .5*SAX(IS)+SSM
S2 = .5*SAX(IS)-SSM
SP = SQRT(S1*S1+S2*S2-S1*S2)
FRS(IJ,IS) = SSM/SHEAR(MC(IJ))
FRD(IJ,IS) = SP/SYIELD
653 CONTINUE
C*****COMPUTE THE ENERGY HERE BUT ADD IT AFTER 230 (NO RUPTURE)
633 SUMSEI = 0.0
SUMDEI = 0.0
SUMSEJ = 0.0
SUMDEJ = 0.0
SUMSE = 0.0
SUMDE = 0.0
C*****DON'T USE AN IJ IF IT'S A DRI ELEMENT
IF(IJPR(IJ).NE.0) GO TO 632
DO 631 K = 1,6
SUMSEI = SUMSEI + FSI(K)*DI(K)
SUMDEI = SUMDEI + FDI(K)*DI(K)
SUMSEJ = SUMSEJ + FSJ(K)*DJ(K)
SUMDEJ = SUMDEJ + FDJ(K)*DJ(K)
SUMSE = SUMSEI + SUMSEJ
SUMDE = SUMDEI + SUMDEJ
631 CONTINUE
C
C
C UPDATE DEFLECTIONS AND CHECK FOR RUPTURE. FIRST CORRECT Y AND Z
C DEFLECTIONS BY REMOVING COMPONENTS DUE TO ROTATION OF MASSES.
632 D(2) = D(2) - XXLB*D(9)/2.
D(3) = D(3) + XXLB*D(8)/2.
IJL = 6*(IJ-1)
DO 230 L = 1,6

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1500 0836 IJL = IJL+1
1500 0837 T = VEE(IJL)+D(L)
1500 0838 TF=FIN(T,L,IJ)
1500 0839 FEE(IJL)=TF
1500 0840 VEE(IJL) = T
1500 0841 IF(T) 240,250,250
1500 0842 240 IF(ABS(T)-VMAXN(IJL)) 251,260,260
1500 0843 250 IF(T-VMAXN(IJL)) 251,260,260
1500 0844 260 IRUPSH(IJ)=1
1500 0845 IF(T) 252,253,253
1500 0846 252 PRINT 1040,IJ,L,VEE(IJL),VMAXN(IJL),TIME
1500 0847 NDIR=-1
1500 0848 1040 FORMAT(IH1,'NEG.DIRECTION RUPTURE'//IX,'BEAM',2X,'DIRECTION',3X,
1500 0849 1 'MAGNITUDE',6X,'ALLOWABLE',6X,'TIME'//IX,I5,5X,I5,1P3E15.6)
1500 0850 GO TO 256
1500 0851 253 PRINT 1050,IJ,L,VEE(IJL),VMAXN(IJL),TIME
1500 0852 NDIR=1
1500 0853 1050 FORMAT(IH1,'POS.DIRECTION RUPTURE'//IX,'BEAM',2X,'DIRECTION',3X,
1500 0854 1 'MAGNITUDE',6X,'ALLOWABLE',6X,'TIME'//IX,I5,5X,I5,1P3E15.6)
1500 0855 GO TO 256
1500 0856 251 IF(TF) 274,271,271
1500 0857 274 IF(ABS(TF)-FMAXN(IJL)) 230,255,255
1500 0858 271 IF(TF-FMAXN(IJL)) 230,255,255
1500 0859 255 IRUPSH(IJ)=1
1500 0860 IF(TF) 272,273,273
1500 0861 272 PRINT 1040,IJ,L,FEE(IJL),FMAXN(IJL),TIME
1500 0862 NDIR=-1
1500 0863 GO TO 256
1500 0864 273 PRINT 1050,IJ,L,FEE(IJL),FMAXN(IJL),TIME
1500 0865 NDIR=1
1500 0866 C CALCULATE STUFF FOR YIELDING AND RUPTURE SUMMARY TABLE,
1500 0867 C (RUPTURE ONLY HERE).
1500 0868 C
1500 0869 256 KRCONT = KRCONT+1
1500 0870 TKR(KRCONT) = TIME
1500 0871 KRBEAM(1,KRCONT) = IJ
1500 0872 KRBEAM(3,KRCONT) = L
1500 0873 KRBEAM(4,KRCONT)=NDIR
1500 0874 GO TO 1000
1500 0875 230 CONTINUE
1500 0876 SEIJ(IJ) = SEIJ(IJ)+SUMSE
1500 0877 DEIJ(IJ) = DEIJ(IJ)+SUMDE
1500 0878 C SUM OVER BOTH TIME AND BEAMS.
1500 0879 C
1500 0880 C
1500 0881 XSE(I) = XSE(I) + SUMSEI
1500 0882 XDE(I) = XDE(I) + SUMDEI
1500 0883 IF(IJ.NE.81) GO TO 280
1500 0884 C FOR TRANSVERSE BEAMS, ADD ENERGY AT J=81 END OF BEAM TO I MASS.
1500 0885 C
1500 0886 C
1500 0887 XSE(I) = XSE(I) + SUMSEJ

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1304 0878 XDE(I) = XDE(I) + SUMDEJ
1304 0879 GO TO 282
1304 0880 280 XSE(J) = XSE(J) + SUMSEJ
1304 0881 XDE(J) = XDE(J) + SUMDEJ
C
C FOR A SYMMETRICAL MODEL WE MUST ADD SE AND DE CONTRIBUTIONS
C FROM THE OPPOSITE BEAMS THAT ARE NOT INPUT EXPLICITLY. WE
C DO NOT DO THIS FOR TRANSVERSE BEAMS OR THOSE ON THE
C AIRPLANE CL.
C
1304 0882 282 IF(SYMF LG.NE.1.OR.J.EQ.81.OR.CLTEST(IJ).EQ.1.) GO TO 238
1304 0883 SEI(IJ) = SEI(IJ)+SUMSE
1304 0884 DEI(IJ) = DEI(IJ)+SUMDE
1304 0885 XSE(I) = XSE(I) + SUMSEI
1304 0886 XSE(J) = XSE(J) + SUMSEJ
1304 0887 XDE(I) = XDE(I) + SUMDEI
1304 0888 XDE(J) = XDE(J) + SUMDEJ
1304 0889 238 IF (IJPR(IJ).NE.0) DRI(IJ) = -6.55D0*VEE(6*(IJ-1)+1)
C
C NOW ADD FSI AND FDI AND CALL IT FSI. SAME AT J. WE NO
C LONGER NEED SEPARATE STRAIN AND DAMPING FORCES.
C
1304 0892 DO 270 J2=1,6
1304 0893 FSI(J2) = FSI(J2) + FDI(J2)
1304 0894 FSJ(J2) = FSJ(J2) + FDJ(J2)
1304 0895 270 CONTINUE
C
C CONVERT BEAM FORCES TO MASS AXES AND REVERSE SIGNS TO GET
C FORCES ACTING ON MASSES. USE TRANSPOSE OF AIJTAJ OR AIJTAI.
C
1304 0906 IF (IJPR(IJ).NE.0) GO TO 6210
1304 0907 T1 = -FSI(1)
1304 0908 T2 = -FSI(2)
1304 0909 T3 = -FSI(3)
1304 0910 FSI(1) = AIJTAI(1)*T1+AIJTAI(2)*T2+AIJTAI(3)*T3
1304 0911 FSI(2) = AIJTAI(4)*T1+AIJTAI(5)*T2+AIJTAI(6)*T3
1304 0912 FSI(3) = AIJTAI(7)*T1+AIJTAI(8)*T2+AIJTAI(9)*T3
1304 0913 T1 = -FSI(4)
1304 0914 T2 = -FSI(5)
1304 0915 T3 = -FSI(6)
1304 0916 FSI(4) = AIJTAI(1)*T1+AIJTAI(2)*T2+AIJTAI(3)*T3
1304 0917 FSI(5) = AIJTAI(4)*T1+AIJTAI(5)*T2+AIJTAI(6)*T3
1304 0918 FSI(6) = AIJTAI(7)*T1+AIJTAI(8)*T2+AIJTAI(9)*T3
1304 0919 6210 IF(J.EQ.81) GO TO 6200
1304 0920 T1 = -FSJ(1)
1304 0921 T2 = -FSJ(2)
1304 0922 T3 = -FSJ(3)
1304 0923 FSJ(1) = AIJTAJ(1)*T1+AIJTAJ(2)*T2+AIJTAJ(3)*T3
1304 0924 FSJ(2) = AIJTAJ(4)*T1+AIJTAJ(5)*T2+AIJTAJ(6)*T3
1304 0925 FSJ(3) = AIJTAJ(7)*T1+AIJTAJ(8)*T2+AIJTAJ(9)*T3
1304 0926 T1 = -FSJ(4)
1304 0927 T2 = -FSJ(5)
1304 0928 T3 = -FSJ(6)
1304 0929
1304 0930
1304 0931
1304 0932
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1304 0921      FSJ(4) = AIJTAJ(3)*T1+AIJTAJ(2)*T2+AIJTAJ(1)*T3
1304 0922      FSJ(5) = AIJTAJ(4)*T1+AIJTAJ(5)*T2+AIJTAJ(6)*T3
1304 0923      FSJ(6) = AIJTAJ(7)*T1+AIJTAJ(8)*T2+AIJTAJ(9)*T3
1304 0924      6200 CONTINUE
C
C      TO GET THE BEAM MOMENTS AT MASS J, WE MUST ACCOUNT FOR THE
C      MOMENTS DUE TO THE BEAM FORCES AT NODE POINT (J,N), WHICH
C      IS OFFSET FROM MASS J BY THE VECTOR (RX,RY,RZ). THESE VECTOR
C      ELEMENTS ARE SUBSCRIPTED BY NODE POINT, FROM 1 TO NNP, AND
C      ARE IN MASS J AXES.
C      IF(N.EQ.0.OR.J.EQ.61) GO TO 3410
C
C      MOMENTS AT J, MASS J AXES.
C
1304 0925      FSJ(4) = FSJ(4) + FSJ(3)*RY(JJ) - FSJ(2)*RZ(JJ)
1304 0926      FSJ(5) = FSJ(5) - FSJ(3)*RX(JJ) + FSJ(1)*RZ(JJ)
1304 0927      FSJ(6) = FSJ(6) + FSJ(2)*RX(JJ) - FSJ(1)*RY(JJ)
1304 0928      3410 CONTINUE
C
C      MOMENTS AT I, MASS I AXES. SKIP FOR DRI ELEMENTS.
C
1304 0929      IF(IJPR(IJ).NE.0) GO TO 264
1304 0930      IF(M.EQ.0) GO TO 266
1304 0931      FSI(4) = FSI(4) + FSI(3)*RY(JI) - FSI(2)*RZ(JI)
1304 0932      FSI(5) = FSI(5) - FSI(3)*RX(JI) + FSI(1)*RZ(JI)
1304 0933      FSI(6) = FSI(6) + FSI(2)*RX(JI) - FSI(1)*RY(JI)
1304 0934      GO TO 266
1304 0935      264 DO 265 JJJ=1,6
1304 0936      FSI(JJJ) = 0.
1304 0937      265 CONTINUE
C
C      FOR SYMFLG = 1., WE LATER DOUBLE ALL XZ AND M INTERNAL
C      AND DAMPING LOADS ACTING ON A MASS ON THE AIRPLANE
C      PLANE OF SYMMETRY. SINCE WE DO THIS FOR ALL BEAMS,
C      HERE WE MUST HALVE THE LOADS FOR BEAMS THAT LIE
C      ENTIRELY IN THE PLANE OF SYMMETRY, SINCE THESE LOADS
C      SHOULD NOT BE DOUBLED. CLTEST(IJ) IS NE ZERO FOR THIS
C      CONDITION.
C
1304 0938      266 CONTINUE
1304 0939      IF(SYMFLG.NE.1.OR.CLTEST(IJ).EQ.0.) GO TO 5001
1304 0940      DO 5002 JJJ=1,6
1304 0941      FSJ(JJJ) = FSJ(JJJ)/2.
1304 0942      FSI(JJJ) = FSI(JJJ)/2.
1304 0943      5002 CONTINUE
C
C      NOW SUM FORCES AT MASSES I AND J. SUMMING OVER BEAMS.
C
1304 0944      5001 XX(I) = XX(I) + FSI(1)
1304 0945      XY(I) = XY(I) + FSI(2)
1304 0946      XZ(I) = XZ(I) + FSI(3)
1304 0947      XL(I) = XL(I) + FSI(4)
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1000 01453  XN(I) = XN(I) + FSI(5)
1000 01454  XN(I) = XN(I) + FSI(6)
1000 01455  IF(I.EQ.81) GO TO 1000
1000 01457  XX(J) = XX(J) + FSJ(1)
1000 01458  XY(J) = XY(J) + FSJ(2)
1000 01459  XZ(J) = XZ(J) + FSJ(3)
1000 01460  XL(J) = XL(J) + FSJ(4)
1000 01461  XN(J) = XN(J) + FSJ(5)
1000 01462  XN(J) = XN(J) + FSJ(6)
1000 01463  1000 CONTINUE
C
C      END OF MAIN INTERNAL BEAM IJ LOOP.
C
      IS=9*(MVP-1)
      DO 1010 KS=1,9
      IS=IS+1
1010 01464  API(KS)=BIJ(IS)
C      FINISH COMPUTING DERIVATIVES
C      SET COUNTER=0 FOR ACCEL PULSE
      NPTS=0
      NPTS=0
      DO 2000 I = 1,NM
      IS = 9*(I-1)
      DO 330 KS = 1,9
      IS = IS+1
      AI(OT(KS)) = CIJ(IS)
330 01465  AI(KS) = BIJ(IS)
C      DO CRASH FORCES
      DO 460 JI=1,6
      XC(JI) = 0.
460 01466  CONTINUE
      DO 340 IKH=1,NSP
      IF(I.EQ.II(IKH)) GO TO 400
340 01467  CONTINUE
      GO TO 440
400 01468  CALL CFORCE
C      (20),(23),(24)
440 01469  XA = HGT(I)-ALIFT(I)*WTOT
      SX = XX(I)+XA*AI(3)+XC(1)
      SY = XY(I)+XA*AI(6)+XC(2)
      SZ = XZ(I)+XA*AI(9)+XC(3)
      SL = XL(I)+XC(4)
      SM = XM(I)+XC(5)
      SN = XN(I)+XC(6)
C
C      IF WE HAVE A SYMMETRIC CASE (SYMFLG.NE.0) AND THE MASS WE ARE
C      CONSIDERING IS ON THE AIRPLANE CENTERLINE (YDP(I)=0), THEN WE
C      MUST CORRECT THE TOTAL FORCES AND MOMENTS TO ACCOUNT FOR THE
C      BEAMS ON THE OTHER SIDE, NOT CALCULATED, THAT CONNECT TO THIS MASS.
C
      IF(SYMFLG.EQ.0.OR.YDP(I).NE.0.) GO TO 1011
      SY = 0.
      SL = 0.
1000 01470  00012070
1000 01471  00012080
1000 01472  00012090
1000 01473  00012100
1000 01474  00012110
1000 01475  00012120
1000 01476  00012130
1000 01477  00012140
1000 01478  00012150
1000 01479  00012160
1000 01480  00012170
1000 01481  00012180
1000 01482  00012190
1000 01483  00012200
1000 01484  00012210
1000 01485  00012220
1000 01486  00012230
1000 01487  00012240
1000 01488  00012250
1000 01489  00012260
1000 01490  00012270
1000 01491  00012280
1000 01492  00012290
1000 01493  00012300
1000 01494  00012310
1000 01495  00012320
1000 01496  00012330
1000 01497  00012340
1000 01498  00012350
1000 01499  00012360
1000 01500  00012370
1000 01501  00012380
1000 01502  00012390
1000 01503  00012400
1000 01504  00012410
1000 01505  00012420
1000 01506  00012430
1000 01507  00012440
1000 01508  00012450
1000 01509  00012460
1000 01510  00012470
1000 01511  00012480
1000 01512  00012490
1000 01513  00012500
1000 01514  00012510
1000 01515  00012520
1000 01516  00012530
1000 01517  00012540
1000 01518  00012550
1000 01519  00012560
1000 01520  00012570
1000 01521  00012580
1000 01522  00012590

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1300 8996      SN = 0.
1300 8997      IF(SYMFLG.EQ.2.) GO TO 1011
1300 8998      SX = SX+XX(I)
1300 8999      SZ = SZ+XZ(I)
1300 9000      SM = SM+XM(I)
1300 9001
1300 9002      C GET P,Q,R,U,V,W
1300 9003      1011 PP = P(I)
1300 9004      QQ = Q(I)
1300 9005      RR = R(I)
1300 9006      UU = U(I)
1300 9007      VV = V(I)
1300 9008      WW = W(I)
1300 9009
1300 9010      C MASS
1300 9011      ZH=366.0/MST(I)
1300 9012      IF(TIME.NE.0.) GO TO 343
1300 9013      XACF(I) = XACC(I)
1300 9014      YACF(I) = YACC(I)
1300 9015      ZACF(I) = ZACC(I)
1300 9016
1300 9017      C TEMP CALCS
1300 9018      XACF(I)=0.
1300 9019      YACF(I)=0.
1300 9020      ZACF(I)=0.
1300 9021
1300 9022      C (25)
1300 9023      343 UDOTI = UDOT(I)
1300 9024      VDOTI = VDOT(I)
1300 9025      WDOTI = WDOT(I)
1300 9026      UDOT(I)=SX*ZH-QQ*MM+RR*VV
1300 9027      VDOT(I)=SY*ZH-RR*UU+PP*WW
1300 9028      WDOT(I)=SZ*ZH-PP*VV+QQ*UU
1300 9029      IF(NACC.EQ.0) GO TO 341
1300 9030      CALL ACCELTI,UDOT(I),VDOT(I),WDOT(I),PDOT(I),QDOT(I),RDOT(I),
1300 9031      1TIME,NPTSP,NPTS)
1300 9032      NPTSP=NPTS
1300 9033      341 XACCI(I)=(UDOT(I)+QQ*MM-RR*VV)/366.
1300 9034      YACCI(I)=(VDOT(I)+RR*UU-PP*WW)/366.
1300 9035      ZACCI(I)=(WDOT(I)+PP*VV-QQ*UU)/366.
1300 9036      XACFDI = XACFI(I)
1300 9037      YACFDI = YACFI(I)
1300 9038      ZACFDI = ZACFI(I)
1300 9039      IF(PFIL.EQ.0.) GO TO 344
1300 9040      XACFD(I) = (XACCI(I)-XACFI(I))/PFIL
1300 9041      YACFD(I) = (YACCI(I)-YACFI(I))/PFIL
1300 9042      ZACFD(I) = (ZACCI(I)-ZACFI(I))/PFIL
1300 9043      GO TO 345
1300 9044      344 XACFD(I) = 0.
1300 9045      YACFD(I) = 0.
1300 9046      ZACFD(I) = 0.
1300 9047
1300 9048      C (26)
1300 9049      345 T1 = -XZI(I)*PP-YZI(I)*QQ+ZI(I)*RR+HEZ(I)
1300 9050      T2 = XII(I)*PP-XVI(I)*QQ-XZI(I)*RR+HEX(I)
1300 9051      T3 = -XVI(I)*PP+YI(I)*QQ-YZI(I)*RR+HEY(I)
1300 9052      SL = SL-QQ*T1+RR*T3
1300 9053      SM = SM-RR*T2+PP*T1
1300 9054
1300 9055      00012600
1300 9056      00012610
1300 9057      00012620
1300 9058      00012630
1300 9059      00012640
1300 9060      00012650
1300 9061      00012660
1300 9062      00012670
1300 9063      00012680
1300 9064      00012690
1300 9065      00012700
1300 9066      00012710
1300 9067      00012720
1300 9068      00012730
1300 9069      00012740
1300 9070      00012750
1300 9071      00012760
1300 9072      00012770
1300 9073      00012780
1300 9074      00012790
1300 9075      00012800
1300 9076      00012810
1300 9077      00012820
1300 9078      00012830
1300 9079      00012840
1300 9080      00012850
1300 9081      00012860
1300 9082      00012870
1300 9083      00012880
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1300 9086      00012910
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1300 9088      00012930
1300 9089      00012940
1300 9090      00012950
1300 9091      00012960
1300 9092      00012970
1300 9093      00012980
1300 9094      00012990
1300 9095      00013000
1300 9096      00013010
1300 9097      00013020
1300 9098      00013030
1300 9099      00013040
1300 9100      00013050
1300 9101      00013060
1300 9102      00013070
1300 9103      00013080
1300 9104      00013090
1300 9105      00013100
1300 9106      00013110
1300 9107      00013120

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1000 1864.7      SN = SN-PP*T3+QQ*T2
C (25)
      DEL = DEL(I)
      PDOTI = PDOT(I)
      PDOT(I) = DEL*(SL*XI1(I)+SH*XI2(I)+SN*XI3(I))
      QDOT(I) = QDOT(I)
      QDOT(I) = DEL*(SL*XI2(I)+SH*XI5(I)+SN*XI4(I))
      RDOT(I) = RDOT(I)
      RDOT(I) = DEL*(SL*XI3(I)+SH*XI4(I)+SN*XI6(I))
      FOR A SYMMETRICAL CASE,CONSTRAIN THE ACCELERATIONS OF THE
      CENTERLINE MASSES.
C
C
      IF(SYMPFLG.EQ.0.OR.YDP(I).NE.0.) GO TO 342
      VDOT(I) = 0.
      PDOT(I) = 0.
      RDOT(I) = 0.
      XDOTI = XDOT(I)
      YDOTI = YDOT(I)
      ZDOTI = ZDOT(I)
      PHDOTI = PHIDOT(I)
      THDOTI = THEDOT(I)
      PSIDOTI = PSIDOT(I)
      IF(TIME) 1900,1900,300
C
C
      ...VARIABLE INTEGRATION ADDED 11/09/77 DHS...
C
      UP = U(I)
      UI = TT*U(I)+ET*(UOLD(I)+DTHALF*(UDOT(I)+UDOTI))
      ERR = AMAX1(ERR,
      1/(ABS(UDOT(I))-UDOTI)*DELTA1/
      2  AMAX1(ABS(UOLD(I))+ABS(U(I))-UOLD(I)),1.D-06))
C
      VP = V(I)
      VI = TT*V(I)+ET*(VOLD(I)+DTHALF*(VDOT(I)+VDOTI))
      ERR = AMAX1(ERR,
      1/(ABS(VDOT(I))-VDOTI)*DELTA1/
      2  AMAX1(ABS(VOLD(I))+ABS(V(I))-VOLD(I)),1.D-06))
C
      WP = W(I)
      WI = TT*W(I)+ET*(WOLD(I)+DTHALF*(WDOT(I)+WDOTI))
      ERR = AMAX1(ERR,
      1/(ABS(WDOT(I))-WDOTI)*DELTA1/
      2  AMAX1(ABS(WOLD(I))+ABS(W(I))-WOLD(I)),1.D-06))
C
      PP = P(I)
      PI = TT*P(I)+ET*(POLD(I)+DTHALF*(PDOT(I)+PDOTI))
      ERR = AMAX1(ERR,
      1/(ABS(PDOT(I))-PDOTI)*DELTA1/
      2  AMAX1(ABS(POLD(I))+ABS(P(I))-POLD(I)),1.D-06))
C
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AD-A055 898

LOCKHEED-CALIFORNIA CO BURBANK

GENERAL AVIATION AIRPLANE STRUCTURAL CRASHWORTHINESS USER'S MAN--ETC(U)

FEB 78 M A GAMON

DOT-FA75WA-3707

UNCLASSIFIED

LR-28307

FAA/RD-77/189-VOL-1

NL

3 OF 7
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C
C
ISN 1079      QP = Q(I)
ISN 1080      Q(I) = TT*Q(I)+ET*(QOLD(I)+DTHALF*(QDOT(I)+QDOTI))
ISN 1081      ERR = AMAX1(ERR,
1(ABS(QDOT(I)-QDOTI)*DELTA)/
2  ANAX1(ABS(QOLD(I))+ABS(Q(I)-QOLD(I)),1.D-06))

C
C
ISN 1082      RP = R(I)
ISN 1083      R(I) = TT*R(I)+ET*(ROLD(I)+DTHALF*(RDOT(I)+RDOTI))
ISN 1084      ERR = AMAX1(ERR,
1(ABS(RDOT(I)-RDOTI)*DELTA)/
2  ANAX1(ABS(ROLD(I))+ABS(R(I)-ROLD(I)),1.D-06))

C
C
C CHANGE ERR DEFINITION FOR ENERGY BASED VARIABLE DT SCHEME.
C
C
ISN 1085      IF(IVAR.EQ.2) ERR=DEVMAX*THAX/TIME
ISN 1087      XI(I) = TT*X(I)+ET*(XOLD(I)+DTHALF*(XDOT(I)+XDOTI))
ISN 1088      Y(I) = TT*Y(I)+ET*(YOLD(I)+DTHALF*(YDOT(I)+YDOTI))
ISN 1089      Z(I) = TT*Z(I)+ET*(ZOLD(I)+DTHALF*(ZDOT(I)+ZDOTI))
ISN 1090      PHI(I) = TT*PHI(I)+ET*(PHIOLD(I)+DTHALF*(PHIDOT(I)+PHIDOTI))
ISN 1091      THETA(I) = TT*THETA(I)+ET*(THEOLD(I)+DTHALF*(THEDOT(I)+THEDOTI))
ISN 1092      PSI(I) = TT*PSI(I)+ET*(PSIOLD(I)+DTHALF*(PSIDOT(I)+PSIDOTI))
ISN 1093      PIN(I) = TT*PIN(I)+ET*(PINOLD(I)+DTHALF*(PIDOT(I)+PIDOTI))
ISN 1094      QIN(I) = TT*QIN(I)+ET*(QINOLD(I)+DTHALF*(QIDOT(I)+QIDOTI))
ISN 1095      RIN(I) = TT*RIN(I)+ET*(RINOLD(I)+DTHALF*(RIDOT(I)+RIDOTI))

C
C
C XACI ETC ARE MASS IMPULSE CALCS 2-5-79
C
ISN 1096      XACI=XACF(I)
ISN 1097      YACI=YACF(I)
ISN 1098      ZACI=ZACF(I)
ISN 1099      XACF(I) = TT*XACF(I)+ET*(XAFOLD(I)+DTHALF*(XACFD(I)+XACFDI))
ISN 1100      YACF(I) = TT*YACF(I)+ET*(YAFOLD(I)+DTHALF*(YACFD(I)+YACFDI))
ISN 1101      ZACF(I) = TT*ZACF(I)+ET*(ZAFOLD(I)+DTHALF*(ZACFD(I)+ZACFDI))
ISN 1102      XIMP(I)=TT*XIMP(I)+ET*(XIMPOLD(I)+DTHALF*(XIMPD(I)+XIMPDI))
ISN 1103      YIMP(I)=TT*YIMP(I)+ET*(YIMPOLD(I)+DTHALF*(YIMPD(I)+YIMPDI))
ISN 1104      ZIMP(I)=TT*ZIMP(I)+ET*(ZIMPOLD(I)+DTHALF*(ZIMPD(I)+ZIMPDI))
ISN 1105      IF ((IPENSW(I).NE.0).OR.(I.EQ.MVP).OR.(MVP.EQ.0)) GO TO 1900

C
C
C CONTROL VOLUME PENETRATION CALCULATIONS
C
ISN 1107      TP1=X(I)-X(MVP)
ISN 1108      TP2=Y(I)-Y(MVP)
ISN 1109      TP3=Z(I)-Z(MVP)
ISN 1110      XPI=API(1)*TP1+API(2)*TP2+API(3)*TP3
ISN 1111      YPI=API(4)*TP1+API(5)*TP2+API(6)*TP3
ISN 1112      ZPI=API(7)*TP1+API(8)*TP2+API(9)*TP3
ISN 1113      IF ((-XNBAR.GT.XPI).OR.(XPI.GT.XPBAR)) GO TO 1900
ISN 1115      IF ((-YNBAR.GT.YPI).OR.(YPI.GT.YPBAR)) GO TO 1900
ISN 1117      IF ((-ZNBAR.GT.ZPI).OR.(ZPI.GT.ZPBAR)) GO TO 1900
ISN 1119      KPEN=KPEN+1

```

```

ISN 1120 IPEN(KPEN)=I
ISN 1121 TPEN(KPEN)=TIME
ISN 1122 IPENSW(I)=1
ISN 1123 PRINT 1080, I, TIME
ISN 1124 1080 FORMAT(1H0, ' CONTROL VOLUME PENETRATED BY MASS ', I2, ', TIME=',
1 F10.5)

C
C ZERO XCE AND XFE FOR ALL I'S PRIOR TO ENERGY CALCS BELOW.
C
1900 XCE(I) = 0.
XFE(I) = 0.
2000 CONTINUE
IF(NNP.EQ.0) GO TO 2008

C NOW CALCULATE THE VELOCITIES AND ACCELERATIONS OF THE NODE
C POINTS. THESE ARE USED ONLY FOR OUTPUT DATA.
C
DO 4000 J=1,NNP
I = INP(J)
OMCRX = -R(I)*RY(J)+Q(I)*RZ(J)
OMCRY = R(I)*RX(J)-P(I)*RZ(J)
OMCRZ = -Q(I)*RX(J)+P(I)*RY(J)
OMCCRZ = -R(I)*OMCRY+Q(I)*OMCRZ
OMCCRY = R(I)*OMCRX-P(I)*OMCRZ
OMCCRX = -Q(I)*OMCRX+P(I)*OMCRY
UNP(J) = U(I)+OMCRX
VNP(J) = V(I)+OMCRY
WNP(J) = W(I)+OMCRZ
IS = 9*(I-1)
DO 4010 KS=1,9
IS = IS+1
AI(KS) = BIJ(IS)
CONTINUE
TX = AI(1)*RX(I)+AI(4)*RY(J)+AI(7)*RZ(J)
TY = AI(2)*RX(I)+AI(5)*RY(J)+AI(8)*RZ(J)
TZ = AI(3)*RX(I)+AI(6)*RY(J)+AI(9)*RZ(J)
XNP(J) = X(I)+TX
YNP(J) = Y(I)+TY
ZNP(J) = Z(I)+TZ
XONP(J) = AI(1)*UNP(J)+AI(4)*VNP(J)+AI(7)*WNP(J)
YONP(J) = AI(2)*UNP(J)+AI(5)*VNP(J)+AI(8)*WNP(J)
ZONP(J) = AI(3)*UNP(J)+AI(6)*VNP(J)+AI(9)*WNP(J)
ACX = -ROOT(I)*RY(J)+QOOT(I)*RZ(J)
ACY = ROOT(I)*RX(J)-POOT(I)*RZ(J)
ACZ = -QOOT(I)*RX(J)+POOT(I)*RY(J)
XACCNPI(J) = XACC(I)+(ACX+OMCCRX)/386.
YACCNPI(J) = YACC(I)+(ACY+OMCCRY)/386.
ZACCNPI(J) = ZACC(I)+(ACZ+OMCCRZ)/386.
IF(TIME.NE.0.) GO TO 4020
XACNPF(J) = XACCNPI(J)
YACNPF(J) = YACCNPI(J)
ZACNPF(J) = ZACCNPI(J)
4020 XNPFDJ = XNPFD(J)

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ISN 1167 YNPFJ = YNPFJ(J)
ISN 1168 ZNPFJ = ZNPFJ(J)
ISN 1169 IF (PFIL.EQ.0.) GO TO 4030
ISN 1170 YNPFJ(J) = (XACNPI(J)-ZACNPF(J))/PFIL
ISN 1171 YNPFJ(J) = (YACNPI(J)-ZACNPF(J))/PFIL
ISN 1172 ZNPFJ(J) = (ZACNPI(J)-ZACNPF(J))/PFIL
ISN 1173 GO TO 4050
ISN 1174
ISN 1175 4030 YNPFJ(J) = 0.
ISN 1176 YNPFJ(J) = 0.
ISN 1177 ZNPFJ(J) = 0.
ISN 1178 4050 IF (TIME) 4000,4000,4040
C XACNPI,XINPI(I) ETC ARE MASS NODE POINT IMPULSE CALCS 2-5-79
C
ISN 1179 4040 XACNPI=XACNPF(J)
ISN 1180 YACNPI=YACNPF(J)
ISN 1181 ZACNPI=ZACNPF(J)
ISN 1182 XACNPF(J)=TT*XACNPI(J)+ET*(XACNPF(J)+DTHALF*(XNPFJ(J)+XNPFJ(J))
ISN 1183 YACNPF(J)=TT*YACNPF(J)+ET*(YACNPF(J)+DTHALF*(YNPFJ(J)+YNPFJ(J))
ISN 1184 ZACNPF(J)=TT*ZACNPF(J)+ET*(ZACNPF(J)+DTHALF*(ZNPFJ(J)+ZNPFJ(J))
ISN 1185 XINPI(J)=TT*XINPI(J)+ET*(XINPI(J)+DTHALF*(XACNPF(J)
1 *XACNPI))
ISN 1186 YINPI(J)=TT*YINPI(J)+ET*(YINPI(J)+DTHALF*(YACNPF(J)
1 *YACNPI))
ISN 1187 ZINPI(J)=TT*ZINPI(J)+ET*(ZINPI(J)+DTHALF*(ZACNPF(J)
1 *ZACNPI))
ISN 1188 4000 CONTINUE
C
C ...CHECK INTEGRATION ERROR AND VARY DELTAT IF NECESSARY...
C
ISN 1189 2008 CONTINUE
ISN 1190 IF (IVAR.EQ.0) GO TO 2010
ISN 1191 IF (TIME) 2010,2010,2015
ISN 1192 2015 DELTA = 0.
ISN 1193 DT2 = 2. * DELTAT
ISN 1194 IF (ERR.LT.EL) DELTA = RATHMAX
ISN 1195 IF ((ERR.GT.EU) .AND. (DELTAT.GT. MINDT)) DELTA = RATHIN
ISN 1196 IF ((DELTA.EQ.0.) .AND. (IPC.EQ.1)) DELTA = 1.0
ISN 1197 IF (DELTA.EQ.0.) GO TO 2010
ISN 1201 IF (IPC.NE.1.) GO TO 2019
ISN 1203 TREL = DMOD(TIME+DELTAT,TPRINT)
ISN 1205 TLEFT = TPRINT - TREL
ISN 1206 MPTSP = (TLEFT/DELTAT) + .5
ISN 1207 DELT1 = TLEFT / MPTSP
ISN 1208 IPPINI = MPTSP + IPC + 1
ISN 1209 GO TO 2018
ISN 1210 2019 MPTS = IPPINI - IPC
ISN 1211 IF ((MPTS.EQ.0) .OR. (MPTS.EQ.1)) GO TO 2010
ISN 1212 TREL = DMOD(TIME+DELTAT,TPRINT)
ISN 1214 TLEFT = TPRINT - TREL
ISN 1215 MPTSP = ((MPTS-1)/DELTA) + .5
ISN 1216 DELT1 = TLEFT / MPTSP
ISN 1217 IPPINI = IPC + MPTSP + 1
ISN 1218 DTX = DELT1 - DELTAT
ISN 1219 2016

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```

ISN 1220 IF (DTX - EQ. 0.) GO TO 2010
ISN 1222 TIME1 = TIME
ISN 1223 DT2 = DELTAT + DELT1
ISN 1224 DELTAT = DELT1
ISN 1225 DTHALF = .5 * DELTAT
ISN 1226 IPRINT = IPRINI
00015250
00015260
00015270
00015280
00015290
00015300
00015310
00015320
00015330
00015340
00015350
00015360
00015370
00015380
00015390
00015400
00015410
00015420
00015430
00015440
00015450
00015460
00015470
00015480
00015490
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00015590
00015600
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00015620
00015630
00015640
00015650
00015660
00015670
00015680
00015690
00015700
00015710
00015720
00015730
00015740
00015750
00015760
00015770

C
C ENERGY CALCULATIONS BY MASS. CEIK AND CEIKF ALREADY SUMMED OVER
C TIME. NOW SUM OVER SPRINGS FOR GIVEN MASS.
C
2010 DO 2011 IKM=1,NSP
I = II(IKM)
XCE(I) = XCE(I) + CEIK(IKM)
XFE(I) = XFE(I) + CEIKF(IKM)
2011 CONTINUE
C
C SET ZINIT(I)=Z(I) AT TIME=0
C
IF (TIME - NE. 0.) GO TO 2012
DO 2014 I=1,NM
ZINIT(I)=Z(I)
2014 CONTINUE
2012 XETOTL = 0.
KETOTL = 0.
PETOTL = 0.
SETOTL = 0.
DETOTL = 0.
FETOTL = 0.
DEVMAX = 0.
DO 2016 I = 1,NM
C*****DON'T USE AN I IF IT'S = TO A J OF A DRI I,J PAIR
DO 2017 IJ = 1,NB
IF (IJPR(IJ) - EQ. 0) GO TO 2017
IF (I.NE.JG(IJ)) GO TO 2017
PEI(I) = 0.0
KEI(I) = 0.0
GO TO 2020
2017 CONTINUE
PEI(I) = -MGT(I)*Z(I)+ALIFT(I)*MTOT*(Z(I)-ZINIT(I))
KEI(I) = .5*(MGT(I)*(U(I)*U(I)+V(I)*V(I)+W(I)*W(I))/386.0
1 +P(I)*P(I)+X(I)*Q(I)+XY(I)*R(I)*XZ(I))
2 +Q(I)*P(I)+X(I)*Q(I)+Y(I)*R(I)+Y(I)*YZ(I))
3 +R(I)*P(I)+XZ(I)*Q(I)+YZ(I)*R(I)+Z(I))
C
C FOR A SYMMETRICAL MODEL WE MUST ADD KE AND PE CONTRIBUTIONS
C FROM THE OPPOSITE MASSES THAT ARE NOT INPUT EXPLICITLY.
C
IF (SYMFLG.NE.1.OR.YDP(I).EQ.0.) GO TO 2020
PEI(I) = 2.*PEI(I)
KEI(I) = 2.*KEI(I)
2020 XETOT(I) = KEI(I)+PEI(I)+XSE(I)+XDE(I)+XCE(I)+XFE(I)
C
ISN 1227
ISN 1228
ISN 1229
ISN 1230
ISN 1231
ISN 1232
ISN 1234
ISN 1235
ISN 1236
ISN 1237
ISN 1238
ISN 1239
ISN 1240
ISN 1241
ISN 1242
ISN 1243
ISN 1244
ISN 1245
ISN 1246
ISN 1247
ISN 1249
ISN 1251
ISN 1252
ISN 1253
ISN 1254
ISN 1255
ISN 1256
ISN 1257
ISN 1259
ISN 1260
ISN 1261

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C      C      SUM OVER MASSES TO CHECK WITH OTHER ENERGY PRINT.
C      C      KETOTL = KETOTL + KEI(I)
C      C      PETOTL = PETOTL + PEI(I)
C      C      SETOTL = SETOTL + XSE(I)
C      C      DETOTL = DETOTL + XDE(I)
C      C      CETOTL = CETOTL + XCE(I)
C      C      FETOTL = FETOTL + XFE(I)
C      C      XETOTL = XETOTL + XETOT(I)
C      C      IF(IME.NE.0.) GO TO 2024
C      C      XETOT(I) = XETOT(I)
C      C      2024 IF(XETOT(I).NE.0) GO TO 2022
C      C      XPCT(I) = 100.
C      C      GO TO 2030
C      C      2022 XPCT(I) = XETOT(I)/XETOT(I)*100.
C      C      2030 DEV = ABS(XPCT(I)-100.)
C      C      DEVMAX = AMAX1(DEVMAX,DEV)
C      C      2016 CONTINUE
C      C      C      VOLUME CHANGE CALCULATIONS
C      C      IF(NVCH) 2001,2001,2002
C      C      2002 FLIP = 0.
C      C      DO 2003 MI=1,NVCH
C      C      VOL(MI) = 1.
C      C      DO 2004 I=1,6
C      C      SUMX = 0.
C      C      SUMY = 0.
C      C      SUMZ = 0.
C      C      EACH ROW OF KMATR CONTAINS THE FOUR CORNER NUMBERS FOR THE
C      C      APPROPRIATE SIDE OF THE CUBE
C      C      EACH ROW OF INBUFF CONTAINS THE ACTUAL MASS NUMBERS FOR THE
C      C      EIGHT CORNERS OF THE VOLUME
C      C      DO 2005 J=1,4
C      C      K = KMATR(I,J)
C      C      L = INBUFF(MI,K)
C      C      FOR A SYMMETRICAL MODEL THE MASS NUMBER L MAY BE 0, SO WE USE
C      C      THE MASS NUMBER FOR CORNER (K-1) AND CHANGE THE SIGN OF THE Y
C      C      COORDINATE. SEE PG. 1-66 OF LR27699, KRASH USERS MANUAL.
C      C      IF(L.NE.0) GO TO 2100
C      C      L = INBUFF(MI,K-1)
C      C      Y(L) = -Y(L)
C      C      FLIP = 1.
C      C      2100 SUMX = SUMX + X(L)
C      C      SUMY = SUMY + Y(L)
C      C      SUMZ = SUMZ + Z(L)
C      C      IF(FLIP.NE.1.) GO TO 2005
C      C      Y(L) = -Y(L)

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ISN 1262
ISN 1263
ISN 1264
ISN 1265
ISN 1266
ISN 1267
ISN 1268
ISN 1269
ISN 1270
ISN 1271
ISN 1272
ISN 1273
ISN 1274
ISN 1275
ISN 1276
ISN 1277
ISN 1278
ISN 1279

ISN 1280
ISN 1281
ISN 1282
ISN 1283
ISN 1284
ISN 1285
ISN 1286
ISN 1287

ISN 1288
ISN 1289
ISN 1290

ISN 1291
ISN 1293
ISN 1294
ISN 1295
ISN 1296
ISN 1297
ISN 1298
ISN 1299
ISN 1301

A-66

00016310
00016320
00016330
00016340
00016350
00016360
00016370
00016380
00016390
00016400
00016410
00016420
00016430
00016440
00016450
00016460
00016470
00016480
00016490
00016500
00016510

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ISN 1302      FLIP = 0.
ISN 1303      2005 CONTINUE
ISN 1304      XVOL(I,1) = SUMX/4.00
ISN 1305      XVOL(I,2) = SUMY/4.00
ISN 1306      XVOL(I,3) = SUMZ/4.00
ISN 1307      2004 CONTINUE
C              NOW WE HAVE THE XYZ COORDINATES OF THE CENTERS OF THE SIX
C              SIDES OF VOLUME M
DO 2006 I=1,3
SUM = 0.
DO 2007 J=1,3
DXVOL = XVOL(2*I,J) - XVOL(2*I-1,J)
SUM = SUM + DXVOL*DXVOL
2007 CONTINUE
VOLLEN(MI,I) = SQRT(SUM)
DLVOL(MI,I) = VOLLEN(MI,I)-VOLLENZ(MI,I)
VOL(MI) = VOL(MI)*VOLLEN(MI,I)
2006 CONTINUE
2003 CONTINUE
2001 RETURN
END

```



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ISN 0023 C NM,NB,I,J,IG(150),JG(150),
ISN 0024 D NI(900),NM(40),I,PR(150)
ISN 0025 EQUIVALENCE (XTHOLD(1,1),XYZIJJ(1)),(XTHOLD(1,2),XYZIJJ(1))
ISN 0026 EQUIVALENCE (S1,SINCOS(1)),(C1,SINCOS(2)),(S2,SINCOS(3))
ISN 0027 EQUIVALENCE (C2,SINCOS(4)),(S3,SINCOS(5)),(C3,SINCOS(6))
ISN 0028 EQUIVALENCE (XK(1),XK3(1,1,1))
ISN 0029 SIN(X) = DSIN(X)
ISN 0030 COS(X) = DCOS(X)
ISN 0031 SQR(X) = DSORT(X)
ISN 0032 ATAN2(Y,X) = DATAN2(Y,X)
ISN 0033 PI = 3.1415926535897932400
ISN 0034 IOLD=0
ISN 0035 DO 1100 I = 1,NM
ISN 0036 ARG=PHIDP(I)
ISN 0037 S1=SIN(ARG)
ISN 0038 C1=COS(ARG)
ISN 0039 ARG=THEDP(I)
ISN 0040 S2=SIN(ARG)
ISN 0041 C2=COS(ARG)
ISN 0042 ARG=PSIDP(I)
ISN 0043 S3=SIN(ARG)
ISN 0044 C3=COS(ARG)
ISN 0045 DO 1085 J = 1,6
ISN 0046 T=SINCOS(J)
ISN 0047 IF (T) 1070,1085,1075
ISN 0048 1070 T=-T
ISN 0049 1075 IF(T-1.E-10) 1080,1085,1085
ISN 0050 1080 SINCOS(J)=0.
ISN 0051 1085 CONTINUE
ISN 0052 J=9*(I-1)
ISN 0053 C MOVE AI'S TO OLD AI'S
ISN 0054 DO 1090 J2 = 1,9
ISN 0055 1090 OAI(J+J2)=BIJ(J+J2)
ISN 0056 S1S2=S1*S2
ISN 0057 C1S2=C1*S2
ISN 0058 BIJ(J+1)=C2*C3
ISN 0059 BIJ(J+2)=C2*S3
ISN 0060 BIJ(J+3)=-S2
ISN 0061 BIJ(J+4)=-C1*S3+S1S2*C3
ISN 0062 BIJ(J+5)=C1*C3+S1S2*S3
ISN 0063 BIJ(J+6)=S1*C2
ISN 0064 BIJ(J+7)=S1*S3+C1S2*C3
ISN 0065 BIJ(J+8)=-S1*C3+C1S2*S3
ISN 0066 BIJ(J+9)=C1*C2
ISN 0067 1100 CONTINUE
ISN 0068 PRINT 2021
ISN 0069 2021 FORMAT(/ IX,'BEAM UNCOUPLED,UNDAMPED FREQUENCIES (CPS)' /
ISN 0070 1 2X,'IJ',2X,'I',2X,'J',2X,'M',2X,'N',
ISN 0071 2 5X,'(1)',9X,'(2)',9X,'(3)',9X,'(4)',9X,
ISN 0072 3 '(5)',9X,'(6)')
ISN 0073 C
ISN 0074 DO 1010 IJ = 1,NB
ISN 0075 I = IG(IJ)

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ISM 0069      J = J6(IJ)
ISM 0070      M = M6(IJ)
ISM 0071      N = N6(IJ)
ISM 0072      IF(J.NE.0) GO TO 3300
ISM 0073      J = 81
ISM 0074      IF(M.NE.0) GO TO 3301
ISM 0075      C
C
C      IF J.EQ.0, WE HAVE A SYMMETRICAL MODEL IN WHICH BEAM IJ
C      CONNECTS NODE POINT (I,M) TO AN IMAGINARY POINT (J,N=0)
C      LOCATED SYMMETRICALLY ACROSS THE AIRPLANE PLANE OF SYMMETRY
C      (X-Z PLANE). FOR THESE TRANSVERSE BEAMS, THE CONDITIONS AT (J,N)
C      ARE DEDUCED FROM THE STATE AT (I,M). J IS CHANGED TO 81 BECAUSE
C      THE IBM 360-91 WILL NOT ACCEPT A ZERO SUBSCRIPTED VECTOR.
C
C      IF M.EQ.0, THERE IS NO NODE POINT AT I.
C
C      3302 XH00I = -XDP(I)
C      YH00I = -YDP(I)
C      ZH00I = -ZDP(I)
C      GO TO 3303
C
C      THIS LOOP GETS NODE POINT NUMBER JI KNOWING I AND M.
C
C      3301 DO 3305 JI=1,MNP
C      IF(I.EQ.INP(JI).AND.M.EQ.MNP(JI)) GO TO 3306
C      3305 CONTINUE
C      3306 XH00I = -XHDP(JI)
C      YH00I = -YHDP(JI)
C      ZH00I = -ZHDP(JI)
C      3303 IF(J.NE.0) GO TO 3310
C
C      IF J.EQ.81, WE HAVE A SYMMETRICAL MODEL. NOW CALCULATE
C      CONDITIONS AT J,M BASED ON KNOWLEDGE OF STATE AT I,M.
C
C      XH00J = XH00I
C      YH00J = -YH00I
C      ZH00J = ZH00I
C      GO TO 3320
C      3308 IF(M.EQ.0) GO TO 3302
C      GO TO 3301
C      3310 IF(M.NE.0) GO TO 3311
C
C      IF M.EQ.0, THERE IS NO NODE POINT AT J.
C
C      XH00J = -XHDP(J)
C      YH00J = -YDP(J)
C      ZH00J = -ZDP(J)
C      GO TO 3320
C
C      THIS LOOP GETS NODE POINT NUMBER JJ KNOWING J AND N.
C
C      3311 DO 3312 JJ=1,MNP
C      IF(J.EQ.INP(JJ).AND.N.EQ.MNP(JJ)) GO TO 3313

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00000940
00000950
00000960
00000970
00000980
00000990
00001000
00001010
00001020
00001030
00001040
00001050
00001060
00001070
00001080
00001090
00001100
00001110
00001120
00001130
00001140
00001150
00001160
00001170
00001180
00001190
00001200
00001210
00001220
00001230
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00001360
00001370
00001380
00001390
00001400
00001410
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00001450
00001460

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ISN 0106      3312 CONTINUE
ISN 0107      3313 XHODJ = -XNPDPI(JJ)
ISN 0108      YHODJ = -YNPDPI(JJ)
ISN 0109      ZHODJ = -ZNPDPPI(JJ)

C
C
C      ALL OF THE ABOVE PATHS LEAD TO HERE. WE NOW HAVE POSITIONS
C      (XHOD,ETC.) OF BOTH ENDS OF BEAM IJ.

C
C      3320 XIJ = XHODJ-XHODI
C      YIJ = YHODJ-YHODI
C      ZIJ = ZHODJ-ZHODI

C
C      CALCULATE AIJ. FIRST CALCULATE PHIIJ, THEIJ, PSIIJ.
C
C      PHIIJ(IJ) = 0.
C      IF(XIJ.EQ.0.AND.YIJ.EQ.0.) GO TO 3330
C      PSIIJ(IJ) = ATAN2(YIJ,XIJ)
C      GO TO 3340
C      3330 PSIIJ(IJ) = 0.
C      3340 THEIJ(IJ) = -ATAN2(ZIJ,SGRT(XIJ*XIJ+YIJ*YIJ))

C
C      ZERO OUT VERY SMALL SIN AND COS TERMS.
C
C      ARG = PHIIJ(IJ)
C      S1 = SIN(ARG)
C      C1 = COS(ARG)
C      ARG = THEIJ(IJ)
C      S2 = SIN(ARG)
C      C2 = COS(ARG)
C      ARG = PSIIJ(IJ)
C      S3 = SIN(ARG)
C      C3 = COS(ARG)
C      DO 3392 J1 = 1,6
C      T = SINCOS(J1)
C      IF(T) 3394,3392,3398
C      3394 T = -T
C      3396 IF(T-1.E-10) 3396,3392,3392
C      3396 SINCOS(J1) = 0.0
C      3392 CONTINUE
C      S1S2 = S1*S2
C      C1S2 = C1*S2
C      AIJ(1) = C2*C3
C      AIJ(2) = C2*S3
C      AIJ(3) = -S2
C      AIJ(4) = -C1*S3 + S1S2*C3
C      AIJ(5) = C1*C3 + S1S2*S3
C      AIJ(6) = S1*C2
C      AIJ(7) = S1*S3 + C1S2*C3
C      AIJ(8) = -S1*C3 + C1S2*S3
C      AIJ(9) = C1*C2
C      J2 = 9*(IJ-1)
C      CBIJ = CBARI(IJ)
C      IF ((IOLD.NE.0).AND.(I.EQ.IOLD)) GO TO 1120

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```

00001470
00001480
00001490
00001500
00001510
00001520
00001530
00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
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00001800
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00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960
00001970
00001980
00001990
00002000
00002010

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ISN 0151      IS=9*(I-1)
ISN 0152      DO 1110 J2 = 1,9
ISN 0153      IS=IS+1
ISN 0154      1110 AI(J2)=BIJ(IS)
ISN 0155      1120 IOLD=I
ISN 0156      IF(J.NE.01) GO TO 1121

C
C IF J=01,WE HAVE A SYMMETRICAL MODEL AND MUST CALCULATE AJ BASED
C ON AI RATHER THAN EULER ANGLES FOR MASS J,WHICH DOESNT EXIST.
C
DO 1123 J2=1,9
AJ(J2) = AI(J2)
1123 CONTINUE
AJ(2) = -AJ(2)
AJ(4) = -AJ(4)
AJ(6) = -AJ(6)
AJ(8) = -AJ(8)
GO TO 1122
1121 IS=9*(J-1)
DO 1125 J2 = 1,9
IS=IS+1
1125 AJ(J2) = BIJ(IS)

C
C CALCULATE AIJTAJ AND AIJTAI. FILL TEMP WITH EITHER AJ OR AI.
C
1122 DO 6000 I3=1,2
DO 6010 I4=1,9
IF(I3.EQ.2) GO TO 6020
TEMP(I4) = AJ(I4)
GO TO 6010
6020 TEMP(I4) = AI(I4)
6010 CONTINUE
L2 = 0
DO 6030 K2=1,3
DO 6040 J2=1,3
L2 = L2+1
SUMH(L2) = 0.
DO 6050 I2=1,3
SUMH(L2) = SUMH(L2) + AIJ(3*(J2-1)+I2)*TEMP(3*(K2-1)+I2)
6050 CONTINUE
IF(I3.EQ.2) GO TO 6060
AIJTAJ(L2) = SUMH(L2)
GO TO 6040
6060 AIJTAI(L2) = SUMH(L2)
6040 CONTINUE
6030 CONTINUE
6000 CONTINUE

C
C COMPUTE BEAM FREQUENCY AND DAMPING CONSTANTS.
C
KKS=I
DO 1312 KS = 1,2
IF (KS.EQ.2.AND.J.NE.01) KKS=J

```

ISN 0198
ISN 0199
ISN 0200
ISN 0201
ISN 0202
ISN 0203
ISN 0204
ISN 0205
ISN 0206

XTHOLD(1,KS)=XI(KKS)
XTHOLD(2,KS)=XYI(KKS)
XTHOLD(3,KS)=XZI(KKS)
XTHOLD(4,KS)=YI(KKS)
XTHOLD(5,KS)=YI(KKS)
XTHOLD(6,KS)=YI(KKS)
XTHOLD(7,KS)=XZI(KKS)
XTHOLD(8,KS)=YI(KKS)
XTHOLD(9,KS)=YI(KKS)

1312

C MASS I AND J INERTIAS ARE IN XYZIJI AND XYZIJJ WHICH ARE
C EQUIVALENT TO XTHOLD. NOW TRANSFORM BOTH TO BEAM IJ AXES
C BY PREMULTIPLYING BY AIJTAI(OR AIJTAJ) AND POSTMULTIPLYING
C BY THE TRANSPOSE OF SAME. XII AND XIJ ARE DIAGONAL ELEMENTS
C OF RESULTING INERTIA MATRIX FOR MASS I AND J, IN BEAM AXES.
C

ISN 0207
ISN 0208
ISN 0209
ISN 0210
ISN 0211
ISN 0212
ISN 0213
ISN 0214
ISN 0215
ISN 0216
ISN 0217
ISN 0218
ISN 0219
ISN 0220
ISN 0221
ISN 0222
ISN 0223
ISN 0224
ISN 0225
ISN 0226
ISN 0227
ISN 0228
ISN 0229
ISN 0230

ABT1=XYZIJI(1)*AIJTAI(1)+XYZIJI(4)*AIJTAI(4)+XYZIJI(7)*AIJTAI(7)
ABT2=XYZIJI(2)*AIJTAI(1)+XYZIJI(5)*AIJTAI(5)+XYZIJI(8)*AIJTAI(8)
ABT3=XYZIJI(3)*AIJTAI(1)+XYZIJI(6)*AIJTAI(6)+XYZIJI(9)*AIJTAI(9)
ABT4=XYZIJI(1)*AIJTAI(2)+XYZIJI(4)*AIJTAI(4)+XYZIJI(7)*AIJTAI(7)
ABT5=XYZIJI(2)*AIJTAI(2)+XYZIJI(5)*AIJTAI(5)+XYZIJI(8)*AIJTAI(8)
ABT6=XYZIJI(3)*AIJTAI(2)+XYZIJI(6)*AIJTAI(6)+XYZIJI(9)*AIJTAI(9)
ABT7=XYZIJI(1)*AIJTAI(3)+XYZIJI(4)*AIJTAI(4)+XYZIJI(7)*AIJTAI(7)
ABT8=XYZIJI(2)*AIJTAI(3)+XYZIJI(5)*AIJTAI(5)+XYZIJI(8)*AIJTAI(8)
ABT9=XYZIJI(3)*AIJTAI(3)+XYZIJI(6)*AIJTAI(6)+XYZIJI(9)*AIJTAI(9)
XXII(1) = AIJTAI(1)*ABT1+AIJTAI(4)*ABT2+AIJTAI(7)*ABT3
XXII(2) = AIJTAI(2)*ABT4+AIJTAI(5)*ABT5+AIJTAI(8)*ABT6
XXII(3) = AIJTAI(3)*ABT7+AIJTAI(6)*ABT8+AIJTAI(9)*ABT9
ABT1=XYZIJJ(1)*AIJTAJ(1)+XYZIJJ(4)*AIJTAJ(4)+XYZIJJ(7)*AIJTAJ(7)
ABT2=XYZIJJ(2)*AIJTAJ(1)+XYZIJJ(5)*AIJTAJ(5)+XYZIJJ(8)*AIJTAJ(8)
ABT3=XYZIJJ(3)*AIJTAJ(1)+XYZIJJ(6)*AIJTAJ(6)+XYZIJJ(9)*AIJTAJ(9)
ABT4=XYZIJJ(1)*AIJTAJ(2)+XYZIJJ(4)*AIJTAJ(4)+XYZIJJ(7)*AIJTAJ(7)
ABT5=XYZIJJ(2)*AIJTAJ(2)+XYZIJJ(5)*AIJTAJ(5)+XYZIJJ(8)*AIJTAJ(8)
ABT6=XYZIJJ(3)*AIJTAJ(2)+XYZIJJ(6)*AIJTAJ(6)+XYZIJJ(9)*AIJTAJ(9)
ABT7=XYZIJJ(1)*AIJTAJ(3)+XYZIJJ(4)*AIJTAJ(4)+XYZIJJ(7)*AIJTAJ(7)
ABT8=XYZIJJ(2)*AIJTAJ(3)+XYZIJJ(5)*AIJTAJ(5)+XYZIJJ(8)*AIJTAJ(8)
ABT9=XYZIJJ(3)*AIJTAJ(3)+XYZIJJ(6)*AIJTAJ(6)+XYZIJJ(9)*AIJTAJ(9)
XXIJ(1) = AIJTAJ(1)*ABT1+AIJTAJ(4)*ABT2+AIJTAJ(7)*ABT3
XXIJ(2) = AIJTAJ(2)*ABT4+AIJTAJ(5)*ABT5+AIJTAJ(8)*ABT6
XXIJ(3) = AIJTAJ(3)*ABT7+AIJTAJ(6)*ABT8+AIJTAJ(9)*ABT9

C NOW CALCULATE EQUIVALENT MASS AND FREQUENCY. FINALLY,
C DAMPING CONSTANT = CBIJ/PI/FREQ. THIS IS USED IN DERIV.

ISN 0231
ISN 0232
ISN 0233
ISN 0234
ISN 0235
ISN 0236
ISN 0237
ISN 0238
ISN 0239
ISN 0240

DO 1032 K=1,3
IF(J.NE.81) GO TO 1034
XMAS(K) = WGT(I)/2./386.
XMAS(K+3) = XXII(K)/2.
GO TO 1036
1034 XMAS(K) = WGT(I)*WGT(J)/(WGT(I)+WGT(J))/386.
XMAS(K+3) = XXII(K)*XXIJ(K)/(XXII(K)+XXIJ(K))
1036 FREQ(K) = SQRT(XK3(K,K,IJ)/XMAS(K))/2/PI
IF(FREQ(K).NE.0.) GO TO 1400

00002550
00002560
00002570
00002580
00002590
00002600
00002610
00002620
00002630
00002640
00002650
00002660
00002670
00002680
00002690
00002700
00002710
00002720
00002730
00002740
00002750
00002760
00002770
00002780
00002790
00002800
00002810
00002820
00002830
00002840
00002850
00002860
00002870
00002880
00002890
00002900
00002910
00002920
00002930
00002940
00002950
00002960
00002970
00002980
00002990
00003000
00003010
00003020
00003030
00003040
00003050
00003060
00003070

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ISN 0242      C(K,IJ) = 0.
ISN 0243      GO TO 1410
ISN 0244      1400 C(K,IJ) = CBIJ/PI/FREQ(K)
ISN 0245      1410 FREQ(K+3) = SQRT(XK3(K+3,K+3,IJ)/XMAS(K+3))/2/PI
ISN 0246      IF(FREQ(K+3).NE.0.) GO TO 1420
ISN 0247      C(K+3,IJ) = 0.
ISN 0248      GO TO 1032
ISN 0249      1420 C(K+3,IJ) = CBIJ/PI/FREQ(K+3)
ISN 0250      1032 CONTINUE
ISN 0251      PRINT 1030,IJ,IG(IJ),JG(IJ),NG(IJ),(FREQ(K),K=1,6)
ISN 0252      1030 FORMAT(1X,5I3,1P6E12.4)
ISN 0253      1010 CONTINUE
ISN 0254      PRINT 1021
ISN 0255      1021 FORMAT( / 1X, 'DAMPING TERMS (LB/IN/SEC, TRANSLATIONS (1)-(3) AND LB-
ISN 0256      1IN-SEC, ROTATIONS (4)-(6))' / 2X, 'IJ', 2X, 'I', 2X, 'J', 2X, 'M', 2X, 'N',
ISN 0257      2 7X, '(1)', 12X,
ISN 0258      3 ' (2)', 12X, '(3)', 12X, '(4)', 12X, '(5)', 12X, '(6)' )
ISN 0259      PRINT 1025,(IJ,IG(IJ),JG(IJ),NG(IJ),NG(IJ),
ISN 0260      1 (C(K,IJ),K=1,6),IJ=1,NG)
ISN 0261      1022 FORMAT(1X,5I3,1P6E15.5)
ISN 0262      PRINT 2053
ISN 0263      2053 FORMAT( / 1X, 'EULER ANGLES, BEAM IJ TO AIRPLANE (RADIANs)' )
ISN 0264      PRINT 2301
ISN 0265      2301 FORMAT(2X, 'IJ I J M', 4X, 'THEIJO(IJ)', 5X, 'PSIIJO(IJ)' )
ISN 0266      PRINT 2300,(IJ,IG(IJ),JG(IJ),NG(IJ),NG(IJ),
ISN 0267      1 THEIJO(IJ),PSIIJO(IJ),IJ=1,NG)
ISN 0268      2300 FORMAT (1X,5I3,1P2E15.5)
ISN 0269      RETURN
ISN 0270      END

```

DATE 79.177/14.16.02

OS/360 FORTRAN H

LEVEL 21.8 (JUN 74)

LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,MAP,NODEIT,ID,XREF
C DATA SET D2334ECHO AT LEVEL 002 AS OF 07/20/78

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00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280
00000290

DATA SET 0235460000 A LEVEL 002 AS OF 07720778
SUBROUTINE ECHO
  DIMENSION CARD (20)
  N = 0
  WRITE (6, 10)
  10 FORMAT (1H1, 30X, 'ECHO OF THE INPUT DATA IN CARD IMAGE FORMAT',
    1 ' 0', 18X, '1', 9X, '2', 9X, '3', 9X, '4', 9X, '5', 9X, '6', 9X,
    2 ' 7', 9X, '8', / 10H CARD NO. , 8 (10H1234567890 ) / )
  20 N = N + 1
  IF (MOD (N, 51) .EQ. 0 ) WRITE (6, 10)
  READ (5, 30, ERR=40, END=70) CARD
  30 FORMAT (20A4)
  WRITE (6, 50) N, CARD
  50 FORMAT (I6, 2X, 20A4)
  GO TO 20
  40 WRITE (6, 60)
  60 FORMAT ('0 10. I/O ERROR ON READ - WILL REWIND INPUT FILE AND
    RETURN' )
  70 REWIND 5
  RETURN
END

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LEVEL 21.8 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.16.06

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,NAP,NOEDIT,IO,XREF

C DATA SET D2334EULER AT LEVEL 001 AS OF 03/24/76

SUBROUTINE EULER(A,PHI,THETA,PSI)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(9)
SIN(X) = DSIN(X)
COS(X) = DCOS(X)
S1 = SIN(PHI)
C1 = COS(PHI)
S2 = SIN(THETA)
C2 = COS(THETA)
S3 = SIN(PSI)
C3 = COS(PSI)
A(1) = C2*C3
A(2) = C2*S3
A(3) = -S2
A(4) = -C1*S3+S1*S2*C3
A(5) = C1*C3+S1*S2*S3
A(6) = S1*C2
A(7) = S1*S3+C1*S2*C3
A(8) = -S1*C3+C1*S2*S3
A(9) = C1*C2
RETURN
END

ISN 0002
ISN 0003
ISN 0004
ISN 0005
ISN 0006
ISN 0007
ISN 0008
ISN 0009
ISN 0010
ISN 0011
ISN 0012
ISN 0013
ISN 0014
ISN 0015
ISN 0016
ISN 0017
ISN 0018
ISN 0019
ISN 0020
ISN 0021
ISN 0022
ISN 0023

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00000050
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00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000210
00000220

LEVEL 21.8 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.16.11

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
DATA SET D2334FSHEL AT LEVEL 002 AS OF 05/17/78
SUBROUTINE FSHELL(ARRAY,KEY,N)

ISN 0002 C
ISN 0003 C
ISN 0004 C
IMPLICIT REAL*8(A-H,O-Z)
INTEGER*2 N

THIS IS A FORTRAN SUBROUTINE FOR SORTING AN INDEPENDENT ARRAY OF
SIZE N INTO ASCENDING ORDER(ALGEBRAICALLY LEAST FIRST), AND
PROVIDING A 'KEY' ARRAY WHICH WILL ALLOW SUBROUTINE SHELLX TO
RETURN DEPENDENT ARRAYS TO THEIR ORIGINAL CORRESPONDENCE WITH THE
INDEPENDENT ARRAY.

ISN 0005 C
DIMENSION ARRAY(1),KEY(1)

ESTABLISH THE INITIAL CONDITION OF THE KEY ARRAY.

ISN 0006 C
ISN 0007 C
DO 10 I=1, N
10 KEY(I) = I

ESTABLISH THE INITIAL CONDITION FOR M, M IS THE CURRENT NUMBER
OF SUBSETS INTO WHICH IARRAY HAS BEEN PARTITIONED.

ISN 0008 C
M = N

REDUCE M, WHEN THE ALGORITHM PROCEEDS WITH THE REDUCED M, THE
EFFECT IS A MERGE OF THE OLD SUBSETS INTO ABOUT HALF AS MANY
NEW. INITIALLY, IARRAY IS PARTITIONED INTO ABOUT N/2 SUBSETS.
EACH OF WHICH CONTAINS 2 ELEMENTS, WITH THE EXCEPTION THAT ONE
SUBSET WILL CONTAIN 3 ELEMENTS IF N IS ODD. IT IS RECOMMENDED
THAT A SAMPLE PROBLEM BE WORKED BY HAND TO UNDERSTAND THE
MECHANISM OF THE PARTITIONING.

ISN 0009 C
20 M = M / 2

TEST THE REDUCED M. IF M IS ZERO, THE ENTIRE IARRAY HAS BEEN
SORTED, AND CONTROL IS RETURNED TO THE CALLING PROGRAM.

ISN 0010 C
ISN 0011 C
IF(M) 30,30,40
30 RETURN

SET K=N-M. THE ELEMENTS IN IARRAY FROM IARRAY(1) TO IARRAY(K)

00000010
00000015
00000020
00000025
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
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00000200
00000210
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00000230
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00000320
00000330
00000340
00000350
00000360
00000370
00000380

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00000390
00000400
00000410
00000420
00000430
00000440
00000450
00000460
00000470
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00000560
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00000620
00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700
00000710
00000720
00000730
00000740
00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820

C      WILL BE USED AS 'BASE' ELEMENTS FOR COMPARISONS. THAT IS,
C      IARRAY(I) WILL BE COMPARED WITH IARRAY(I+M).  THUS, ALL
C      ELEMENTS IN IARRAY WILL ENTER THE COMPARISON SEQUENCE.
C
C      40 K = N - M
C      DO 70 J=1, K
C
C      SINCE THE INDEX ADDRESSING THE 'BASE' ELEMENT MAY BE MODIFIED
C      'BACKWARDS' BY THE FOLLOWING CODE, SET I=J AND USE I FOR
C      THE 'BASE' INDEX. THIS PRESERVES THE CORRECT VALUE OF J FOR THE
C      NEXT 'BASE'.
C      I = J
C
C      II IS CREATED TO REFERENCE THE NEXT HIGHEST ELEMENT IN THE
C      CURRENT SUBSET, WHICH IS TO BE COMPARED WITH IARRAY(I).
C      50 II = I + M
C      COMPARE ARRAY(I) WITH ARRAY(II)
C      IF (ARRAY(I) - ARRAY(II)) 70,70,60
C
C      60 TIMBO = ARRAY(I)
C      ARRAY(II) = ARRAY(II)
C      ARRAY(II) = TIMBO
C      TIMBO = KEY(I)
C      KEY(II) = KEY(II)
C      KEY(II) = TIMBO
C
C      I = I - M
C      IF (I) 70,70,50
C
C      THE ELEMENT IS PROPERLY PLACED IN ITS SUBSET. EXAMINE THE NEXT
C      'BASE' ELEMENT.
C
C      70 CONTINUE
C
C      ALL OF THE M SUBSETS HAVE BEEN SORTED
C      GO TO 20
C      END

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ISN 0031	COTTON/INAC/7BS(40),FSPOI(40),SCPI(40),JBS(40),	00000410
	1 KKSPI(5,200),EXSP(5,200),TSP(200),STEMP1(40),STEMP2(40),	00000420
	2 STEMP3(40),STEMP4(40),STEMP5(40),KKONT	00000430
ISN 0032	COTTON/INDEAC/ NACC	00000440
ISN 0033	COTTON/INIC/ XDP(80),ZDP(80),PHDP(80),PSIDP(80),	00000450
	1 THEDP(80),PPR,RPR,RPR,XGIN,ZGIN,PHIPR,PSIPR,THEPR,	00000460
	2 XGDOT,YGDOT,ZGDOT	00000470
	COTTON/INIDCP/ YDP(80)	00000480
ISN 0034	COTTON/INPR/ NDIR,NSP	00000490
ISN 0035	COTTON/INCFIC/ BETA	00000500
ISN 0036	COTTON/INCFIN/ THAX,IPRINT	00000510
ISN 0037	COTTON/CONEM/ DAMPC,RUNMCO,RUNMCO	00000520
ISN 0038	COTTON/CONEM/ NNP	00000530
ISN 0039	COTTON/CONEM/ NNP	00000540
ISN 0040	COTTON/CONEM/ NNP	00000550
ISN 0041	COTTON/CONEM/ NNP	00000560
ISN 0042	COTTON/CONEM/ NNP	00000570
ISN 0043	COTTON/CONEM/ NNP	00000580
ISN 0044	COTTON/CONEM/ NNP	00000590
	1 YOLEO(20),BOLEO(20),FAOI(20),XEXT(20),XKCOMP(20),FCQUL(20),	00000600
	2 ALHAP,IGOLEO(20),JGOLEO(20),MGOLEO(20),NGOLEO(20),NOLEO	00000610
	COTTON/CONALL/ C(6,150),PI(80),Q(80),R(80),U(80),V(80),W(80),X(81),	00000620
	1 Y(81),Z(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),	00000630
	2 YI(80),ZI(80),YII(80),XZI(80),YZI(80),AIJ(9),BIJ(720),	00000640
	3 DRII(150),DAI(720),VEE(900),MGT(80),PHI(80),THETA(80),PSI(80),	00000650
	4 PDOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),	00000660
	5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,	00000670
	6 XACC(80),YACC(80),ZACC(80),AIDOT(9),	00000680
	7 PHIIJ(150),THEIJ(150),PSIIJ(150),SUMDF(6,150),TITLE,	00000690
	8 XLBAR(40),FSFAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),	00000700
	9 DPIN(81),DQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),	00000710
	A CEIK(40),	00000720
	B SBAR(40),KUN(40),MAXNM,MAXIGS,MAXTBL,	00000730
	C NI,NB,I,J,IG(150),JG(150),	00000740
	D NI(900),NI(40),IJPR(150)	00000750
	COTTON/CONTR8/ 6	00000760
	COTTON/UB/ DB(150),IJUB(150),NJB	00000770
	COTTON/STUFF/ NEWI(80),NEWIJ(150),NHOLD,NBOLD	00000780
	COTTON/CONTR4/ KR ,LDP ,LDPI	00000790
	COTTON/CONTR4/ND,NVBHM,NFBHM,NHI,NKM,NLB,	00000800
	1 NPH ,NHTL ,NPTS ,NVBM ,IJPR ,IPHDP,NFBM	00000810
	COTTON/CONTR2/ IQ ,JQ ,NPQ ,INBUF ,	00000820
	1 NKMVEC,IJSVE	00000830
	COTTON/INAC/ACCEL(300),TIM(300),INDEX(50,2),JAY(50,2),KOUNT	00000840
	EQUIVALENCE (XK(1),XK3(1,1,1))	00000850
	EQUIVALENCE (VMAX(1),VMAX2(1)),(FMAX(1),FMAX2(1))	00000860
	EQUIVALENCE (VMAXN(1),VMAX3(1)),(FMAXN(1),FMAX3(1))	00000870
	EQUIVALENCE (MASSNO(1),INDEX(1,1)),(DIR(1),INDEX(1,2))	00000880
	DO 1 I=1,NH	00000890
	NEWI(I) = 0	00000900
	1 CONTINUE	00000910
	NHNEW = NH	00000920
	NHOLD = NH	00000930
	NHOLD = NNP	

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ISM 0104      2020 INP(NSPNEH) = NEHI(I)
ISM 0105      MP(NSPNEH) = M
ISM 0106      2010 CONTINUE
ISM 0107      NNP = NSPNEH

C
C      CARDS 0300
C
2000 IF(NSP.EQ.0) GO TO 41
NSPNEH = NSP
DO 30 J=1,NSP
  I = II(J)
  K = KK(J)
  M = MM(J)
  IF(M.EQ.0) GO TO 2003
  DO 2004 JJ=1,NNP
    IF(I.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 2005
  2004 CONTINUE
  2005 IF(NEHI(I).EQ.0.AND.YNPOP(JJ).EQ.0.) GO TO 30
    GO TO 2006
  2003 IF(NEHI(I).EQ.0) GO TO 30
  2006 NSPNEH = NSPNEH+1
  II(NSPNEH) = NEHI(I)
  KK(NSPNEH) = K
  MM(NSPNEH) = M
  IF(M.EQ.0) GO TO 2007
  IF(NEHI(I).NE.0) GO TO 2007
  II(NSPNEH) = I
  MM(NSPNEH) = MNP(NMNP(JJ))
  2007 XLBAR(NSPNEH) = XLBAR(J)
  IF(IK.EQ.2) XLBAR(NSPNEH) = -XLBAR(NSPNEH)
  XM(NSPNEH) = XM(J)
  XKE(NSPNEH) = XKE(J)
  XMAX(NSPNEH) = XMAX(J)
  GFLEX(NSPNEH) = GFLEX(J)

C
C      CARDS 0400
C
SI(NSPNEH) = SI(J)
SA(NSPNEH) = SA(J)
SB(NSPNEH) = SB(J)
SF(NSPNEH) = SF(J)
FSPOI(NSPNEH) = FSPOI(J)
FSPOF(NSPNEH) = FSPOF(J)
CDAMP(NSPNEH) = CDAMP(J)
FSPOP(NSPNEH) = FSPOP(J)
SCP(NSPNEH) = SCP(J)
STEMP1(NSPNEH) = STEMP1(J)
STEMP2(NSPNEH) = STEMP2(J)
STEMP3(NSPNEH) = STEMP3(J)
STEMP4(NSPNEH) = STEMP4(J)
STEMP5(NSPNEH) = STEMP5(J)
30 CONTINUE
NSP = NSPNEH

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ISM 0108
ISM 0110
ISM 0111
ISM 0112
ISM 0113
ISM 0114
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ISM 0121
ISM 0123
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ISM 0155
ISM 0156
ISM 0157
ISM 0159

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ISN 0159      41 CONTINUE
C
C      CARDS 0500
C
ISN 0160      IF(NB.EQ.0) GO TO 101
ISN 0161      DO 99 I=1,NB
ISN 0162      NEWIJ(I) = 0
ISN 0163      99 CONTINUE
ISN 0164      NENEW = NB
ISN 0165      NBOLD = NB
ISN 0166      DO 50 K=1,NB
ISN 0167      I = IG(K)
ISN 0168      J = JG(K)
ISN 0169      M = MG(K)
ISN 0170      N = NG(K)
ISN 0171      IF(M .EQ. 0) GO TO 70
ISN 0172      DO 71 JJ=1, NNPOLD
ISN 0173      IF(I .NE. INP(JJ) .OR. M .NE. MNP(JJ)) GO TO 71
ISN 0174      IF(J .NE. JNP(JJ) .EQ. 0.0) GO TO 72
ISN 0175      GO TO 51
ISN 0176      71 CONTINUE
ISN 0177      PRINT 2030
ISN 0178      2030 FORMAT(5X, '3. DATA ERROR IN GENMOD AT 2030')
ISN 0179      STOP
ISN 0180      70 IF(YDPI(I) .NE. 0.0) GO TO 51
ISN 0181      72 IF(N .EQ. 0) GO TO 73
ISN 0182      DO 74 JJ=1, NNPOLD
ISN 0183      IF(J .NE. INP(JJ) .OR. N .NE. MNP(JJ)) GO TO 74
ISN 0184      IF(YNDP(JJ) .EQ. 0.0) GO TO 50
ISN 0185      GO TO 90
ISN 0186      74 CONTINUE
ISN 0187      PRINT 2040
ISN 0188      2040 FORMAT(5X, '4. DATA ERROR IN GENMOD AT 2040')
ISN 0189      STOP
ISN 0190      73 IF(YDPI(J) .EQ. 0.0) GO TO 50
ISN 0191      GO TO 90
ISN 0192      51 IF(J .NE. 0) GO TO 90
ISN 0193      JG(K) = NENWI(I)
ISN 0194      NG(K) = M
ISN 0195      GO TO 50
ISN 0196      C
ISN 0197      C
ISN 0198      C
ISN 0199      C
ISN 0200      C
ISN 0201      C
ISN 0202      C
ISN 0203      C
ISN 0204      C
ISN 0205      C
ISN 0206      90 NENEW = NENWI*1
ISN 0207      NEWIJ(K) = NENEW
ISN 0208      IF(YDPI(I).EQ.0.OR.YDPI(J).EQ.0.) GO TO 52
ISN 0209      C
ISN 0210      C
ISN 0211      C
ISN 0212      C
ISN 0213      C
ISN 0214      C
ISN 0215      C
ISN 0216      C
ISN 0217      C
ISN 0218      C
ISN 0219      C
ISN 0220      C
ISN 0221      C
ISN 0222      C
ISN 0223      C
ISN 0224      C
ISN 0225      C
ISN 0226      C
ISN 0227      C
ISN 0228      C
ISN 0229      C
ISN 0230      C
ISN 0231      C
ISN 0232      C
ISN 0233      C
ISN 0234      C
ISN 0235      C
ISN 0236      C
ISN 0237      C
ISN 0238      C
ISN 0239      C
ISN 0240      C
ISN 0241      C
ISN 0242      C
ISN 0243      C
ISN 0244      C
ISN 0245      C
ISN 0246      C
ISN 0247      C
ISN 0248      C
ISN 0249      C
ISN 0250      C
ISN 0251      C
ISN 0252      C

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ISN 0214      GO TO 80
ISN 0215      52 ITEST = 0
ISN 0216      IF(YDP(I).EQ.0.) GO TO 53
C
C      MASS I IS OFF X-Z PLANE, J IS ON.
C      GET NODE POINT NUMBER JN FOR MASS J.
C
ISN 0218      IF(N.NE.0) GO TO 55
ISN 0220      MG(NBNEW) = 0
ISN 0221      GO TO 57
ISN 0222      55 DO 54 JN=1,NNP
ISN 0223      IF(INP(JN).EQ.J.AND.MNP(JN).EQ.N) GO TO 56
ISN 0225      54 CONTINUE
ISN 0226      56 MG(NBNEW) = N
ISN 0227      IF(NENP(JN).EQ.0) GO TO 57
ISN 0229      MG(NBNEW) = MNP(NENP(JN))
ISN 0230      57 MG(NBNEW) = M
ISN 0231      IG(NBNEW) = J
ISN 0232      JG(NBNEW) = NEHI(I)
ISN 0233      GO TO 80
ISN 0234      53 IF(YDP(J).EQ.0.) GO TO 59
C
C      MASS I IS ON X-Z PLANE, J IS OFF.
C      GET NODE POINT NUMBER JN FOR MASS I.
C
ISN 0236      60 IF(M.NE.0) GO TO 61
ISN 0238      MG(NBNEW) = 0
ISN 0239      GO TO 62
ISN 0240      61 DO 63 JN=1,NNP
ISN 0241      IF(INP(JN).EQ.I.AND.MNP(JN).EQ.M) GO TO 64
ISN 0243      63 CONTINUE
ISN 0244      64 MG(NBNEW) = M
ISN 0245      IF(NENP(JN).EQ.0) GO TO 62
ISN 0247      MG(NBNEW) = MNP(NENP(JN))
ISN 0248      62 IF(ITEST.NE.0) GO TO 58
ISN 0250      NG(NBNEW) = N
ISN 0251      IG(NBNEW) = I
ISN 0252      JG(NBNEW) = NEHI(J)
ISN 0253      GO TO 80
C
C      BOTH MASSES I AND J ARE ON X-Z PLANE.
C
ISN 0254      59 ITEST = 1
ISN 0255      IG(NBNEW) = I
ISN 0256      JG(NBNEW) = J
ISN 0257      GO TO 60
ISN 0258      58 IF(N.NE.0) GO TO 150
ISN 0260      NG(NBNEW) = 0
ISN 0261      GO TO 80
ISN 0262      150 DO 151 JN=1,NNP
ISN 0263      IF(INP(JN).EQ.J.AND.MNP(JN).EQ.N) GO TO 152
ISN 0265      151 CONTINUE
ISN 0266      152 NG(NBNEW) = N

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ISN 0267 IF(NEMNP(JN),EQ.0) GO TO 80
ISN 0269 NG(NBNEW) = MNP(NEMNP(JN))
C
C ALL ABOVE STUFF GETS I,J,M AND N FOR NEW BEAM.
C NOW SET ITS PARAMETERS EQUAL TO THOSE FOR ITS TWIN.
C
80 MC(NBNEW) = MC(K)
AA(NBNEW) = AA(K)
YY(NBNEW) = YY(K)
ZZ(NBNEW) = ZZ(K)
XJ(NBNEW) = XJ(K)
Z1(NBNEW) = Z1(K)
Z2(NBNEW) = Z2(K)
XIQ(NBNEW)=XIQ(K)
PY(NBNEW) = PY(K)
PYJ(NBNEW)=PYJ(K)
PZ(NBNEW) = PZ(K)
PZJ(NBNEW)=PZJ(K)
SF26(NBNEW)=SF26(K)
SF35(NBNEW)=SF35(K)
SF26J(NBNEW)=SF26J(K)
SF35J(NBNEW)=SF35J(K)
CBAR(NBNEW) = CBAR(K)
IJPR(NBNEW) = 0
IJUB(NBNEW)=IJUB(K)
DB(NBNEW)=DB(K)
50 CONTINUE
NB = NBNEW
101 CONTINUE
C
C CARDS 0601 AND UP
C
IF(ND.EQ.0) GO TO 102
CDUM = .01
IF(DAMPC.NE.0.) CDUM = DAMPC
ND = 0
DO 103 IJ=1,NB
IF(CBAR(IJ).EQ.CDUM) GO TO 103
ND = ND+1
103 CONTINUE
102 CONTINUE
IF(NLEO.EQ.0.) GO TO 709
NLEON=NLEO
DO 701 J=1,NLEO
DO 702 IJ=1,NBOLD
IF(IGOLEO(J).EQ. IG(IJ).AND.JGOLEO(J).EQ. JG(IJ).AND.MGOLEO(J)
1.EQ.MG(IJ).AND. NGOLEO(J).EQ.NG(IJ)) GO TO 703
702 CONTINUE
703 IF(NEWIJ(IJ).EQ.0) GO TO 701
JI=NEWIJ(IJ)
NLEON=NLEON+1
IGOLEO(NLEON)=IG(JI)
JGOLEO(NLEON)=JG(JI)

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ISN 0270
ISN 0271
ISN 0272
ISN 0273
ISN 0274
ISN 0275
ISN 0276
ISN 0277
ISN 0278
ISN 0279
ISN 0280
ISN 0281
ISN 0282
ISN 0283
ISN 0284
ISN 0285
ISN 0286
ISN 0287
ISN 0288
ISN 0289
ISN 0290
ISN 0291
ISN 0292

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ISN 0293
ISN 0295
ISN 0296
ISN 0298
ISN 0299
ISN 0300
ISN 0302
ISN 0303
ISN 0304
ISN 0305
ISN 0307
ISN 0308
ISN 0309
ISN 0310

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ISN 0312
ISN 0313
ISN 0315
ISN 0316
ISN 0317
ISN 0318

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ISN 0319	MGELEO(NOLEON)=MG(JI)	00003599
ISN 0320	NGOLEO(NOLEON)=NG(JI)	00003600
ISN 0321	EOLFO(NOLEON)=EOLFO(J)	00003610
ISN 0322	FAGI(NOLEON)=FAGI(J)	00003620
ISN 0323	FAAI(NOLEON)=FAA(J)	00003630
ISN 0324	EXPLOE(NOLEON)=EXPLOE(J)	00003640
ISN 0325	YMAX(NOLEON)=YMAX(J)	00003650
ISN 0326	BOLEOI(NOLEON)=BOLEOI(J)	00003660
ISN 0327	BROLEOI(NOLEON)=BROLEO(J)	00003670
ISN 0328	XEXT(NOLEON)=XEXT(J)	00003680
ISN 0329	XKCOMP(NOLEON)=XKCOMP(J)	00003690
ISN 0330	FCOU(LNOLEON)=FCOU(LJ)	00003700
ISN 0331	701 CONTINUE	00003710
ISN 0332	NOLEO=NOLEON	00003720
ISN 0333	709 CONTINUE	00003730
C		00003740
C	CARDS 0700	00003750
C	IF(NLB.EQ.0) GO TO 250	00003760
C		00003770
C	SEARCH NONLINEAR BEAM SPECIFICATION TABLE (CARDS 0701 TO 0700+NLB)	00003780
C	TO DETERMINE WHICH NEW ELEMENTS ARE TO BE ADDED.	00003790
C		00003800
C		00003810
ISN 0336	DO 240 K=1,180	00003820
ISN 0337	OLDNLB(K) = 0	00003830
ISN 0338	240 CONTINUE	00003840
ISN 0339	NLBOLD = NLB	00003850
ISN 0340	NLBNEW = NLB	00003860
ISN 0341	DO 200 K=1,NLBOLD	00003870
ISN 0342	I = IQ(K)	00003880
ISN 0343	J = JQ(K)	00003890
ISN 0344	M = MQ(K)	00003900
ISN 0345	N = NQ(K)	00003910
C		00003920
C	IF J,EQ.0 IN OLD TABLE,CHANGE IT TO NEW(I) FOR BIG MODEL	00003930
C	TO AGREE WITH NEW BEAM NUMBERING.	00003940
C		00003950
ISN 0346	IF(J,EQ.0) J = NEW(I)	00003960
ISN 0348	DO 210 IJ=1,NBOLD	00003970
ISN 0349	IF(I,EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))	00003980
	1 GO TO 220	00003990
ISN 0351	210 CONTINUE	00004000
ISN 0352	220 IF(NEWIJ(IJ),EQ.0) GO TO 200	00004010
C		00004020
C	IF THERE IS A NEW BEAM CORRESPONDING TO THE OLD ONE,INCREMENT	00004030
C	THE NLBNEW COUNTER AND SET THE NEW TABLE PARAMETERS EQUAL TO	00004040
C	THE OLD VALUES EXCEPTING THE IJ IDENTIFICATION,OTHERWISE BYPASS.	00004050
C		00004060
	NLBNEW = NLBNEW+1	00004070
ISN 0354	IQ(NLBNEW) = IG(NEWIJ(IJ))	00004080
ISN 0355	JQ(NLBNEW) = JG(NEWIJ(IJ))	00004090
ISN 0356	MQ(NLBNEW) = MG(NEWIJ(IJ))	00004100
ISN 0357	NQ(NLBNEW) = NG(NEWIJ(IJ))	00004110


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ISN 0394      NORI = NORINH
ISN 0395      340 CONTINUE
C
C      CARDS 1200
C
ISN 0396      IF(INVCH.EQ.0) GO TO 360
C
C      SET EVEN NUMBERED CORNER MASS NUMBERS EQUAL TO NEW MASSES
C      ACROSS FROM ODD NUMBERED CORNER MASSES.
C
ISN 0398      DO 380 I=1,NVCH
ISN 0399      DO 370 K=2,6,2
ISN 0400      INBUFF(I,K) = NEWI(INBUFF(I,K-1))
ISN 0401      370 CONTINUE
ISN 0402      380 CONTINUE
ISN 0403      360 CONTINUE
C
C      CARDS 1300
C
ISN 0404      IF(INVBM.EQ.0) GO TO 450
ISN 0406      NVBM = NVBM
ISN 0407      DO 410 JI=1,NVBM
ISN 0408      IF(JG(IJVM(JI)).EQ.0) JG(IJVM(JI)) = NEWI(IJVM(JI))
ISN 0410      I = IG(IJVM(JI))
ISN 0411      J = JG(IJVM(JI))
ISN 0412      M = MG(IJVM(JI))
ISN 0413      N = NG(IJVM(JI))
ISN 0414      DO 420 IJ=1,NBOLD
ISN 0415      IF(I.EQ.IG(IJ).AND..J.EQ.JG(IJ).AND..M.EQ.MG(IJ).AND..N.EQ.NG(IJ))
1 GO TO 430
ISN 0417      420 CONTINUE
ISN 0418      430 IF(NEWI(IJ).EQ.0) GO TO 410
ISN 0420      NVBM = NVBM+1
ISN 0421      IJVM(NVBM) = NEWI(IJ)
ISN 0422      DO 440 L=1,6
ISN 0423      VMAX2(L,NEWI(IJ)) = VMAX2(L,IJ)
ISN 0424      440 CONTINUE
ISN 0425      410 CONTINUE
ISN 0426      NVBM = NVBM
ISN 0427      450 CONTINUE
ISN 0428      IF(INVBM.EQ.0) GO TO 460
ISN 0430      NVBM = NVBM
ISN 0431      DO 461 JI=1,NVBM
ISN 0432      IF(JG(IJVM(JI)).EQ.0) JG(IJVM(JI)) = NEWI(IG(IJVM(JI)))
ISN 0434      I = IG(IJVM(JI))
ISN 0435      J = JG(IJVM(JI))
ISN 0436      M = MG(IJVM(JI))
ISN 0437      N = NG(IJVM(JI))
ISN 0438      DO 462 IJ=1,NBOLD
ISN 0439      IF (I.EQ.IG(IJ).AND..J.EQ.JG(IJ).AND..M.EQ.MG(IJ).AND..N.EQ.NG(IJ))
1 GO TO 463
ISN 0441      462 CONTINUE
ISN 0442      463 IF(NEWI(IJ).EQ.0) GO TO 461

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ISN 0444 NVBMM=NVBMM+1
ISN 0445 IJFMM(NVBMM)=NEWIJ(IJ)
ISN 0446 DO 465 L=1,6
ISN 0447 VMAX3(L,NEWIJ(IJ))=VMAX3(L,IJ)
ISN 0448
ISN 0449 465 CONTINUE
ISN 0450 461 CONTINUE
ISN 0451 NVBMM=NVBMM
ISN 0452 460 CONTINUE
ISN 0453 IF(NFBM.EQ.0) GO TO 400
ISN 0454 NFBMM=NFBM
ISN 0455 DO 451 JI=1,NFBM
ISN 0456 IF(JG(IJFMM(JI)).EQ.0) JG(IJFMM(JI)) = NEWIJG(IJFMM(JI))
ISN 0457 J = JG(IJFMM(JI))
ISN 0458 M = MG(IJFMM(JI))
ISN 0459 N = NG(IJFMM(JI))
ISN 0460 DO 452 IJ=1,NBOLD
ISN 0461 IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).
ISN 0462 AND.N.EQ.NG(IJ)) GO TO 453
ISN 0463
ISN 0465 452 CONTINUE
ISN 0466 453 IF(NEWIJ(IJ).EQ.0) GO TO 451
ISN 0467 NFBMM=NVBMM+1
ISN 0468 IJFMM(NFBMM) = NEWIJ(IJ)
ISN 0469 DO 455 L=1,6
ISN 0470 FMAX2(L,NEWIJ(IJ))=FMAX2(L,IJ)
ISN 0471
ISN 0472 455 CONTINUE
ISN 0473 451 CONTINUE
ISN 0474 NFBM=NFBMM
ISN 0475 400 CONTINUE
ISN 0476 IF(NFBM.EQ.0) GO TO 470
ISN 0477 NFBMM=NFBM
ISN 0478 DO 471 JI=1,NFBM
ISN 0479 IF(JG(IJFMM(JI)).EQ.0) JG(IJFMM(JI))=NEWIJG(IJFMM(JI))
ISN 0480 I=IG(IJFMM(JI))
ISN 0481 J=JG(IJFMM(JI))
ISN 0482 M=MG(IJFMM(JI))
ISN 0483 N=NG(IJFMM(JI))
ISN 0484 DO 472 IJ=1,NBOLD
ISN 0485 IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
ISN 0486 1 GO TO 473
ISN 0487
ISN 0489 472 CONTINUE
ISN 0490 473 IF(NEWIJ(IJ).EQ.0) GO TO 471
ISN 0491 NFBMM=NVBMM+1
ISN 0492 IJFMM(NFBMM)=NEWIJ(IJ)
ISN 0493 DO 475 L=1,6
ISN 0494 FMAX3(L,NEWIJ(IJ))=FMAX3(L,IJ)
ISN 0495
ISN 0496 475 CONTINUE
ISN 0497 471 CONTINUE
ISN 0498 NFBM=NFBM
ISN 0499 470 CONTINUE
ISN 0500 LL=0
ISN 0501 L=KOUNT

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ISN 0502      IF(NACC.EQ.0) GO TO 490
ISN 0504      NACNEW=NACC
ISN 0505      DO 476 K=1,NACC
ISN 0506      I=MASSNO(K)
ISN 0507      IF(NEWI(I).EQ.0) GO TO 491
ISN 0509      NACNEW=NACNEW+1
ISN 0510      IN=NEWI(I)
ISN 0511      MASSNO(NACNEW)=IN
ISN 0512      DIR(NACNEW)=DIR(K)
ISN 0513      NPTS(NACNEW)=NPTS(K)
ISN 0514      JAY(NACNEW,1)=NACNEW
ISN 0515      JJ=NPTS(K)
ISN 0516      DO 477 JK=1,JJ
ISN 0517      L=L+1
ISN 0518      LL=LL+1
ISN 0519      TIM(LL)=TIM(LL)
ISN 0520      ACCEL(LL)=ACCEL(LL)
ISN 0521      477 CONTINUE
ISN 0522      KOUNT=KOUNT+NPTS(K)
ISN 0523      IF(KOUNT.GT.300) GO TO 478
ISN 0525      491 CONTINUE
ISN 0526      NACC=NACNEW
ISN 0527      476 CONTINUE
ISN 0528      GO TO 490
ISN 0529      478 PRINT 479,NACC,KOUNT
ISN 0530      479 FORMAT(IX,'7.ERROR IN ACCEL TIME DATA INPUT'/IX,'NUMACL,KOUNT=',
ISN 0531      1 215)
ISN 0531      490 CONTINUE
C
ISN 0532      C CARDS 1400
ISN 0534      IF(NHI.EQ.0) GO TO 500
ISN 0535      NHINEM = NHI
ISN 0536      DO 510 K=1,NHI
ISN 0537      I = INBUF(K)
ISN 0539      IF(NEWI(I).EQ.0) GO TO 510
ISN 0540      NHINEM = NHINEM+1
ISN 0541      IN = NEWI(I)
ISN 0542      INBUF(NHINEM) = IN
ISN 0543      ALIFT(IN) = ALIFT(I)
ISN 0544      HEX(IN) = HEX(I)
ISN 0545      HEY(IN) = HEY(I)
ISN 0546      HEZ(IN) = HEZ(I)
ISN 0547      XYI(IN) = XYI(I)
ISN 0548      YZI(IN) = YZI(I)
ISN 0549      XZI(IN) = XZI(I)
ISN 0550      510 CONTINUE
ISN 0551      NHI = NHINEM
C
C CARDS 1500
C
ISN 0552      IF(NPH.EQ.0) GO TO 530
ISN 0554      NPHNEW = NPH

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00006240
00006250
00006260
00006270
00006280
00006290
00006300
00006310
00006320
00006330
00006340
00006350
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00006370
00006380
00006390
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00006590
00006600
00006610
00006620
00006630
00006640
00006650
00006660
00006670
00006680
00006690
00006700
00006710
00006720
00006730
00006740
00006750
00006760

DO 540 J=1,NPH
  I = IPHDP(J)
  IF(NEW(I),EQ.0) GO TO 540
  NPHNEW = NPHNEW+1
  IN = NEW(I)
  PHDP(IN) = -PHDP(I)
  THDP(IN) = THDP(I)
  PSIDP(IN) = -PSIDP(I)
  IPHDP(NPHNEW) = IN
  540 CONTINUE
  NPH = NPHNEW
C
C
C
  CARDS 1600
C
DO 570 IJ=1,NBOLD
  IF(NEW(IJ),EQ.0) GO TO 570
  IJN = NEW(IJ)
  PHIJ(IJN) = -PHIJ(IJ)
  THEIJ(IJN) = THEIJ(IJ)
  PSIIJ(IJN) = -PSIIJ(IJ)
  570 CONTINUE
  530 CONTINUE
C
C
C
  CARDS 2100
C
  IF(NKM,EQ.0) GO TO 600
  NKHNEW = NKM
  DO 610 IJ=1,NBOLD
    IF(NKHVEC(IJ),EQ.0.OR.NEW(IJ),EQ.0) GO TO 610
    NKHNEW = NKHNEW+1
    IJN = NEW(IJ)
    NKHVEC(IJN) = 1
    DO 620 K=1,6
      DO 620 L=1,6
        XK3(L,K,IJN) = XK3(L,K,IJ)
      620 CONTINUE
    610 CONTINUE
    NKM = NKHNEW
  600 CONTINUE
  IF(PUNMOD,EQ.0) GO TO 700
  IPUNCH = 7
C
C
C
  CARD 0001,0002
C
  WRITE(IPUNCH,1000) TITLE
C
C
C
  CARD 0003
C
  WRITE(IPUNCH,1010) NM,NSP,NB,NLB,NS,NVP,NVCH,NDRI,NPL,NACC,NVBM,
1 NHT,NPH,NO
C
C
C
  CARD 0004
C

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ISN 0597      C      WRITE(IPUNCH,1020) IPRINT,DELTAT,THAX,PLOHT,RUNMOD,NKM
              C      CARD 0005
              C
ISN 0598      C      LINE = 005
ISN 0599      C      WRITE(IPUNCH,1030) XGDOT,YGDOT,ZGDOT,LINE
              C
              C      CARD 0006
              C
ISN 0600      C      LINE = 006
ISN 0601      C      WRITE(IPUNCH,1030) PPR,QPR,RPR,LINE
              C
              C      CARD 0007
              C
ISN 0602      C      LINE = 007
ISN 0603      C      WRITE(IPUNCH,1040) PHIPR,THEPR,PSIPR,XGIN,ZGIN,BETA,LINE
              C
              C      CARDS 0100
              C
ISN 0604      C      LINE = 101
ISN 0605      C      DO 900 I=1,NM
ISN 0606      C      WRITE(IPUNCH,1050) WGT(I),XDP(I),YDP(I),ZDP(I),XI(I),YI(I),ZI(I),
              C      1 LINE
              C      LINE = LINE+1
              C      900 CONTINUE
              C
              C      CARDS 0200
              C
ISN 0609      C      IF(INP.EQ.0) GO TO 904
ISN 0611      C      LINE = 201
ISN 0612      C      WRITE(IPUNCH,1055) (MNP(I),INP(I),XNPDP(I),YNPDP(I),ZNPDP(I),
              C      1 I=1,NNP),LINE
              C
              C      CARDS 0300
              C
ISN 0613      C      904 LINE = 301
ISN 0614      C      DO 905 J=1,NSP
ISN 0615      C      WRITE(IPUNCH,1060) MM(J),II(J),KK(J),XLBAR(J),XHU(J),XKE(J),
              C      1 XHAX(J),LINE
              C      LINE = LINE+1
              C      905 CONTINUE
              C
              C      CARDS 0400
              C
ISN 0618      C      LINE = 401
ISN 0619      C      DO 910 J=1,NSP
ISN 0620      C      WRITE(IPUNCH,1040) SI(J),SA(J),SB(J),SF(J),FSPOT(J),FSPOF(J),
              C      1 LINE
              C      LINE = LINE+1
              C      910 CONTINUE
              C
              C      CARDS 0500
              C

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ISN 0623      LINE = 501
ISN 0624      DO 915 I=1,NB
ISN 0625      WRITE(IPUNCH,1070) MG(I),IG(I),NG(I),JG(I),E(I),AA(I),G(I),
ISN 0626      1 YY(I),ZZ(I),PY(I),PZ(I),LINE
ISN 0627      LINE = LINE+1
                915 CONTINUE
                C
                C CARD 0600
                C
                C WRITE(IPUNCH,1080) DAMPC
                C
                C CARDS 0601 AND UP
                C
                C
                C LINE = 601
                C DO 920 IJ=1,NB
                C WRITE(IPUNCH,1090) MG(IJ),IG(IJ),NG(IJ),JG(IJ),CBAR(IJ),LINE
                C LINE = LINE+1
                C 920 CONTINUE
                C
                C CARDS 0700
                C
                C CARDS 0800
                C
                C CARDS 1000
                C
                C CARD 1100
                C
                C CARDS 1101 AND UP
                C
                C CARDS 1200
                C
                C CARDS 1300
                C
                C CARDS 1400
                C
                C CARDS 1500
                C
                C CARDS 1600
                C
                C CARDS 1700,1800
                C
                C CARDS 2000
                C
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C
C
C
C

CARDS 2100

1000 FORMAT(20A4)
1010 FORMAT(I4I5,7X,'003')
1020 FORMAT(I10,1P3E10.3,20X,F5.1,I5,7X,'004')
1030 FORMAT(1P3E10.3,46X,I4)
1040 FORMAT(1P6E10.3,16X,I4)
1050 FORMAT(1P7E10.3,6X,I4)
1055 FORMAT(2I5,1P3E10.3,36X,I4)
1060 FORMAT(3I5,1P4E10.3,21X,I4)
1070 FORMAT(2I2,I3,1P5E10.3,2I5,6X,I4)
1080 FORMAT(1P5E10.3,67X,'600')
1090 FORMAT(4I5,1P5E10.3,46X,I4)
700 RETURN
END

LEVEL 21.8 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.16.41

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,

SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,IO,XREF

DATA SET D2334IC AT LEVEL 003 AS OF 06/25/79

DATA SET D2332NIC AT LEVEL 007 AS OF 12/01/77

DATA SET D2332NIC AT LEVEL 005 AS OF 11/04/77

DATA SET D2332MIC AT LEVEL 002 AS OF 09/02/77

SUBROUTINE IC

IMPLICIT REAL*8 (A-H,O-Z)

REAL*8 KUN

REAL*4 CLTEST

INTEGER*4 PY(150),PZ(150),PYJ(150),PZJ(150)

INTEGER*4 TITLE(40)

INTEGER*2 NI,NN

INTEGER*2 INBUFF

INTEGER*2 IJPR,IG,JG

INTEGER*2 II(40),KK(40),MM(40),NG(150),INP(50),MNP(50)

DIMENSION XMPR(3),ABARPR(3,3),ANGDPR(3),DPR(3,3),AIDP(3,3),

1 AIC(3,3),ADPR(3,3),VJPI(80,3),APR(3,3),VIP(3,3),XV(3)

DIMENSION XK3(6,6,150),YZMIN(150)

DIMENSION RX(50),RY(50),RZ(50),XNPD(50),YNDP(50),ZNDP(50)

DIMENSION XNP(50),YNP(50),ZNP(50),XDNP(50),YDNP(50),ZDNP(50)

DIMENSION UNP(50),VNP(50),MNP(50),XACCN(50),YACCN(50),ZACCN(50)

DIMENSION IMDRI(80)

COMMON/DEINPR/ AA(150),E(150),Y(150),ZZ(150),XIQ(150),

1 XLBI(150),ZI(150),Z2(150),MC(150),XJ(150),SF26(150),SF35(150),

2 SF26J(150),SF35J(150),PY,PZ,PYJ,PZJ,NSC,NPIN

COMMON/CFIC/ SINBET,COSBET,ABETA(9)

COMMON/DINICP/ STENSI(20),SCOMPI(20),SHEAR(20),EE(20),GG(20),

1 FINI(6,150),VOL(5),VZERO(5),KHATRI(6,4),NVCH,INBUFF(5,8)

COMMON/INIC/ XDP(80),ZDPI(80),PHIDPI(80),PSIDPI(80),

1 THEDPI(80),PPR,PPR,RPR,XGIN,ZGIN,PHIPR,PSIPR,THEPR,

2 XGDOT,YGDOT,ZGDOT

COMMON/INIDCP/ YDP(80)

COMMON/INCFIC/ BETA

COMMON/INPR/ MDRI,NSP

COMMON/HCFI/ SYHFLG

COMMON/NP0012/ HG,NG,INP,MNP

COMMON/NP0112/ II,KK,MH

COMMON/NP0014/ NNP

COMMON/NP00R8/ RX,RY,RZ

COMMON/NP01R8/ XNP,YNP,ZNP,UNP,VNP,MNP,XDNP,YDNP,ZDNP,

1 XACCNP,YACCNP,ZACCNP,SBUCKR(150),PCR(150)

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ISN 0031	COMMON/NP02R8/ XNPD, YNPD, ZNPD	00000410
ISN 0032	COMMON/OLEO/ EOLE(20), FA(20), EXP(20), YMAX(20),	00000420
	1 YOLE(20), BOLE(20), BROLE(20), XKEXT(20), XKCHP(20), FCOUL(20),	00000430
	2 ALPHAP, IGOLE(20), JGOLE(20), MGOLE(20), NGOLE(20), NOLE	00000440
ISN 0033	COMMON/DEIC/ WTOT, CLTEST(150)	00000450
ISN 0034	COMMON/COMALL/ C(6,150), P(60), R(60), U(60), V(60), W(60), X(60),	00000460
	1 Y(60), Z(60), AI(9), AJ(9), SC(40), XC(6), XK(5400), XI(80),	00000470
	2 YI(60), ZI(60), XZI(60), YZI(60), AIJ(9), BIJ(720),	00000480
	3 DRI(150), OAI(720), VEE(900), MGT(60), PHI(60), THETA(60), PSI(60),	00000490
	4 PDOT(60), QDOT(60), RDOT(60), UDOT(60), VDOT(60), WDOT(60), XDOT(60),	00000500
	5 YDOT(60), ZDOT(60), PHIDOT(60), THEDOT(60), PSIDOT(60), TIME, DELTAT,	00000510
	6 XACCI(60), YACCI(60), ZACC(60), AIDOT(9),	00000520
	7 PHIJ(150), THEIJ(150), PSIIJ(150), SUMDF(6,150), TITLE,	00000530
	8 XLBAR(40), FSPBAR(40), VEEDOT(3,3), DX(60), DY(60), DZ(60),	00000540
	9 DPINI(60), DQINI(60), DRINI(60), SEIJ(150), DEIJ(150), CEIK(40),	00000550
	A CEIKF(40),	00000560
	B SBARI(40), KUNI(40), MAXNM, MAXIGS, MAXTBL,	00000570
	C NI, NB, I, J, IG(150), JG(150),	00000580
	D NI(900), NN(40), IJFR(150)	00000590
ISN 0035	COMMON/IPIC/ NIC	00000600
ISN 0036	EQUIVALENCE (PPR, XHPR(1)), (QPR, XHPR(2)), (RPR, XHPR(3)),	00000610
	1 (PHIDPR, ANGDP(1)), (THEDPR, ANGDP(2)), (PSIDPR, ANGDP(3))	00000620
	EQUIVALENCE (XK(1), XK3(1,1,1))	00000630
	SIN(X) = DSIN(X)	00000640
	COS(X) = DCOS(X)	00000650
	SGRT(X) = DSGRT(X)	00000660
	ARSINI(X) = DARSIN(X)	00000670
	ATAN2(Y,X) = DATAN2(Y,X)	00000680
	AMINI(X,Y) = DMINI(X,Y)	00000690
	ABS(X) = DABS(X)	00000700
	WTOT = 0.0	00000710
	PI = 3.1415926535897932400	00000720
	PI2 = PI/2.	00000730
	PIN = -PI	00000740
	PI2N = -PI2	00000750
	BETAR = BETA*PI/180.	00000760
	SINBET = DSIN(BETAR)	00000770
	COSBET = DCOS(BETAR)	00000780
	ABETA(1) = COSBET	00000790
	ABETA(2) = 0.	00000800
	ABETA(3) = -SINBET	00000810
	ABETA(4) = 0.	00000820
	ABETA(5) = 1.	00000830
	ABETA(6) = 0.	00000840
	ABETA(7) = SINBET	00000850
	ABETA(8) = 0.	00000860
	ABETA(9) = COSBET	00000870
	KHATRI(1,1) = 3	00000880
	KHATRI(1,2) = 4	00000890
	KHATRI(1,3) = 7	00000900
	KHATRI(1,4) = 8	00000910
	KHATRI(2,1) = 1	00000920
ISN 0067	KHATRI(2,2) = 2	00000930

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ISN 0068      KMATRI(2,3) = 5
ISN 0069      KMATRI(2,4) = 6
ISN 0070      KMATRI(3,1) = 1
ISN 0071      KMATRI(3,2) = 3
ISN 0072      KMATRI(3,3) = 5
ISN 0073      KMATRI(3,4) = 7
ISN 0074      KMATRI(4,1) = 2
ISN 0075      KMATRI(4,2) = 4
ISN 0076      KMATRI(4,3) = 6
ISN 0077      KMATRI(4,4) = 8
ISN 0078      KMATRI(5,1) = 1
ISN 0079      KMATRI(5,2) = 2
ISN 0080      KMATRI(5,3) = 3
ISN 0081      KMATRI(5,4) = 4
ISN 0082      KMATRI(6,1) = 5
ISN 0083      KMATRI(6,2) = 6
ISN 0084      KMATRI(6,3) = 7
ISN 0085      KMATRI(6,4) = 8
ISN 0086      IF(BETA.EQ.90.D0) GO TO 2000
ISN 0087      TANGENT = SINBET/COSBET
ISN 0088      ZSLMAX = 0.0
ISN 0089      DO 2002 I=1,6
ISN 0090      DO 2002 K=1,150
ISN 0091      FINT(I,K) = 0.00
ISN 0092
ISN 0093      2002 CONTINUE
ISN 0094      PRINT 2001
ISN 0095      2001 FORMAT(1H1 / 1X, 'MODEL PARAMETERS')
ISN 0096      DO 2006 I=1,NM
ISN 0097      IMORI(I) = 0
ISN 0098      2006 CONTINUE
ISN 0099      DO 2004 IJ=1,NB
ISN 0100      IF(IJPR(IJ).NE.0) IMORI(JG(IJ))=1
ISN 0101      2004 CONTINUE
ISN 0102      DO 2010 I = 1,NM
ISN 0103      IF(IMORI(I).NE.0) GO TO 2010
ISN 0104      WTOT = WTOT+MGT(I)
ISN 0106
ISN 0107      C
ISN 0108      C
ISN 0109      C
ISN 0110      IF(SYMPFG.NE.1.OR.YDP(I).EQ.0.) GO TO 2010
ISN 0111      WTOT = WTOT+MGT(I)
ISN 0112      2010 CONTINUE
ISN 0113      PRINT 2011,WTOT
ISN 0114      2011 FORMAT(1X, 'VEHICLE WT = ',1PE12.6)
ISN 0115      XGOP = 0.0
ISN 0116      YGOP = 0.0
ISN 0117      ZGOP = 0.0
ISN 0118      DO 2020 I = 1,NM
ISN 0119      IF(IMORI(I).NE.0) GO TO 2020
ISN 0120      XGOP = XGOP+MGT(I)*XDP(I)
ISN 0121      YGOP = YGOP+MGT(I)*YDP(I)
ISN 0122      ZGOP = ZGOP+MGT(I)*ZDP(I)
ISN 0123      IF(SYMPFG.NE.1.OR.YDP(I).EQ.0.) GO TO 2020

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ISN 0124  XGDP = XGDP+MGT(I)*XDP(I)
ISN 0125  YGDP = YGDP-MGT(I)*YDP(I)
ISN 0126  ZGDP = ZGDP+MGT(I)*ZDP(I)
ISN 0127  2020 CONTINUE
ISN 0128  XGDP = XGDP/WTOT
ISN 0129  YGDP = YGDP/WTOT
ISN 0130  ZGDP = ZGDP/WTOT
ISN 0131  PRINT 2013
ISN 0132  2013 FORMAT(/ IX, 'VEHICLE CG POSITION')
ISN 0133  PRINT 2012, XGDP, YGDP, ZGDP
ISN 0134  2012 FORMAT(IX, 'X (FS) = ', IPE12.5 /
1 IX, 'Y (BL) = ', IPE12.5 /
1 IX, 'Z (WL) = ', IPE12.5)

C APRIME AND ABAPRIME (3)
CALL EULER(APR, PHIPR, THEPR, PSIPR)
S1 = SIN(PHIPR)
C1 = COS(PHIPR)
S2 = SIN(THEPR)
C2 = COS(THEPR)

C NOW ABAPRIME (4)
ABAPR(1,1) = 1.0
ABAPR(2,1) = 0.0
ABAPR(3,1) = 0.0
ABAPR(1,2) = S1*S2/C2
ABAPR(2,2) = C1
ABAPR(3,2) = S1/C2
ABAPR(1,3) = C1*S2/C2
ABAPR(2,3) = -S1
ABAPR(3,3) = C1/C2

C ANGLE DOT PRIMES (6)
CALL MATVEC(ABAPR, XHPR, ANGDP, 0)

C D PRIME (7)
DPR(1,1) = 0.0
DPR(1,2) = THEDP*S1-PSIDPR*C1*C2
DPR(1,3) = THEDP*C1+PSIDPR*S1*C2
DPR(2,1) = -DPR(1,2)
DPR(2,2) = 0.0
DPR(2,3) = -PHIDPR+PSIDPR*S2
DPR(3,1) = -DPR(1,3)
DPR(3,2) = -DPR(2,3)
DPR(3,3) = 0.0

C A DOT PRIME (8)
CALL MATMUL(APR, DPR, ADPR)
ZCHMAX = 0.0
ZSLMAX = 0.
DO 2040 I = 1, NM
CALL EULER(AIDP, PHIDP(I), THEDP(I), PSIDP(I))
CALL MATMUL(APR, AIDP, AIC)
THETA(I) = -ARSIN(AIC(3,1))
IF (THEPR.GT.PI2.AND.THEPR.LE.PI) THETA(I)=PI-THETA(I)
IF (THEPR.LT.PI2.AND.THEPR.GE.PIN) THETA(I)=PIN-THETA(I)
CT = 1./COS(THETA(I))
PHI(I) = ARSIN(AIC(3,2)*CT)

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ISN 0135  00001470
ISN 0136  00001480
ISN 0137  00001490
ISN 0138  00001500
ISN 0139  00001510
ISN 0140  00001520
ISN 0141  00001530
ISN 0142  00001540
ISN 0143  00001550
ISN 0144  00001560
ISN 0145  00001570
ISN 0146  00001580
ISN 0147  00001590
ISN 0148  00001600
ISN 0149  00001610
ISN 0150  00001620
ISN 0151  00001630
ISN 0152  00001640
ISN 0153  00001650
ISN 0154  00001660
ISN 0155  00001670
ISN 0156  00001680
ISN 0157  00001690
ISN 0158  00001700
ISN 0159  00001710
ISN 0160  00001720
ISN 0161  00001730
ISN 0162  00001740
ISN 0163  00001750
ISN 0164  00001760
ISN 0165  00001770
ISN 0166  00001780
ISN 0167  00001790
ISN 0168  00001800
ISN 0169  00001810
ISN 0170  00001820
ISN 0171  00001830
ISN 0172  00001840
ISN 0173  00001850
ISN 0174  00001860
ISN 0175  00001870
ISN 0176  00001880
ISN 0177  00001890
ISN 0178  00001900
ISN 0179  00001910
ISN 0180  00001920
ISN 0181  00001930
ISN 0182  00001940
ISN 0183  00001950
ISN 0184  00001960
ISN 0185  00001970
ISN 0186  00001980
ISN 0187  00001990

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ISN 0172      PSI(I) = ARSIN(AIC(2,1)*CT)
ISN 0173      VJP(I,1) = XGDP-YDP(I)
ISN 0174      VJP(I,2) = YGDP-YDP(I)
ISN 0175      VJP(I,3) = ZGDP-ZDP(I)
ISN 0176      2040 CONTINUE
C
C      CALCULATE VECTOR COMPONENTS FROM MASS I TO NODE POINT M
C      FOR ALL NNP NODE POINTS.
C
ISN 0177      IF(NNP.EQ.0) GO TO 2051
ISN 0179      DO 3000 JJ=1,NNP
ISN 0180      I = INP(JJ)
ISN 0181      T1 = XDP(I)-XNPDP(JJ)
ISN 0182      T2 = YDP(I)-YNPDP(JJ)
ISN 0183      T3 = ZDP(I)-ZNPDP(JJ)
C
C      THESE ARE IN (-) AIRPLANE AXES. CONVERT TO BODY AXES BY
C      MULTIPLYING BY AIDP TRANSPOSE. THIS NORMALLY IS UNITY.
C
ISN 0184      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0185      RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
ISN 0186      RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
ISN 0187      RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
ISN 0188      3000 CONTINUE
C
C      DETERMINE LOWEST SPRING.
C
ISN 0189      2051 DO 2050 IKM=1,NSP
ISN 0190      I = II(IKM)
ISN 0191      K = KK(IKM)
ISN 0192      M = MM(IKM)
ISN 0193      IF(M.NE.0) GO TO 2052
ISN 0195      RRX = 0.
ISN 0196      RRY = 0.
ISN 0197      RYZ = 0.
ISN 0198      GO TO 2054
ISN 0199      2052 DO 2056 JJ=1,NNP
ISN 0200      IF(II.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 2058
ISN 0202      2056 CONTINUE
ISN 0203      2058 RRX = RX(JJ)
ISN 0204      RRY = RY(JJ)
ISN 0205      RYZ = RZ(JJ)
ISN 0206      2054 CONTINUE
C
C      EQUATIONS (1-122) FOR AI.
C
ISN 0207      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0208      CALL MATMUL(APR,AIDP,AIC)
ISN 0209      DVRI = AIC(1,1)*RRX+AIC(1,2)*RRY+AIC(1,3)*RRZ
ISN 0210      DVRI = AIC(3,1)*RRX+AIC(3,2)*RRY+AIC(3,3)*RRZ
ISN 0211      VC = AIC(3,K)*XLBAR(IKM)+DVR3
ISN 0212      VCX = AIC(1,K)*XLBAR(IKM)+DVR1
ISN 0213      DO 2062 L=1,3

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ISN 0214 VC = VC*APR(3,L)*VJP(I,L)
ISN 0215 VCX = VCX*APR(1,L)*VJP(I,L)
ISN 0216 2062 CONTINUE
ISN 0217 ZSL = VCX*SINBET+VC*COSEBET
ISN 0218 IF(VC-ZCHAX) 2064,2064,2066
ISN 0219 2066 ZCHAX = VC
ISN 0220 2064 IF(ZSL-ZSLMAX) 2050,2050,2068
ISN 0221 2068 ZSLMAX = ZSL
ISN 0222 2050 CONTINUE
ISN 0223 PRINT 2014
ISN 0224 2014 FORMAT(/ 1X,'VEHICLE INERTIAS (IN-LB-SEC**2)')
ISN 0225 XIG = 0
ISN 0226 YIG = 0
ISN 0227 ZIG = 0
ISN 0228 DO 2015 I=1,NM
ISN 0229 IF(IMORI(I).NE.0) GO TO 2015
ISN 0230 XARM = XDP(I) - XGDP
ISN 0231 YARM = YDP(I) - YGDP
ISN 0232 ZARM = ZDP(I) - ZGDP
ISN 0233 GOODY1 = MGT(I)*(YARM*YARM+ZARM*ZARM)/386.
ISN 0234 GOODY2 = MGT(I)*(XARM*XARM+ZARM*ZARM)/386.
ISN 0235 GOODY3 = MGT(I)*(XARM*XARM+YARM*YARM)/386.
ISN 0236 XIG = XIG+XI(I)+GOODY1
ISN 0237 YIG = YIG+YI(I)+GOODY2
ISN 0238 ZIG = ZIG+ZI(I)+GOODY3
ISN 0239 IF(SYMF1G.NE.1.OR.YDP(I).EQ.0.) GO TO 2015
ISN 0240 XIG = XIG+XI(I)+GOODY1
ISN 0241 YIG = YIG+YI(I)+GOODY2
ISN 0242 ZIG = ZIG+ZI(I)+GOODY3
ISN 0243 2015 CONTINUE
ISN 0244 PRINT 2016,XIG,YIG,ZIG
ISN 0245 2016 FORMAT(1X,'(XX) = ',1PE11.5 / 1X,'(YY) = ',1PE11.5 / 1X,
ISN 0246 '1'(ZZ) = ',1PE11.5)
ISN 0247 ZSL = -ZSLMAX-.001
ISN 0248 ZG = -ZCHAX-.001
ISN 0249 IF(BETA) 2101,2101,2102
ISN 0250 2101 XG = 0.
ISN 0251 GO TO 2220
ISN 0252 2102 IF(BETA-90.) 2103,2104,2103
ISN 0253 2104 XG = ZSL
ISN 0254 GO TO 2220
ISN 0255 2103 ZSLG = -ZSL/COSEBET
ISN 0256 DELZ = -ZG-ZSLG*ZGIN
ISN 0257 XG = DELZ/TANBET
ISN 0258 2220 PRINT 2105
ISN 0259 2105 FORMAT(/ 1X,'VEHICLE CG INITIAL GROUND COORDINATES' /
ISN 0260 1 1X,'XCG IS THE DISTANCE FROM SLOPE/GROUND INTERSECTION TO VEHICLE
1 CG,+FORWARD' /
2 CG,+FORWARD' /
3 1X,'ZCG IS THE DISTANCE FROM GROUND PLANE TO VEHICLE CG,+DOWN')
ISN 0261 DELXG = XG-XGIN
ISN 0262 DELZG = ZG-ZGIN
ISN 0263 PRINT 2091,DELXG,DELZG
ISN 0264 2091 FORMAT(1X,'XCG = ',1PE12.5 / 1X,'ZCG = ',1PE12.5)

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ISN 0265 DO 2022 IJ=1,NB
ISN 0266 I = IG(IJ)
ISN 0267 J = JG(IJ)
ISN 0268 M = MG(IJ)
ISN 0269 N = NG(IJ)
ISN 0270 IF(M.EQ.0) GO TO 5020
ISN 0271 DO 5010 JI=1,NP
ISN 0272 IF(JI.EQ.INP(JI)).AND.M.EQ.MNP(JI)) GO TO 5020
ISN 0273 5010 CONTINUE
ISN 0274 5020 IF(N.EQ.0) GO TO 5030
ISN 0275 DO 5040 JJ=1,NP
ISN 0276 IF(JJ.EQ.INP(JJ)).AND.N.EQ.NMP(JJ)) GO TO 5030
ISN 0277 5040 CONTINUE
ISN 0278 C
ISN 0279 C THE FOLLOWING CODE GETS CLTEST(IJ),WHICH IS 1 IF BEAM IJ
ISN 0280 C LIES ENTIRELY IN THE CENTER PLANE OF THE AIRPLANE.THIS
ISN 0281 C IS USED IN DERIV FOR A NUMBER OF TESTS.
ISN 0282 5030 CLTEST(IJ) = 0.
ISN 0283 IF(SYMFLE.NE.1.) GO TO 2022
ISN 0284 IF(YDP(I).NE.0.OR.YDP(J).NE.0.) GO TO 2022
ISN 0285 C
ISN 0286 C BOTH MASSES ON CENTERLINE.
ISN 0287 C
ISN 0288 IF(M.EQ.0.AND.N.EQ.0) GO TO 5000
ISN 0289 IF(M.EQ.0) GO TO 5001
ISN 0290 IF(N.EQ.0) GO TO 5002
ISN 0291 IF(YNPD(JI).EQ.0.AND.YNPD(JJ).EQ.0.) GO TO 5000
ISN 0292 GO TO 2022
ISN 0293 5001 IF(YNPD(JJ).EQ.0.) GO TO 5000
ISN 0294 GO TO 2022
ISN 0295 5002 IF(YNPD(JI).EQ.0.) GO TO 5000
ISN 0296 GO TO 2022
ISN 0297 5000 CLTEST(IJ) = 1.
ISN 0298 2022 CONTINUE
ISN 0299 C
ISN 0300 C LOOPC
ISN 0301 C
ISN 0302 2150 DO 2090 I = 1,NM
ISN 0303 CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0304 CALL MATMUL(APR,AIDP,AIC)
ISN 0305 VIP(1) = VJP(I,1)
ISN 0306 VIP(2) = VJP(I,2)
ISN 0307 VIP(3) = VJP(I,3)
ISN 0308 C (14)
ISN 0309 CALL MATVEC(APR,VIP,XV,0)
ISN 0310 XV(1) = XV(1)+XG-XGIN
ISN 0311 XV(3) = XV(3)+ZG-ZGIN
ISN 0312 X(I) = XV(1)
ISN 0313 Y(I) = XV(2)
ISN 0314 Z(I) = XV(3)
ISN 0315 C (15)
ISN 0316 CALL MATVEC(ADPR,VIP,XV,0)

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ISN 0317      XV(1) = XV(1)+XGDOT
ISN 0318      XV(2) = XV(2)+YGDOT
ISN 0319      XV(3) = XV(3)+ZGDOT
ISN 0320      XDOT(I) = XV(1)
ISN 0321      YDOT(I) = XV(2)
ISN 0322      ZDOT(I) = XV(3)

C (16)
ISN 0323      CALL MATVEC(AIC,XV,VIP,1)
ISN 0324      U(I) = VIP(1)
ISN 0325      V(I) = VIP(2)
ISN 0326      W(I) = VIP(3)

C (17)
ISN 0327      CALL MATVEC(AIDP,XMPR,VIP,1)
ISN 0328      P(I) = VIP(1)
ISN 0329      Q(I) = VIP(2)
ISN 0330      R(I) = VIP(3)

C AIBAR (18)
ISN 0331      S1 = SIN(PHI(I))
ISN 0332      C1 = COS(PHI(I))
ISN 0333      S2 = SIN(THETA(I))
ISN 0334      C2 = COS(THETA(I))
ISN 0335      ABARPR(1,2) = S1*S2/C2
ISN 0336      ABARPR(2,2) = C1
ISN 0337      ABARPR(3,2) = S1/C2
ISN 0338      ABARPR(1,3) = C1*S2/C2
ISN 0339      ABARPR(2,3) = -S1
ISN 0340      ABARPR(3,3) = C1/C2

C (19)
ISN 0341      CALL MATVEC(ABARPR,VIP,XV,0)
ISN 0342      PHIDOT(I) = XV(1)
ISN 0343      THEDOT(I) = XV(2)
ISN 0344      PSIDOT(I) = XV(3)

C END LOOP C
ISN 0345      2090 CONTINUE
ISN 0346      IF(INP.EQ.0) GO TO 4000
ISN 0347      DO 4010 JJ=1,NNP
ISN 0348      I = INP(JJ)
ISN 0349      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0350      CALL MATMUL(APR,AIDP,AIC)
ISN 0351      TX = AIC(1,1)*RX(JJ)+AIC(1,2)*RY(JJ)+AIC(1,3)*RZ(JJ)
ISN 0352      TY = AIC(2,1)*RX(JJ)+AIC(2,2)*RY(JJ)+AIC(2,3)*RZ(JJ)
ISN 0353      TZ = AIC(3,1)*RX(JJ)+AIC(3,2)*RY(JJ)+AIC(3,3)*RZ(JJ)
ISN 0354      XNP(JJ) = X(I)+TX
ISN 0355      YNP(JJ) = Y(I)+TY
ISN 0356      ZNP(JJ) = Z(I)+TZ
ISN 0357      4010 CONTINUE
ISN 0358      4000 CONTINUE
ISN 0359      IF(NOLEO.EQ.0) GO TO 4020
ISN 0360      DO 4022 J=1,NOLEO
ISN 0361      YOLEO(J)=0.
ISN 0362      4024 YNEM=-FAD(J)*(EOLEO(J)/(EOLEO(J)-YOLEO(J)))*EXPOLE(J)
ISN 0363      YNEM=(YNEM+FAA(J))/XKEXT(J)
ISN 0364      ERR=ABS(YNEM-YOLEO(J))
ISN 0365
ISN 0366

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00004000
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00004110

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ISN 0367 YOLEO(J)=YNEW
ISN 0368 IF(ERR.LT.0.0001) GO TO 4022
ISN 0370 GO TO 4024
ISN 0371 4022 CONTINUE
C
C YOLEO = AXIAL COMPRESSION DISTANCE OF STRUT MEASURED FROM THE
C FULLY EXTENDED POSITION
C
ISN 0372 4020 IF(NIC.LE.0) RETURN
C
C COMPUTE PREL. UNCOUPLED LOADS AND DEFLECTIONS
C
C PRINT 5011
ISN 0374 5011 FORMAT(/ / 1X, 'BEAM LOADS')
ISN 0375 PRINT 5012
ISN 0376 5012 FORMAT(/ / 6X, 'BEAM', 19X, 'AXIAL LOAD', 19X, 'SHEAR FORCE', 22X,
ISN 0377 * 'MOMENT', 20X, 'BEAM' / 2X, 'I J I J M N', 3X, 'BUCKLING',
* 4X, 'TENSION COMPRESSION LATERAL(Y) VERTICAL(Z)', 3X,
* 'ROLL(X)', 5X, 'PITCH(Y)', 5X, 'YAW(Z)', 3X, 'I J I J M N' /
DO 2400 IJ=1,NB
ISN 0378 IF(Y(IJ).LE.ZZ(IJ)) GO TO 5013
ISN 0379 YZMIN(IJ)=ZZ(IJ)
ISN 0381 GO TO 5014
ISN 0382 5013 YZMIN(IJ)=YY(IJ)
C
C YZMIN = MIN. CROSS SECTION AREA INERTIA
C
ISN 0383 5013 YZMIN(IJ)=YY(IJ)
C
C CALC. FORCES AND MOMENTS
C
C AXIAL FORCES
ISN 0384 5014 PCRFY=4.*PI*PI*E(IJ)*Y(IJ)/(XLB(IJ)**2)
ISN 0385 PCRFZ=4.*PI*PI*E(IJ)*Z(IJ)/(XLB(IJ)**2)
ISN 0386 PTENS=STENS(MC(IJ))*AA(IJ)
ISN 0387 PCOMP=SCOMP(MC(IJ))*AA(IJ)
C
C SHEAR FORCES
ISN 0388 FY=-.67*SHEAR(MC(IJ))*AA(IJ)
ISN 0389 FZ=FY
C
C MOMENTS
ISN 0390 IF(XIQ(IJ).NE.0.) GO TO 400
ISN 0392 THOMX = 0.
ISN 0393 GO TO 410
ISN 0394 400 THOMX=SHEAR(MC(IJ))/XIQ(IJ)
ISN 0395 410 SYIELD = AMINI(SCOMP(MC(IJ)),STENS(MC(IJ)))
ISN 0396 IF(ZI(IJ).NE.0.) GO TO 420
ISN 0398 BENDMY = 0.
ISN 0399 GO TO 430
ISN 0400 420 BENDMY=SYIELD*Y(IJ)/ZI(IJ)
ISN 0401 430 IF(Z2(IJ).NE.0.) GO TO 440
ISN 0403 BENDMZ = 0.
ISN 0404 GO TO 450
ISN 0405 440 BENDMZ=SYIELD*Z(IJ)/Z2(IJ)
C
C CHECK BEAM END CONDITIONS.
C
ISN 0406 450 IF(PY(IJ).EQ.0.AND.PYJ(IJ).EQ.0) GO TO 100
ISN 0408 IF(PY(IJ).EQ.0.OR.PYJ(IJ).EQ.0) GO TO 110

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ISN 0410      C PINNED-PINNED.
ISN 0411      PCRY = PCRFY/4.
ISN 0412      BENDMY = 0.
ISN 0413      FZ = 0.
ISN 0414      GO TO 120
ISN 0415      C FIXED-PINNED.
ISN 0416      110 PCRY = PCRFY/2.
ISN 0417      GO TO 120
ISN 0418      C FIXED-FIXED
ISN 0419      100 PCRY = PCRFY
ISN 0420      120 IF(PZ(IJ)).EQ.0.AND.PZJ(IJ).EQ.0) GO TO 200
ISN 0421      IF(PZ(IJ)).EQ.0.OR.PZJ(IJ).EQ.0) GO TO 210
ISN 0422      C PINNED-PINNED.
ISN 0423      PCRZ = PCRFZ/4.
ISN 0424      BENDMZ = 0.
ISN 0425      FY = 0.
ISN 0426      GO TO 220
ISN 0427      C FIXED-PINNED.
ISN 0428      210 PCRZ = PCRFZ/2.
ISN 0429      GO TO 220
ISN 0430      C FIXED-FIXED
ISN 0431      200 PCRZ = PCRFZ
ISN 0432      220 PCR(IJ) = PCRZ
ISN 0433      IF(PCRY.LT.PCRZ) PCR(IJ)=PCRY
ISN 0434      5018 PRINT 5015,(IJ,IG(IJ),JG(IJ),NG(IJ),PCRP(IJ),PTENS,
ISN 0435      1 PCOMP,FY,FZ,TMOHX,BENDMY,BENDMZ,IJ,IG(IJ),JG(IJ),NG(IJ))
ISN 0436      5015 FORMAT(1X,5I3,1P8E12.4,5I3)
ISN 0437      2400 CONTINUE
ISN 0438      PRINT 5050
ISN 0439      5050 FORMAT(/ / 1X,'BEAM DEFLECTIONS')
ISN 0440      PRINT 5051
ISN 0441      5051 FORMAT(/ / 6X,'BEAM',17X,'DEFLECTION',25X,'TRANSLATION DUE TO',23X,
ISN 0442      * 'ROTATION ABOUT' / 2X,'IJ I J M N',2X,'BUCKLING',4X,
ISN 0443      * 'TENSION COMPRESSION F(Y)',7X,'F(Z)',7X,'BH(Z)',6X,
ISN 0444      * 'BH(Y)',5X,'X-AXIS Y-AXIS Z-AXIS' / )
ISN 0445      C CALC.DEFLECTIONS
ISN 0446      C
ISN 0447      C AXIAL DEFLECTIONS
ISN 0448      C
ISN 0449      DO 2500 IJ=1,NB
ISN 0450      SYIELD = AMINI(SCOMP(MC(IJ)),STENS(MC(IJ)))
ISN 0451      IF(XK3(1,1,IJ)).EQ.0.0) GO TO 5330
ISN 0452      XDEFB = PCR(IJ)/XK3(1,1,IJ)
ISN 0453      XDEFT=STENS(MC(IJ))*AA(IJ)/XK3(1,1,IJ)
ISN 0454      XDEFC=SCOMP(MC(IJ))*AA(IJ)/XK3(1,1,IJ)
ISN 0455      GO TO 5340
ISN 0456      5330 XDEFB = 0.0
ISN 0457      XDEFT = 0.0
ISN 0458      XDEFC = 0.0
ISN 0459      5340 CONTINUE
ISN 0460      C DUE TO SHEAR FORCES
ISN 0461      IF(XK3(2,2,IJ)).EQ.0.0) GO TO 5350
ISN 0462      5350
ISN 0463      00004650
ISN 0464      00004660
ISN 0465      00004670
ISN 0466      00004680
ISN 0467      00004690
ISN 0468      00004700
ISN 0469      00004710
ISN 0470      00004720
ISN 0471      00004730
ISN 0472      00004740
ISN 0473      00004750
ISN 0474      00004760
ISN 0475      00004770
ISN 0476      00004780
ISN 0477      00004790
ISN 0478      00004800
ISN 0479      00004810
ISN 0480      00004820
ISN 0481      00004830
ISN 0482      00004840
ISN 0483      00004850
ISN 0484      00004860
ISN 0485      00004870
ISN 0486      00004880
ISN 0487      00004890
ISN 0488      00004900
ISN 0489      00004910
ISN 0490      00004920
ISN 0491      00004930
ISN 0492      00004940
ISN 0493      00004950
ISN 0494      00004960
ISN 0495      00004970
ISN 0496      00004980
ISN 0497      00004990
ISN 0498      00050000
ISN 0499      00050010
ISN 0500      00050020
ISN 0501      00050030
ISN 0502      00050040
ISN 0503      00050050
ISN 0504      00050060
ISN 0505      00050070
ISN 0506      00050080
ISN 0507      00050090
ISN 0508      00050100
ISN 0509      00050110
ISN 0510      00050120
ISN 0511      00050130
ISN 0512      00050140
ISN 0513      00050150
ISN 0514      00050160
ISN 0515      00050170

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ISN 0452      YDSF=.67*SHEAR(MC(IJ))*AA(IJ)/XX3(2,2,IJ)
ISN 0453      GO TO 5360
ISN 0454      5350 YDSF = 0.0
ISN 0455      5360 IF(XX3(3,3,IJ).EQ.0.0) GO TO 5370
ISN 0456      ZDSF=.67*SHEAR(MC(IJ))*AA(IJ)/XX3(3,3,IJ)
ISN 0457      GO TO 5380
ISN 0458      5370 ZDSF = 0.0
ISN 0459      5380 CONTINUE
ISN 0460      C
ISN 0461      DEF. DUE TO BEND.FORCE ((K55/DEL)*FORCE)
ISN 0462      YHOMZ=4.*SYIELD*ZZ(IJ)/(Z2(IJ)*XLB(IJ))*XX3(2,2,IJ))
ISN 0463      GO TO 5400
ISN 0464      5390 YHOMZ = 0.0
ISN 0465      5400 IF(XX3(3,3,IJ).EQ.0.0) GO TO 5410
ISN 0466      ZHOMY=4.*SYIELD*YY(IJ)/(Z1(IJ)*XLB(IJ))*XX3(3,3,IJ))
ISN 0467      GO TO 5420
ISN 0468      5410 ZHOMY = 0.0
ISN 0469      5420 CONTINUE
ISN 0470      C
ISN 0471      TORSIONAL ROTATION
ISN 0472      IF(XX3(4,4,IJ).NE.0.0) GO TO 5317
ISN 0473      ROTX=0.0
ISN 0474      GO TO 5318
ISN 0475      5317 ROTX-SHEAR(MC(IJ))/XIQ(IJ)/XX3(4,4,IJ)
ISN 0476      C
ISN 0477      BEND. ROTATION ((K33/DEL)*HOM.)
ISN 0478      5318 IF(XX3(5,5,IJ).EQ.0.0) GO TO 5430
ISN 0479      ROTY=4.*SYIELD*YY(IJ)/(Z1(IJ))*XX3(5,5,IJ))
ISN 0480      GO TO 5440
ISN 0481      5430 ROTY = 0.0
ISN 0482      5440 IF(XX3(6,6,IJ).EQ.0.0) GO TO 5450
ISN 0483      ROTZ=4.*SYIELD*ZZ(IJ)/(Z2(IJ))*XX3(6,6,IJ))
ISN 0484      GO TO 5460
ISN 0485      5450 ROTZ = 0.0
ISN 0486      5460 CONTINUE
ISN 0487      5319 PRINT 5319, (IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),XDEFB,XDEFT,XDEFC,
ISN 0488      1 YDSF,ZDSF,YHOMZ,ZHOMY,ROTX,ROTY,ROTZ)
ISN 0489      5319 FORMAT(1X,5I3,1P10E11.3)
ISN 0490      2500 CONTINUE
ISN 0491      RETURN
ISN 0492      END

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 * *****

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  COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
    SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
  C DATA SET D2334IFRNT AT LEVEL 009 AS OF 06/25/79
  C DATA SET D2332GIR AT LEVEL 002 AS OF 05/02/78
  C DATA SET D2332VIR AT LEVEL 004 AS OF 01/26/78
  C DATA SET D2332HIR AT LEVEL 008 AS OF 01/12/78
    SUBROUTINE INPRINT
  C
  ISN 0002 IMPLICIT REAL*8 (A-H,O-Z)
  ISN 0003 REAL*8 KUN
  ISN 0004 REAL*8 LBAR,MU,KE,CASEIN,CASOUT,MINDT
  ISN 0005 REAL*4 KR(2700),SLOPE,XKS,XKI,XKR,LDP(180),LDP1(180)
  ISN 0006 INTEGER*4 PY(150),PZ(150),PJ(150),PZJ(150),RUNIN,RUNOUT
  ISN 0007 INTEGER*4 TITLE(40),BLANK,STOP
  ISN 0008 INTEGER*4 DIR
  ISN 0009 INTEGER*2 IJVM(150),IJFM(150),IJVMH(150),IJFMH(150)
  ISN 0010 INTEGER*2 MQ(180),NQ(180)
  ISN 0011 INTEGER*2 CHUG,INBUFF,IIN,II(40),KK(40),INBUF(80)
  ISN 0012 INTEGER*2 IQ(180),JQ(180),LQ(180),NPQ(180),NLSFLG,IJPR
  ISN 0013 INTEGER*2 NL,NL,IBS,IG,JG
  ISN 0014 INTEGER*2 NPLT,NPFCT,IPFCT,ITPL,NMPTS,MNUM,ISCALE
  ISN 0015 INTEGER*2 NTOL1,NTOL2,NTOL3
  ISN 0016 INTEGER*2 IJSAVE(180)
  ISN 0017 INTEGER*2 NKHVEC(150)
  ISN 0018 INTEGER*2 MH(40),MG(150),NG(150),INP(50),MNP(50)
  ISN 0019 DIMENSION G(150),XP(8),YP(8),ZP(8),VMAX2(6,150),FMAX2(6,150)
  ISN 0020 DIMENSION VMAX3(6,150),FMAX3(6,150)
  ISN 0021 DIMENSION XK3(6,6,150)
  ISN 0022 DIMENSION IJPT(14),VMAXT(6),FMAXT(6)
  ISN 0023 DIMENSION MASSNO(50),DIR(50),NPTS(50)
  ISN 0024 DIMENSION IPHDP(80)
  ISN 0025 COMMON/IBALL/ IBUFI(20)
  ISN 0026 COMMON/DEIN/ XNBAR,XPBAR,YNBAR,YNBAR,ZNBAR,ZNBAR,VOLLENZ(5,3),
  ISN 0027 1 FMAX(900),HEX(80),HEY(80),HEZ(80),ALIFT(80),VMAX(900),VMAXN(900),
  2 FMAXN(900),XKS(2700),XKI(2700),XKR(2700),NLSFLG(900),CHUG(180),
  3 HVP
  ISN 0029 COMMON/DEINPR/ AA(150),E(150),YY(150),ZZ(150),XIQ(150),
  1 XIB(150),ZL(150),Z2(150),HC(150),XJ(150),SF26(150),SF35(150),
  2 SF26J(150),SF35J(150),PY,PZ,PYJ,PZJ,NSC,NPIN
  ISN 0030 COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),EE(20),GG(20),
  1 FINI(6,150),VOLI(5),VZERO(5),KHATRI(6,4),NVCH,INBUFF(5,8)
  ISN 0031 COMMON/DOIN/ CBAR(150)
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ISN 0032	COMMON/DEIR/ PLM26(150), PLM35(150), PLM26J(150), PLM35J(150)	00000410
ISN 0033	COMMON/CFIR/ SIFL(40), SIFL(40), SIFL(40), SIFL(40), XKEFL(40)	00000420
ISN 0034	COMMON/INAC/ACCEL(300), TIM(300), INDEX(50,2), JAY(50,2), KOUNT	00000430
ISN 0035	COMMON/INCF/ SAI(40), SBI(40), SF(40), SI(40), XHU(40), XKE(40),	00000440
ISN 0036	1 XHAXI(40), FSPDF(40), FSPDI(40), GFLX(40), CDAMPI(40), PLOMT	00000450
	COMMON/PPLTS/ XSCALE(10), YSCALE(10), NPLT, NPFT, IPFT, ITPL(10),	00000460
	* NMPTS(10), NMUM(50,10), ISCALE(10)	00000470
ISN 0037	COMMON/INDEAC/ NACC	00000480
ISN 0038	1 THEDP(80), PPR, QPR, RPR, XGIN, ZGIN, PHIPR, PSIPR, THEPR,	00000490
	2 XGDOT, YGDOT, ZGDOT	00000500
ISN 0039	COMMON/INIDCP/ YDP(80)	00000510
ISN 0040	COMMON/INPR/ NDRI, NSP	00000520
ISN 0041	COMMON/INCFIC/ BETA	00000530
ISN 0042	COMMON/IRDE/ PFIL	00000540
ISN 0043	COMMON/MACFIN/ TMAX, IPRINT	00000550
ISN 0044	COMMON/MCFIII/ SYMFLG	00000560
ISN 0045	COMMON/COMNEW/ DAMPC, RUNMOD, FUNMOD	00000570
ISN 0046	COMMON/NP0012/ MG, NG, INP, INP	00000580
ISN 0047	COMMON/NP0112/ II, KK, MH	00000590
ISN 0048	COMMON/NP0212/ MQ, NQ, IJVM, IJFH, IJVM, IJFH	00000600
ISN 0049	COMMON/NP0014/ NNP	00000610
ISN 0050	COMMON/NP02R8/ XNDP, YNDP, ZNDP	00000620
ISN 0051	COMMON/OLEO/EOLEO(20), FAOI(20), EXPOLE(20), YMAX(20),	00000630
	1 YOLEO(20), BOLEO(20), BROLEO(20), XKEXT(20), XKCOMP(20), FCOUL(20),	00000640
	2 ALPHAP, IGOLEO(20), JGOLEO(20), MGOLEO(20), NGOLEO(20), NOLEO	00000650
	COMMON/COMALL/ C(6,150), P(80), Q(80), R(80), U(80), V(80), W(80), X(81),	00000660
	1 Y(81), Z(81), AI(9), AJ(9), SC(40), XC(6), XK(5400), XI(80),	00000670
	2 YI(80), ZI(80), XZI(80), YZI(80), AIJ(9), BIJ(720),	00000680
	3 DRI(150), OAI(720), VEEI(900), MGT(80), PHI(80), THETA(80), PSI(80),	00000690
	4 PDOT(80), QDOT(80), RDOT(80), UDOT(80), VDOT(80), XDOT(80),	00000700
	5 YDOT(80), ZDOT(80), PHIDOT(80), THEDOT(80), PSIDOT(80), TIME, DELTAT,	00000710
	6 XACC(80), YACC(80), ZACC(80), AIDOT(9),	00000720
	7 PHILJ(150), THEIJ(150), PSIIJ(150), SUMDF(6,150), TITLE,	00000730
	8 XLBAR(40), FSPBAR(40), VEEDOT(3,3), DX(81), DY(81), DZ(81),	00000740
	9 DPINI(81), DQIN(81), DRIN(81), SEIJ(150), DEIJ(150), CEIK(40),	00000750
	A CEIKF(40),	00000760
	B SBARI(40), KUN(40), MAXNM, MAXIGS, MAXTBL,	00000770
	C NI, NB, I, J, IG(150), JG(150),	00000780
	D NI(900), NNI(40), IJPR(150)	00000790
ISN 0052	COMMON/ININPR/ NSF, NTF, NDE, NSPD, NED, NS, NRP, NINP	00000800
	COMMON/COMTR8/ G	00000810
ISN 0053	COMMON/UB/ DB(150), IJUB(150), NUB	00000820
ISN 0054	COMMON/STUFF/ NEWI(80), NEWIJ(150), NHOLD, NBOLD	00000830
ISN 0055	COMMON/COMTR4/ KR , LDP , LDP1	00000840
ISN 0056	COMMON/COMTR4/ND, NYBTR, NFBTR, NHI, NKH, NLB,	00000850
ISN 0057	1 COMMON/COMTR12/ Iq , Jq , NPTS , NVBM , IJPR , IPHOP, NFBM	00000860
ISN 0058	COMMON/COMTR12/ Iq , Jq , NPTS , NVBM , IJPR , IPHOP, NFBM	00000870
ISN 0059	1 NKVREC, IJSAVE	00000880
ISN 0060	COMMON/INOUT/ FCUT, NTOL1, NTOL2, NTOL3	00000890
ISN 0061	COMMON/IPIC/ NIC	00000900
ISN 0062	COMMON/RESTRT/ CASEIN, RUNIN, MSECIN, CASOUT, RUNOUT, MSCOUT(5)	00000910
ISN 0063	COMMON /VARINT/ MINDT, DT2, TPRINT, EL, EU, RATHIN, RATHAX, IPC, IVAR	00000920
		00000930


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ISN 0064      EQUIVALENCE (XK(1),XK3(1,1,1))
ISN 0065      EQUIVALENCE (VMAX(1),VMAX2(1)),(FMAX(1),FMAX2(1))
ISN 0066      EQUIVALENCE (VMAXN(1),VMAX3(1)),(FMAXN(1),FMAX3(1))
ISN 0067      EQUIVALENCE (HASSNO(1),INDEX(1,1))
ISN 0068      EQUIVALENCE (DIR(1),INDEX(1,2))
ISN 0069      SQRT(X) = DSQRT(X)
ISN 0070      ABS(X) = DABS(X)
ISN 0071      PI = 3.141592653500

C      CARD 0001,0002
C
C      PRINT 5500, TITLE
ISN 0072
ISN 0073      5500 FORMAT(1H1,20A4,/,1X,20A4)

C      CARD 0003
C
C      PRINT 5504
ISN 0074
ISN 0075      5504 FORMAT(/,1X,'PROGRAM SIZE DATA',/)

C      CARD 0004
C
C      PRINT 5507,NM,NSP,NB,NLB,NHI,MVP,NVCH,NDRI,NMTL,NACC,NVBH,
ISN 0076      1 NVBHN,NFBM,NFBMN,NPH,ND,NKM,NNP
ISN 0077      5507 FORMAT(1X,'NUMBER OF:',/,33X,'NON-',45X,'NON-',5X,'NON-',/,33X,
1 'ZERO',43X,'STANDARD',1X,'STANDARD',1X,'NON-',4X,'NON-',14X,
2 'NO',/,27X,'KP',4X,'HE OR',4X,'MASS',3X,'VOLUME',3X,'ORI',5X,
3 'MTL',3X,'ACCEL',3X,'MAX',5X,'MAX',3X,'ZERO',2X,
4 'STANDARD STIFFNESS NODE',/,1X,'MASSES',2X,'SPRINGS',
5 2X,'BEAMS',2X,'TABLES',3X,'IXY',4X,'PENETR',1X,
6 'CHANGE',1X,'ELEMENTS',1X,'TYPES',3X,'TABLES',2X,'DEFL',4X,
7 'FORCE',2X,'5HPHI',2X,'DAMPING',2X,'MATRICES',/,
8 82X,'NVB',6X,'NFB',/,3X,'NM',
9 6X,'NSP',5X,'NB',5X,'NLB',5X,'NHI',5X,'MVP',5X,'NVCH',4X,
A 'NDRI',3X,'NMTL',5X,'NACC',3X,'+',3X,'+',3X,'+',3X,'+',4X,
B 'NPH',6X,'ND',7X,'NKM',5X,'NNP',/,
C 1X,I4,2I8,I7,I8,I8,I9,I8,I7,I9,I5,3(I4),I7,2I9,I8)
ISN 0078
ISN 0079      PRINT 5961,NSC,NIC,NTOL1,NTOL2,NTOL3
5961 FORMAT(/,2X,'NSC=',15,5X,'NIC=',15,5X,'NTOL1=',15,2',
1 5X,'NTOL2=',15,2',5X,'NTOL3=',15,2')
ISN 0080      PRINT 5962,NOLEO,ALPHA
5962 FORMAT(/,2X,'NO OF OLEO STRUTS=',15,5X,'ALPHA=',PIE10.3)
ISN 0081
ISN 0082      PRINT 1000,CASEIN,CASOUT,RUNIN,RUNOUT,MSECIN,MSCOUT
ISN 0083      1000 FORMAT(/,2X,'PROGRAM DATA MANAGEMENT CONTROL DATA',
1 //10X,'RESTART:',T20,'TITLE - ',A8,
2 T50,'SAVE:',156,'TITLE - ',A8,
3 /T20,'CASE - ',I4,I56,'CASE - ',I4,
4 /T20,'TIME - ',I4,I56,'TIMES - ',I5,I4)
ISN 0084
ISN 0085      PRINT 1008,IVAR,EL,EU,RATHIN,RATMAX
1008 FORMAT(/,2X,'VARIABLE INTEGRATION CONTROL DATA',
1 //5X,'VAR. INT. FLAG = ',I1,
2 2X,'EL = ',F6.3,2X,'EU = ',F6.3,
3 2X,'LOWER RATIO = ',F5.2,2X,'UPPER RATIO = ',F5.2)
ISN 0086      PRINT 5501

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ISN 0087 5501 FORMAT(//,1X,'PROGRAM CONTROL DATA',//,
1 3X,'PRINT INTERVAL',11X,'INTEGRATION',9X,'MAX',10X,
2 'PLOW FORCE',9X,'FILTER CUTOFF',7X,'CASE TYPE',/,
3 1X,'INTEGRATION INTERVAL',9X,'INTERVAL',11X,'TIME',
4 9X,'STARTING TIME',9X,'FREQUENCY',9X,'INDICATOR',//,
5 8X,'DP/DT',20X,'DT',14X,'TMAX',13X,'PLOWT',15X,'FCUT',14X,
6 'RUNMOD')
ISN 0088 PRINT 5503, IPRINT,DELTAT,TMAX,PLOWT,FCUT,RUNMOD
ISN 0089 5503 FORMAT(8X,14,18X,F8.6,9X,F8.6,12X,F7.5,10X,F7.3,12X,F7.3)
ISN 0090 IF(FCUT.EQ.0.) GO TO 5509
ISN 0092 PFIL = 1./(2.*PI*FCUT)
ISN 0093 GO TO 5511
ISN 0094 5509 PFIL = 0.
C
C CARD 0005,006,007
C
ISN 0095 5511 PRINT 3000,NSF,NTF,NDE,NSPD,NED,NS,NRP,NIMP
ISN 0096 3000 FORMAT(//,1X,'TIME HISTORY PRINT CONTROL CARDS',//,
1 2X,'STRAIN',3X,'TOTAL',4X,'BEAM',6X,'EXT.SPRING',
2 2X,'ENERGY',2X,'STRESS',2X,'ACCEL',2X,'IMPULSE',2X,'FORCES',
3 2X,'FORCES',1X,'DEFLECTIONS',5X,'DATA',6X,'DATA',
4 4X,'DATA',3X,'DATA',3X,'DATA',4X,12,18,19,112,111,18,17,18)
ISN 0097 IF(NPLT.EQ.0) GO TO 5519
ISN 0099 5513 PRINT 3002,NPLT,NPCT
ISN 0100 3002 FORMAT(//,1X,'NO.OF MASS POSITION PLOTS EACH TIME=',15,10X,
* 'PLOT PRINT FACTOR =',15)
ISN 0101 PRINT 3003
ISN 0102 3003 FORMAT(//,1X,'PLANE I.D.',5X,'NO.OF POINTS')
ISN 0103 PRINT 3004,(ITPL(J),NMPTS(J),J=1,NPLT)
ISN 0104 3004 FORMAT(3X,15,8X,15)
ISN 0105 GO TO 5510
ISN 0106 5519 PRINT 3001
ISN 0107 3001 FORMAT(//,1X,'NO.MASS POSITION PLOTS')
ISN 0108 5510 PRINT 4000
ISN 0109 4000 FORMAT(//,1X,'VEHICLE INITIAL CONDITIONS',//,
1 1X,'VEHICLE TRANSLATIONAL VELOCITIES IN GROUND AXES (IN/SEC)',/
2 1X,'VEHICLE ROTATIONAL VELOCITIES IN VEHICLE AXES (RAD/SEC)',/
3 1X,'EULER ANGLES OF VEHICLE RELATIVE TO GROUND (RADIAN)',//
4 9X,'XGDOT',13X,'YGDOT',13X,'ZGDOT',11X,'P',16X,'Q',16X,
5 'R',10X,'PHI',13X,'THETA',13X,'PSI',/)
ISN 0110 PRINT 5502, XGDOT,YGDOT,ZGDOT
ISN 0111 PRINT 5502, PPR,QPR,RPR
ISN 0112 PRINT 5502, PHIPR,THEPR,PSIPR
ISN 0113 5502 FORMAT(3(5X,1PE13.5))
ISN 0114 PRINT 4003
ISN 0115 4003 FORMAT(//,1X,'GENERALIZED SURFACE DATA',/)
ISN 0116 3999 PRINT 3999,BETA,XGIN,ZGIN
ISN 0117 3999 FORMAT(1X,'BETA =',F5.1,' DEGREES',/,1X,'XGIN =',F5.1,/,
1 1X,'ZGIN =',F5.1)
C
C BEAM AND MASS NUMBERING CORRESPONDENCE (LEFT/RIGHT) DATA
C
ISN 0118 IF(RUNMOD.LT.2) GO TO 1010

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ISN 0120      NMAX = MAX0(NFOLD,NBOLD)
ISN 0121      PRINT 1050
ISN 0122      1050 FORMAT(/,1X,'CORRESPONDING MASS AND BEAM NUMBERS FOR',
1              'LEFT AND RIGHT SIDES OF AIRPLANE')
ISN 0123      PRINT 1051
ISN 0124      1051 FORMAT(3X,'MASSES',23X,'BEAMS',/1X,'LEFT RIGHT',12X,'LEFT',
1              14X,'RIGHT',3X,'I',5X,'I',9X,'IJ I J M N IJ ',
2              'I J M N')
ISN 0125      DO 1020 I=1,NMAX
ISN 0126      IF(I.GT.NFOLD) GO TO 1030
ISN 0127      IF(I.GT.NBOLD) GO TO 1040
ISN 0128      INEW = NEWI(I)
ISN 0129      IJNEW = NEWIJ(I)
ISN 0130      IF(IJNEW.NE.0) GO TO 1042
ISN 0131      IGT = 0
ISN 0132      JGT = 0
ISN 0133      MGT = 0
ISN 0134      NGT = 0
ISN 0135      GO TO 1044
ISN 0136      1042 IGT = IG(IJNEW)
ISN 0137      JGT = JG(IJNEW)
ISN 0138      MGT = MG(IJNEW)
ISN 0139      NGT = NG(IJNEW)
ISN 0140      GO TO 1020
ISN 0141      1044 PRINT 1052,I,INEW,I,IG(I),JG(I),MG(I),NG(I),IJNEW,IGT,JGT,MGT,NGT
ISN 0142      GO TO 1020
ISN 0143      1030 IJNEW = NEWIJ(I)
ISN 0144      IF(IJNEW.NE.0) GO TO 1046
ISN 0145      IGT = 0
ISN 0146      JGT = 0
ISN 0147      MGT = 0
ISN 0148      NGT = 0
ISN 0149      GO TO 1048
ISN 0150      1046 IGT = IG(IJNEW)
ISN 0151      JGT = JG(IJNEW)
ISN 0152      MGT = MG(IJNEW)
ISN 0153      NGT = NG(IJNEW)
ISN 0154      GO TO 1020
ISN 0155      1048 PRINT 1053,I,IG(I),JG(I),MG(I),NG(I),IJNEW,IGT,JGT,MGT,NGT
ISN 0156      GO TO 1020
ISN 0157      1040 PRINT 1052,I,NEWI(I)
ISN 0158      1020 CONTINUE
ISN 0159      1052 FORMAT(2X,I2,4X,I2,5X,2(3X,5I3))
ISN 0160      1053 FORMAT(15X,2(3X,5I3))
ISN 0161      1010 PRINT 5498
ISN 0162      5498 FORMAT(/,1X,'MASS DATA')
ISN 0163      PRINT 5499
ISN 0164      5499 FORMAT(/,9X,'WEIGHTS',11X,'MASS COORDINATES F.S.B.L.M.L.',10X,
1              'MASS MOMENTS OF INERTIA (LB-IN-SEC*2)',/)
ISN 0165      PRINT 5505
ISN 0166      5505 FORMAT(2X,'I',8X,'W',14X,3HX'',12X,3HZ'',12X,3XZ'',12X,'IX',
1              13X,'IY',13X,'IZ',10X,'I')
ISN 0167      C
ISN 0168      C
ISN 0169      C
ISN 0170      CARDS 0100

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ISN 0169      PRINT 5506, (I,MGT(I),XDP(I),YDP(I),ZDP(I),XI(I),YI(I),ZI(I),I,
ISN 0170      1 I=1,NM)
              5506 FORMAT(1X,I2,1P7E15.5,4X,I2)
C
ISN 0171      CARDS 0200
ISN 0173      C
ISN 0174      IF(NNP.EQ.0) GO TO 5534
              PRINT 2000
              FORMAT(//,1X,'NODE POINT DATA',//,
ISN 0175      1 3X,'MASS',2X,'N.P.',4X,'NODE POINT COORDINATES F.S.,B.L.,M.L.',
ISN 0176      2 /,5X,'I',4X,'M',8X,3H'',11X,3H'',12X,3H'')
              PRINT 4001, (INP(I),MNP(I),XMPDP(I),YMPDP(I),ZMPDP(I),I=1,NNP)
              4001 FORMAT(1X,2I5,1P3E15.5)
C
ISN 0177      CARDS 0300
ISN 0179      C
ISN 0180      5534 IF(NSP.EQ.0) GO TO 5535
ISN 0181      PRINT 4004
ISN 0182      4004 FORMAT(//,1X,'EXTERNAL SPRING DATA')
              PRINT 4008
              4008 FORMAT(//,17X,'FREE',9X,'FRICTION',7X,'BOTTOMING',7X,'PLOWING',
              1 8X,'GROUND',//,
              2 5X,'SPRING',5X,'LENGTH',7X,'COEFFICIENT',6X,'SPRING',9X,'FORCE',
              3 8X,'FLEXIBILITY',/)
              PRINT 5515
ISN 0183      5515 FORMAT(3X,'I',2X,'K',2X,'M',
ISN 0184      1 5X,'LBAR(IKM)',6X,'MU(IKM)',8X,'KE(IKM)',8X,
              2 'FORCE(IKM)',5X,'GFLEX(IKM)')
              PRINT 5516, (II(J),KK(J),MM(J),XLBAR(J),XMU(J),XKE(J),XMAX(J),
ISN 0185      1 GFLEX(J),J=1,NSP)
              5516 FORMAT(1H,3I3,1P5E15.5)
ISN 0186      PRINT 4009
ISN 0187      4009 FORMAT(/2X,'SPRING',23X,'DEFLECTION COORDINATES',25X,'SPRING AXIAL
ISN 0188      1 FORCES',/)
              PRINT 5517
ISN 0189      5517 FORMAT(3X,'I',2X,'K',2X,'M',6X,'SI(IKM)',8X,'SA(IKM)',8X,
ISN 0190      1 'SB(IKM)',8X,'SF(IKM)',7X,'FSPOI(IKM)',5X,'FSPOF(IKM)',6X,
              2 'CRIT.DAMP',4X,'CDAMP(IKM)')
C
ISN 0191      C
ISN 0192      C
ISN 0193      DO 10 J=1,NSP
ISN 0194      SIFL(J) = SI(J) + FSPOI(J)*GFLEX(J)
ISN 0195      SABL(J) = SA(J) + FSPOI(J)*GFLEX(J)
ISN 0196      SBFL(J) = SB(J) + FSPOF(J)*GFLEX(J)
ISN 0197      SFFL(J) = SF(J) + FSPOF(J)*GFLEX(J)
ISN 0198      IF(XKE(J).EQ.0.) GO TO 20
ISN 0199      XKEFL(J) = 1./(GFLEX(J)+1./XKE(J))
ISN 0200      GO TO 10
ISN 0201      20 XKEFL(J) = 0.
              10 CONTINUE
C
              CARDS 0400
              C
              00002530
              00002540
              00002550
              00002560
              00002570
              00002580
              00002590
              00002600
              00002610
              00002620
              00002630
              00002640
              00002650
              00002660
              00002670
              00002680
              00002690
              00002700
              00002710
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              00002750
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              00002770
              00002780
              00002790
              00002800
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              00002820
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              00002840
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              00002880
              00002890
              00002900
              00002910
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              00002930
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              00002970
              00002980
              00002990
              00003000
              00003010
              00003020
              00003030
              00003040
              00003050

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ISN 0202      C      DO 5160 IKM=1,NSP
ISN 0203      I = II(IKM)
ISN 0204      K = KK(IKM)
ISN 0205      M = MM(IKM)
ISN 0206      XKUN=FSP0I(IKM)/SI(IKM)
ISN 0207      SRT=2.*SQRT(XKUN*WGT(I)/386.4)*CDAMP(IKM)
ISN 0208      SRT=2.*SQRT(XKUN*WGT(I)/386.4)*CDAMP(IKM)
ISN 0209      PRINT 5518,I,K,M,SI(IKM),SAI(IKM),SB(IKM),SF(IKM),FSP0I(IKM),
ISN 0210      1 FSP0F(IKM),CDAMP(IKM),SRT
ISN 0211      5518 FORMAT(1H,3I3,1P8E15.5)
ISN 0212      CDAMP(IKM)=SRT
ISN 0213      5160 CONTINUE
ISN 0214      C
ISN 0215      C      CARDS 0500
ISN 0216      C
ISN 0217      C      MAT. PROP. VALUES
ISN 0218      C      MC=1(4130 STEEL),2(6150H STEEL),3(STAINLESS 3000 SERIES),
ISN 0219      C      4(AL.2024-T3),5(AL.6061-T3),6(CAST AL.B195-T4)
ISN 0220      C      7(LOW MOD.MAT.),8(JUNK),9,10(SPINE FOR DRI)
ISN 0221      C
ISN 0222      EE(1)=30.E06
ISN 0223      EE(2)=30.E06
ISN 0224      EE(3)=28.E06
ISN 0225      EE(4)=10.5E06
ISN 0226      EE(5)=10.0E06
ISN 0227      EE(6)=EE(5)
ISN 0228      EE(7)=1.0E06
ISN 0229      EE(8)=1.0E06
ISN 0230      EE(9)=1.0E06
ISN 0231      EE(10)=1.0E06
ISN 0232      GG(1)=GG(1)
ISN 0233      GG(2)=GG(1)
ISN 0234      GG(3)=12.5E06
ISN 0235      GG(4)=4.0E06
ISN 0236      GG(5)=3.8E06
ISN 0237      GG(6)=3.8E06
ISN 0238      GG(7)=.30E06
ISN 0239      GG(8)=0.
ISN 0240      GG(9)=.30E06
ISN 0241      GG(10)=.30E06
ISN 0242      STENS(1)=75000.
ISN 0243      STENS(2)=205000.
ISN 0244      STENS(3)=70000.
ISN 0245      STENS(4)=47000.
ISN 0246      STENS(5)=35000.
ISN 0247      STENS(6)=16000.
ISN 0248      STENS(7)=16000.
ISN 0249      STENS(8)=16000.
ISN 0250      STENS(9)=16000.
ISN 0251      STENS(10)=16000.
ISN 0252      SCOMP(1)=75000.
ISN 0253      SCOMP(2)=205000.

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ISN 0244 SCOMP(3)=46000.
ISN 0245 SCOMP(4)=39000.
ISN 0246 SCOMP(5)=34000.
ISN 0247 SCOMP(6)=16000.
ISN 0248 SCOMP(7)=16000.
ISN 0249 SCOMP(8)=16000.
ISN 0250 SCOMP(9)=16000.
ISN 0251 SCOMP(10)=16000.
ISN 0252 SHEAR(1)=37500.
ISN 0253 SHEAR(2)=80000.
ISN 0254 SHEAR(3)=36000.
ISN 0255 SHEAR(4)=22000.
ISN 0256 SHEAR(5)=17000.
ISN 0257 SHEAR(6)=17000.
ISN 0258 SHEAR(7)=17000.
ISN 0259 SHEAR(8)=17000.
ISN 0260 SHEAR(9)=17000.
ISN 0261 SHEAR(10)=17000.
ISN 0262 IF(NKIVEC(IJ).NE.0) GO TO 5306
ISN 0263 DO 5305 L=1,6
ISN 0265 DO 5305 K=1,6
ISN 0266 XX3(L,K,IJ) = 0.
ISN 0267
ISN 0268
ISN 0269
ISN 0270
ISN 0271
ISN 0272
ISN 0273
ISN 0274

ISN 0275 XDP( I )
ISN 0276 YDP( I )
ISN 0277 ZDP( I )
ISN 0278 IF(J.EQ.0) GO TO 5212
ISN 0280 XDP( J )
ISN 0281 YDP( J )
ISN 0282 ZDP( J )
ISN 0283

ISN 0285
ISN 0287
ISN 0288
ISN 0290
ISN 0291

5535 DO 5306 IJ=1,NB
IF(NKIVEC(IJ).NE.0) GO TO 5306
DO 5305 L=1,6
DO 5305 K=1,6
XX3(L,K,IJ) = 0.
5305 CONTINUE
5306 CONTINUE
C
C CALCULATE BEAM LENGTHS
DO 5054 IJ=1,NB
I = IG(IJ)
J = JG(IJ)
M = MG(IJ)
N = NG(IJ)
C
C FIRST ASSUME BEAM ENDS ARE AT MASS POINTS.
C
C
XDP( I ) = XDP( I )
YDP( I ) = YDP( I )
ZDP( I ) = ZDP( I )
IF(J.EQ.0) GO TO 5212
XDP( J ) = XDP( J )
YDP( J ) = YDP( J )
ZDP( J ) = ZDP( J )
5212 IF(M.EQ.0.AND.N.EQ.0) GO TO 5210
C
C IF NOT, AT LEAST ONE BEAM END CONNECTS TO A NODE POINT RATHER
C THAN A MASS POINT.
C
C FIRST CHECK END I.
C
IF(M.EQ.0) GO TO 5220
DO 5230 JJ=1,NNP
IF(I.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 5240
5230 CONTINUE
5240 XDP( I ) = XNPDPI( JJ )

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00003590
00003600
00003610
00003620
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00003640
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00003980
00003990
00004000
00004010
00004020
00004030
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00004070
00004080
00004090
00004100
00004110

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ISN 0292      YDPI = YNPDP(JJ)
ISN 0293      ZDPI = ZNPDP(JJ)
ISN 0294      5220 IF(N.EQ.0) GO TO 5210
ISN 0296      DO 5260 JJ=1,NIP
ISN 0297      IF(IJ.EQ.INP(JJ)).AND.N.EQ.NIP(JJ)) GO TO 5270
ISN 0299      5260 CONTINUE
ISN 0300      5270 XDPJ = XNPDP(JJ)
ISN 0301      YDPJ = YNPDP(JJ)
ISN 0302      ZDPJ = ZNPDP(JJ)
ISN 0303      5210 IF(IJ.NE.0) GO TO 5299
C
C   FOR A SYMMETRICAL MODEL, DATA FOR POINT J DOES NOT EXIST.
C
      XLB(IJ) = 2.*ABS(YDPI)
      GO TO 5054
ISN 0305      5299 DELXDP = XDPJ-XDPI
ISN 0306      DELYDP = YDPJ-YDPI
ISN 0307      DELZDP = ZDPJ-ZDPI
ISN 0308      XLB(IJ) = SQRT(DELXDP*DELXDP+DELYDP*DELYDP+DELZDP*DELZDP)
ISN 0309      5054 CONTINUE
ISN 0310      5301 PRINT 5301
ISN 0311      PRINT 5309
ISN 0312      5309 FORMAT(/,1X,'MATERIAL PROPERTIES')
ISN 0313      PRINT 5309
ISN 0314      5309 FORMAT(/,2X,'MATERIAL',5X,'MODULUS OF',10X,
ISN 0315      1 'MODULUS OF',10X,'TENSION',10X,'COMPRESS.',11X,
ISN 0316      2 'SHEAR',/4X,'NO.',8X,'ELASTICITY',
ISN 0317      3 11X,'RIGIDITY',11X,'STRESS',13X,'STRESS',11X,'STRESS',/)
ISN 0318      PRINT 5310,(IJ,EE(IJ),GG(IJ),STENS(IJ),SCOMP(IJ),
ISN 0319      1 SHEAR(IJ),IJ=1,10)
ISN 0320      5310 FORMAT(4X,I2,7X,IPE12.4,8X,E12.4,9X,OPF8.0,10X,F8.0,10X,F8.0)
ISN 0321      IF(NMTL.EQ.0) GO TO 200
ISN 0322      DO 2 LL=1,NMTL
ISN 0323      IJ = IBUF1(LL)
ISN 0324      PRINT 5310,IJ,EE(IJ),GG(IJ),STENS(IJ),SCOMP(IJ),SHEAR(IJ)
ISN 0325      2 CONTINUE
ISN 0326      C COMPUTE STIFFNESS MATRIX
ISN 0327      200 DO 5307 IJ=1,NB
ISN 0328      IF(NKHVEC(IJ).NE.0) GO TO 5307
ISN 0329      E(IJ)=EE(MC(IJ))
ISN 0330      G(IJ)=GG(MC(IJ))
ISN 0331      EOL = E(IJ)/XLB(IJ)
ISN 0332      EOL2 = EOL/XLB(IJ)
ISN 0333      EOL3 = EOL2/XLB(IJ)
C
C   FOR MAN AND DRI TYPE ELEMENTS (TYPES 9 AND 10), CALCULATE AREA
C   AND DAMPING. THESE OVERRIDE ANY INPUT VALUES.
C
      IF(MC(IJ).EQ.9) GO TO 30
      IF(MC(IJ).EQ.10) GO TO 40
      GO TO 100
C
C   MAN ELEMENT.
C
ISN 0332
ISN 0333
ISN 0336

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ISN 0337 30 AAI(J) = 10.2276E-6*XLB(IJ)*MGT(JG(IJ))
ISN 0338 CBAR(IJ) = 0.3*SQRT(1. + MGT(JG(IJ))/MGT(IG(IJ)))
ISN 0339 GO TO 100

C DRI ELEMENT.
C
C
40 AAI(J) = 6.5456E-6*XLB(IJ)*MGT(JG(IJ))
CBAR(IJ) = 0.22*SQRT(1. + MGT(JG(IJ))/MGT(IG(IJ)))
IJPR(IJ) = 1
100 XK3(1,1,IJ) = EOL*AA(IJ)
XK3(2,2,IJ) = EOL3*12.*ZZ(IJ)
XK3(3,3,IJ) = EOL3*12.*YY(IJ)
XK3(4,4,IJ) = 6(IJ)*XJ(IJ)/XLB(IJ)
XK3(5,5,IJ) = EOL*4.*YY(IJ)
XK3(6,6,IJ) = EOL*4.*ZZ(IJ)
XK3(2,6,IJ) = EOL2*(-6.)*ZZ(IJ)
XK3(5,3,IJ) = EOL2*6.*YY(IJ)
XK3(3,5,IJ) = EOL2*6.*YY(IJ)
XK3(6,2,IJ) = EOL2*(-6.)*ZZ(IJ)
5307 CONTINUE
C
C CARDS 0601 AND UP
C
5308 PRINT 5308
5308 FORMAT(/,1X,'INTERNAL BEAM DATA')
5309 PRINT 5302
5302 FORMAT(/,55X,'DISTANCES FROM NEUTRAL',30X,'M',/,55X,
1 'AXIS TO EXTREME FIBRES TORSION',13X,'DAMPING T',/,7X,'BEAM',
2 8X,'AREA',9X,'MOMENTS OF INERTIA',7X,'ZBIJ AXIS YBIJ AXIS ',
3 'PARAMETER LENGTH',5X,'RATIO L P-CODES BEAM',/
4 109X,'Y Z Y Z')
PRINT 5303
5303 FORMAT(2X,'IJ I J M N A',8X,'IYY',7X,'IZZ',
1 8X,'JX',8X,'ZI',8X,'XIQ',6X,'XLB',7X,'CBAR ',
2 'HC I I J I J I J M N')
PRINT 5304,(IJ,IG(IJ),JG(IJ),NG(IJ),AA(IJ),YY(IJ),
1 ZZ(IJ),XJ(IJ),ZI(IJ),Z2(IJ),XIQ(IJ),XLB(IJ),CBAR(IJ),
2 HC(IJ),PY(IJ),PZ(IJ),PJ(IJ),IJ,IG(IJ),JG(IJ),
3 NG(IJ),NG(IJ),IJ=1,NB)
5304 FORMAT(1X,513,1P9E10.3,512,513)
C
C UNSYMMETRICAL BEAM CARDS.
C
IF(NB.EQ.0) GO TO 4050
PRINT 4022
4022 FORMAT(/,1X,'UNSYMMETRICAL BEAM DATA')
PRINT 4024
4024 FORMAT(/,20X,'TENSION-',/,18X,'COMPRESSION',/,6X,
1 'BEAM',11X,'FLAG',5X,'DEADBAND')
PRINT 4026
4026 FORMAT(/,2X,'IJ I J M N',5X,'IJOB',8X,'DB')
DO 4028 IJ=1,NB
IF(IJOB(IJ).EQ.0) GO TO 4028

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ISN 0373      PRINT 4030,IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),IJUB(IJ),DB(IJ)
ISN 0374      4030 FORMAT(IX,5I3,I8,<X,1P1E10.3)
ISN 0375      4028 CONTINUE
C
C      PINNED-END BEAMS AND PLASTIC HINGES
C
ISN 0376      4050 IF(NPIN.EQ.0) GO TO 4020
ISN 0377      PRINT 4052
ISN 0378      4052 FORMAT(//,1X,'PLASTIC HINGE AND END-FIXITY DATA')
ISN 0379      PRINT 4053
ISN 0380      4053 FORMAT(/,6X,'BEAM',7X,'P-CODES',13X,'SHAPE FACTORS',25X,'PLASTIC',
ISN 0381      1 1X,'HINGE MOMENTS')
ISN 0382      PRINT 4054
ISN 0383      4054 FORMAT(/,2X,'IJ I J M N IYIZJYZ',4X,'SF35',4X,'SF26',4X,
ISN 0384      1 'SF35J',3X,'SF26J',3X,'PLM35',7X,'PLM26',7X,'PLM35J',6X,'PLM26J',
ISN 0385      4055 FORMAT(IX,5I3,IX,4I2,3X,4F6.3,2X),4(1P1E10.3,2X))
ISN 0386      DO 4056 IJ=1,NB
ISN 0387      IF(PY(IJ).EQ.0 .AND. PZ(IJ).EQ.0 .AND. PYJ(IJ).EQ.0 .AND.
ISN 0388      1 PZJ(IJ).EQ.0) GO TO 4056
ISN 0389      PLM26(IJ)=SF26(IJ)*STENS(MC(IJ))*ZZ(IJ)/Z2(IJ)
ISN 0390      PLM35(IJ)=SF35(IJ)*STENS(MC(IJ))*YY(IJ)/Z1(IJ)
ISN 0391      PLM26J(IJ)=SF26J(IJ)*STENS(MC(IJ))*ZZ(IJ)/Z2(IJ)
ISN 0392      PLM35J(IJ)=SF35J(IJ)*STENS(MC(IJ))*YY(IJ)/Z1(IJ)
ISN 0393      I=IG(IJ)
ISN 0394      J=JG(IJ)
ISN 0395      M=MG(IJ)
ISN 0396      N=NG(IJ)
ISN 0397      PRINT 4055,IJ,I,J,M,N,PY(IJ),PZ(IJ),PYJ(IJ),PZJ(IJ),SF35(IJ),
ISN 0398      1 SF26(IJ),SF35J(IJ),SF26J(IJ),PLM35(IJ),PLM26(IJ),PLM35J(IJ),
ISN 0399      2 PLM26J(IJ)
ISN 0400      4056 CONTINUE
C
C      CARDS 0700
C
ISN 0401      4020 IF(NOLEO.EQ.0) GO TO 4021
ISN 0402      PRINT 4031
ISN 0403      4031 FORMAT(//,1X,'OLEO STRUT BEAM DATA'//)
ISN 0404      PRINT 4032
ISN 0405      4032 FORMAT( 20X,'BEAM AIR CURVE PARAMETERS')
ISN 0406      PRINT 4033
ISN 0407      4033 FORMAT(/2X,'IJ I J M N',7X,'EOLEO',7X,'FAO',7X,'FAA',5X,
ISN 0408      1 'EXPOLE',5X,'YMAX')
ISN 0409      DO 4042 J=1,NOLEO
ISN 0410      DO 4041 IJ=1,NB
ISN 0411      IF(IGOLEO(IJ).EQ.IG(IJ).AND.JGOLEO(IJ).EQ.JG(IJ).AND.MGOLEO(IJ)
ISN 0412      1 .EQ.MG(IJ).AND.NGOLEO(IJ).EQ.NG(IJ)) GO TO 4045
ISN 0413      4041 CONTINUE
ISN 0414      4045 PRINT 4034,IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),EOLEO(IJ),FAO(IJ),
ISN 0415      1 FAA(IJ),EXPOLE(IJ),YMAX(IJ)
ISN 0416      4034 FORMAT(IX,5I3,5X,1P5E10.3)
ISN 0417      4042 CONTINUE
ISN 0418      PRINT 4035
ISN 0419      4035 FORMAT(/20X,'BEAM DAMPING CONSTANTS.COULOMB FRICTION AND LINEAR '
ISN 0420      0005180
ISN 0421      0005190
ISN 0422      0005200
ISN 0423      0005210
ISN 0424      0005220
ISN 0425      0005230
ISN 0426      0005240
ISN 0427      0005250
ISN 0428      0005260
ISN 0429      0005270
ISN 0430      0005280
ISN 0431      0005290
ISN 0432      0005300
ISN 0433      0005310
ISN 0434      0005320
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ISN 0436      0005340
ISN 0437      0005350
ISN 0438      0005360
ISN 0439      0005370
ISN 0440      0005380
ISN 0441      0005390
ISN 0442      0005400
ISN 0443      0005410
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ISN 0445      0005430
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ISN 0468      0005660
ISN 0469      0005670
ISN 0470      0005680
ISN 0471      0005690
ISN 0472      0005700

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ISN 0416      1 'SPRINGS (EXTENSION&COMPRESSION)')
ISN 0417      PRINT 4036
ISN 0418      4036 FORMAT(2X,'IJ I J M N',8X,'BOLEO',4X,'BROLEO',5X,'XKEXT',
ISN 0419      1 5X,'XKCOMP',4X,'FCOUL')
ISN 0420      DO 4044 J=1,NLEO
ISN 0421      DO 4043 IJ=1,NB
ISN 0422      IF(IJGOLEO(J),EQ,IG(IJ),AND,JGOLEO(J),EQ,JG(IJ),AND,MGOLEO(J)
ISN 0423      1 EQ,MG(IJ),AND,NGOLEO(J),EQ,NG(IJ)) GO TO 4046
ISN 0424      4043 CONTINUE
ISN 0425      4046 PRINT 4034,IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),BOLEO(J),BROLEO(J),
ISN 0426      1 XKEXT(IJ),XKCOMP(J),FCOUL(J)
ISN 0427      4044 CONTINUE
ISN 0428      4021 IF(NLB.EQ.0) GO TO 5540
ISN 0429      4014 PRINT 4014
ISN 0430      4015 FORMAT(2X,'STANDARD',9X,'LINEAR',7X,'BOTTOMING',/,
ISN 0431      1 13X,'BEAM',13X,'DIRECTION',3X,'TABLE NO.',6X,'DEFLECTION',5X,
ISN 0432      2 'DEFLECTION',/)
ISN 0433      PRINT 5930
ISN 0434      5930 FORMAT(4X,'IJ',4X,'I',4X,'J',4X,'M',4X,'N',8X,'L',
ISN 0435      1 11X,'NP',12X,'LDP',12X,'LDP1')
ISN 0436      PRINT 5940,(IJSAVE(I),IQ(I),JQ(I),MQ(I),NQ(I),LQ(I),
ISN 0437      1 NPQ(I),LDP(I),LDP1(I),I=1,NLB)
ISN 0438      5940 FORMAT(1X,515,4X,15,8X,15,5X,1P2E15.5)
ISN 0439      K = -14
ISN 0440      DO 5070 I = 1,NLB
ISN 0441      NP = NPQ(I)
ISN 0442      IF(NP.LE.15) GO TO 5055
ISN 0443      C*****TOO MANY POINTS IN KR TABLE, ABORT
ISN 0444      PRINT 5980, NP,I
ISN 0445      STOP
ISN 0446      5980 FORMAT(1H1,'8. ',15,' POINTS IN KR TABLE',I3,' (MAX IS 15)')
ISN 0447      C*****SET CHUG TO 1.16,31,...
ISN 0448      5055 K = K+15
ISN 0449      CHUG(I) = K
ISN 0450      ICH = CHUG(I)-1
ISN 0451      LDP = LINEAR DEFLECTION POINT
ISN 0452      NPQ.EQ.5,6,7,8,OR 9 COMPUTE KR'S
ISN 0453      NPQ.EQ.10 INPUT KR'S
ISN 0454      NPQ.LT.5 ERROR
ISN 0455      IF(NP.GE.10) GO TO 5082
ISN 0456      KR(ICH+1) = 1.
ISN 0457      KR(ICH+2) = 1.
ISN 0458      KR(ICH+5) = 0.
ISN 0459      KR(ICH+6) = 0.
ISN 0460      KR(ICH+7) = 0.
ISN 0461      KR(ICH+8) = 0.
ISN 0462      XKR(ICH+1) = 0.
ISN 0463      XKR(ICH+2) = LDP(I)
ISN 0464      XKR(ICH+3) = 1.001*LDP(I)
ISN 0465      XKR(ICH+6) = 10.*LDP(I)
ISN 0466      GO TO (5087,5087,5087,5087,5083,5084,5085,5086,5091,5082),NP
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ISN 0459 5087 PRINT 5088,NP
ISN 0460 5088 FORMAT(IX // '9. NUMBER OF LINEAR DEFLECTION POINTS NOT',
* ' ACCEPTABLE VALUE = ',I2)
ISN 0461 STOP
ISN 0462 5083 KR(ICH+3) = 0.
ISN 0463 KR(ICH+4) = 0.
ISN 0464 XKR(ICH+4) = 10.*LDP(I)
ISN 0465 XKR(ICH+5) = 20.*LDP(I)
ISN 0466 GO TO 5082
ISN 0467 5084 KR(ICH+3) = -.25
ISN 0468 KR(ICH+4) = -.25
ISN 0469 XKR(ICH+4) = 4.*LDP(I)
ISN 0470 XKR(ICH+5) = 4.001*LDP(I)
ISN 0471 GO TO 5082
ISN 0472 5085 KR(ICH+3) = -.5
ISN 0473 KR(ICH+4) = -.5
ISN 0474 XKR(ICH+4) = 3.*LDP(I)
ISN 0475 XKR(ICH+5) = 3.001*LDP(I)
ISN 0476 XKR(ICH+7) = 20.*LDP(I)
ISN 0477 GO TO 5082
ISN 0478 5086 KR(ICH+3) = -1.
ISN 0479 KR(ICH+4) = -1.
ISN 0480 XKR(ICH+4) = 2.*LDP(I)
ISN 0481 XKR(ICH+5) = 2.001*LDP(I)
ISN 0482 XKR(ICH+7) = 15.*LDP(I)
ISN 0483 XKR(ICH+8) = 20.*LDP(I)
ISN 0484 GO TO 5082
ISN 0485 5091 KR(ICH+3) = -1.
ISN 0486 KR(ICH+4) = -1.
ISN 0487 KR(ICH+7) = 1.
ISN 0488 KR(ICH+8) = 1.
ISN 0489 KR(ICH+9) = 1.
ISN 0490 XKR(ICH+4) = 2.*LDP(I)
ISN 0491 XKR(ICH+5) = 2.001*LDP(I)
ISN 0492 XKR(ICH+6) = LDP(I)
ISN 0493 XKR(ICH+7) = 1.001*LDP(I)
ISN 0494 XKR(ICH+8) = 20.*LDP(I)
ISN 0495 XKR(ICH+9) = 30.*LDP(I)
ISN 0496 GO TO 5082
C
C CARDS 0800
C
ISN 0497 5082 PRINT 5960,IQ(I),JQ(I),MQ(I),NQ(I),LQ(I)
ISN 0498 5960 FORMAT(IH0,'KR TABLE FOR I,J,M,N,L =',5I5)
ISN 0499 5970 PRINT5970, (J,XKR(ICH+J),KR(ICH+J),J=1,NP)
ISN 0500 5970 FORMAT(IH ,I3,IP2E15.5)
C*****COMPUTE SLOPES AND INTERCEPTS
NP=1 = NP-1
DO 5080 J = 1,NPH1
SLOPE = (KR(ICH+J)-KR(ICH+J+1))/(XKR(ICH+J)-XKR(ICH+J+1))
XKS(ICH+J) = SLOPE
5080 XKI(ICH+J) = KR(ICH+J)-SLOPE*XKR(ICH+J)
C*****MOVE ENDPOINTS 'WAY OUT

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ISN 0506      XKR(ICH+1) = -1.E35
ISN 0507      XKR(ICH+NP) = 1.E35
ISN 0508
5070 CONTINUE
C
C   CARDS 1000 DELETED 6/4/77
C
C   CARD 1100
C
5540 IF(NVP.EQ.0) GO TO 5065
PRINT 4016
4016 FORMAT(//,1X,'VOLUME PENETRATION DATA',/)
PRINT 5538,NVP
5538 FORMAT(1X,'MASS USED TO IDENTIFY CONTROL VOLUME = ',I3)
PRINT 4017
4017 FORMAT(1X,'DISTANCE FROM MASS MEASURED ALONG POSITIVE (P) AND NEGATIVE (N) AXES')
PRINT 5530
5530 FORMAT(7X,'XN',14X,'XP',14X,'YN',14X,'YP',14X,'ZN',14X,'ZP')
PRINT 5522,XNBAR,XPBAR,YNBAR,YPBAR,ZNBAR,ZPBAR
5522 FORMAT(1X,1P6E15.5)
C
C   CARDS 1101 AND UP
C
5065 IF(NDRI.EQ.0) GO TO 5056
PRINT 5531
5531 FORMAT(//,1X,'DRI ELEMENTS',//,2X,'I',2X,'J')
JORI = 2*NDRI
PRINT 5532,((IJPRT(J),J=1,JORI)
5532 FORMAT(2I3)
C
C   CARDS 1200
C
5056 IF(NVCH.EQ.0) GO TO 6000
PRINT 5601
5601 FORMAT(//,1X,'VOLUME CHANGE DATA',/)
FLIPP = 0.
DO 5620 I=1,NVCH
PRINT 5607
5607 FORMAT(9X,'MASS',/,1X,'POINT',2X,'NUMBER',14X,
1 'MASS COORDINATES',/,11X,'I',8X,3HX'',12X,3HY'',12X,3HZ'')
DO 5621 K=1,8
J = INBUFF(I,K)
IF(J.NE.0) GO TO 5623
J = INBUFF(I,K-1)
YDP(J) = -YDP(J)
FLIPP = 1.
5623 XP(K) = XDPI(J)
YP(K) = YDPI(J)
ZP(K) = ZDPI(J)
IF(FLIPP.NE.1.) GO TO 5621
YDP(J) = -YDP(J)
FLIPP = 0.
5621 PRINT 5622,K,J,XP(K),YP(K),ZP(K)

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ISN 0551 5622 FORMAT(IX,I3,I8,IP3E15.5)
ISN 0552     AVG1 = (XP(1)+XP(2)+XP(5)+XP(6))* .25
ISN 0553     AVG2 = (XP(3)+XP(4)+XP(7)+XP(8))* .25
ISN 0554     DLX = -AVG1+AVG2
ISN 0555     AVG2 = (YP(2)+YP(4)+YP(6)+YP(8))* .25
ISN 0556     AVG1 = (YP(1)+YP(5)+YP(3)+YP(7))* .25
ISN 0557     DLY = AVG1-AVG2
ISN 0558     AVG1 = (ZP(1)+ZP(2)+ZP(3)+ZP(4))* .25
ISN 0559     AVG2 = (ZP(5)+ZP(6)+ZP(7)+ZP(8))* .25
ISN 0560     DLZ = AVG1-AVG2
ISN 0561     PRINT 5604
ISN 0562     5604 FORMAT(/,16X,'VOLUME SIDE LENGTHS',13X,'INITIAL VOLUME',/,
1 8X,'DELX',11X,'DELY',11X,'DELZ',11X,'VZERO')
ISN 0563     VZERO(I) = DLX+DLY+DLZ
ISN 0564     PRINT 5605,DLX,DLY,DLZ,VZERO(I)
ISN 0565     5605 FORMAT(IX,IP4E15.5,/)
ISN 0566     VOLENZ(I,1) = DLX
ISN 0567     VOLENZ(I,2) = DLY
ISN 0568     VOLENZ(I,3) = DLZ
ISN 0569     5620 CONTINUE
C
C
C CARDS 1300
C
ISN 0570 6300 IF(NVBH.EQ.0) GO TO 5178
ISN 0572     PRINT 5525
ISN 0573     5525 FORMAT(/,1X,'NON-STANDARD MAXIMUM DEFLECTIONS',/,
1 36X,'MAXIMUM DEFLECTIONS',/,4X,'BEAM',31X,'VMAX(I,J,L) L=',/,
2 2X,'I',2X,'J',2X,'L',2X,'M',2X,'N',
3 5X,'1',11X,'2',11X,'3',11X,'4',
4 11X,'5',11X,'6',/)
ISN 0574     DO 5170 JI=1,NVBH
ISN 0575     I = IG(IJVM(JI))
ISN 0576     J = JG(IJVM(JI))
ISN 0577     M = MG(IJVM(JI))
ISN 0578     N = NG(IJVM(JI))
ISN 0579     DO 5171 IJ=1,NB
ISN 0580     IF(I.EQ.IG(IJ)).AND.(J.EQ.JG(IJ)).AND.
1 M.EQ.MG(IJ).AND.(N.EQ.NG(IJ)) GO TO 5172
ISN 0582     5171 CONTINUE
ISN 0583     5172 PRINT 5190,IJ,I,J,M,N,(VMAX2(L,IJ),L=1,6)
ISN 0584     5190 FORMAT(IX,5I3,1P6E12.4)
ISN 0585     5170 CONTINUE
ISN 0586     5178 IF(NVBH.EQ.0) GO TO 5191
ISN 0588     PRINT 5536
ISN 0589     5536 FORMAT(/,1X,'NON-STANDARD MAXIMUM NEGATIVE DEFLECTION',/,
1 36X,'MAXIMUM DEFLECTIONS',/,4X,'BEAM',31X,'VMAXN(I,J,L) L=',/,
2 2X,'I',2X,'J',2X,'L',2X,'M',2X,'N',
3 5X,'1',11X,'2',11X,'3',11X,'4',11X,'5',11X,'6',/)
ISN 0590     DO 5192 JI=1,NVBH
ISN 0591     I = IG(IJVM(JI))
ISN 0592     J = JG(IJVM(JI))
ISN 0593     M = MG(IJVM(JI))
ISN 0594     N = NG(IJVM(JI))

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ISN 0595      DO 5193 IJ=1,NB
ISN 0596      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ)).AND.
ISN 0598      1 M.EQ.MG(IJ)).AND.N.EQ.NG(IJ)) GO TO 5194
ISN 0599      5193 CONTINUE
ISN 0600      5194 PRINT 5190,IJ,I,J,M,N,(VMAX3(L,IJ),L=1,6)
ISN 0601      5192 CONTINUE
ISN 0602      5191 IF(NFBM.EQ.0) GO TO 5199
ISN 0603      PRINT 5526
ISN 0604      5526 FORMAT(/,1X,'NON-STANDARD MAXIMUM FORCES',/,36X,'MAXIMUM',
ISN 0605      16X,'FORCES',/,4X,'BEAM',31X,'FMAX(I,J,L) L=',/
ISN 0606      22X,'IJ',2X,'I',2X,'J',2X,'M',2X,'N',5X,'1',11X,'2',11X,'3',
ISN 0607      31X,'4',11X,'5',11X,'6',/)
ISN 0608      DO 5180 JI=1,NFBM
ISN 0609      I = IG(IJFM(JI))
ISN 0610      J = JG(IJFM(JI))
ISN 0611      M = MG(IJFM(JI))
ISN 0612      N = NG(IJFM(JI))
ISN 0613      DO 5181 IJ=1,NB
ISN 0614      IF (I.EQ.IG(IJ)).AND.J.EQ.JG(IJ)).AND.M.EQ.
ISN 0615      1MG(IJ)).AND.N.EQ.NG(IJ)) GO TO 5182
ISN 0616      5181 CONTINUE
ISN 0617      5182 PRINT 5190,IJ,I,J,M,N,(FMAX2(L,IJ),L=1,6)
ISN 0618      5180 CONTINUE
ISN 0619      5199 IF(NFBM.EQ.0) GO TO 6001
ISN 0620      PRINT 5537
ISN 0621      5537 FORMAT(/,1X,'NON-STANDARD MAXIMUM NEGATIVE FORCES',/,
ISN 0622      1 36X,'MAXIMUM',6X,'FORCES',/,4X,'BEAM',31X,'FMAXN(I,J,L) L=',/
ISN 0623      2 2X,'IJ',2X,'I',2X,'J',2X,'M',2X,'N',5X,'1',11X,'2',11X,'3',
ISN 0624      3 11X,'4',11X,'5',11X,'6',/)
ISN 0625      DO 5195 JI=1,NFBM
ISN 0626      I=IG(IJFM(JI))
ISN 0627      J=JG(IJFM(JI))
ISN 0628      M=MG(IJFM(JI))
ISN 0629      N=NG(IJFM(JI))
ISN 0630      DO 5197 IJ=1,NB
ISN 0631      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ)).AND.M.EQ.MG(IJ)).AND.
ISN 0632      1 N.EQ.NG(IJ)) GO TO 5196
ISN 0633      5197 CONTINUE
ISN 0634      5196 PRINT 5190,IJ,I,J,M,N,(FMAX3(L,IJ),L=1,6)
ISN 0635      5195 CONTINUE
ISN 0636      C
ISN 0637      C CARDS 1400
ISN 0638      C
ISN 0639      6001 IF(NHI.EQ.0) GO TO 6002
ISN 0640      PRINT 4006
ISN 0641      4006 FORMAT(/,1X,'MASSES HAVING NONZERO ANGULAR MOMENTA (HE)',/,/
ISN 0642      1 1X,'CROSS PRODUCTS OF INERTIA (IXY,IYZ,IXZ)',/,
ISN 0643      2 1X,'OR LIFT CONSTANTS (LC)',/)
ISN 0644      PRINT 5512
ISN 0645      5512 FORMAT(5X,'I',6X,'LC',10X,'HEX',9X,'HEY',9X,'HEZ',9X,'IXY',9X,
ISN 0646      1 'IYZ',9X,'IXZ')
ISN 0647      DO 5120 I = 1,NHI
ISN 0648      PRINT 5508,INBUF(I),ALIFT(INBUF(I)),HEX(INBUF(I)),HEY(INBUF(I)),

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ISN 0639      1HEZ(INBUF(I)),XYI(INBUF(I)),YZI(INBUF(I)),XZI(INBUF(I))
ISN 0640      5506 FORMAT(IX,IS,IP7E12.4)
              5120 CONTINUE
              C
              C      CARDS 1500
              C
              6002 IF(NPH.EQ.0) GO TO 6003
              DO 5550 J=1,NPH
              PRINT 5570
              5570 FORMAT(IX,'NONZERO PHIDP,THEDP,PSIDP',/,9X,'I',3X,'PHIDP',10X,
              1 'THEDP',10X,'PSIDP')
              I = IPHDP(J)
              PRINT 5555,I,PHIDP(I),THEDP(I),PSIDP(I)
              5555 FORMAT(IX,I10,IP3E15.5)
              5550 CONTINUE
              C
              C      CARDS 1600
              C
              PRINT 5571
              5571 FORMAT(IX,'BEAM EULER ANGLES',/,1X,'IJ',2X,'I',2X,'J',3X,
              1 'PHIJ',10X,'THEIJ',10X,'PSIJI')
              DO 5552 J=1,NB
              PRINT 5557,J,IG(J),JG(J),PHIJ(J),THEIJ(J),PSIJI(J)
              5557 FORMAT(II3,IP3E15.5)
              5552 CONTINUE
              C
              C      CARDS 1700,1800
              C
              6003 IF(NACC.EQ.0) GO TO 6005
              PRINT 7001
              7001 FORMAT(//,1X,'ACCELERATION INPUT TABLE DATA')
              PRINT 7006
              7006 FORMAT(//,1X,'MASS LOCATION DIRECTION NO. PTS.')
              DO 7010 I=1,NACC
              PRINT 7009,MASSNO(I),DIR(I),NPTS(I)
              7009 FORMAT(6X,I2,12X,I2,9X,I2)
              7010 CONTINUE
              PRINT 7007
              7007 FORMAT(//,1X,'PT',7X,'TIME',11X,'ACCEL')
              L=0
              DO 7002 I=1,NACC
              K=NPTS(I)
              DO 7002 J=1,K
              L=L+1
              PRINT 7008,L,TIM(L),ACCEL(L)
              7008 FORMAT(IX,I2,2(5X,1PE10.3))
              7002 CONTINUE
              C
              C      CARDS 2100
              C
              6005 PRINT 5524
              5524 FORMAT(////,1X,'I,J,M,N',/,1X,'K-MATRIX FOR INTERNAL BEAM IJ')
              DO 5528 IJ=1,NB

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PAGE 018

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PRINT 5529,IG(IJ),JG(IJ),MG(IJ),NG(IJ)
5529 FORMAT(1X,4I3)
PRINT 5533,((XK3(L,K,IJ),L=1,6),K=1,6)
5533 FORMAT(1X,1P6E15.5)
5528 CONTINUE
RETURN
END

ISN 0679
ISN 0680
ISN 0681
ISN 0682
ISN 0683
ISN 0684
ISN 0685

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COMPILER OPTIONS - NAME= MAIN.OPT=02,LINECNT=55,SIZE=0600K,
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	SOURCE	BCD	NOLLIST	NODECK	LOAD	MAP	NOEDIT	ID	XREF
C	DATA SET	D2334IPUT	AT LEVEL	012	AS OF	06/25/79			
C	DATA SET	D2332VIU	AT LEVEL	001	AS OF	01/17/78			
C	DATA SET	D2332NIU	AT LEVEL	002	AS OF	11/09/77			
C	DATA SET	D2332NIU	AT LEVEL	001	AS OF	11/02/77			
C	DATA SET	D2332VINPU	AT LEVEL	004	AS OF	10/04/77			
C	DATA SET	D2332QIU	AT LEVEL	001	AS OF	07/26/77			
	SUBROUTINE INPUT								

ISBN 0002

TSN 0003
IMPLICIT REAL*8 (A-H,O-Z)

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IMPLICIT REAL*8 (A-H,O-Z)
REAL*8 KUN,CASEIN,CASOUT,HINDT
REAL*8 LBAR,MU,KE
REAL*4 KRI(2700),SLOPE,XKS,XKI,XKR,LDP(180),LDP1(180)
INTEGER*4 PY(150),PZ(150),PYJ(150),PZJ(150),PTEPH(4)
INTEGER*4 TITLE(40),BLANK,STOP,RUNIN,RUNOUT
INTEGER*4 DIR
INTEGER*2 CHUG,INBUFF,II(40),KK(40),INBUFF(80)
INTEGER*2 IJVM(150),IJFM(150),IJVM1(150),IJFM1(150)
INTEGER*2 MQ(180),NQ(180)
INTEGER*2 IQ(180),JQ(180),LQ(180),NPQ(180),NL5FLG,IJPR
INTEGER*2 N1,N11BS,IG,JG
INTEGER*2 NTOL1,NTOL2,NTOL3
INTEGER*2 NPLT,NPFCT,IPFCT,ITPL,NMPTS,MNUM,ISCALE
INTEGER*2 IJSAVE(180)
INTEGER*2 NKHVEC(150)
INTEGER*2 MH(40),HG(150),NG(150),INP(150),MNP(50)
INTEGER*2 NMPE,NMPE,NBFP,NBDP,NSEP,NDRP,NSTP,NENP,
  JHASS(50,10),JNODE(50,8),JBHF(50,4),JBMD(50,4),
  JBMS(50,6),JENG(50,4),JENR(50,4),JDR1(10),
  NMEN,NMEN,NBDM,NBDM,NSEM,NDRM,NSTM,NENM,NPRINT
  DIMENSION G(150),VMAX2(6,150),FMAX2(6,150)
  DIMENSION FMAX3(6,150),VMAX3(6,150),PTEPH(4)
  DIMENSION XK3(6,6,150)
  DIMENSION IJPR1(14),VMAXT(6),FMAXT(6)
  DIMENSION NBSNO(50),DIR(50),NPTS(50)
  DIMENSION IPHDP(80)
  DIMENSION XNPDPI(50),YNPDPI(50),ZNPDPI(50)
  COMMON/IBALL/ IBUFL(20)
  COMMON/PPLTS/ YSCALE(10),YSCALE(10),NPLT,NPFCT,IPFCT,ITPL
  * NMPTS(10),MNUM(50,10),ISCALE(10)
  COMMON/DEIN/ XNBAR,XPBAR,YNBAR,YPBAR,ZNBAR,ZPBAR,VOLENZ(5
1 FMAX(900),HEX(80),HEY(80),HEZ(80),ALIFT(80),VMAX(900),V

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ISN 0021	
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ISN 0031	2 FMAXN(900),XKS(2700),XKI(2700),XKR(2700),NLSFLG(900),CHUG(180), 3 MYP COMMON/DEINPR/ AA(150),E(150),Y(150),ZZ(150),XIQ(150), 1 XLB(150),ZI(150),ZZ(150),MC(150),XJ(150),SF26(150),SF35(150), 2 SF26J(150),SF35J(150),PY,PZ,PYJ,PZJ,NSC,NPIN COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),EE(20),GG(20), 1 FINT(6,150),VOL(5),VZERO(5),KMATRI(6,4),NVCH,INBUFF(5,8) COMMON/DOIN/ CBAR(150) COMMON/INAC/ACCEL(300),TIMI(300),INDEX(50,2),JAY(50,2),KOUNT COMMON/INCF/ SA(40),SB(40),SF(40),SI(40),XMU(40),XKE(40), 1 XHAX(40),FSPOF(40),FSPOI(40),GFLEX(40),CDAMP(40),PLOMT COMMON/INDEAC/ NACC COMMON/INIC/ XDP(80),ZDPI(80),PHIDPI(80),PSIDPI(80), 1 THEDPI(80),PPR,QPR,RPR,XGIN,ZGIN,PHIPR,PSIPR,THEPR, 2 XGDOT,YGDOT,ZGDOT COMMON/INIDCP/ YDP(80) COMMON/INPR/ NDRI,NSP COMMON/INCFIC/ BETA COMMON/MACFIN/ THAX,IPRINT COMMON/MCFIII/ SYHFLG COMMON/CONNEW/ DAHPC,RUNHOD,PUNHOD COMMON/NP0012/ MG,NG,INP,MNP COMMON/NP0212/ II,KK,MM COMMON/NP0112/ MQ,NQ,IJVM,IJFH,IJVM,IJFH COMMON/NP0014/ NIP COMMON/NP02R8/ XNPDP,YNPDP,ZNPDP COMMON/VOLEO/EOLEO(20),FAO(20),FAAI(20),EXPOLE(20),YMAX(20), 1 YOLEO(20),BOLEO(20),BROLEO(20),XKEXT(20),XKCOMP(20),FCOUL(20), 2 ALPHAP,IGOLEO(20),JGOLEO(20),NGOLEO(20),NGOLEO(20),NOLEO COMMON/COMALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81), 1 Y(81),Z(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80), 2 YI(80),ZI(80),XYI(80),XZI(80),YZI(80),AIJ(9),BIJ(720), 3 DRI(150),OAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80), 4 PLOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80), 5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT, 6 XACC(80),YACC(80),ZACC(80),AIDOT(9), 7 PHIIJ(150),THEIJ(150),PSIIJ(150),SUMDF(6,150),TITLE, 8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81), 9 DPIN(81),DQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40), A CEIKF(40), B SBAR(40),KUN(40),MAXNM,MAXIGS,MAXTBL, C NM,NB,I,J,IG(150),JG(150), D NI(900),NK(40),IJPR(150) COMMON/IPC/ NIC COMMON/ININPR/ NSF,NTF,NDE,NSPD,NED,NS,NRP,NIMP COMMON/UB/ DB(150),IUB(150),NUB COMMON/COMTR8/ 6 COMMON/COMTR4/ KR ,LDP ,LDP1 COMMON/COMPI4/ ND,NVBM,NFBMN,NHI,NKM,NLB, 1 NPH ,NMTL ,NPTS ,NVBM ,IJPRT ,IPHP,NFBM COMMON/COMI2/ IQ ,JQ ,NPq ,INBUF , 1 NKMVEC,IJSAVE COMMON/INOUT/ FCUT,NTOLI,NTOL2,NTOL3	00000410 00000420 00000430 00000440 00000450 00000460 00000470 00000480 00000490 00000500 00000510 00000520 00000530 00000540 00000550 00000560 00000570 00000580 00000590 00000600 00000610 00000620 00000630 00000640 00000650 00000660 00000670 00000680 00000690 00000700 00000710 00000720 00000730 00000740 00000750 00000760 00000770 00000780 00000790 00000800 00000810 00000820 00000830 00000840 00000850 00000860 00000870 00000880 00000890 00000900 00000910 00000920 00000930
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ISN 0059      COMMON/OTPLT/ NHEP,NNEP,NBFP,NBDP,NSEP,NDRP,NSTP,NENP,
*              JHSS,JNODE,JHMF,JHMD,JHMS,JSPR,JENG,JURI,
*              NHEM,NNEW,NBFM,NBDM,NSEM,NDRM,NSTM,NENN,NPRINT
ISN 0060      COMMON /RESTR/ CASEIN,RUNIN,MSECIN,CASOUT,RUNOUT,MSCOUT(5)
ISN 0061      COMMON /VARINT/ HINDT,DT2,TPRINT,EL,EU,RATHIN,RATHAX,IPC,IVAR
ISN 0062      EQUIVALENCE (XK(1),XK3(1,1,1))
ISN 0063      EQUIVALENCE (VMAX(1),VMAX2(1)),(FMAX(1),FMAX2(1))
ISN 0064      EQUIVALENCE (VMAXN(1),VMAX3(1)),(FMAXN(1),FMAX3(1))
ISN 0065      EQUIVALENCE (MASSNO(1),INDEX(1,1))
ISN 0066      EQUIVALENCE (DIR(1),INDEX(1,2))
ISN 0067      DATA STOP/'END '/
ISN 0068      DATA BLANK/' '
ISN 0069      SORT(X) = DSORT(X)
ISN 0070      ABS(X) = DABS(X)

C
C      INITIALIZATION
C
DO 1 I=1,150
  NKWVEC(I) = 0
  SF26(I)=0.
  SF35(I)=0.
  SF26(J(I))=0.
  SF35(J(I))=0.
1 CONTINUE
DO 5130 I = 1,MAXNH
  ALIFT(I) = 0.0
  HEX(I) = 0.0
  HEY(I) = 0.0
  HEZ(I) = 0.0
  XYZ(I) = 0.0
  YZI(I) = 0.0
  XZI(I) = 0.0
  PHIDP(I) = 0.0
  THEDP(I) = 0.0
  PSIDP(I) = 0.0
5130 CONTINUE
MXIGS6 = 6*MAXIGS
DO 5010 I = 1,MXIGS6
  5010 NLSFLG(I) = 0
C
C      CARD 0001,0002
C
READ 5100,(TITLE(I),I=1,20)
FORMAT(20A4)
IF(TITLE(1).EQ.STOP) RETURN
READ 5100,(TITLE(I),I=21,40)
TITLE(19) = BLANK
TITLE(20) = BLANK
TITLE(39) = BLANK
TITLE(40) = BLANK
C
C      CARD 0003
C
ISN 0071      ISN 0072      ISN 0073      ISN 0074      ISN 0075      ISN 0076      ISN 0077      ISN 0078      ISN 0079      ISN 0080      ISN 0081      ISN 0082      ISN 0083      ISN 0084      ISN 0085      ISN 0086      ISN 0087      ISN 0088      ISN 0089      ISN 0090      ISN 0091      ISN 0092
ISN 0093      ISN 0094      ISN 0095      ISN 0097      ISN 0098      ISN 0099      ISN 0100      ISN 0101
00000940
00000950
00000960
00000970
00000980
00000990
00001000
00001010
00001020
00001030
00001040
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00001080
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00001100
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00001120
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00001190
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00001370
00001380
00001390
00001400
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ISN 0102      C      READ 5100,DUMMY
               C
               C      CARD 0004
ISN 0103      C      READ 5200,NM,NP,NB,NLB,NNP,NPIN,NUB,NORI,NOLEO,NACC,MVP,NVCH,
               C      1 NNTL,NO
ISN 0104      C      READ 5200,NVBM,NFBM,NVBMN,NFBMN,NKM,NHI,NPH,NTOLL,NTOL2,NTOL3,
               C      1 NSC,NIC
ISN 0105      C      5200 FORMAT(14I5,2I1)
               C
               C      NSC EQ.OR LESS 0 THEN NO STRESS CALC.
               C      NIC EQ.OR LESS 0 THEN NO PREL. LOADS/DEFLS IN SUBROUTINE IC
               C
               C      CARDS 0005, 0006
ISN 0106      C
ISN 0107      C      READ 5203,CASEIN,RUNIN,MSECIN
ISN 0108      C      READ 5203,CASOUT,RUNOUT,MSCOUT
               C      5203 FORMAT(A8,2X,6I10)
               C
               C      CARD 0007
ISN 0109      C
ISN 0110      C      READ 5201,IPRINT,DELTAT,THAX,PLOMT,FCUT,RUNMOD
ISN 0111      C      MINDT = 0.1 * DELTAT
ISN 0112      C      TPRINT = IPRINT * DELTAT
ISN 0113      C      READ 5201,IVAR,EL,EU,RATHIN,RATHAX
               C      5201 FORMAT(I10,5E10.0)
               C
               C      CARDS 0008, 0009
ISN 0114      C
ISN 0115      C      READ 5200,NSF,NTF,NDE,NSPD,NED,NS,NRP,NIMP
ISN 0116      C      IF(NTOLL.NE.0) GO TO 5570
ISN 0117      C      NTOLL=1
ISN 0118      C      5570 IF(NTOL2.NE. 0) GO TO 5571
ISN 0119      C      NTOL2=10
ISN 0120      C      5571 IF(NTOL3.NE.0) GO TO 5572
ISN 0121      C      NTOL3=30
ISN 0122      C
ISN 0123      C      NTOL1=ALLOWABLE ENERGY GROWTH TOLERANCE IN PER CENT(%)
               C      NTOL2=ALLOWABLE INDIVIDUAL NEGATIVE ENERGY IN PER CENT(%)
               C      NTOL3=ALLOWABLE MASS DEVIATION TOLERANCE IN PER CENT(%)
               C      NIMP=MASS IMPULSE PRINT 2/1/79
ISN 0124      C
ISN 0125      C      5572 READ 5200,NMEP,NNEP,NBFP,NBDP,NSTP,NSEP,NENP,NDRP,NPLT,NPFCT
               C      IPFCT = -1
               C
               C      NSF=STRAIN FORCE,NTF=TOTAL FORCE,NDE=BEAM DEFL.,NSPD=EXT.SP.RING
               C      DATA,NED=MASS&BEAM ENERGY PRINT,NS=STRESS PRINT,NRP=
               C      TRANS.ACCEL(FILTERED&FILTERED)ONLY
               C      NSF,NTF,NDE,NSPD,NED,NS, EQ. OR LESS THAN 0 NO PRINT
               C      NRP EQ.OR LESS THAN 0 ONLY TRANS.ACCELS PRINT,>0 ALL MASS RESPONSE0001960
               C      0001970
               C      NUB=NO.OF UNSYMMETRICAL BEAMS
               C      NMEP,NNEP,NBFP,NBDP,NSTP,NSEP,NENP,NDRP ARE THE HISTORY PLOTS FOR
               C      0001980
               C      0001990

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C MASSPOINTS,NODE POINTS,BEAM FORCES,BEAM DEFLECTIONS,STRESSES,
C EXT. SPRINGS,DRI'S,RESPECTIVELY
C NPLT=NO.MASS POSITION PLOTS AT SELECTED INTERVALS
C NENP=TIME HISTORY PLOT OF STRAIN & DAMPING ENERGY
C
C      IF(NSC.GT.0) GO TO 5210
C      NS=0
C      5210 CONTINUE
C      IF(DELTA.T,LE.0.) GO TO 5000
C      IF(NM,LE.0) GO TO 5000
C
C      CARD 0010
C
C      READ 5300,XGDOT,YGDOT,ZGDOT
C
C      CARD 0011
C
C      READ 5300,PPR,QPR,RPR
C
C      CARD 0012
C
C      READ 5300,PHIPR,THEPR,PSIPR,XGIN,ZGIN,BETA
C      5300 FORMAT(6E10.0)
C
C      CARDS 0100
C
C      READ 5301,(MGT(I),XDP(I),YDP(I),ZDP(I),XI(I),YI(I),ZI(I),I=1,NM)
C      5301 FORMAT(7E10.0)
C
C      CARDS 0200
C
C      IF(MNP.EQ.0) GO TO 5534
C      READ 4001,(MNP(I),INP(I),XNPDP(I),YNPDP(I),ZNPDP(I),I=1,NNP)
C      4001 FORMAT(2I5,3E10.0)
C
C      CLEAR EXTERNAL SPRING FLAGS (AND THE ASSOCIATED DATA ALTHOUGH THIS
C      SHOULD NOT BE NECESSARY BECAUSE WE ONLY USE IT IF THE FLAG IS 1.
C      HOWEVER, THEY MUST BE CLEARED FOR THE SEARCH WHICH PRINTS THE INPUT.)
C
C      5534 IF(NSP.EQ.0) GO TO 5535
C      DO 5132 IKM=1,NSP
C      XLBAR(IKM) = 0.
C      XPU(IKM) = 0.
C      XVE(IKM) = 0.
C      SI(IKM) = 0.
C      SA(IKM) = 0.
C      SB(IKM) = 0.
C      SF(IKM) = 0.
C      FPOI(IKM) = 0.
C      FSPDF(IKM) = 0.
C      CDAMP(IKM)=0.
C      5132 CONTINUE
C
ISN 0126
ISN 0128
ISN 0129
ISN 0130
ISN 0132

ISN 0134

ISN 0135

ISN 0136
ISN 0137

ISN 0138
ISN 0139

ISN 0140
ISN 0142
ISN 0143

ISN 0144
ISN 0146
ISN 0147
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ISN 0153
ISN 0154
ISN 0155
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ISN 0157

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C      CARDS 0300
C      READ 5810, (MM(J), II(J), KK(J), XLBAR(J), XPU(J), XKE(J), XMAX(J),
1 6FLEX(J), J=1, NSP)
5810 FORMAT(12, 13, 15, 5E10.0)
C
C      CARDS 0400
C      DO 5160 IKM=1, NSP
5160 CONTINUE
C      READ 5301, SI(IKM), SA(IKM), SB(IKM), SF(IKM), FSP01(IKM), FSP0F(IKM),
1 CDAMP(IKM)
5160 CONTINUE
C      E-MODULUS OF ELASTICITY, A=AREA, G=MODULUS OF RIGIDITY
C      XJ=POLAR MOMENT OF INERTIA, YY=MOMENT OF INERTIA ABOUT THE Y AXIS
C      ZZ=MOMENT OF INERTIA ABOUT THE Z AXIS, XLB=MEMBER LENGTH
C      YY IS USED WITH (3,5) TERMS (Z, THETA)
C      ZZ IS USED WITH (2,6) TERMS (Y, PSI)
C
C      CARDS 0500
C      5535 READ 5306, (MG(IJ), IG(IJ), JG(IJ), AG(IJ), XJ(IJ), YY(IJ),
1 ZI(IJ), XIQ(IJ), ZI(IJ), ZI(IJ), MC(IJ), IJ=1, NB)
5306 FORMAT(2, 12, 13, 5E10.0, 2F5.0, I2)
C      DO 6101 IJ=1, NB
6101 CONTINUE
C      IF(XJ(IJ).NE.0.0) GO TO 6102
C      XJ(IJ)=YY(IJ)+ZZ(IJ)
C      PY(IJ) = 0
C      PZ(IJ) = 0
C      PY(IJ) = 0
C      PZ(IJ) = 0
6101 CONTINUE
C
C      CARDS 0600
C      IF(NMTL.EQ.0) GO TO 2
C      DO 4 LL=1, NMTL
4 CONTINUE
C      READ 3, K, EE(K), GG(K), STENS(K), SCOMP(K), SHEAR(K)
C      ISUF1(LL) = K
3 FORMAT(15, 5X, 5E10.0)
C
C      CARDS 0700
C      2 IF(NPIN.EQ.0) GO TO 6112
C      DO 6120 JI=1, NPIN
6120 CONTINUE
C      READ 6122, M, I, N, J, (PTEMP(K), K=1, 4), (PTEMPH(K), K=1, 4)
6122 FORMAT(2, 12, 13, 4I5, 4E10.0)
C      DO 6124 IJ=1, NB
6124 CONTINUE
C      IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
1 GO TO 6126
6124 CONTINUE
C      6126 PY(IJ) = PTEMP(1)
C      PZ(IJ) = PTEMP(2)

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ISN 0192      PT(J,IJ) = PTEMP(3)
ISN 0193      PZ(J,IJ) = PTEMP(4)
ISN 0194      SF35(IJ)=PTEMPH(1)
ISN 0195      SF26(IJ)=PTEMPH(2)
ISN 0196      SF35(J,IJ)=PTEMPH(3)
ISN 0197      SF26(J,IJ)=PTEMPH(4)
ISN 0198      6120 CONTINUE
C
C      CAPDS 0000
C
ISN 0199      6112 DO 6111 IJ=1,NB
ISN 0200          IAS(IJ)=0
ISN 0201      6111 DB(IJ)=0
ISN 0202          IF(NJB.EQ.0) GO TO 6110
ISN 0203          DO 6114 JI=1,NJB
ISN 0204              READ 6116 M,I,N,J,IJTEMP,DBTEMP
ISN 0205              6116 FORMAT(2(12,13),15,E10.0)
ISN 0206              DO 6118 IJ=1,NB
ISN 0207                  IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ)).AND.M.EQ.MG(IJ)).AND.N.EQ.NG(IJ))
ISN 0208                      1 GO TO 6119
ISN 0210      6118 CONTINUE
ISN 0211      6119 IAS(IJ)=IJTEMP
ISN 0212      DB(IJ)=DBTEMP
ISN 0213      6114 CONTINUE
C
C      CAPD 0900
C
ISN 0214      6110 IF(NOLEO.EQ.0) GO TO 6210
ISN 0215      READ 5301,ALPHAP
ISN 0216          READ 5306,(MGOLEO(IJ),ISOLEO(IJ),NGOLEO(IJ),JGOLEO(IJ),
ISN 0217              1 EOLEO(IJ),FAO(IJ),FAA(IJ),EYPOLE(IJ),YMAX(IJ),IJ=1,NOLEO)
ISN 0218          READ 5306,(MGOLEO(IJ),ISOLEO(IJ),NGOLEO(IJ),JGOLEO(IJ),
ISN 0219              1 BOLEO(IJ),BPOLEO(IJ),XEXT(IJ),XCOMP(IJ),FCOUL(IJ),IJ=1,NOLEO)
ISN 0220      6210 READ 5400,DAMPC
ISN 0221          5400 FORMAT(10.0)
C
C      DAMPC=DAMPING COEFF. FOR ALL BEAMS
C      NO STANDARD DAMPC VALUE AS OF 3/79 VALUE MUST BE INPUT
C      IF NO.NE.0 SET DESIRED CBAP TO VALUE READ IN
C
ISN 0221      COUN=DAMPC
ISN 0222      DO 5549 IJ=1,NB
ISN 0223      5549 CBAP(IJ) = COUN
C
C      CAPDS 0901 AND UP
C
ISN 0224      IF(NB.EQ.0) GO TO 5543
ISN 0225      DO 5544 JI=1,NB
ISN 0226          READ 5547 M,I,N,J,COUN
ISN 0227      5547 FORMAT(2(12,13),E10.0)
ISN 0228          DO 5544 IJ=1,NB
ISN 0229              IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ)).AND.M.EQ.MG(IJ)).AND.N.EQ.NG(IJ))
ISN 0230                  1 CBAP(IJ) = COUN

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ISN 0232      5544 CONTINUE
C
C      CARDS 1000
C
ISN 0233      5543 IF(NLB.EQ.0) GO TO 5541
ISN 0235      MXTBL1 = MAXTBL+1
ISN 0236      IF(NLB.GT.MXTBL1) GO TO 5921

C*****KR TABLE INPUT
C IN DERIV. TO SEE IF THERE IS A TABLE FOR A PARTICULAR IJL, WE LOOK
C AT NLSFLG(IJL) AND IF IT IS NON-ZERO, IT WILL BE THE TABLE NUMBER
C FOR THAT IJL. WE STILL USE SLOPES AND INTERCEPTS FOR THE
C INTERPOLATION BUT WE MUST FIND WHICH INTERVAL IN X WE'RE IN.
C THIS IS DONE BY KEEPING, FOR EACH TABLE, A POINTER TO THE LOWER X OF
C THE INTERVAL WE WERE IN AT THE LAST INTEGRATION STEP
C (INTEGER*2 CHUG(80)) ON THE GROUNDS THAT WE'RE PROBABLY
C STILL IN THAT INTERVAL. IF WE'RE NOT IN THAT INTERVAL, WE CHECK
C ONE BY ONE IN THE APPROPRIATE DIRECTION UNTIL WE FIND THE RIGHT
C INTERVAL AND WE SAVE THAT IN CHUG AND DO THE INTERPOLATION.
C XI(I) AND X(NPQ) FOR EACH TABLE ARE REPLACED BY VERY LARGE (E35)
C NEGATIVE AND POSITIVE NUMBERS SO THAT WE NEED NEVER CHECK FOR BEING
C OUT OF THE TABLE AND ALSO SO WE DON'T EVEN HAVE TO KNOW HOW MANY
C POINTS IN THE TABLE. (IF AN ARGUMENT EXCEEDS 1.E35 WE'LL BOHB
C SOONER OR LATER). THIS ALLOWS VERY RAPID TABLE SEARCH AND
C INTERPOLATION.
C*****INPUT KR TABLE SPECS
C DO TO NUMBER OF TABLES INPUT
DO 5090 I = 1,NLB
  READ 5900,MQ(I),IQ(I),NQ(I),JQ(I),LQ(I),NPQ(I),LDP(I),LDP1(I)
5900 FORMAT(2I2,I3,2I5,2E10.0)
C*****HUNT FOR I,J PAIR SO WE CAN STORE NONLINEAR BEAM I IN NLSFLG
DO 5030 J = 1,NB
  IF(IQ(I).EQ.IG(J).AND.JQ(I).EQ.JG(J).AND.MQ(I).EQ.MG(J)
    1 .AND.NQ(I).EQ.NG(J)) GO TO 5040
5030 CONTINUE
C*****NO SUCH I,J PAIR, ABORT
PRINT 5910,IQ(I),JQ(I),MQ(I),NQ(I)
STOP
5910 FORMAT('H1','5. NON-EXISTENT I,J PAIR IN KR TABLE SPECS',4I5)
C*****FOUND IT
5040 NLSFLG(6*(J-1)+LQ(I)) = I
  IJSAVE(I) = J
5090 CONTINUE
  GO TO 5540
C*****TOO MANY KR TABLES, ABORT
5921 PRINT 5920
STOP
5920 FORMAT('H1','6. TOO MANY KR TABLES')
C
C      CARDS 1100
C
ISN 0255      5540 K = -14
ISN 0256      DO 5070 I = 1,NLB
ISN 0257      NP = NPQ(I)

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A-B1


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ISN 0258      K = K+15
ISN 0259      CHUG(I) = K
ISN 0260      ICH = CHUG(I)-1
ISN 0261      IF(NP.LT.10) GO TO 5070
C
C      IF NP.GE.10,ME READ KR TABLE DIRECTLY
C
ISN 0263      READ 5950, (XKR(ICH+J),KR(ICH+J),J=1,NP)
ISN 0264      5950 FORMAT(2E10.0)
ISN 0265      5070 CONTINUE
C
C      CARD 1200
C
ISN 0266      5541 IF(MVP.EQ.0) GO TO 5065
ISN 0268      READ 5300,XNBAR,XPBAR,YNBAR,YPBAR,ZNBAR,ZPBAR
C
C      CARDS 1201 AND UP
C
ISN 0269      5065 DO 5580 IJ=1,NB
ISN 0270      IJPR(IJ) = 0
ISN 0271      5580 CONTINUE
ISN 0272      IF(NDRI.EQ.0) GO TO 5056
ISN 0274      NDRI = NDRI
ISN 0275      LDRI = NDRI/7+.9
ISN 0276      DO 5560 JI=1,LDRI
ISN 0277      READ 5561, (IJPR(J),J=1,14)
ISN 0278      5561 FORMAT(14I5)
ISN 0279      DO 5560 I=1,7
ISN 0280      DO 5560 IJ=1,NB
ISN 0281      IF(IJPR(2*I-1).EQ.IG(IJ).AND.IJPR(2*I).EQ.JG(IJ)) IJPR(IJ) = 1
ISN 0283      5560 CONTINUE
C
C      CARDS 1210
C
ISN 0284      5056 IF(INVCH.EQ.0) GO TO 6000
ISN 0286      DO 5611 I=1,NVCH
ISN 0287      READ 5602, (INBUFF(I,J),J=1,8)
ISN 0288      5602 FORMAT(8I5)
ISN 0289      5611 CONTINUE
C
C      CARDS 1300, 1400
C
C*****STANDARD VMAX = 100
ISN 0290      6000 DO 5180 I = 1,MXIGS6
ISN 0291      5180 VMAX(I) = 100.0
ISN 0292      IF(NVBM.EQ.0) GO TO 5185
ISN 0294      DO 5170 JI=1,NVBM
ISN 0295      READ 5620,M,I,N,J,(VMAXT(K),K=1,6)
ISN 0296      5620 FORMAT(2(I2,I3),6E10.0)
ISN 0297      DO 5171 IJ=1,NB
ISN 0298      IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).
1 AND.N.EQ.NG(IJ)) GO TO 5172
ISN 0300      5171 CONTINUE

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ISN 0301 5172 IJWH(JI) = IJ
ISN 0302 DO 5173 L=1,6
ISN 0303 VMAX2(L,IJ)=VMAXT(L)
ISN 0304 5173 CONTINUE
ISN 0305 5170 CONTINUE
ISN 0306 5185 DO 5190 I=1,MXIG56
ISN 0307 5190 VMAXN(I)=100.0
ISN 0308 IF(NBWN.EQ.0) GO TO 5178
ISN 0309 DO 5186 JI=1,NBWN
ISN 0310 READ 5820, M,I,N,J, (VMAXT(K),K=1,6)
ISN 0311 DO 5187 IJ=1,NB
ISN 0312 IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
ISN 0313 1 GO TO 5188
ISN 0315 5187 CONTINUE
ISN 0316 5188 IJWH(JI)=IJ
ISN 0317 DO 5189 L=1,6
ISN 0318 VMAX3(L,IJ)=VMAXT(L)
ISN 0319 5189 CONTINUE
ISN 0320 5186 CONTINUE
ISN 0321 C STANDARD FMAX=1.E10
ISN 0322 5178 DO 5177 I=1,MXIG56
ISN 0323 5177 FMAX(I)=1.E10
ISN 0324 DO 5181 JI=1,NBWN
ISN 0325 READ 5820,M,I,N,J, (FMAXT(K),K=1,6)
ISN 0326 DO 5182 IJ=1,NB
ISN 0327 IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).
ISN 0328 1 AND.N.EQ.NG(IJ)) GO TO 5183
ISN 0330 5182 CONTINUE
ISN 0331 5183 IJWH(JI) = IJ
ISN 0332 DO 5184 L=1,6
ISN 0333 FMAX2(L,IJ)=FMAXT(L)
ISN 0334 5184 CONTINUE
ISN 0335 5181 CONTINUE
ISN 0336 6100 DO 6201 I=1,MXIG56
ISN 0337 6201 FMAXN(I)=1.E10
ISN 0338 IF(NBWN.EQ.0) GO TO 6001
ISN 0339 DO 6202 JI=1,NBWN
ISN 0340 READ 5820, M,I,N,J, (FMAXT(K),K=1,6)
ISN 0341 DO 6103 IJ=1,NB
ISN 0342 IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
ISN 0343 1 GO TO 6104
ISN 0345 6103 CONTINUE
ISN 0346 6104 IJWH(JI)=IJ
ISN 0347 DO 6105 L=1,6
ISN 0348 FMAX3(L,IJ)=FMAXT(L)
ISN 0349 6105 CONTINUE
ISN 0350 6202 CONTINUE
ISN 0351 C CARDS 1500
ISN 0352 C
ISN 0353 6001 IF(NWI.EQ.0) GO TO 6002
ISN 0354 DO 5120 I = 1,NHI

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ISN 0354      READ 5000,INBUF(I),ALIFT(INBUF(I)),HEX(INBUF(I)),HEY(INBUF(I)),
              1HEZ(INBUF(I)),XYI(INBUF(I)),YZI(INBUF(I)),XZI(INBUF(I))
ISN 0355      5000 FORMAT(I5,E5.0,6E10.0)
ISN 0356      5120 CONTINUE
C
C      CARDS 1600
C
ISN 0357      6002 IF(NPH.EQ.0) GO TO 6003
ISN 0359      DO 5550 J=1,NPH
ISN 0360      READ 5551,IPHDP(J),T1,T2,T3
ISN 0361      I=IPHDP(J)
ISN 0362      PHIDP(I)=T1
ISN 0363      THEDP(I)=T2
ISN 0364      PSIDP(I)=T3
ISN 0365      5551 FORMAT(I5,5X,3E10.0)
ISN 0366      5550 CONTINUE
C
C      CARDS 1700
C
ISN 0367      6003 IF(NACC.EQ.0) GO TO 6005
ISN 0369      IF(NACC.GT.50) GO TO 7003
ISN 0371      KOUNT = 0
ISN 0372      DO 7010 I=1,NACC
ISN 0373      READ 7000,MASSNO(I),DIR(I),NPTS(I)
ISN 0374      7000 FORMAT(3I5)
ISN 0375      JAY(I,1) = I
ISN 0376      JAY(I,2) = NPTS(I)
ISN 0377      KOUNT = KOUNT+NPTS(I)
ISN 0378      IF(KOUNT.GT.300) GO TO 7003
ISN 0380      7010 CONTINUE
C
C      CARDS 1800
C
ISN 0381      L=0
ISN 0382      DO 7002 I=1,NACC
ISN 0383      K=NPTS(I)
ISN 0384      DO 7002 J=1,K
ISN 0385      L=L+1
ISN 0386      READ 7004,TIM(L),ACCEL(L)
ISN 0387      7004 FORMAT(2E10.0)
ISN 0388      7002 CONTINUE
ISN 0389      GO TO 6005
ISN 0390      7003 PRINT 7005,NACC,KOUNT
ISN 0391      7005 FORMAT(IX,'7. ERROR IN ACCEL TIME DATA INPUT' / IX,
              *      'NUMACL,KOUNT = ',2I5)
C
C      CARDS 2000
C
ISN 0392      6005 IF(NKM.EQ.0) GO TO 5000
ISN 0394      DO 5521 I=1,NKM
ISN 0395      READ 5520,M,I,N,J
ISN 0396      5520 FORMAT(2I2,I3)
ISN 0397      DO 5523 I2=1,NB

```

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ISN 0390      IF(I.EQ.IG(I2).AND.J.EQ.J6(I2).AND.M.EQ.M6(I2).AND.N.EQ.N6(I2))
1  IJ=I2
5523 CONTINUE
ISN 0400      NRVEC(IJ) = 1
ISN 0401      READ 5300,((XK3(L,K,IJ),L=1,6),K=1,6)
ISN 0402      5521 CONTINUE
ISN 0403      5000 CONTINUE
ISN 0404
C
C      NPLT=NO. OF PLOTS EACH TIME(MAX. OF 10)
C      ITPL =DESCRIBES PLANE 1=XY,2=XZ,3=YZ
C      NMPTS=NO. OF POINTS FOR A PLOT CURRENTLY=NO.MASS POINTS
C      NMUM=MASS NUMBERS TO BE PLOTTED
C
ISN 0405      IF(NPLT.EQ. 0) GO TO 100
ISN 0407      DO 200 IP=1,NPLT
ISN 0408      READ 5400, ITPL(IP),NMPTS(IP),ISCALE(IP),XSCALE(IP),YSCALE(IP)
ISN 0409      NPT = NMPTS(IP)
ISN 0410      READ 5410, (NMUM(JP,IP), JP=1, NPT)
ISN 0411      5400 FORMAT(3I5,5X,2E10.5)
ISN 0412      5410 FORMAT(14I5)
ISN 0413      200 CONTINUE
ISN 0414      100 CONTINUE
ISN 0415      IF(NHEP.EQ. 0) GO TO 8000
ISN 0417      DO 8010 I=1, NHEP
ISN 0418      READ 5200, (JMASS(I,J), J=1, 10)
ISN 0419      8010 CONTINUE
ISN 0420      8000 IF(NHEP.EQ. 0) GO TO 8020
ISN 0421      DO 8030 I=1, NHEP
ISN 0422      READ 5200, (JNODE(I,J), J=1, 8)
ISN 0423      8030 CONTINUE
ISN 0424      8020 IF(NBFP.EQ. 0) GO TO 8040
ISN 0425      DO 8050 I=1, NBFP
ISN 0427      READ 5200, (JBHF(I,J), J=1, 4)
ISN 0428      8050 CONTINUE
ISN 0429      8040 IF(NBOP.EQ. 0) GO TO 8060
ISN 0430      DO 8070 I=1, NBOP
ISN 0432      READ 5200, (JBHD(I,J), J=1, 4)
ISN 0433      8070 CONTINUE
ISN 0434      8060 IF(NSTP.EQ. 0) GO TO 8080
ISN 0435      DO 8090 I=1, NSTP
ISN 0437      READ 5200, (JBHS(I,J), J=1, 6)
ISN 0438      8090 CONTINUE
ISN 0439      8080 IF(NSEP.EQ. 0) GO TO 8100
ISN 0440      DO 8110 I=1, NSEP
ISN 0442      READ 5200, (JSPP(I,J), J=1, 4)
ISN 0443      8110 CONTINUE
ISN 0444      8100 IF(NENP.EQ. 0) GO TO 8101
ISN 0445      DO 8102 I=1, NENP
ISN 0447      READ 5200, (JENG(I,J), J=1, 3)
ISN 0448      8102 CONTINUE
ISN 0449      8101 IF(NDRP.EQ. 0) GO TO 8120
ISN 0450      DO 8130 I=1, NDRP
ISN 0452      READ 5200, JDRP(I)
ISN 0453

```


PAGE 013

00006240
00006250
00006260

0130 CONTINUE
0120 RETURN
END

ISN 0454
ISN 0455
ISN 0456

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LEVEL 21.6 (JUN 74) OS/360 FORTRAN H DATE 79.177/14.31.14

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
C DATA SET 02334ITERP AT LEVEL 003 AS OF 06/25/79
SUBROUTINE INTERP(IREF,TT,YOUT)
IMPLICIT REAL*8 (A-H,O-Z)
COMMON/TINAC/ACCEL(300),TIM(300),INDEX(50,2),JAY(50,2)
XNUM=ACCEL(IREF+1)-ACCEL(IREF)
XDEN=TIM(IREF+1)-TIM(IREF)
SLOPE=XNUM/XDEN
YOUT=ACCEL(IREF)+SLOPE*(TT-TIM(IREF))
6400 FORMAT(5E15.6)
RETURN
END
ISN 0002
ISN 0003
ISN 0004
ISN 0005
ISN 0006
ISN 0007
ISN 0008
ISN 0009
ISN 0010
ISN 0011

00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
C DATA SET D2334HAMUL AT LEVEL 001 AS OF 03/24/76
ISN 0002 SUBROUTINE MATMUL(A,B,C)
ISN 0003 IMPLICIT REAL*8 (A-H,O-Z)
ISN 0004 DIMENSION A(3,3),B(3,3),C(3,3)
C A*B TO C
ISN 0005 DO 10 I = 1,3
ISN 0006 DO 10 J = 1,3
ISN 0007 SUM = 0.0
ISN 0008 DO 20 K = 1,3
ISN 0009 20 SUM = SUM+A(I,K)*B(K,J)
ISN 0010 10 C(I,J) = SUM
ISN 0011 RETURN
ISN 0012 END
00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120

```

LEVEL 21.6 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.31.24

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECT=55,SIZE=0600K,

SOURCE,BCD,NOLIST,NODECK,LOAD,NAP,NODEIT,LD,XREF

C DATA SET D2334MAVEC AT LEVEL 001 AS OF 03/24/76

ISN 0002 SUBROUTINE MATVEC(A,V,P,ISW)

ISN 0003 IMPLICIT REAL*8 (A-H,O-Z)

ISN 0004 DIMENSION A(3,3),V(3),P(3)

C A*V TO P IF ISW = 0, ELSE A*V TO P

DO 10 I = 1,3

SUM = 0.0

DO 20 K = 1,3

IF(ISW) 40,30,40

30 SUM = SUM+A(I,K)*V(K)

GO TO 20

40 SUM = SUM+A(K,I)*V(K)

20 CONTINUE

10 P(I) = SUM

RETURN

END

ISN 0005
ISN 0006
ISN 0007
ISN 0008
ISN 0009
ISN 0010
ISN 0011
ISN 0012
ISN 0013
ISN 0014
ISN 0015
00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150

LEVEL 21.0 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.31.27

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*
*****

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*****
*
* COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
* SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
* DATA SET D2334PAPLO AT LEVEL 005 AS OF 07/19/78
* SUBROUTINE PAPLOT(V,M,XSCALE,YSCALE,MASS,NMPTS,ISCALE)
* IMPLICIT REAL*8(A-H,O-Z)
*
* INTEGER*4 S,6
* INTEGER*2 NMPTS,MASS,ISCALE
*
* SUBROUTINE TO GENERATE ONLINE PAPER PLOTS
*
* DIMENSION V(1),M(1),S(105),BX(500),G(9),X(101),Y(101),NM(10),
* MASS(1),XAXIS(11),YAXIS(9),M(101),NM(101,2)
* DATA S(1),S(105)/((4X,''),)/
* DATA G/1X,'1H2','1H3','1H4','1H5','1H6','1H7','1H8','1H9',
* '1H0',/
*
* IAXIS = 10
*
* SET UP SCALE VALUES FOR INDEPENDANT 'X' ARRAY
*
* XMAX = -1.0E10
* YMAX = -1.0E10
* XMIN = 1.0E10
* YMIN = 1.0E10
* DO 10 I=1, NMPTS
*   XMAX = DMAX1(V(I),XMAX)
*   XMIN = DMIN1(V(I),XMIN)
*   YMAX = DMAX1(M(I),YMAX)
*   YMIN = DMIN1(M(I),YMIN)
*   X(I) = V(I)
*   Y(I) = M(I)
*   M(I) = MASS(I)
* 10 CONTINUE
* IF(ISCALE .EQ. 3) GO TO 50
* DX = XMAX - XMIN
* DY = YMAX - YMIN
*
* IF ISCALE=1 SELECT SCALES INDEPENDENTLY BASED ON X AND Y
* IF ISCALE=0 SELECT SCALES OF EQUAL MAGNITUDE
* IF(ISCALE .EQ. 1) GO TO 118
*
*****

```

A-140

```

ISM 0030 IFIDY .GT. DX) DX = DY
ISM 0032 IFIDY .GT. DY) DY = DX
ISM 0034 110 CONTINUE
ISM 0035 DX = DX / 10.0
ISM 0036 DY = DY / 8.0

C
ISM 0037 IAX = YMIN / DY
ISM 0038 YAXIS(1) = IAX * DY
ISM 0039 IF(YAXIS(1) .LT. 0.0) YAXIS(1) = YAXIS(1) - DY
ISM 0041 IAX = (YMAX / DY) + 1
ISM 0042 YSCALE = ((IAX * DY) - YAXIS(1)) / 8.0
ISM 0043 IAX = XMIN / DX
ISM 0044 XAXIS(1) = IAX * DX
ISM 0045 IF(XAXIS(1) .LT. 0.0) XAXIS(1) = XAXIS(1) - DX
ISM 0047 IAX = (XMAX / DX) + 1
ISM 0048 XSCALE = ((IAX * DX) - XAXIS(1)) / 10.0
ISM 0049 GO TO 60
ISM 0050 50 CONTINUE
ISM 0051 IAX = YMIN / YSCALE
ISM 0052 YAXIS(1) = IAX * YSCALE
ISM 0053 IF(YAXIS(1) .LT. 0.0) YAXIS(1) = YAXIS(1) - YSCALE
ISM 0055 IAX = XMIN / XSCALE
ISM 0056 XAXIS(1) = IAX * XSCALE
ISM 0057 IF(XAXIS(1) .LT. 0.0) XAXIS(1) = XAXIS(1) - XSCALE
ISM 0059 60 CONTINUE
ISM 0060 DO 90 I=2, 9
ISM 0061 YAXIS(I) = YAXIS(1) + (I - 1) * YSCALE
ISM 0062 90 CONTINUE
ISM 0063 DO 120 I=2, 11
ISM 0064 XAXIS(I) = XAXIS(1) + (I - 1) * XSCALE
ISM 0065 120 CONTINUE
ISM 0066 IF(YMAX .GT. YAXIS(9) .OR. XMAX .GT. XAXIS(11)) WRITE(6,7040)
7040 FORMAT(2X,'*** WARNING *** ONE OR MORE MASS POINTS ARE NOT',
* ' INCLUDED IN THE FOLLOWING PLOT BECAUSE THE COORDINATES',
* ' OF THE POINT(S) ARE' / 24X, 'OUTSIDE THE LIMITS OF THE',
* ' PLOT.')
ISM 0069 X1 = XAXIS(1)
ISM 0070 DX = XAXIS(11) - XAXIS(1)
ISM 0071 DY = YAXIS(9) - YAXIS(1)

C
C REORDER DEPENDENT 'Y' ARRAY IN MONOTONICALLY INCREASING MAGNITUDE
C
C CALL FSHELL(Y,BX,NMPTS)
C
C REORDER INDEPENDENT 'X' ARRAY IN CORRESPONDENCE WITH PRESENT 'Y'
C ARRAY
C
C CALL SHELL(X,BX,NMPTS)
C
C CALL SHELL(BX,M,NMPTS)
C
C LINE LOCATES HORIZONTAL AXIS
C

```

A-141

```

ISN 0075      YFIRST = YAXIS(1)
ISN 0076      YLAST = YAXIS(9)
C
ISN 0077      IF(YLAST .LE. 0.0) WRITE(6,7030)('XAXIS(1), I=1, 11)
C
C      LOCATE FIRST VERTICAL SCALE MARK
C      MARK LOCATES '-' IN VERTICAL SCALE
C
ISN 0079      MARK = 0
ISN 0080      L0 = (-YFIRST * 48.0 / DY) + 1.5
ISN 0081      IF(L0 .GT. 49) L0 = 49
ISN 0083      J = 1
ISN 0084      N = 1
ISN 0085      NL = 50
C
C      START LINE LOOP
C
ISN 0086      C 100 CONTINUE
C
C      IDENTIFY CURRENT PRINT LINE NUMBER
C
ISN 0087      NL = 50 - N
C
C      SET UP I1 AND I2 FOR NORMAL PRINT LINE
C
ISN 0088      I1 = 1
ISN 0089      I2 = 3
ISN 0090      IF(NL .EQ. 1 .AND. YLAST .GT. 0.0) GO TO 110
ISN 0092      IF(NL .NE. L0) GO TO 125
C
C      SET UP I1 AND I2 FOR ZERO AXIS PRINT LINE
C
ISN 0094      C 110 CONTINUE
ISN 0095      I1 = 4
ISN 0096      I2 = 5
ISN 0097      C 125 CONTINUE
ISN 0098      DO 150 I=5, 104
ISN 0099      S(I) = G(I1)
ISN 0100      C 150 CONTINUE
ISN 0101      S(2) = G(9)
ISN 0102      S(3) = G(8)
ISN 0103      S(4) = G(12)
C
C      PUT HORIZONTAL SCALE MARKS IN 'S' ARRAY
C
ISN 0104      IF(NL .EQ. 1 .AND. YLAST .GT. 0.0) GO TO 115
ISN 0106      IF(NL .NE. L0) GO TO 160
ISN 0108      C 115 CONTINUE
ISN 0109      DO 155 I1=14, 104, 10
ISN 0110      155 S(I1) = G(5)
ISN 0111      C 160 CONTINUE
C
C      START DIMINISHING LOOP ON DEPENDENT ARRAY LINE I.D.

```

```

C
ISN 0112      KT = 0
ISN 0113      DO 250 I2=J, NMPTS
ISN 0114      JJ = I2
ISN 0115      K = NMPTS - I2 + 1
ISN 0116      IF(Y(K) .GT. YAXIS(9)) GO TO 250
ISN 0117      L = ((Y(K) - YFIRST) * 48.0 / DY) + 1.5
ISN 0118      IF(L - NL) 260,200,250
ISN 0119      200 CONTINUE
ISN 0120

C
ISN 0121      C CALCULATE LOCATION IN 'S' ARRAY FOR DATA POINT I.D.
ISN 0122      II = ((X(K) - X1) * 100.0 / DX) + 4.5
ISN 0123      IF(X(K) .GT. XAXIS(11)) GO TO 250
ISN 0124      S(II) = G(2)
ISN 0125      KT = KT + 1
ISN 0126      MM(KT,1) = II
ISN 0127      MM(KT,2) = K
ISN 0128      250 CONTINUE
ISN 0129      J = NMPTS
ISN 0130      GO TO 275
ISN 0131      260 J = JJ
ISN 0132      275 N = N + 1

C
ISN 0133      IF(KT .EQ. 0) GO TO 190
ISN 0134      DO 140 I=4, 104
ISN 0135      IF(S(I) .NE. G(2)) GO TO 140
ISN 0136      DO 170 II=1, KT
ISN 0137      II = MM(II,1)
ISN 0138      K = MM(II,2)
ISN 0139      IF(I .EQ. II) GO TO 180
ISN 0140      170 CONTINUE
ISN 0141      GO TO 140
ISN 0142      180 CONTINUE
ISN 0143      IF(M(K) .LT. 10) GO TO 20
ISN 0144      IX = M(K) / 10
ISN 0145      IY = M(K) - (IX * 10)
ISN 0146      IF(IY .EQ. 0) IY = 10
ISN 0147      IF(II .GE. 103) GO TO 30
ISN 0148      IF(S(II+1) .EQ. G(2) .OR. S(II+2) .EQ. G(2)) GO TO 30
ISN 0149      S(II+1) = MM(IX)
ISN 0150      S(II+2) = MM(IY)
ISN 0151      GO TO 140
ISN 0152      30 IF(II .LE. 5) GO TO 140
ISN 0153      IF(S(II-1) .EQ. G(2) .OR. S(II-2) .EQ. G(2)) GO TO 140
ISN 0154      S(II-1) = MM(IY)
ISN 0155      S(II-2) = MM(IX)
ISN 0156      GO TO 140
ISN 0157      20 IF(II .GE. 104) GO TO 40
ISN 0158      IF(S(II+1) .EQ. G(2)) GO TO 40
ISN 0159      S(II+1) = MM(M(K))
ISN 0160      GO TO 140
ISN 0161      40 IF(II .LE. 4) GO TO 140
ISN 0162

```

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00001480
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00001980
00001990

```



```

0002000 IF(S11-1) .EQ. G(2)) GO TO 140
0002010 S(11-1) = MIN(MK))
0002020 140 CONTINUE
0002030 150 CONTINUE
0002040
0002050
0002060
0002070
0002080
0002090
0002100
0002110
0002120
0002130
0002140
0002150
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0002170
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0002370
0002380
0002390
0002400
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0002440
0002450
0002460

```

C TEST FOR SCALE MARK LOCATION
 C IF(MARK .NE. 0) GO TO 350
 C PLACE VERTICAL SCALE MARK IN 'S' ARRAY
 C IF(S(4) .NE. G(2)) S(4) = G(5)
 C S(2) = G(7)
 C IAXIS = IAXIS - 1
 C WRITE(6,S) YAXIS(IAXIS)
 C RESET MARK INDEX
 C MARK = 6
 C GO TO 340
 C 350 CONTINUE
 C GENERATE ONE LINE OF PLOTTING
 C WRITE(6,S)
 C DECREMENT MARK INDEX
 C 340 MARK = MARK - 1
 C TEST FOR LAST LINE TO DETERMINE IF PLOT IS COMPLETED
 C IF(NL .GT. 1) GO TO 100
 C END OF PLOT. PRINT MAXIMUMS, MINIMUMS, AND SCALES
 C IF(VLAST .LE. 0.0) GO TO 130
 C PRINT 7030, (YAXIS(I), I=1, 11)
 C 130 CONTINUE
 C RETURN
 C FORMATS
 C 7000 FORMAT(1X)
 C 7030 FORMAT(8X,11(1X,E9.3))
 C END

A-144


```

00000411      MSW=3  
60 DO 90 I=1,NP  
   IF(A(I)-PP(MSW)) 70,75,75  
70 IF(A(I)-PH(MSW)) 80,90,90  
80 PH(MSW)=A(I)  
GO TO 90  
75 PP(MSW)=A(I)  
90 CONTINUE  
  
C C C C C C  
*****  
REFERENCE AND SCALE FACTOR ARE CALCULATED  
*****  
C C C C C C  
IF(MSW-(M-1)/20,40,92  
92 CONTINUE  
XMI=0.  
XMI=PP(1)  
DO 96 I=1,3  
   IF(PPI(XMI-XH) 93,94,94  
94 XH=PP(I)  
93 IF(PHI(XMI-XHI) 95,95,96  
95 XMI=P(HI)  
96 CONTINUE  
A(2)=PP(2)  
A(3)=PH(2)  
P(2)=PP(3)  
PM(2)=PH(3)  
P(3)=A(2)  
PM(3)=A(3)  
NRA=104-(N-1)*10  
RA=NRA  
SF=(XH-XMI)/RA  
SFT=10.*SF  
IFSF.EQ.0.0 SF=1.0  
IF(ABS(XH-XMI).LT.1.E-6)GO TO 97  
REF= ABS(XMI/(XM-XHI))*RA+1.5  
GO TO 98  
97 REF=1.5  
98 NR=REF  
   IF(N-2)/100,105,110  
100 PRINT 912, SFT  
105 PRINT 911, SFT  
    GO TO 120  
    GO TO 120  
110 PRINT 910, SFT  
120 PRINT 920  
    DO 200 I=1,NP  
     PLOT(NR)=PRD  
L=Y1(I)/SF+REF  
PLOT(L)=STAR  
IF(M.EQ.1)GO TO 130  
K=Y2(I)/SF+REF  
PLOT(K)=EQ
```

A-147


```
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*****
```

```
COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
```

```
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
```

```
DATA SET D2334PREPL AT LEVEL 004 AS OF 06/25/79
```

```
DATA SET D2332VPP AT LEVEL 001 AS OF 01/17/78
```

```
DATA SET D2332VPPREP AT LEVEL 006 AS OF 10/07/77
```

```
SUBROUTINE PREPLT(IPRINT,NM,NMP,NB,NSP,NORI,NSECIN)
```

```
IN SUBROUTINE PREPLT, OUTPUT DATA FROM KRASH ARE SHUFFLED AND
PROCESSED FOR SUBSEQUENT USE IN SUBROUTINE PLOTT.
```

```
INTEGER*2 NMEP,NNEP,NBFP,NBDP,NSEP,NDRP,NSTP,NENP,
```

```
* JHASS(50,10),JNODE(50,8),JBHF(50,4),JBMD(50,4),
```

```
* JBHS(50,6),JSPR(50,4),JENG(50,3),JDRI(10),
```

```
* NMEN,NNEW,NBFW,NBDM,NSEM,NDRM,NSTM,NENM,NPRINT
```

```
REAL*8 TPRINT,THAX
```

```
DIMENSION WORK(900)
```

```
DIMENSION AM(31,27),TM(31),IM(31)
```

```
DIMENSION AN(41,18),TN(41),IN(41),IMH(41)
```

```
DIMENSION AB(51,8),TB(51),IBG(51),JBG(51),MBG(51),
```

```
* NBG(51),IB(51)
```

```
DIMENSION AT(51,10),TT(51),ITG(51),JTG(51),MTG(51),
```

```
* NTG(51),IT(51)
```

```
DIMENSION AS(41,6),TS(41),ISM(41),ISN(41)
```

```
DIMENSION AE(51,4),TE(51),IEG(51),JEG(51),MEG(51),NEG(51),IE(51)
```

```
DIMENSION AD(101),TD(101),IDH(101)
```

```
DIMENSION AV(201,3),TV(201)
```

```
COMMON/MACFIN/ THAX,IPRINT
```

```
COMMON/OTPLT/ NMEP,NNEP,NBFP,NBDP,NSEP,NDRP,NSTP,NENP,
```

```
* JHASS,JNODE,JBHF,JBMD,JBHS,JSPR,JENG,JDRI,
```

```
* NMEN,NNEW,NBFW,NBDM,NSEM,NDRM,NSTM,NENM,NPRINT
```

```
EQUIVALENCE (WORK(1),AM(1,1)),(WORK(838),TM(1)),
```

```
* (WORK(869),IM(1))
```

```
EQUIVALENCE (WORK(1),AN(1,1)),(WORK(738),TN(1)),
```

```
* (WORK(779),IN(1)),(WORK(820),IMH(1))
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```
EQUIVALENCE (WORK(1),AB(1,1)),(WORK(409),TB(1)),
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* (WORK(460),IBG(1)),(WORK(511),JBG(1)),
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```
* (WORK(562),IBG(1)),(WORK(613),NBG(1)),
```

```
* (WORK(664),IB(1))
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EQUIVALENCE (WORK(1),AT(1,1)),(WORK(511),TT(1)),
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* (WORK(562),ITG(1)),(WORK(613),JTG(1)),
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ISN 0020      *      (WORK(664),MTG(1)),(WORK(715),NTG(1)),
ISN 0021      *      (WORK(766),IT(1))
ISN 0022      *      EQUIVALENCE (WORK(1),AS(1,1)),(WORK(247),TS(1)),
ISN 0023      *      (WORK(1288),ISM(1)),(WORK(329),ISN(1))
ISN 0024      *      EQUIVALENCE (WORK(1),AE(1,1)),(WORK(205),TE(1)),
ISN 0025      *      (WORK(1256),IEG(1)),(WORK(307),JEG(1)),
ISN 0026      *      (WORK(1358),MEG(1)),(WORK(409),NEG(1)),
ISN 0027      *      (WORK(460),IE(1))
ISN 0028      *      EQUIVALENCE (WORK(1),AD(1)),(WORK(102),TD(1)),
ISN 0029      *      (WORK(203),IDM(1))
ISN 0030      *      EQUIVALENCE (WORK(1),AV(1,1)),(WORK(604),TV(1))
ISN 0031      *      TREST = MSECIN * 0.001
ISN 0032      *      NDT = ((TMAX - TREST) / TPRINT) + 1.00001
ISN 0033      *      PLOT MASS POINT DATA IF REQUESTED
ISN 0034      *      REMIND 12
ISN 0035      *      IF(NHEP .LE. 0) GO TO 70
ISN 0036      *      PRINT 7000, NHEP
ISN 0037      *      FORMAT (1H1,5X,15,2X,'MASS PLOT FLAG SUMMARY')
ISN 0038      *      DO 7010 I=1, NHEP
ISN 0039      *      PRINT 7020, (JMASS(I,J), J=1, 10)
ISN 0040      *      FORMAT (10X,10I8)
ISN 0041      *      REMIND 1
ISN 0042      *      L = 1
ISN 0043      *      ICNT = 0
ISN 0044      *      NCNT = 0
ISN 0045      *      DO 10 I=1, NHEP
ISN 0046      *      IFIND = 0
ISN 0047      *      IF(NHEP .EQ. 0) GO TO 15
ISN 0048      *      DO 20 J=1, NDT
ISN 0049      *      DO 30 K=1, NHEP
ISN 0050      *      READ(1) (TH(L),DUPPY,IM(L),(AM(L,M),DUPPY, M=1, 27))
ISN 0051      *      IF(IM(L) .NE. JMASS(I,1)) GO TO 30
ISN 0052      *      IFIND = 1
ISN 0053      *      L = L + 1
ISN 0054      *      ICNT = ICNT + 1
ISN 0055      *      30 CONTINUE
ISN 0056      *      20 CONTINUE
ISN 0057      *      IF(IFIND .EQ. 1) GO TO 35
ISN 0058      *      15 PRINT 6023, JMASS(I,1)
ISN 0059      *      6023 FORMAT(1H1,5X,'18. UNABLE TO FIND DATA FOR MASS',15,
ISN 0060      *      ' PLOTS FOR THIS MASS WILL BE SUPPRESSED.')
ISN 0061      *      35 IF((ICNT+NDT).LE.30) GO TO 50
ISN 0062      *      NCNT = 1
ISN 0063      *      DO 40 K=1, ICNT
ISN 0064      *      WRITE(12) (TH(K),IM(K),(AM(K,M), M=1, 27))
ISN 0065      *      40 CONTINUE
ISN 0066      *      ICNT = 0
ISN 0067      *      L = 1
ISN 0068      *      50 CONTINUE

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ISN 0066 REMIND 1
ISN 0067 10 CONTINUE
ISN 0068 IF(ICNT.EQ.30.OR.NCNT.EQ.0) GO TO 65
ISN 0070 DO 60 K=1, ICNT
ISN 0071 WRITE(12) (TM(K),IM(K),(AM(K,M), M=1, 27))
ISN 0072 60 CONTINUE
ISN 0073 65 CONTINUE
ISN 0074 IF(NCNT.NE.0) REMIND 12
ISN 0076 IFIND = 0
ISN 0077 IC = 0
ISN 0078 DO 85 I=1, NHEP
ISN 0079 IF(IFIND.EQ.1) GO TO 2010
ISN 0081 IC = IC + 1
ISN 0082 IF(NCNT.EQ.0) GO TO 2000
ISN 0084 IF(IC.GT.NHEP) GO TO 81
ISN 0086 ICNT = 1
ISN 0087 DO 90 J=1, NDT
ISN 0088 READ(12) (TH(J),IM(J),(AM(J,K), K=1, 27))
ISN 0089 90 CONTINUE
ISN 0090 GO TO 2010
ISN 0091 2000 ICNT = IC * NDT + 1 - NDT
ISN 0092 2010 CONTINUE
ISN 0093 IF(IM(ICNT).EQ.JMASS(I,1)) GO TO 45
ISN 0095 IFIND = 1
ISN 0096 GO TO 80
ISN 0097 45 IFIND = 0
ISN 0098 IF(JMASS(I,2).EQ.0) GO TO 100
ISN 0100 PRINT 6000, IM(ICNT)
ISN 0101 6000 FORMAT(1H1,5X,'MASS ',I3,3X,'DISPLACEMENTS(IN)' //
* 1X,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
* CALL PLOTT(3,NDT,TH(ICNT),AM(ICNT,1),AM(ICNT,2),AM(ICNT,3))
100 CONTINUE
IF(JMASS(I,3).EQ.0) GO TO 110
PRINT 6001, IM(ICNT)
6001 FORMAT(1H1,5X,'MASS ',I3,3X,'EULER ANGLES(RADIAN)' //
* 1X,'TIME(SEC)',3X,'PHI',6X,'THETA',6X,'PSI')
* CALL PLOTT(3,NDT,TH(ICNT),AM(ICNT,16),AM(ICNT,17),AM(ICNT,18))
110 CONTINUE
IF(JMASS(I,4).EQ.0) GO TO 120
PRINT 6002, IM(ICNT)
6002 FORMAT(1H1,5X,'MASS ',I3,3X,'VELOCITY(IN/SEC) - GROUND AXES' //
* 1X,'TIME(SEC)',2X,'XDOT',6X,'YDOT',6X,'ZDOT')
* CALL PLOTT(3,NDT,TH(ICNT),AM(ICNT,4),AM(ICNT,5),AM(ICNT,6))
120 CONTINUE
IF(JMASS(I,5).EQ.0) GO TO 130
PRINT 6003, IM(ICNT)
6003 FORMAT(1H1,5X,'MASS ',I3,3X,'VELOCITY(IN/SEC) - MASS AXES' //
* 1X,'TIME(SEC)',4X,'U',9X,'V',9X,'W')
* CALL PLOTT(3,NDT,TH(ICNT),AM(ICNT,7),AM(ICNT,8),AM(ICNT,9))
130 CONTINUE
IF(JMASS(I,6).EQ.0) GO TO 140
PRINT 6004, IM(ICNT)
6004 FORMAT(1H1,5X,'MASS ',I3,3X,'ROTATIONAL VELOCITY(RAD/SEC)' //

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*      1X,'TIME(SEC)',4X,'P',9X,'Q',9X,'R')
      CALL PLOTT(3,NDT,TM,AM(ICNT,19),AM(ICNT,20),AM(ICNT,21))
140 CONTINUE
      IF(JMASS(1,7).EQ.0) GO TO 150
      PRINT 6005, IM(ICNT)
6005 FORMAT(1H1,5X,'MASS ',13,3X,'UNFILTERED ACCELERATION(G''S)'
*      // 1X,'TIME(SEC)',2X,'XACC',6X,'YACC',6X,'ZACC')
      CALL PLOTT(3,NDT,TM(ICNT),AM(ICNT,10),AM(ICNT,11),AM(ICNT,12))
150 CONTINUE
      IF(JMASS(1,8).EQ.0) GO TO 160
      PRINT 6006, IM(ICNT)
6006 FORMAT(1H1,5X,'MASS ',13,3X,'FILTERED ACCELERATION(G''S)'
*      // 1X,'TIME(SEC)',2X,'XACCF',5X,'YACCF',5X,'ZACCF')
      CALL PLOTT(3,NDT,TM(ICNT),AM(ICNT,13),AM(ICNT,14),AM(ICNT,15))
160 CONTINUE
      IF(JMASS(1,9).EQ.0) GO TO 80
      PRINT 6007, IM(ICNT)
6007 FORMAT(1H1,5X,'MASS ',13,3X,'ROTATIONAL ACCELERATION(RAD/SEC**2)'
*      // 1X,'TIME(SEC)',2X,'PDOT',6X,'QDOT',6X,'ROOT')
      CALL PLOTT(3,NDT,TM(ICNT),AM(ICNT,22),AM(ICNT,23),AM(ICNT,24))
80 CONTINUE
      IF(JMASS(1,10).EQ.0) GO TO 85
      PRINT 6038, IM(ICNT)
6038 FORMAT(1H1,5X,'MASS ',13,3X,'MASS IMPULSES'//1X,'TIME(SEC)',
1 2X,'XIMP',6X,'YIMP',6X,'ZIMP')
      CALL PLOTT(3,NDT,TM(ICNT),AM(ICNT,25),AM(ICNT,26),AM(ICNT,27))
85 CONTINUE
81 IF(ICNT.NE.0) REMIND 12
70 CONTINUE

C      PLOT NODE POINT DATA IF REQUESTED
C
      IF(NNEP.LE.0) GO TO 170
      PRINT 7030, NNEP
      FORMAT(1H1,5X,15,2X,'NODE PLOT FLAG SUMMARY')
      DO 7040 I=1, NNEP
      PRINT 7050, (JNODE(I,J),J=1,8)
7050 FORMAT(10X,8I8)
7040 REMIND 2
      L = 1
      ICNT = 0
      NCNT = 0
      DO 180 I=1, NNEP
      IFIND = 0
      IF(NNEP.EQ.0) GO TO 185
      DO 190 J=1, NDT
      DO 200 K=1, NNEW
      READ(2) (TN(L),DUPY,IMP(L),IN(L),AM(L,M),DUPY,M=1,18))
      IF(IN(L).NE.JNODE(I,1).OR.IMP(L).NE.JNODE(I,2)) GO TO 200
      IFIND = 1
      L = L + 1
      ICNT = ICNT + 1
      END

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ISM 0179      200 CONTINUE
ISM 0180      190 CONTINUE
ISM 0181      IF(IFIND .EQ. 1) GO TO 195
ISM 0182      185 PRINT 6024, JNODE(I,2), JNODE(I,1)
ISM 0183      6024 FORMAT(1H1,5X,'19. UNABLE TO FIND DATA FOR MASS',I5,
ISM 0184      *' NODE',I5,'. PLOTS FOR THIS NODE WILL BE SUPPRESSED.')
ISM 0185      195 IF((ICNT + NDT) .LE. 40) GO TO 210
ISM 0186      NCNT = 1
ISM 0187      DO 220 K=1, ICNT
ISM 0188      WRITE(12) (TN(K), INH(K), IN(K), (AN(K,M), M=1,18))
ISM 0189      220 CONTINUE
ISM 0190      ICNT = 0
ISM 0191      L = 1
ISM 0192      210 CONTINUE
ISM 0193      REMIND 2
ISM 0194      180 CONTINUE
ISM 0195      IF(ICNT .EQ. 40 .OR. NCNT .EQ. 0) GO TO 230
ISM 0196      DO 240 K=1, ICNT
ISM 0197      WRITE(12) (TN(K), INH(K), IN(K), (AN(K,M), M=1,18))
ISM 0198      240 CONTINUE
ISM 0199      230 CONTINUE
ISM 0200      IF(ICNT .NE. 0) REMIND 12
ISM 0201      IFIND = 0
ISM 0202      IC = 0
ISM 0203      DO 255 I=1, NNEP
ISM 0204      IF(IFIND .EQ. 1) GO TO 2030
ISM 0205      IC = IC + 1
ISM 0206      IF(ICNT .EQ. 0) GO TO 2020
ISM 0207      IF(IC .GT. NNEW) GO TO 251
ISM 0208      ICNT = 1
ISM 0209      DO 260 J=1, NDT
ISM 0210      READ(12) (TN(J), INH(J), IN(J), (AN(J,K), K=1,18))
ISM 0211      260 CONTINUE
ISM 0212      GO TO 2030
ISM 0213      2020 ICNT = IC * NDT + 1 - NDT
ISM 0214      2030 CONTINUE
ISM 0215      IF(INH(ICNT) .EQ. JNODE(I,2) .AND. IN(ICNT) .EQ. JNODE(I,1))
ISM 0216      * GO TO 265
ISM 0217      IFIND = 1
ISM 0218      GO TO 250
ISM 0219      265 IFIND = 0
ISM 0220      IF(JNODE(I,3) .EQ. 0) GO TO 270
ISM 0221      PRINT 6008, INH(ICNT), IN(ICNT)
ISM 0222      6008 FORMAT(1H1,5X,'MASS ',I3,3X,'NODE ',I3,3X,'DISPLACEMENTS(IN)'
ISM 0223      * 1X,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
ISM 0224      CALL PLOTT(3,NDT,TN(ICNT),AN(ICNT,1),AN(ICNT,2),AN(ICNT,3))
ISM 0225      270 CONTINUE
ISM 0226      IF(JNODE(I,4) .EQ. 0) GO TO 280
ISM 0227      PRINT 6009, INH(ICNT), IN(ICNT)
ISM 0228      6009 FORMAT(1H1,5X,'MASS ',I3,3X,'NODE ',I3,3X,'VELOCITY(IN/SEC) - GROUND'
ISM 0229      *ND AXES' // 1X,'TIME(SEC)',2X,'XDOT',6X,'YDOT',6X,'ZDOT')
ISM 0230      CALL PLOTT(3,NDT,TN(ICNT),AN(ICNT,4),AN(ICNT,5),AN(ICNT,6))
ISM 0231      280 CONTINUE
ISM 0232
ISM 0233
ISM 0234
ISM 0235
ISM 0236
ISM 0237

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ISN 0230      IF(JNODE(I,5).EQ.0) GO TO 290
ISN 0240      PRINT 6010, INH(ICNT), INH(ICNT)
ISN 0241      6010 FORMAT(1H1,5X,'MASS ',I3,3X,'NODE ',I3,3X,'VELOCITY(IN/SEC) - MASS000002550
* AXES' // 1X,'TIME(SEC)',4X,'U',9X,'V',9X,'W')
ISN 0242      CALL PLOTT(3,NDT,TN(ICNT),ANH(ICNT,7),ANH(ICNT,8),ANH(ICNT,9))
ISN 0243      290 CONTINUE
ISN 0244      IF(JNODE(I,6).EQ.0) GO TO 300
ISN 0245      PRINT 6011, INH(ICNT), INH(ICNT)
ISN 0246      6011 FORMAT(1H1,5X,'MASS ',I3,3X,'NODE ',I3,3X,'UNFILTERED ACCELERATION000002610
* (G'S)' // 1X,'TIME(SEC)',2X,'XACCF',6X,'YACCF',6X,'ZACCF')
ISN 0247      CALL PLOTT(3,NDT,TN(ICNT),ANH(ICNT,10),ANH(ICNT,11),ANH(ICNT,12))
ISN 0248      300 CONTINUE
ISN 0249      IF(JNODE(I,7).EQ.0) GO TO 250
ISN 0250      PRINT 6012, INH(ICNT), INH(ICNT)
ISN 0251      6012 FORMAT(1H1,5X,'MASS ',I3,3X,'NODE ',I3,3X,'FILTERED ACCELERATION(600002670
* 'S)' // 1X,'TIME(SEC)',2X,'XACCF',5X,'YACCF',5X,'ZACCF')
ISN 0252      CALL PLOTT(3,NDT,TN(ICNT),ANH(ICNT,13),ANH(ICNT,14),ANH(ICNT,15))
ISN 0253      250 CONTINUE
ISN 0254      IF(JNODE(I,8).EQ.0) GO TO 255
ISN 0255      PRINT 6039, INH(ICNT), INH(ICNT)
ISN 0256      6039 FORMAT(1H1,5X,'MASS ',I3,3X,'NODE ',I3,3X,'NODE IMPULSES(6-SEC)'
ISN 0257      1 // 1X,'TIME(SEC)',2X,'XIMPNP',5X,'YIMPNP',5X,'ZIMPNP')
ISN 0258      CALL PLOTT(3,NDT,TN(ICNT),ANH(ICNT,16),ANH(ICNT,17),ANH(ICNT,18))
ISN 0259      255 CONTINUE
ISN 0260      251 IF(NCNT.NE.0) REMIND 12
ISN 0261      170 CONTINUE
ISN 0262      C
ISN 0263      C
ISN 0264      C
ISN 0265      PLOT BEAM ELEMENT FORCE DATA IF REQUIRED
ISN 0266      IF(NBFP.LE.0) GO TO 320
ISN 0267      PRINT 7060, NBFP
ISN 0268      7060 FORMAT (1H1,5X,I5,2X,'BEAM FORCE PLOT FLAG SUMMARY')
ISN 0269      DO 7070 I=1, NBFP
ISN 0270      PRINT 7080, (JBMF(I,J), J=1, 4)
ISN 0271      7080 FORMAT (10X,4I8)
ISN 0272      7070 CONTINUE
ISN 0273      REMIND 3
ISN 0274      L = 1
ISN 0275      ICNT = 0
ISN 0276      NCNT = 0
ISN 0277      DO 330 I=1, NBFP
ISN 0278      IFIND = 0
ISN 0279      IF(NBFW.EQ.0) GO TO 335
ISN 0280      DO 340 J=1, NDT
ISN 0281      DO 350 K=1, NBFW
ISN 0282      READ(3) (TB(L),DUPHY,IB(L),IBG(L),JBG(L),MBG(L),NBG(L),
ISN 0283      * (AB(L,M),DUPHY,M=1,8))
ISN 0284      IF(TB(L).NE. JBMF(I,1)) GO TO 350
ISN 0285      IFIND = 1
ISN 0286      L = L + 1
ISN 0287      L = L + 1
ISN 0288      ICNT = ICNT + 1
ISN 0289      350 CONTINUE
ISN 0290      340 CONTINUE
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ISN 0291      IF(IFIND .EQ. 1) GO TO 345
ISN 0292      335 PRINT 6025, JBMF(I,1)
ISN 0293      6025 FORMAT(1H1,5X,'2C. UNABLE TO FIND DATA FOR BEAM',15,
ISN 0294      * ' . FORCE PLOTS FOR THIS BEAM WILL BE SUPPRESSED.')
ISN 0295      345 IF((ICNT + NDT) .LE. 50) GO TO 360
ISN 0296      NCNT = 1
ISN 0297      DO 370 K=1, ICNT
ISN 0298      WRITE(12) (TB(K),IB(K),JBG(K),MBG(K),NBG(K),(AB(K,M),
ISN 0299      * M=1, 8))
ISN 0300      370 CONTINUE
ISN 0301      ICNT = 0
ISN 0302      L = 1
ISN 0303      360 CONTINUE
ISN 0304      REMIND 3
ISN 0305      330 CONTINUE
ISN 0306      IF(ICNT .EQ. 50 .OR. NCNT .EQ. 0) GO TO 380
ISN 0307      DO 390 K=1, ICNT
ISN 0308      WRITE(12) (TB(K),IB(K),JBG(K),MBG(K),NBG(K),(AB(K,M),
ISN 0309      * M=1, 8))
ISN 0310      390 CONTINUE
ISN 0311      380 CONTINUE
ISN 0312      IF(NCNT .NE. 0) REMIND 12
ISN 0313      IFIND = 0
ISN 0314      IC = 0
ISN 0315      DO 400 I=1, NBFP
ISN 0316      IF(IFIND .EQ. 1) GO TO 2050
ISN 0317      IC = IC + 1
ISN 0318      IF(NCNT .EQ. 0) GO TO 2040
ISN 0319      IF(IC .GT. NBFM) GO TO 401
ISN 0320      ICNT = 1
ISN 0321      DO 410 J=1, NDT
ISN 0322      READ(12) (TB(J),IB(J),JBG(J),MBG(J),NBG(J),(AB(J,M),
ISN 0323      * M=1, 8))
ISN 0324      410 CONTINUE
ISN 0325      GO TO 2050
ISN 0326      2040 ICNT = IC * NDT + 1 - NDT
ISN 0327      2050 CONTINUE
ISN 0328      IF(IB(ICNT) .EQ. JBMF(I,1)) GO TO 415
ISN 0329      IFIND = 1
ISN 0330      GO TO 400
ISN 0331      415 IFIND = 0
ISN 0332      IF(JBMF(I,2) .EQ. 0) GO TO 420
ISN 0333      PRINT 6013, IB(ICNT),IBG(ICNT),MBG(ICNT),JBG(ICNT),NBG(ICNT)
ISN 0334      6013 FORMAT(1H1,5X,'BEAM ',13,3X,'I,M =',14,' ',12,5X,'J,N =',14,' ',
ISN 0335      * '12,5X,'AXIAL AND SHEAR FORCES(LB)' // 1X,'TIME(SEC)',3X,
ISN 0336      * 'FX',8X,'FY',8X,'FZ')
ISN 0337      CALL PLOT(13,NBT,TB(ICNT),ABI(ICNT,1),AB(ICNT,2),AB(ICNT,3))
ISN 0338      420 CONTINUE
ISN 0339      IF(JBMF(I,3) .EQ. 0) GO TO 430
ISN 0340      PRINT 6014, IB(ICNT),IBG(ICNT),MBG(ICNT),JBG(ICNT),NBG(ICNT)
ISN 0341      6014 FORMAT(1H1,5X,'BEAM ',13,3X,'I,M =',14,' ',12,5X,'J,N =',14,' ',
ISN 0342      * '12,5X,'MOMENTS AT I,M(IN-LB)' // 1X,'TIME(SEC)',
ISN 0343      * '3X,'MX',8X,'MY',8X,'MZ')
ISN 0344      430 CONTINUE
ISN 0345      440 CONTINUE

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ISN 0346      CALL PLOTT(3,NDT,TB(ICNT),AB(ICNT,4),AB(ICNT,5),AB(ICNT,7))
ISN 0347      430 CONTINUE
ISN 0348      IF(JBHF(I,4) .EQ. 0) GO TO 400
ISN 0350      PRINT 6015, IB(ICNT),JBG(ICNT),MBG(ICNT),JBG(ICNT),NBG(ICNT)
ISN 0351      6015 FORMAT(IH1,5X,'BEAM ',I3,3X,'I,M = ',I4,',',I2,5X,'J,N = ',I4,',',
*             12,5X,'MOMENTS AT J,(IN-LB)' // 1X,'TIME(SEC)',
*             3X,'MX',8X,'MY',8X,'MZ')
ISN 0352      CALL PLOTT(3,NDT,TB(ICNT),AB(ICNT,4),AB(ICNT,6),AB(ICNT,8))
ISN 0353      400 CONTINUE
ISN 0354      401 IF(NCNT .NE. 0) REMIND 12
ISN 0356      320 CONTINUE

C
C   PLOT BEAM ELEMENT DEFLECTION DATA IF REQUIRED
C
      IF(NBOP .LE. 0) GO TO 440
      PRINT 7090, NBOP
      7090 FORMAT (IH1,5X,I5,2X,'BEAM DEFLECTION PLOT FLAG SUMMARY')
      DO 7100 I=1, NBOP
      PRINT 7080, (JBMD(I,J), J=1, 4)
      7100 CONTINUE
      REMIND 4
      L = 1
      ICNT = 0
      NCNT = 0
      DO 450 I=1, NBOP
      IFIND = 0
      IF(NBOW .EQ. 0) GO TO 455
      DO 460 J=1, NDT
      DO 470 K=1, NBOW
      READ(4) (TB(L),DUMY,IB(L),JBG(L),JBG(L),MBG(L),NBG(L),
*             (AB(L,M),DUMY,M=1, 8))
      IF(IB(L) .NE. JBMD(I,1)) GO TO 470
      IFIND = 1
      L = L + 1
      ICNT = ICNT + 1
      470 CONTINUE
      460 CONTINUE
      455 PRINT 6026, JBMD(I,1)
      6026 FORMAT(IH1,5X,'21. UNABLE TO FIND DATA FOR BEAM',I5,
*             ' DEFLECTION PLOTS FOR THIS BEAM WILL BE SUPPRESSED.')
      465 IF((ICNT + NDT) .LE. 50) GO TO 480
      NCNT = 1
      DO 490 K=1, ICNT
      WRITE(12) (TB(K),IB(K),JBG(K),JBG(K),MBG(K),NBG(K),
*             (AB(K,M),M=1, 8))
      490 CONTINUE
      ICNT = 0
      L = 1
      480 CONTINUE
      REMIND 4
      450 CONTINUE
      IF(ICNT .EQ. 50 .OR. NCNT .EQ. 0) GO TO 500

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ISN 0399      DO 510 K=1, ICNT
ISN 0400      WRITE(12) (TB(K),IB(K),IBG(K),JBG(K),MBG(K),NBG(K),
*              (AB(K,M), M=1, 8))
ISN 0401      510 CONTINUE
ISN 0402      500 CONTINUE
ISN 0403      IF(INCNT.NE. 0) REMIND 12
ISN 0404      IFIND = 0
ISN 0405      IC = 0
ISN 0406      DO 520 I=1, NBDP
ISN 0407      IF(IFIND.EQ. 1) GO TO 2070
ISN 0408      IC = IC + 1
ISN 0409      IF(INCNT.EQ. 0) GO TO 2060
ISN 0410      IF(IC.GT. NBDW) GO TO 521
ISN 0411      ICNT = 1
ISN 0412      DO 530 J=1, NDT
ISN 0413      READ(12) (TB(J),IB(J),IBG(J),JBG(J),MBG(J),NBG(J),
*              (AB(J,M), M=1, 8))
ISN 0414      530 CONTINUE
ISN 0415      GO TO 2070
ISN 0416      2060 ICNT = IC * NDT + 1 - NDT
ISN 0417      2070 CONTINUE
ISN 0418      IF(IB(INCNT).EQ. JBMD(I,1)) GO TO 535
ISN 0419      IFIND = 1
ISN 0420      GO TO 520
ISN 0421      535 IFIND = 0
ISN 0422      IF(JBMD(I,2).EQ. 0) GO TO 540
ISN 0423      PRINT 6016, IB(INCNT),IBG(INCNT),MBG(INCNT),JBG(INCNT),NBG(INCNT)
ISN 0424      PRINT 6016, 'BEAM ',I3,X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
ISN 0425      '12,5X,'RELATIVE DEFLECTIONS*J-I*(IN)' // IX,'TIME(SEC)',
ISN 0426      '4X,'X',9X,'Y',9X,'Z')
ISN 0427      CALL PLOTT(3,NDT,TB(INCNT),AB(INCNT,1),AB(INCNT,2),AB(INCNT,3))
ISN 0428      540 CONTINUE
ISN 0429      IF(JBMD(I,3).EQ. 0) GO TO 550
ISN 0430      PRINT 6017, IB(INCNT),IBG(INCNT),MBG(INCNT),JBG(INCNT),NBG(INCNT)
ISN 0431      PRINT 6017, 'BEAM ',I3,X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
ISN 0432      '12,5X,'RELATIVE ROTATIONS*J-I*(DEGREE)' // IX,'TIME(SEC)',
ISN 0433      '3X,'PHI',6X,'THETA',6X,'PSI')
ISN 0434      CALL PLOTT(3,NDT,TB(INCNT),AB(INCNT,4),AB(INCNT,5),AB(INCNT,6))
ISN 0435      550 CONTINUE
ISN 0436      IF(JBMD(I,4).EQ. 0) GO TO 520
ISN 0437      PRINT 6018, IB(INCNT),IBG(INCNT),MBG(INCNT),JBG(INCNT),NBG(INCNT)
ISN 0438      PRINT 6018, 'BEAM ',I3,X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
ISN 0439      '12,5X,'RELATIVE ROTATIONS*J-I*(DEGREE)' // IX,'TIME(SEC)',
ISN 0440      '3X,'PHI',6X,'THETA',6X,'PSI')
ISN 0441      CALL PLOTT(3,NDT,TB(INCNT),AB(INCNT,4),AB(INCNT,7),AB(INCNT,8))
ISN 0442      520 CONTINUE
ISN 0443      521 IF(INCNT.NE. 0) REMIND 12
ISN 0444      440 CONTINUE
ISN 0445      C
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ISN 1000      C

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7110 FORMAT (I1,5X,I5,2X,'BEAM STRESS PLOT FLAG SUMMARY')
DO 7120 I=1, NSTP
PRINT 7130, (JBMS(I,J), J=1, 6)
7130 FORMAT (10X,6I8)
7120 CONTINUE
REWIND 13
L = 1
ICNT = 0
NCNT = 0
DO 860 I=1, NSTP
IFIND = 0
IF(NSTW .EQ. 0) GO TO 865
DO 870 J=1, NDT
DO 880 K=1, NSTW
DO READ(13) (TT(I,L),DUMTY,IT(L),JTG(L),MTG(L),NTG(L),
* (AT(L,M),DUMRY,M=1,10))
IF(JT(L) .NE. JBMS(I,1)) GO TO 880
IFIND = 1
L = L + 1
ICNT = ICNT + 1
860 CONTINUE
870 CONTINUE
865 PRINT 6029, JBMS(I,1)
6029 FORMAT(I1,5X,'22. UNABLE TO FIND DATA FOR BEAM',I5,
* ' STRESS PLOTS FOR THIS BEAM WILL BE SUPPRESSED.')
875 IF(ICNT + NDT) .LE. 50) GO TO 890
NCNT = 1
DO 900 K=1, ICNT
WRITE(12) (TT(K),IT(K),JTG(K),JTG(K),MTG(K),MTG(K),
* (AT(K,M),M=1,10))
900 CONTINUE
ICNT = 0
L = 1
890 CONTINUE
REWIND 13
860 CONTINUE
IF(ICNT .EQ. 50 .OR. NCNT .EQ. 0) GO TO 910
DO 920 K=1, ICNT
WRITE(12) (TT(K),IT(K),JTG(K),JTG(K),MTG(K),MTG(K),
* (AT(K,M),M=1,10))
920 CONTINUE
910 CONTINUE
IF(NCNT .NE. 0) REWIND 12
IFIND = 0
IC = 0
DO 930 I=1, NSTP
IF(IFIND .EQ.1) GO TO 2090
IC = IC + 1
IF(NCNT .EQ. 0) GO TO 2080
IF(IC .GT. NSTW) GO TO 931
ICNT = 1
DO 940 J=1, NDT

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AD-A055 898

LOCKHEED-CALIFORNIA CO BURBANK

F/G 1/2

GENERAL AVIATION AIRPLANE STRUCTURAL CRASHWORTHINESS USER'S MAN--ETC(U)

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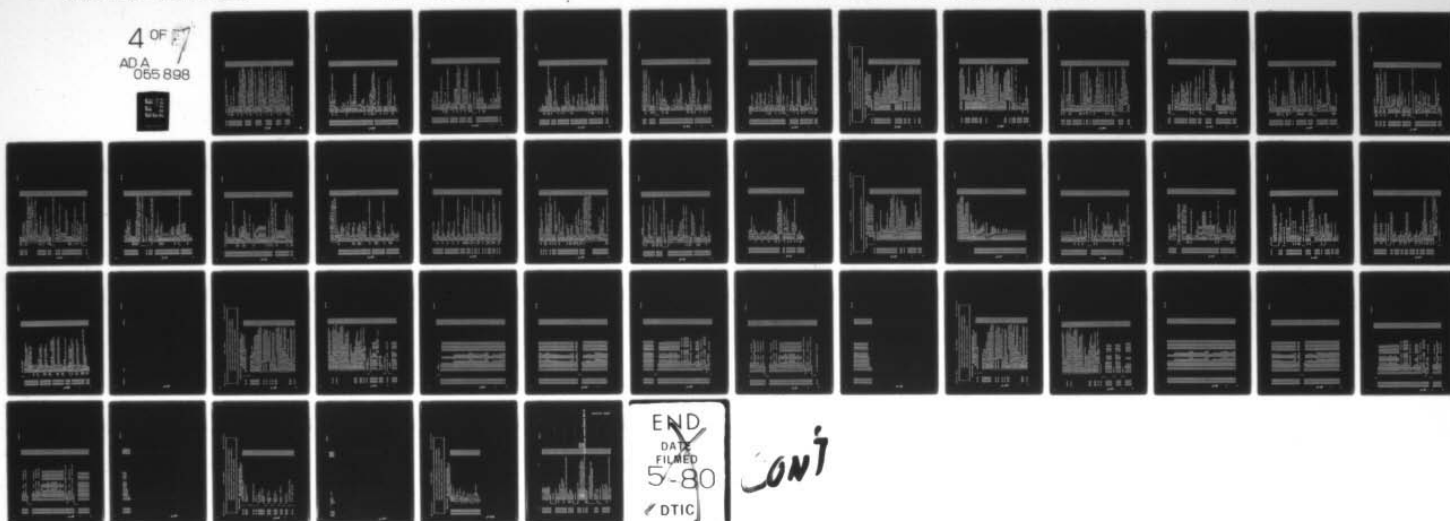
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CONT


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ISN 0551      IF(INSEP .EQ. 0) GO TO 560
ISN 0553      PRINT 7140, NSEP
ISN 0554      7140 FORMAT (1H1,5X,I5,2X,'EXTERNAL SPRING PLOT FLAG SUMMARY')
ISN 0555      DO 7150 I=1, NSEP
ISN 0556      PRINT 7080, (JSPI(I,J), J=1, 4)
ISN 0557      7150 CONTINUE
ISN 0558      REMIND 8
ISN 0559      L = 1
ISN 0560      ICNT = 0
ISN 0561      NCNT = 0
ISN 0562      DO 545 I=1, 40
ISN 0563      DO 545 J=1, 6
ISN 0564      AS(I,J) = 0.0
ISN 0565      545 CONTINUE
ISN 0566      DO 555 I=1, NSEP
ISN 0567      IFIND = 0
ISN 0568      IF(INSEP .EQ. 0) GO TO 556
ISN 0569      DO 560 J=1, NOT
ISN 0570      DO 570 K=1, NSEP
ISN 0571      READ(8) (TSD,DUMY,JSM,JSK,JSN,ADUM1,DUMY2,ADUMY)
ISN 0572      IF(JSM .NE. JSPI(I,1)) .OR. JSN .NE. JSPI(I,2)) GO TO 570
ISN 0573      IFIND = 1
ISN 0574      TS(L) = TSD
ISN 0575      ISM(L) = JSM
ISN 0576      JSN(L) = JSN
ISN 0577      AS(L,JSK) = ADUM1
ISN 0578      AS(L,JSK+3) = ADUM2
ISN 0579      570 CONTINUE
ISN 0580      L = L + 1
ISN 0581      ICNT = ICNT + 1
ISN 0582      560 CONTINUE
ISN 0583      IF(IFIND .EQ. 1) GO TO 565
ISN 0584      556 PRINT 6027, JSPI(I,1),JSPI(I,2)
ISN 0585      6027 FORMAT(1H1,5X,'23. UNABLE TO FIND DATA FOR SPRING',I5,
ISN 0586      * ' NODE',I5,'. PLOTS FOR THIS SPRING WILL BE SUPPRESSED.')
ISN 0587      565 IF((ICNT + NOT) .LE. 40) GO TO 590
ISN 0588      NCNT = 1
ISN 0589      DO 600 K=1, ICNT
ISN 0590      WRITE(12) (TS(K),ISM(K),JSN(K),AS(K,M), M=1, 6))
ISN 0591      600 CONTINUE
ISN 0592      ICNT = 0
ISN 0593      L = 1
ISN 0594      590 CONTINUE
ISN 0595      REMIND 8
ISN 0596      555 CONTINUE
ISN 0597      IF(ICNT .EQ. 40 .OR. NCNT .EQ. 0) GO TO 610
ISN 0598      DO 620 K=1, ICNT
ISN 0599      WRITE(12) (TS(K),ISM(K),JSN(K),AS(K,M), M=1, 6))
ISN 0600      620 CONTINUE
ISN 0601      610 CONTINUE
ISN 0602      IF(INCNT .NE. 0) REMIND 12
ISN 0603      IFIND = 0
ISN 0604      IC = 0
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ISN 0610 DO 630 I=1, NSEP
ISN 0611 IF(IFIND.EQ. 1) GO TO 2110
ISN 0613 IC = IC + 1
ISN 0614 IF(ICNT.EQ. 0) GO TO 2100
ISN 0616 IF(IC.GT. NSEM) GO TO 631
ISN 0618 ICNT = 1
ISN 0619 DO 640 J=1, NDT
ISN 0620 READ(12) (TS(J),ISM(J),ISN(J),(AS(J,M), M=1, 6))
ISN 0621 640 CONTINUE
ISN 0622 GO TO 2110
ISN 0623 2100 ICNT = IC * NDT + 1 - NDT
ISN 0624 2110 CONTINUE
ISN 0625 IF(ISM(ICNT).EQ. JSPPR(I,1).AND. ISN(ICNT).EQ. JSPPR(I,2))
* GO TO 645
IFIND = 1
GO TO 630
645 IFIND = 0
IF(JSPPR(I,3).EQ. 0) GO TO 650
PRINT 6019, ISM(ICNT),ISM(ICNT)
6019 FORMAT(1H1,5X,'EXTERNAL SPRING I,M =',I4,',',I2,5X,
* 'COMPRESSION(IN)' // 1X,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
CALL PLOTT(3,NDT,TS(ICNT),AS(ICNT,1),AS(ICNT,2),AS(ICNT,3))
650 CONTINUE
IF(JSPPR(I,4).EQ. 0) GO TO 630
PRINT 6020, ISM(ICNT),ISM(ICNT)
6020 FORMAT(1H1,5X,'EXTERNAL SPRING I,M =',I4,',',I2,5X,
* 'AXIAL LOAD(LB)' // 1X,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
CALL PLOTT(3,NDT,TS(ICNT),AS(ICNT,4),AS(ICNT,5),AS(ICNT,6))
630 CONTINUE
631 IF(ICNT.NE. 0) REWIND 12
580 CONTINUE
C
C PLOT STRAINEDAMPING ENERGY
C
IF(NEMP.EQ. 0) GO TO 581
PRINT 7161,NEMP
7161 FORMAT(1H1,5X,I5,2X,'STRAIN AND DAMPING PLOT FLAG SUMMARY')
DO 7162 I=1,NEMP
PRINT 7080,(JENG(I,J),J=1,3)
7081 FORMAT(10X,3I8)
7162 CONTINUE
REWIND 11
L=1
NCNT=0
DO 331 I=1,NEMP
IFIND=0
IF(NEMP.EQ. 0) GO TO 336
DO 341 J=1,NDT
DO 351 K=1,NEMP
READ(11) (TE(L),DUMPY,IE(L),JEG(L),MEG(L),JEG(L),NEG(L),
1 (AE(L,M),DUMPY,M=1,4))
IF(IE(L).NE. JENG(I,1)) GO TO 351

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ISN 0666      IFIND=1
ISN 0667      L=L+1
ISN 0668      ICNT=ICNT+1
ISN 0669      351 CONTINUE
ISN 0670      341 CONTINUE
ISN 0671      IF(IFIND.EQ.1) GO TO 346
ISN 0672      336 PRINT 6040,JENG(I,1)
ISN 0673      6040 FORMAT(1H1,5X,'26.UNABLE TO FIND DATA FOR BEAM',15,'.ENERGY PLOTS
ISN 0674      1 FOR THIS BEAM WILL BE SUPPRESSED.')
ISN 0675      346 IF((ICNT.NGT).LE.50) GO TO 361
ISN 0676      NCNT=1
ISN 0677      DO 371 K=1,ICNT
ISN 0678      WRITE(12) (TE(K),IE(K),IEG(K),JEG(K),NEG(K),
ISN 0679      1 (AE(L,M),M=1,4))
ISN 0680      371 CONTINUE
ISN 0681      ICNT=0
ISN 0682      L=1
ISN 0683      361 CONTINUE
ISN 0684      REWIND 11
ISN 0685      331 CONTINUE
ISN 0686      IF(ICNT.EQ.50.OR.NCNT.EQ.0) GO TO 381
ISN 0687      DO 391 K=1,ICNT
ISN 0688      WRITE(12) (TE(K),IE(K),IEG(K),JEG(K),NEG(K),
ISN 0689      1 (AE(L,M),M=1,4))
ISN 0690      391 CONTINUE
ISN 0691      381 CONTINUE
ISN 0692      IF(NCNT.NE.0) REWIND 12
ISN 0693      IFIND=0
ISN 0694      IC=0
ISN 0695      DO 402 I=1,NENP
ISN 0696      IF(IFIND.EQ.1) GO TO 2051
ISN 0697      IC=IC+1
ISN 0698      IF(NCNT.EQ.0) GO TO 2041
ISN 0699      IF(IC.GT.NENM) GO TO 403
ISN 0700      ICNT=1
ISN 0701      DO 411 J=1,NOT
ISN 0702      READ(12) (TE(J),IE(J),IEG(J),JEG(J),NEG(J),
ISN 0703      1 (AE(L,M),M=1,4))
ISN 0704      411 CONTINUE
ISN 0705      GO TO 2051
ISN 0706      2041 ICNT=IC+NOT+1-NOT
ISN 0707      2051 CONTINUE
ISN 0708      IF(IE(ICNT).EQ.JENG(I,1)) GO TO 416
ISN 0709      IFIND=1
ISN 0710      GO TO 402
ISN 0711      416 IFIND=0
ISN 0712      IF(JENG(I,2).EQ.0) GO TO 421
ISN 0713      PRINT 6050,IE(ICNT),IEG(ICNT),JEG(ICNT),NEG(ICNT)
ISN 0714      6050 FORMAT(1H1,5X,'BEAM',13,3X,'I,M=',14,'',12,5X,'J,N=',14,'',12,
ISN 0715      1 5X,'STRAIN ENERGY AND PERCENT',1X,'TIME(SEC)',3X,'SE',8X,
ISN 0716      2 '%')
ISN 0717      CALL PLOTT(2,NOT,TE(ICNT),AE(ICNT,1),AE(ICNT,2))
ISN 0718      421 CONTINUE
ISN 0719
ISN 0720
ISN 0721

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ISN 0722 IF(JENG(I,3).EQ.0) GO TO 431
ISN 0724 PRINT 6051,IE(ICNT),IEG(ICNT),MEG(ICNT),JEG(ICNT),NEG(ICNT)
ISN 0725 6051 FORMAT(IH1,5X,'BEAN',I3,3X,'I,M=',I4,',',I2,5X,'J,N=',I4,
1 ',',I2,5X,'DAMPING ENERGY AND PERCENT',// 1X,'TIME(SEC)',3X,
2 'DE',8X,'%')
ISN 0726 CALL PLOTT(2,NOT,TE(ICNT),AE(ICNT,3),AE(ICNT,4))
ISN 0727 431 CONTINUE
ISN 0728 402 CONTINUE
ISN 0729 403 IF(NCNT.NE.0) REMIND 12
ISN 0731 581 CONTINUE
C
C PLOT DRI MASS DATA IF REQUIRED
C
ISN 0732 IF(NDRP .EQ. 0) GO TO 660
ISN 0734 PRINT 7160, NDRP
ISN 0735 7160 FORMAT (IH1,5X,I5,2X,'DRI PLOT FLAG SUMMARY')
ISN 0736 DO 7170 I=1, NDRP
ISN 0737 PRINT 7180, (JDRI(I))
ISN 0738 7180 FORMAT (10X,I8)
ISN 0739 7170 CONTINUE
ISN 0740 REMIND 9
ISN 0741 L = 1
ISN 0742 ICNT = 0
ISN 0743 NCNT = 0
ISN 0744 DO 670 I=1, NDRP
ISN 0745 IFIND = 0
ISN 0746 IF(NDRM .EQ. 0) GO TO 675
ISN 0748 DO 680 J=1, NDT
ISN 0749 DO 690 K=1, NDRM
ISN 0750 READ(9) (TD(L),DUPPY,IDM(L),AD(L),DUPPY)
ISN 0751 IF(IDM(L) .NE. JDRI(I)) GO TO 690
ISN 0753 IFIND = 1
ISN 0754 L = L + 1
ISN 0755 ICNT = ICNT + 1
ISN 0756 690 CONTINUE
ISN 0757 680 CONTINUE
ISN 0758 IF(IFIND .EQ. 1) GO TO 685
ISN 0760 675 PRINT 6028, JDRI(I)
ISN 0761 6028 FORMAT(IH1,5X,'24. UNABLE TO FIND DATA FOR DRI MASS',I5,
* '. PLOTS FOR THIS DRI MASS WILL BE SUPPRESSED.')
ISN 0762 685 IF((ICNT + NDT) .LE. 100) GO TO 700
ISN 0764 NCNT = 1
ISN 0765 DO 710 K=1, ICNT
ISN 0766 WRITE(12) (TD(K),IDM(K),AD(K))
ISN 0767 710 CONTINUE
ISN 0768 ICNT = 0
ISN 0769 L = 1
ISN 0770 700 CONTINUE
ISN 0771 REMIND 9
ISN 0772 670 CONTINUE
ISN 0773 IF(ICNT .EQ. 100 .OR. NCNT .EQ. 0) GO TO 720
ISN 0775 DO 730 K=1, ICNT
ISN 0776 WRITE(12) (TD(K),IDM(K),AD(K))

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1 FINT(6,150),VOL(5),VZERO(5),KMATR(6,4),MVCH,INBUFF(5,8)
COMMON/ENERGY/ XPCT(80),XETOT(80),XETOTO(80),XSE(80),XDE(80),
1 XCE(80),XFE(80),KEI(80),PEI(80),XETOTL,KETOTL,
2 PETOTL,SETOTL,DETOTL,CETOTL,FEOTL
COMMON/INIDCP/ YDI(80)
COMMON/INPR/ NDRI,NSP
COMMON/MAPR/ ETOTL,ENGSMY,INGSCT
COMMON/MAPR1/ DEV,ETIME,IEER,IESE,IEPSE,IEDE,IEPDE,IECE,IEPCE,
1 IEFE,IEPFE,IEDEV,IEETOT
COMMON/PCFIII/ SYNFLG
COMMON/MP0012/ MG,NG,INP,MNP
COMMON/MP0012/ II,KK,MM
COMMON/MP0014/ NNP
COMMON/MP01R8/ XNP,YNP,ZNP,UNP,VNP,MNP,XDNP,YDNP,ZDNP,
1 XACDNP,YACDNP,ZACDNP,SBUCKR(150),PCR(150)
COMMON/INOUT/ FCUT,NTOL1,NTOL2,NTOL3
COMMON/PRMA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50),
1 ZACNPF(50),XINPF(80),YINPF(80),ZINPF(80),XIMPNI(50),YIMPNI(50),
2 ZIMPNI(50),XIMPOL(80),YIMPOL(80),ZIMPOL(80),XIMPNI(50),
3 YIMPNI(50),ZIMPNI(50)
COMMON/COTALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),
1 Y(81),Z(81),AI(9),AJ(9),AK(9),XC(6),XK(5400),XI(80),
2 YI(80),ZI(80),XZI(80),XZI(80),YZI(80),AIJ(9),BIJ(720),
3 DRI(150),OAI(720),VEE(900),MGT(80),PHI(80),THETA(80),PSI(80),
4 PDOT(80),GDOT(80),RODT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),
5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
6 YACC(80),YACC(80),ZACC(80),AIDOT(9),
7 PHIIJ(150),THEIJ(150),PSIIJ(150),SUMDF(6,150),TITLE,
8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9 DPTN(81),DQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),
A CEIKF(40),
B SBAR(40),KUN(40),MAXNM,MAXTGS,MAXTBL,
C NI,NB,I,J,IG(150),JG(150),
D NI(900),NN(40),IJPR(150)
COMMON/ININPR/ NSF,NTF,NDE,NSPD,NED,NS,NRP,NINP
COMMON/OTPLT/ NTEP,NNEP,NBFP,NBDP,NSEP,NDRP,NSSTP,NENP,
* JHASS,JNODE,JBMF,JBMD,JBMS,JSPR,JENG,JORI,
* NTEH,NNEH,NBHM,NBDH,NSEH,NDRH,NSHM,NPRINT
COMMON /MAX/ IRUPSH(150),IPENSH(80),VEEBAR(900),ZINIT(80),
1 DPHIJ(150),FUB(150)
COMMON /VARINT/ MINDT,DT2,TPRINT,EL,EU,RATHIN,RATHAX,IPC,IVAR
EQUVALENCE (VEE(1),VEE2(1,1))
DATA IPLN /
* X(AFT) - Y(+RIGHT) X(AFT) - Z(+UP) Y(+RIGHT) - Z(+UP) ' /
ILINES = 60
IPL = 6
IF(NRP.LE. 0) IPL = 2
ITTL = 9
C FORCE NEW PAGE
NPR = 1000
DO 3099 I = 1,NN
IF (ILINES-NPR-IPL) 3010,3020,3020
3010 PRINT 3100,TITLE

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ISN 0057 3100 FORMAT(1H1,20A4 / 1X,20A4 / )
ISN 0058 PRINT 3200,TIME,IPC
ISN 0059 3200 FORMAT(1H ,6HTIME =,F9.6,5X,'NUMBER OF INTEGRATION INTERVALS =',
1 I4/)
ISN 0060 IF(NRP .GT. 0) PRINT 3201
ISN 0061 IF(NRP .LE. 0) PRINT 3214
ISN 0062 3201 FORMAT(1X,'MASS DISPLACEMENTS,VELOCITIES,AND ACCELERATIONS' / )
ISN 0063 3214 FORMAT(1X,'NO MASS RESPONSE DATA REQUESTED EXCEPT TRANSLATIONAL
*CELERATIONS' / )
ISN 0064 IF(NRP .LE. 0) GO TO 3018
ISN 0065 PRINT 3300
ISN 0066 PRINT 400
ISN 0067 PRINT 500
ISN 0068 PRINT 600
ISN 0069 3018 PRINT 900
ISN 0070 3300 FORMAT(1H ,18X,1MX,14X,1HY,14X,1HZ,13X,3PHI,11X,5THETA,
1 11X,3RPSI)
ISN 0071 400 FORMAT(1H ,17X,4HXDOT,11X,4HYDOT,11X,4HZDOT,10X,6HPHIDOT,
1 8X,8HTHETADOT,8X,6HPSIDOT)
ISN 0072 500 FORMAT(1H ,18X,1HU,14X,1HV,14X,1HW,14X,1HP,14X,1HQ,14X,1HR)
ISN 0073 600 FORMAT(1H ,17X,4HUDOT,11X,4HVDOT,11X,4HWDOT,11X,4HPDOT,11X,
1 4HQDOT,11X,4HRDOT)
ISN 0074 900 FORMAT (1H ,16X,6HXACCEL,9X,6HYACCEL,9X,6HZACCEL,
1 9X,6HXCACFIL,9X,6HYACFIL,9X,6HZACFIL / )
ISN 0075 NPR = ITTL
ISN 0076 3020 NPR = NPR+1PL
ISN 0077 IF(NRP .LE. 0) GO TO 788
ISN 0078 PRINT 700, I,X(I),Y(I),Z(I),PHI(I),THETA(I),PSI(I)
ISN 0079 PRINT 800, XDOT(I),YDOT(I),ZDOT(I),PHIDOT(I),THETADOT(I),PSIDOT(I)
ISN 0080 PRINT 800, U(I),V(I),W(I),P(I),Q(I),R(I)
ISN 0081 PRINT 800, UDOT(I),VDOT(I),WDOT(I),PDOT(I),QDOT(I),RDOT(I)
ISN 0082 IF(FCUT.EQ.0.) GO TO 1000
ISN 0083 PRINT 800,XACC(I),YACC(I),ZACC(I),XACF(I),YACF(I),ZACF(I)
ISN 0084 GO TO 1010
ISN 0085 1000 PRINT 800, XACC(I),YACC(I),ZACC(I)
ISN 0086 GO TO 1010
ISN 0087 788 IF(FCUT.EQ.0.) GO TO 1001
ISN 0088 PRINT 700,I,XACC(I),YACC(I),ZACC(I),XACF(I),YACF(I),ZACF(I)
ISN 0089 GO TO 1010
ISN 0090 1001 PRINT 700,I, XACC(I),YACC(I),ZACC(I)
ISN 0091 1010 PRINT 800
ISN 0092 C
ISN 0093 C
ISN 0094 WRITE MASS POINT DATA ON UNIT 1 FOR SUBSEQUENT USE IN PREPLT
ISN 0095 IF(NMEP .EQ. 0) GO TO 7000
ISN 0096 DO 7020 IA=1, NMEP
ISN 0097 IF(I .NE. JMASS(IA,1)) GO TO 7020
ISN 0098 WRITE(1) TIME,I,X(I),Y(I),Z(I),XDOT(I),YDOT(I),ZDOT(I),U(I),V(I),
* W(I),XACC(I),YACC(I),ZACC(I),XACF(I),YACF(I),ZACF(I),
* PHI(I),THETA(I),PSI(I),P(I),Q(I),R(I),PDOT(I),QDOT(I),
* RDOT(I),XIMP(I),YIMP(I),ZIMP(I)
ISN 0099 IF(NPRINT .EQ. 0) NMEW = NMEW + 1
ISN 0100 GO TO 7000
ISN 0101
ISN 0102
ISN 0103
ISN 0104
ISN 0105
ISN 0106

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ISN 0107 7020 CONTINUE
ISN 0108 7000 CONTINUE
C
C PRINT NODE POINT DATA IF THERE IS ANY.
C
IF(NMP.EQ.0) GO TO 3099
DO 4000 JJ=1,NMP
  IF(I.NE.INP(JJ)) GO TO 4000
  IF(NMP.LE.0) GO TO 2000
  NPR = NPR+5
  PRINT 701,MNP(JJ),XNP(JJ),YNP(JJ),ZNP(JJ)
  PRINT 800,XONP(JJ),YONP(JJ),ZONP(JJ)
  PRINT 800,UNP(JJ),VNP(JJ),WNP(JJ)
  IF(FCUT.EQ.0.) GO TO 1020
  PRINT 800,XACNP(JJ),YACNP(JJ),ZACNP(JJ),
    1 XACNPF(JJ),YACNPF(JJ),ZACNPF(JJ)
  GO TO 1030
1020 PRINT 800,XACNP(JJ),YACNP(JJ),ZACNP(JJ)
  GO TO 1030
2000 NPR = NPR + 2
  IF(FCUT.EQ.0.0) GO TO 2001
  PRINT 701,MNP(JJ),XACNP(JJ),YACNP(JJ),ZACNP(JJ),
    1 XACNPF(JJ),YACNPF(JJ),ZACNPF(JJ)
  GO TO 1030
2001 PRINT 701,MNP(JJ),XACNP(JJ),YACNP(JJ),ZACNP(JJ)
1030 PRINT 800
C
C WRITE NODE POINT DATA ON UNIT 2 FOR SUBSEQUENT USE IN PREPLT
C
IF(NMP.EQ.0) GO TO 7001
INMP = MNP(JJ)
DO 7030 IA=1, NNEP
  IF(I.NE.JNODE(IA,2).OR. INMP.NE.JNODE(IA,1)) GO TO 7030
  WRITE(2) TIME,I,INMP,XNP(JJ),YNP(JJ),ZNP(JJ),XONP(JJ),
    * YONP(JJ),ZONP(JJ),UNP(JJ),VNP(JJ),WNP(JJ),XACNP(JJ),
    * YACNP(JJ),ZACNP(JJ),XACNPF(JJ),YACNPF(JJ),ZACNPF(JJ),
    * XIMNPF(JJ),YIMNPF(JJ),ZIMNPF(JJ)
  IF(NPRINT.EQ.0) NNEW = NNEW + 1
  GO TO 7001
7030 CONTINUE
7001 CONTINUE
4000 CONTINUE
701 FORMAT(4X,'NODE',I2,1P6E15.5)
700 FORMAT(1H,5HMASS,I2,2X,1P6E15.5)
800 FORMAT(1H,9X,1P6E15.5)
3099 CONTINUE
IF(NIMP.GT.0) PRINT 3215
IF(NIMP.LE.0) PRINT 3216
3215 FORMAT(1X,'MASS IMPULSES(6-SEC)-BASED ON FILTERED ACCELS'//
  1 16X,8HZIMPULSE,7X,8HYIMPULSE,7X,8HZIMPULSE/)
3216 FORMAT (//1X,'NO MASS IMPULSE DATA REQUESTED'//)
IF(NIMP.LE.0) GO TO 3098
DO 3097 I=1,NM

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00001470
00001480
00001490
00001500
00001510
00001520
00001530
00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001740
00001750
00001760
00001770
00001780
00001790
00001800
00001810
00001820
00001830
00001840
00001850
00001860
00001870
00001880
00001890
00001900
00001910
00001920
00001930
00001940
00001950
00001960
00001970
00001980
00001990

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ISN 0159      PRINT 700,I,XIMP(I),YIMP(I),ZIMP(I)
ISN 0160      IF(NNP.EQ.0) GO TO 30%
ISN 0161      DO 30% JJ=1,NNP
ISN 0162      IF(I.NE.INP(JJ)) GO TO 30%
ISN 0163      NPR=NPR+2
ISN 0164      PRINT 701,NNP(JJ),XIMP(JJ),YIMP(JJ),ZIMP(JJ)
ISN 0165      30% CONTINUE
ISN 0166      3097 CONTINUE
ISN 0167      3098 CONTINUE
ISN 0168      PRINT 3202
ISN 0169      3202 FORMAT(1X,'BEAM FORCES' /)
ISN 0170      C
ISN 0171      NSF=OR< 0 NO STRAIN FORCE PRINT
ISN 0172      IF(NSF=0) 3208,3208,3223
ISN 0173      3223 PRINT 3203
ISN 0174      3203 FORMAT(1X,'STRAIN FORCES' /)
ISN 0175      PRINT 830
ISN 0176      830 FORMAT(4X,'I',3X,'J',3X,'M',3X,'N',7X,'FX',11X,'FY',11X,'FZ',11X,
ISN 0177      1 'MX',11X,'MY',10X,'MZ',10X,'MZX',10X,'MZY')
ISN 0178      PRINT 810,(IG(IJ),JG(IJ),MG(IJ),NG(IJ),SUMDF(K,IJ),K=1,4),
ISN 0179      1 SUMDF(5,IJ),SUMDF(6,IJ),SUMDF(6,IJ),SUMDF(6,IJ),I,J=1,NB)
ISN 0180      C
ISN 0181      NTF=OR<0 NO TOTAL FORCE PRINT
ISN 0182      GO TO 3250
ISN 0183      3208 PRINT 850
ISN 0184      850 FORMAT(/ 1X,'NO STRAIN FORCE PRINT')
ISN 0185      3250 IF(NTF=0)3209,3209,3224
ISN 0186      3224 PRINT 3204
ISN 0187      3204 FORMAT(/ 1X,'TOTAL FORCES (STRAIN+DAMPING)' /)
ISN 0188      PRINT 830
ISN 0189      PRINT 810,(IG(IJ),JG(IJ),MG(IJ),NG(IJ),FINT(K,IJ),K=1,4),
ISN 0190      1 FINT(5,IJ),FINT(5,IJ),FINT(6,IJ),FINT(6,IJ),I,J=1,NB)
ISN 0191      GO TO 3251
ISN 0192      3209 PRINT 851
ISN 0193      851 FORMAT(/ 1X,'NO TOTAL FORCE PRINT')
ISN 0194      3251 CONTINUE
ISN 0195      C
ISN 0196      C
ISN 0197      C
ISN 0198      C
ISN 0199      C
ISN 0200      C
ISN 0201      C
ISN 0202      C
ISN 0203      C
ISN 0204      C
ISN 0205      C
ISN 0206      C
ISN 0207      C
ISN 0208      C
ISN 0209      C
ISN 0210      C
ISN 0211      C
ISN 0212      C
ISN 0213      C
ISN 0214      C
ISN 0215      C
ISN 0216      C
ISN 0217      C
ISN 0218      C
ISN 0219      C
ISN 0220      C
ISN 0221      C
ISN 0222      C
ISN 0223      C
ISN 0224      C
ISN 0225      C
ISN 0226      C
ISN 0227      C
ISN 0228      C
ISN 0229      C
ISN 0230      C
ISN 0231      C
ISN 0232      C
ISN 0233      C
ISN 0234      C
ISN 0235      C
ISN 0236      C
ISN 0237      C
ISN 0238      C
ISN 0239      C
ISN 0240      C
ISN 0241      C
ISN 0242      C
ISN 0243      C
ISN 0244      C
ISN 0245      C
ISN 0246      C
ISN 0247      C
ISN 0248      C
ISN 0249      C
ISN 0250      C
ISN 0251      C
ISN 0252      C

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C      NDE=OR<0 NO DEFL.PRINT
3225 PRINT 3205
3205 FORMAT(// 1X,'BEAM RELATIVE DEFLECTIONS AND ROTATIONS AND',
1      ' BEAM EULER ANGLES (INCHES AND DEGREES)')
PRINT 3301
3301 FORMAT(// 5X,'BEAM',16X,'DEFLECTIONS (J-I)',23X,'ROTATIONS (J-I)',
1      16X,'ROTATIONS (J-I)',7X,'EULER ANGLES')
PRINT 3302
3302 FORMAT(// 3X,'I',2X,'J',2X,'M',2X,'N',7X,'X',12X,'Y',12X,'Z',
1      11X,'PHI',9X,'THETA',9X,'PSI',9X,'THETA',9X,'PSI',7X,
2      'THETA',3X,'PSI')
DO 3303 IJ=1,NB
RADEG = 180./3.1415926535
DO 3304 K=1,3
TEMP(K) = RADEG*VEE2(K+3,IJ)
IF(K.GT.2) GO TO 3304
TEMP(K+3) = RADEG*VEEN(K,IJ)
3304 CONTINUE
TEMP(6) = RADEG*THEI(IJ)
TEMP(7) = RADEG*PSII(IJ)
PRINT 3305,IG(IJ),JG(IJ),MG(IJ),NG(IJ),(VEE2(K,IJ),K=1,3),
1      (TEMP(K),K=1,7)
3305 FORMAT(1X,4I3,1P8E13.4,1X,0P2F7.1)
3303 CONTINUE
810 FORMAT (1X,4I4,1P8E13.4)
GO TO 3252
3210 PRINT 852
852 FORMAT(// 1X,'NO BEAM DEFL.PRINT')
3252 CONTINUE
C
C      WRITE BEAM DEFLECTION DATA ON UNIT 4 FOR SUBSEQUENT USE IN PREPLT
C
IF(NBOP .EQ. 0) GO TO 7003
RADEG = 180.0 / 3.1415926535
DO 7008 IJ=1, NB
DO 7050 IA=1, NBOP
IF(IJ .NE. JBND(IA,1)) GO TO 7050
DO 7010 K=1, 3
TEMP(K) = RADEG * VEE2(K+3,IJ)
IF(K .GT. 2) GO TO 7010
TEMP(K+3) = RADEG * VEEN(K,IJ)
7010 CONTINUE
TEMP(6) = RADEG * THEI(IJ)
TEMP(7) = RADEG * PSII(IJ)
IIG = IG(IJ)
IJG = JG(IJ)
IMG = MG(IJ)
ING = NG(IJ)
WRITE(4) TIME,IJ,IIG,IJG,IMG,ING,(VEE2(K,IJ),K=1,3),
*      (TEMP(K),K=1,5)
IF(NPRINT .EQ. 0) NBDW = NBDW + 1
GO TO 7008
7050 CONTINUE

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ISN 0256 7008 CONTINUE
ISN 0257 7003 CONTINUE
ISN 0258 IF(NSPD - 0) 3211,3211,3226
C NSPD=OR<0 NO EXT.SPRING PRINT
ISN 0259 3226 PRINT 3206
ISN 0260 3206 FORMAT(/ / 1X, 'EXTERNAL SPRINGS' /
1 57X, 'GROUND CONTACT POINT LOADS', 13X, 'GROUND CONTACT POINT LOADS',
2 / 59X, 'IN GROUND OR SLOPE AXES', 21X, 'IN MASS AXES' /
3 41X, 'SPRING' / 1X, 'MASS SPRING SPRING', 8X, 'GROUND', 4X,
4 'COMPRESSION', 2X, 'X(+ AFT OR', 4X, 'Y(+ LEFT) Z(+ UP OR NOR-', 6X,
5 'X', 13X, 'Y', 12X, 'Z' / 3X, 'I K M COMPRESSION', 3X,
6 'DEFLECTION', 5X,
7 'LOAD', 6X, 'DOWN SLOPE', 13X, 'MAL TO SLOPE', 2X, '(+ FORWARD)',
8 3X, '(- RIGHT)', 5X, '(- DOWN)' /)
GO TO 3228
ISN 0261 3211 PRINT 853
ISN 0262 853 FORMAT(/ 1X, 'NO EXTERNAL SPRING PRINT')
ISN 0263 GO TO 3227
ISN 0264 3228 DO 3040 IKM=1, NSP
ISN 0265 SCNET = SC(IKM)-DELG(IKM)
ISN 0266 PRINT 820, II(IKM), KK(IKM), MM(IKM), SCNET, DELG(IKM),
ISN 0267 I (FSPRNG(IKM, J), J=1, 7)
ISN 0268 820 FORMAT(1X, 3I3, 1P9E13.5)
ISN 0269 3040 CONTINUE
ISN 0270 3227 CONTINUE
C
C
C WRITE EXTERNAL SPRING DATA ON UNIT 8 FOR SUBSEQUENT USE IN PREPLT
ISN 0271 IF(NSEP .EQ. 0) GO TO 7004
ISN 0272 DO 7060 IA=1, NSEP
ISN 0273 DO 7009 IKM=1, NSP
ISN 0274 IF(II(IKM) .NE. JSPPR(IA, 1) .OR. MM(IKM) .NE. JSPPR(IA, 2))
ISN 0275 * GO TO 7009
* III = III(IKM)
ISN 0277 IKK = KK(IKM)
ISN 0278 IMM = MM(IKM)
ISN 0279 WRITE(8) TIME, III, IKK, IMM, SC(IKM), FSPRNG(IKM, 1)
ISN 0280 IF(NPRINT .EQ. 0) NSEW = NSEW + 1
ISN 0281 7009 CONTINUE
ISN 0282 7060 CONTINUE
ISN 0283 7004 CONTINUE
ISN 0284 IF(NDRI .EQ. 0) GO TO 3076
ISN 0285 PRINT 3207
ISN 0286 3207 FORMAT(/ 1X, 'DRI RESULTS: MASS NO. AND DRI VALUE')
ISN 0287 PRINT 821
ISN 0288 821 FORMAT(1H // 1X, 'MASS', 7X, 'DRI')
ISN 0289 DO 3070 I = 1, NB
ISN 0290 IF(IJPR(I).EQ.0) GO TO 3070
ISN 0291 3065 PRINT 822, JG(I), DRI(I)
ISN 0292 C
ISN 0293 C
ISN 0294 C WRITE BEAM DRI DATA ON UNIT 9 FOR SUBSEQUENT USE IN PREPLT
ISN 0295 C
ISN 0296 IF(NDRP .EQ. 0) GO TO 7005

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ISN 0298      IJG = JG(I)
ISN 0299      DO 7070 IA=1, NORP
ISN 0300      IF(IJG.NE. JORI(IA)) GO TO 7070
ISN 0301      WRITE(9) TIME,IJG,DR(I)
ISN 0302      IF(INPRINT.EQ. 0) NORP = NORP + 1
ISN 0303      GO TO 7005
ISN 0304      7070 CONTINUE
ISN 0305      7005 CONTINUE
ISN 0306      7005 CONTINUE
ISN 0307      3070 CONTINUE
ISN 0308      3076 PRINT 3075,XDOTAP,YDOTAP,ZDOTAP
ISN 0309      3075 FORMAT(/ 1X,'VEHICLE C.G. TRANSLATIONAL VELOCITIES, GROUND AXES, 800003690
ISN 0310      1ASED ON SYSTEM LINEAR MOMENTUM' // 11X,'XDOT',10X,'YDOT',12X,'ZDOT00003700
ISN 0311      2' / 10X,'(+FWD)',7X,'(+RIGHT)',8X,'(+DOWN)' / 4X,IP3E15.5)
ISN 0312      00003720
ISN 0313      00003720
ISN 0314      00003730
ISN 0315      00003740
ISN 0316      00003750
ISN 0317      00003760
ISN 0318      00003770
ISN 0319      00003780
ISN 0320      00003790
ISN 0321      3071 FORMAT(/ 1X,'VOLUME CHANGE DATA' // 48X,'VOLUME LENGTH CHANGES'
ISN 0322      1/ 1X,'VOL. NO.' 5X,'VOL.' 8X,'VOL./VZERO',8X,'DX',13X,'DY',13X,
ISN 0323      2'DZ' /)
ISN 0324      DO 3073 I=1,NVCH
ISN 0325      VOV = VOL(I)/VZERO(I)
ISN 0326      PRINT 3072,I,VOL(I),VOV,(DLVOL(I,J),J=1,3)
ISN 0327      3073 CONTINUE
ISN 0328      3072 FORMAT(1X,16,1P5E15.5)
ISN 0329      822 FORMAT(1H,1X,12,3X,1P5E15.5)
ISN 0330      3074 SURKEI = 0.0
ISN 0331      SURPEI = 0.0
ISN 0332      SURSEI = 0.0
ISN 0333      SURDEI = 0.0
ISN 0334      SURCEI = 0.0
ISN 0335      SURFEI = 0.
ISN 0336      DO 3400 I = 1,NM
ISN 0337      SURPEI = SURPEI+PEI(I)
ISN 0338      SURKEI = SURKEI+KEI(I)
ISN 0339      3400 CONTINUE
ISN 0340      DO 3406 IJ = 1,NB
ISN 0341      SURSEI = SURSEI+SEI(I,IJ)
ISN 0342      SURDEI = SURDEI+DEI(I,IJ)
ISN 0343      3406 CONTINUE
ISN 0344      DO 7200 IJ=1,NB
ISN 0345      IF(ETIME.EQ.0.) GO TO 9003
ISN 0346      PCSE=(SEI(IJ)/SURSEI)*100.
ISN 0347      PCDE=(DEI(IJ)/SURDEI)*100.
ISN 0348      GO TO 9004
ISN 0349      9003 SEI(IJ)=0.
ISN 0350      DEI(IJ)=0.
ISN 0351      PCSE=0.
ISN 0352      PCDE=0.
ISN 0353      00004030
ISN 0354      00004040
ISN 0355      00004050
ISN 0356      00004060
ISN 0357      00004070
ISN 0358      00004080
ISN 0359      00004090
ISN 0360      00004100
ISN 0361      00004110

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ISN 0345 9004 DO 7201 IA=1,NENP
ISN 0346 IF(IJ.NE.JENG(IA,1)) GO TO 7201
ISN 0347 IIG=IG(IJ)
ISN 0348 IJG=JG(IJ)
ISN 0349 IJG=JG(IJ)
ISN 0350 IJG=JG(IJ)
ISN 0351 IJG=JG(IJ)
ISN 0352 WRITE(11) TIME,IJ,IIG,IJG,ING,SEIJ(IJ),PCSE,DEIJ(IJ),PCDE
ISN 0353 IF(NPRINT.EQ.0) NENM=NENM+1
ISN 0354 GO TO 7200
ISN 0355 7201 CONTINUE
ISN 0356 7200 CONTINUE
ISN 0357 IF(INSF.EQ.0) GO TO 3409
ISN 0358 DO 3407 IKM=1,NSP
ISN 0359 SURFEI = SURFEI+CEIKF(IKM)
ISN 0360 SURFEI = SURFEI+CEIK(IKM)
ISN 0361 3407 SURFEI = SURFEI+CEIK(IKM)
ISN 0362 3409 ETOT = SURFEI+SURFEI+SURFEI+SURFEI+SURFEI+SURFEI
ISN 0363 IF(TIME.EQ.0.0) ETOTTO = ETOT
ISN 0364 ETOTR=ETOT/ETOTTO
ISN 0365 XTOLL=NTOLL/100.
ISN 0366 IF((DABS(ETOTR)-1.).LE. XTOLL) GO TO 3770
ISN 0367 IEER=1
ISN 0368 IEETOT=1
ISN 0369 3770 IF(INGSCT.EQ.200) GO TO 3414
ISN 0370 INGSCT = INGSCT+1
ISN 0371 ETIME(INGSCT) = TIME
ISN 0372 DEV(INGSCT) = DEVMAX
ISN 0373 ENGSMT(1,INGSCT) = SURFEI
ISN 0374 ENGSMT(2,INGSCT) = SURFEI
ISN 0375 ENGSMT(3,INGSCT) = SURFEI
ISN 0376 ENGSMT(4,INGSCT) = SURFEI
ISN 0377 ENGSMT(5,INGSCT) = SURFEI
ISN 0378 ENGSMT(6,INGSCT) = SURFEI
ISN 0379 3414 CONTINUE
ISN 0380 3405 FORMAT(// 1X,'ENERGY DISTRIBUTION' //)
ISN 0381 PRINT 3401
ISN 0382 3401 FORMAT(1H0,6X,'TOTAL',7X,'KINETIC',6X,'POTENTIAL',7X,'STRAIN',7X,
ISN 0383 1 'DAMPING',7X,'CRUSHING',6X,'FRICTION' / 6X,'ENERGY',
ISN 0384 2 6(6X,'ENERGY') /)
ISN 0385 PRINT 3402, ETOT,SURFEI,SURFEI,SURFEI,SURFEI,SURFEI,SURFEI
ISN 0386 3402 FORMAT(1X,1P7E14.5)
ISN 0387 PCSE = SURFEI/ETOT
ISN 0388 PCSE = SURFEI/ETOT
ISN 0389 PCSE = SURFEI/ETOT
ISN 0390 PCSE = SURFEI/ETOT
ISN 0391 PCSE = SURFEI/ETOT
ISN 0392 PCSE = SURFEI/ETOT
ISN 0393 PCSE = SURFEI/ETOT
ISN 0394 PCFE = SURFEI/ETOT
ISN 0395 PCFE = SURFEI/ETOT
ISN 0396 PRINT 3403, PCSE,PCSE,PCSE,PCSE,PCSE,PCSE,PCFE
ISN 0397 3403 FORMAT('0 PERCENT OF',2P6F14.3/3X,'TOTAL ENERGY')
ISN 0398 IF(NEED=0) 3601,3601,3229
ISN 0399 C NEED=0. NO INDIVIDUAL ENERGY TERMS PRINTED
ISN 0400 3229 PRINT 3404
ISN 0401 3404 FORMAT(// 6X,'INTERNAL',38X,'EXTERNAL' /

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1 45X, 'BEAM', '41X', 'SPRING' / 7X, 'KINETIC', 9X,
2 'POTENTIAL', 25X, 'STRAIN', 11X, 'DAMPING', 17X, 'CRUSHING', 9X,
3 'FRICTION' / 1X, 'MASS', 2X, 'ENERGY', 5X, 'PCT', 3X, 'ENERGY', 5X,
4 'PCT', 2X, 'I', 2X, 'J', 2X, 'M', 2X, 'N', 3X, 'ENERGY', 5X, 'PCT',
5 3X, 'ENERGY', 5X, 'PCT', 3X, 'I', 1X, 'K', 1X, 'M', 3X, 'ENERGY', 5X, 'PCT',
6 3X, 'ENERGY', 5X, 'PCT' / )
3601 XTOL2=NTOL2/100.
      XTOL3=NTOL3
      MAXEN = MAX0(NM,NB,NSP)
      IF (TIME.EQ.0.0) MAXEN = NM
      DO 3410 IO = 1, MAXEN
      IOPTR = 0
      IF (IO.GT.NM) GO TO 3411
      IOPTR = IOPTR+4
      IF (SUMKEI.NE.0.) GO TO 5000
      PCKE = 0.
      GO TO 5001
5000 PCKE = KEI(IO)/SUMKEI
5001 IF (SUMPEI.NE.0.) GO TO 5002
      PCPE = 0.
      GO TO 5003
5002 PCPE = PEI(IO)/SUMPEI
5003 IF (TIME.EQ.0.0) GO TO 3504
3411 IF (IO.GT.NB) GO TO 3412
      IOPTR = IOPTR+2
      IF (SUMSEI.EQ.0) GO TO 3415
      PCSE = SEI(IO)/SUMSEI
      IF (SUMSEI.GE.0.) GO TO 3700
      IESE=1
      IEER=1
3700 IF (SEI(IO).GE.0. .OR. DABS(SEI(IO)).LE.DABS(SUMSEI*XTOL2))
      1 GO TO 3710
      IEPSE=1
      IEER=1
3710 GO TO 3416
3415 PCSE = 0.
3416 IF (SUMDEI.EQ.0.) GO TO 3417
      PCDE = DEI(IO)/SUMDEI
      IF (SUMDEI.GE.0.) GO TO 3720
      IEDE=1
      IEER=1
3720 IF (DEI(IO).GE.0. .OR. DABS(DEI(IO)).LE.DABS(SUMDEI*XTOL2))
      1 GO TO 3730
      IEPDE=1
      IEER=1
3730 GO TO 3412
3417 PCDE = 0.
3412 IF (IO.GT.NSP) GO TO 3418
      IOPTR = IOPTR+1
      I = II(IO)
      K = KK(IO)
      M = MM(IO)
      CE = CEIK(IO)

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ISM 0401
ISM 0402
ISM 0403
ISM 0404
ISM 0406
ISM 0407
ISM 0408
ISM 0410
ISM 0411
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ISM 0458

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ISN 0459 IF(SUMCEI.NE.0.) GC TO 5010
ISN 0461 PCCE = 0.
ISN 0462 GO TO 5011
ISN 0463 5010 PCCE = CE/SUMCEI
ISN 0464 IF(SUMCEI.GE.0.) GO TO 3740
ISN 0466 IECE=1
ISN 0467 IEER=1
ISN 0468 3740 IF(CEIKF(IO).GE.0. .OR. DABS(CEIKF(IO)).LE.DABS(SUMCEI*XTOL2))
      1 GO TO 5011
      IEPCCE=1
ISN 0470 IEER=1
ISN 0471 5011 FE = CEIKF(IO)
ISN 0472 IF(SUMFEI.NE.0.) GO TO 5012
ISN 0473 PCFE = 0.
ISN 0475 GO TO 3418
ISN 0476 5012 PCFE = FE/SUMFEI
ISN 0477 IF(SUMFEI.GE.0.) GO TO 3750
ISN 0478 IEFE=1
ISN 0480 IEER=1
ISN 0481 3750 IF(CEIKF(IO).GE.0. .OR. DABS(CEIKF(IO)).LE.DABS(SUMFEI*XTOL2))
      1 GO TO 3418
      IEPEFE=1
ISN 0484 IEER=1
ISN 0485 3418 IF(NED=0) 3410,3410,3413
ISN 0486 3413 GO TO (3501,3502,3503,3504,3505,3506,3507), IOPTR
ISN 0487 C*****ONLY CE
ISN 0488 3501 PRINT 3511,I,K,M,CE,PCCE,FE,PCFE
ISN 0489 3511 FORMAT(8X,I4,2I2,1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0490 GO TO 3410
ISN 0491 C*****SE AND DE
ISN 0492 3502 PRINT 3512,IO,IG(IO),JG(IO),MG(IO),NG(IO),SEIJ(IO),PCSE,DEIJ(IO),
ISN 0493 1 PCDE
ISN 0494 3512 FORMAT(39X,5I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0495 C*****SE, DE, CE
ISN 0496 3503 PRINT 3513,IO,IG(IO),JG(IO),MG(IO),NG(IO),
ISN 0497 1 SEIJ(IO),PCSE,DEIJ(IO),PCDE,I,K,M,CE,
ISN 0498 2 PCCE,FE,PCFE
ISN 0499 3513 FORMAT(39X,5I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1,1PE11.3,
ISN 0500 1 2PF6.1,1PE11.3,2PF6.1)
ISN 0501 GO TO 3410
ISN 0502 C*****KE AND PE
ISN 0503 3504 PRINT 3514,IO,KEI(IO),PCKE,PEI(IO),PCPE
ISN 0504 3514 FORMAT(1X,I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0505 GO TO 3410
ISN 0506 C*****KE, PE, CE
ISN 0507 3505 PRINT 3515,IO,KEI(IO),PCKE,PEI(IO),PCPE,I,K,M,CE,PCCE,FE,PCFE
ISN 0508 3515 FORMAT(1X,I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1,1PE11.3,2PF6.1,50X,I4,2I2,
ISN 0509 1 1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0510 GO TO 3410
ISN 0511 C*****KE, PE, SE, DE
ISN 0512 3506 PRINT 3516,IO,KEI(IO),PCKE,PEI(IO),PCPE,IO,IG(IO),JG(IO),
ISN 0513 1 MG(IO),NG(IO),SEIJ(IO),

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ISN 0504      2 PCSE,DEIJ(IO),PCDE
3516 FORMAT(1X,I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1,1X,5I3,
ISN 0505      1 1PE11.3,2PF6.1,1PE11.3,2PF6.1)
GO TO 3410
C*****KE, PE, SE, DE, CE
3507 PRINT 3517,IO,KEI(IO),PCKE,PEI(IO),PCPE,IO,IG(IO),JG(IO),
ISN 0506      1 MG(IO),NG(IO),SEIJ(IO),
2 PCSE,DEIJ(IO),PCDE,I,K,M,CE,PCCE,FE,PCFE
3517 FORMAT(1X,I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1,1X,5I3,1PE11.3,2PF6.1,
ISN 0507      1 1PE11.3,2PF6.1,14,2I2,1PE11.3,2PF6.1,1PE11.3,2PF6.1)
3410 CONTINUE
ISN 0508      PRINT 8000
ISN 0509      8000 FORMAT(/,1X,'DEVIATION OF TOTAL ENERGY OF EACH MASS FROM ',
ISN 0510      1 '100 PERCENT')
PRINT 8002
8002 FORMAT(/,1X,'MASS',2X,'DEVIATION(PERCENT)' /)
DO 8004 I=1,NM
ISN 0511      DEVIAT = XPCT(I)-100.
ISN 0512      IF(DABS(DEVIAT).LE.XTOL3) GO TO 3760
ISN 0513      IEDEV=1
ISN 0514      IEER=1
ISN 0515      3760 IF(XPCT(I).EQ.0) DEVIAT=0.
ISN 0516      PRINT 8006,I,DEVIAT
ISN 0517      8004 CONTINUE
ISN 0518      8006 FORMAT(1X,I3,4X,F12.6)
ISN 0519      3602 GO TO 3230
ISN 0520      3212 PRINT 854
ISN 0521      854 FORMAT (/,1X,'NO ENERGY TERMS PRINTED')
ISN 0522      3230 IF(NS-0) 3213,3213,3231
ISN 0523      C NS EQ OR LESS THAN 0 NO STRESSES ARE PRINTED
ISN 0524      3231 PRINT 3510
ISN 0525      3510 FORMAT(/,1X,'ELEMENT STRESSES')
ISN 0526      PRINT 3519
ISN 0527      3519 FORMAT(/,39X,'RATIO OF CURRENT STRESS / FAILURE STRESS',31X,
ISN 0528      * 9X,'THEORY OF CURRENT' / 8X,'BEAM',12X,'MAXIMUM SHEAR STRESS THEORY',
ISN 0529      * 5X,'BUCK.' /' / 2X,'I',2X,'J',2X,'M',2X,'N',5X,'TOP',5X,
ISN 0530      * 'BOTTOM',6X,'LEFT',5X,'RIGHT',8X,'TOP',5X,'BOTTOM',6X,'LEFT',5X,
ISN 0531      * 'RIGHT',7X,'COMPR. TENSILE CR.BUCK.' / 104X,'STRESS'
ISN 0532      * ,6X,'LOAD' /)
DO 3520 IJ=1,NB
ISN 0533      I = IG(IJ)
ISN 0534      J = JG(IJ)
ISN 0535      M = MG(IJ)
ISN 0536      N = NG(IJ)
ISN 0537      IF(SBUCKR(IJ).GT. 0.0) GO TO 3521
ISN 0538      BLOAD = DABS(SBUCKR(IJ))
ISN 0539      IF(AA(IJ).EQ. 0.0) GO TO 3525
ISN 0540      SAXL = BLOAD * PCR(IJ) / (AA(IJ) * SCOMP(MC(IJ)))
ISN 0541      GO TO 3526
ISN 0542      3525 SAXL = 0.0
ISN 0543      3526 PRINT 3518, IJ,I,J,M,N,(FRS(IJ,IS),IS=1,4),(FRD(IJ,IT),IT=1,4),
ISN 0544      3525 SAXL = 0.0
ISN 0545      3526 PRINT 3518, IJ,I,J,M,N,(FRS(IJ,IS),IS=1,4),(FRD(IJ,IT),IT=1,4),
ISN 0546

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ISN 0547      *      SAXL,BLOAD
ISN 0548      3516 FORMAT(1X,5I3,1X,1P4E10.3,2X,4E10.3,2X,E10.3,10X,E10.3)
ISN 0549      GO TO 3520
ISN 0550      3521 CONTINUE
ISN 0551      BLOAD = 0.0
ISN 0552      IF(AA(IJ)).EQ. 0.0) GO TO 3522
ISN 0553      SAXL = SBUCKR(IJ) * PCR(IJ) / (STENS(MC(IJ)) * AA(IJ))
ISN 0554      GO TO 3523
ISN 0555      3522 SBUCK = 0.0
ISN 0556      3523 PRINT 3524, IJ,I,J,M,N,(FRS(IJ,IS),IS=1,4),(FRD(IJ,IT),IT=1,4),
      *      SAXL
ISN 0557      3524 FORMAT(1X,5I3,1X,1P4E10.3,2X,4E10.3,12X,E10.3)
ISN 0558      3520 CONTINUE
ISN 0559      GO TO 3232
ISN 0560      3213 PRINT 855
ISN 0561      855 FORMAT(/ 1X,'NO STRESS PRINT')
C
C      WRITE BEAM ELEMENT STRESS DATA ON UNIT 13 FOR SUBSEQUENT USE IN
C      PREPLT
C
ISN 0562      3232 IF(INSTP .EQ. 0) GO TO 7100
ISN 0563      DO 7110 IJ=1, NB
ISN 0564      DO 7080 IA=1, NSTP
ISN 0565      IF(IJ .NE. JBMS(IA,1)) GO TO 7080
ISN 0566      I = IG(IJ)
ISN 0567      J = JG(IJ)
ISN 0568      M = MG(IJ)
ISN 0569      N = NG(IJ)
ISN 0570      BLOAD = SBUCKR(IJ)
ISN 0571      IF(BLOAD .GT. 0.0) BLOAD = 0.0
ISN 0572      IF(AA(IJ)).EQ. 0.0) GO TO 3527
ISN 0573      IF(SBUCKR(IJ)).GT. 0.0) GO TO 3528
ISN 0574      SAXL = SBUCKR(IJ) * PCR(IJ) / (AA(IJ) * SCOMP(MC(IJ)))
ISN 0575      GO TO 3529
ISN 0576      3528 SAXL = SBUCKR(IJ) * PCR(IJ) / (AA(IJ) * STENS(MC(IJ)))
ISN 0577      GO TO 3529
ISN 0578      3527 SAXL = 0.0
ISN 0579      3529 CONTINUE
ISN 0580      *      WRITE(13) TIME,IJ,I,J,M,N,(FRS(IJ,IS),IS=1,4),
ISN 0581      (FRD(IJ,IT),IT=1,4),SAXL,BLOAD
ISN 0582      IF(INPRINT .EQ. 0) NSTW = NSTW + 1
ISN 0583      GO TO 7110
ISN 0584      7080 CONTINUE
ISN 0585      7110 CONTINUE
ISN 0586      7100 CONTINUE
ISN 0587      IF(INPLT.EQ.0) GO TO 100
ISN 0588      IPFCT = IPFCT + 1
ISN 0589      IF(IPFCT .EQ. 0 .OR. IPFCT .EQ. NPFACT) GO TO 170
ISN 0590      GO TO 100
ISN 0591      170 CONTINUE
ISN 0592      IPFCT = 0
ISN 0593      DO 110 IP=1,NPLT
ISN 0594      110 NMPTS(IP)
ISN 0595      110 NMPTS(IP)
ISN 0596      110 NMPTS(IP)
ISN 0597      110 NMPTS(IP)
ISN 0598      110 NMPTS(IP)
ISN 0599      110 NMPTS(IP)
ISN 0600      110 NMPTS(IP)
ISN 0601      110 NMPTS(IP)

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ISN 0602      DO 160 IJ=1,NJ
ISN 0603      DO 120 IM=1,NM
ISN 0604      IF(IM .NE. MMUM(IJ,IP)) GO TO 120
ISN 0605      J=ITPL(IP)
ISN 0606      GO TO (130,140,150),J
ISN 0607      130 A(IJ)=-X(IM)
ISN 0608      B(IJ)=Y(IM)
ISN 0609      IFIRST = 1
ISN 0610      ILAST = 5
ISN 0611      GO TO 160
ISN 0612      140 A(IJ)=-X(IM)
ISN 0613      B(IJ) = -Z(IM)
ISN 0614      IFIRST = 6
ISN 0615      ILAST = 10
ISN 0616      GO TO 160
ISN 0617      150 A(IJ)=Y(IM)
ISN 0618      B(IJ) = -Z(IM)
ISN 0619      IFIRST = 11
ISN 0620      ILAST = 15
ISN 0621      GO TO 160
ISN 0622      160 CONTINUE
ISN 0623      120 CONTINUE
ISN 0624      160 CONTINUE
ISN 0625      PRINT 7120, (IPLN(IJ), IJ=IFIRST, ILAST)
ISN 0626      7120 FORMAT(1H1,51X,'MASS POSITION PLOT PLANE ** ',5A4 / 20X,
* 'NOTE *** A MODIFIED RIGHT HAND GROUND COORDINATE',
* ' SYSTEM HAS BEEN USED FOR THIS PLOT ***' / )
*
ISN 0627      PRINT 7130
ISN 0628      7130 FORMAT(4(7X,'MASS HORIZ VERTICAL') /
* 1 4(8X,'NO AXIS AXIS ' ) / )
ISN 0629      PRINT 7140, (MMUM(IJ,IP),A(IJ),B(IJ),IJ=1,NJ)
ISN 0630      7140 FORMAT(4(8X,I2,F10.2,F10.2))
ISN 0631      PRINT 7150
ISN 0632      7150 FORMAT(1X)
ISN 0633      IF(NJ .LE. 12) GO TO 180
ISN 0634      PRINT 7120, IPLN(ITPL(IP))
ISN 0635      180 CALL PAPLOT(A,B,XSCALE(IP),YSCALE(IP),MMUM(1,IP),NMPTS(IP),
* ISCALE(IP))
ISN 0636      110 CONTINUE
ISN 0637      PRINT 7160
ISN 0638      7160 FORMAT(1H1,1X)
ISN 0639      100 CONTINUE
ISN 0640      RETURN
ISN 0641      END
ISN 0642

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COMPILER	OPTIONS	- NAME=	MAIN,OPT=02,LINECNT=55,SIZE=0600K, SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NODEIT,ZD,XREF		
C	DATA SET D2334RC	AT LEVEL 003	AS OF 06/25/79	00000010	
C	DATA SET D2332NRC	AT LEVEL 004	AS OF 12/01/77	00000020	
C	DATA SET D2332NRC	AT LEVEL 002	AS OF 11/04/77	00000030	
C	DATA SET D2332SRC	AT LEVEL 001	AS OF 07/29/77	00000040	
	SUBROUTINE RC			00000050	
C	IMPLICIT REAL*8 (A-H,O-Z)			00000060	
	REAL*8 KUN			00000070	
	REAL*4 CLTEST			00000080	
	INTEGER*4 PY(150),PZ(150),PYJ(150),PZJ(150)			00000090	
	INTEGER*4 TITLE(40)			00000100	
	INTEGER*2 N1,NN			00000110	
	INTEGER*2 INBUFF			00000120	
	INTEGER*2 IJPR,IG,JG			00000130	
	INTEGER*2 MG(150),NG(150),INP(50),MNP(50)			00000140	
	DIMENSION ADP(3,3)			00000150	
	DIMENSION XK(6,6,150),YZMTN(150)			00000160	
	DIMENSION RX(50),RY(50),RZ(50),XNPDP(50),YNPDP(50),ZNPDP(50)			00000170	
	DIMENSION XNP(50),YNP(50),ZNP(50),XONP(50),YONP(50),ZONP(50)			00000180	
	DIMENSION YNP(50),VNP(50),MNP(50),XACCN(50),YACCN(50),ZACCN(50)			00000190	
	DIMENSION INDRII(80)			00000200	
	COMMON/DEINP/ AA(150),E(150),YI(150),ZZ(150),XIQ(150),			00000210	
	1 XILB(150),Z1(150),Z2(150),MC(150),XJ(150),SF26(150),SF35(150),			00000220	
	2 SF26J(150),SF35J(150),PY,PZ,PYJ,PZJ,NSC,NPIN			00000230	
	COMMON/CFIC/ SINBET,COSBET,ABETA(9)			00000240	
	COMMON/DRINCP/ STENS(20),SCOMP(20),SHEAR(20),EE(20),GG(20),			00000250	
	1 FINIT(6,150),VOL(5),VZERO(5),KHATR(6,4),NVCH,INBUFF(5,8)			00000260	
	COMMON/INIC/ XDPI(80),ZDP(80),PHIDP(80),PSIDP(80),			00000270	
	1 THEDPI(80),PPR,QPR,RPR,XGIN,ZGIN,PHIPR,PSIPR,THEPR,			00000280	
	2 XGDOT,YGDOT,ZGDOT			00000290	
	COMMON/INIDCP/ YDP(80)			00000300	
	COMMON/INCFIC/ BETA			00000310	
	COMMON/MCFIII/ SYMFLG			00000320	
	COMMON/NP00I2/ HG,NG,INP,MNP			00000330	
	COMMON/NP00I4/ NNP			00000340	
	COMMON/NP00R8/ RX,RY,RZ			00000350	
	COMMON/NP01R8/ XNP,YNP,ZNP,UNP,VNP,MNP,XONP,YONP,ZONP,			00000360	
	1 XACCNP,YACCNP,ZACCNP,SBUCKR(150),PCR(150)			00000370	
	COMMON/NP02R8/ XNPDP,YNPDP,ZNPDP			00000380	
	COMMON/DEIC/ WTOT,CLTEST(150)			00000390	
	COMMON/COHALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),			00000400	
ISN 0002					
ISN 0003					
ISN 0004					
ISN 0005					
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ISN 0040					


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1 Y(01),Z(01),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),
2 YI(00),ZI(00),XVI(00),XZI(00),YZI(00),AII(9),BIJ(720),
3 DRI(150),OAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80),
4 POOT(80),QOOT(80),ROOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),
5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
6 XACC(80),YACC(80),ZACC(80),AIDOT(9),
7 PHIIJ(150),THEIJ(150),PSIIJ(150),SUMDF(6,150),TITLE,
8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9 OPTIN(81),DQINI(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),
A CEIKF(40),
B SBAP(40),KUNI(40),MAXNM,MAXIGS,MAXTBL,
C NM,MB,I,J,IG(150),JG(150),
D NI(900),NN(40),IJPR(150)
COMMON/TPIC/ NIC
EQUVALENCE (XK(1),XK3(1,1,1))
SINI(X) = DSINI(X)
COS(X) = DCOS(X)
SQRT(X) = DSQRT(X)
ARSIN(X) = DARSIN(X)
ATAN2(Y,X) = DATAN2(Y,X)
AMINI(X,Y) = DMINI(X,Y)
WTOT = 0.0
PI = 3.1415926535897932400
PI2 = PI/2.
PIN = -PI
PI2N = -PI2
BETAR = BETAPI/180.
SINBET = DSIN(BETAR)
COSBET = DCOS(BETAR)
ABETA(1) = COSBET
ABETA(2) = 0.
ABETA(3) = -SINBET
ABETA(4) = 0.
ABETA(5) = 1.
ABETA(6) = 0.
ABETA(7) = SINBET
ABETA(8) = 0.
ABETA(9) = COSBET
KMATR(1,1) = 3
KMATR(1,2) = 4
KMATR(1,3) = 7
KMATR(1,4) = 8
KMATR(2,1) = 1
KMATR(2,2) = 2
KMATR(2,3) = 5
KMATR(2,4) = 6
KMATR(3,1) = 1
KMATR(3,2) = 3
KMATR(3,3) = 5
KMATR(3,4) = 7
KMATR(4,1) = 2
KMATR(4,2) = 4
KMATR(4,3) = 6

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C
ISN 0122 IF(MNP.EQ.0) GO TO 2051
ISN 0124 DO 3000 JJ=1,MNP
ISN 0125 I = INP(JJ)
ISN 0126 T1 = XDP(I)-XNDP(JJ)
ISN 0127 T2 = YDP(I)-YNDP(JJ)
ISN 0128 T3 = ZDP(I)-ZNDP(JJ)

C
ISN 0129 CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0130 RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
ISN 0131 RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
ISN 0132 RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
ISN 0133 3000 CONTINUE
ISN 0134 2051 CONTINUE

C
ISN 0135 2014 PRINT 2014
ISN 0136 2014 FORMAT(/ 1X, 'VEHICLE INERTIAS (IN-LB-SEC**2)')
ISN 0137 XIG = 0
ISN 0138 YIG = 0
ISN 0139 ZIG = 0
ISN 0140 DO 2015 I=1,MH
ISN 0141 IF(IMDRI(I).NE.0) GO TO 2015
ISN 0142 XARM = XDP(I) - XGDP
ISN 0143 YARM = YDP(I) - YGDP
ISN 0144 ZARM = ZDP(I) - ZGDP
ISN 0145 GOODY1 = WGT(I)*(YARM*YARM+ZARM*ZARM)/386.
ISN 0146 GOODY2 = WGT(I)*(XARM*XARM+ZARM*ZARM)/386.
ISN 0147 GOODY3 = WGT(I)*(XARM*XARM+YARM*YARM)/386.
ISN 0148 XIG = XIG+XI(I)+GOODY1
ISN 0149 YIG = YIG+YI(I)+GOODY2
ISN 0150 ZIG = ZIG+ZI(I)+GOODY3
ISN 0151 IF(SYNFLG.NE.1.OR.YDP(I).EQ.0.) GO TO 2015
ISN 0152 XIG = XIG+XI(I)+GOODY1
ISN 0153 YIG = YIG+YI(I)+GOODY2
ISN 0154 ZIG = ZIG+ZI(I)+GOODY3
ISN 0155 2015 CONTINUE
ISN 0156 2016 PRINT 2016,XIG,YIG,ZIG
ISN 0157 2016 FORMAT(1X,'I(XX) = ',1PE11.5 / 1X,'I(YY) = ',1PE11.5 / 1X,
ISN 0159 'I(ZZ) = ',1PE11.5)

C
ISN 0160 DO 2022 IJ=1,NB
ISN 0161 I = IG(IJ)
ISN 0162 J = JG(IJ)
ISN 0163 M = MG(IJ)
ISN 0164 N = NG(IJ)
ISN 0165 IF(M.EQ.0) GO TO 5020
ISN 0166 DO 5010 JI=1,MNP
ISN 0167 IF(I.EQ.INP(JI).AND.M.EQ.MNP(JI)) GO TO 5020
ISN 0168 5010 CONTINUE
ISN 0169 5020 IF(IN.EQ.0) GO TO 5030
ISN 0170 DO 5040 JJ=1,MNP
ISN 0171 IF(J.EQ.INP(JJ).AND.N.EQ.MNP(JJ)) GO TO 5030
ISN 0172
ISN 0173
ISN 0174

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ISN 0176      5040 CONTINUE
C
C   THE FOLLOWING CODE GETS CLTEST(IJ), WHICH IS 1 IF BEAM IJ
C   LIES ENTIRELY IN THE CENTER PLANE OF THE AIRPLANE. THIS
C   IS USED IN DERIV FOR A NUMBER OF TESTS.
C
ISN 0177      5030 CLTEST(IJ) = 0.
ISN 0178      IF(SYNFLG.NE.1.) GO TO 2022
ISN 0180      IF(YDP(IJ).NE.0.OR.YDP(J).NE.0.) GO TO 2022
C
C   BOTH MASSES ON CENTERLINE.
C
ISN 0182      IF(M.EQ.0.AND.N.EQ.0) GO TO 5000
ISN 0184      IF(M.EQ.0) GO TO 5001
ISN 0186      IF(N.EQ.0) GO TO 5002
ISN 0188      IF(YNFDPI(JJ).EQ.0.AND.YNFDPI(JJ).EQ.0.) GO TO 5000
ISN 0190      GO TO 2022
ISN 0191      5001 IF(YNFDPI(JJ).EQ.0.) GO TO 5000
ISN 0193      GO TO 2022
ISN 0194      5002 IF(YNFDPI(JJ).EQ.0.) GO TO 5000
ISN 0196      GO TO 2022
ISN 0197      5000 CLTEST(IJ) = 1.
ISN 0198      2022 CONTINUE
ISN 0199      IF (NIC.LE. 0) RETURN
C
C   COMPUTE PREL. UNCOUPLED LOADS AND DEFLECTIONS
C
ISN 0201      PRINT 5011
ISN 0202      5011 FORMAT(// 1X, 'BEAM LOADS')
ISN 0203      5012 PRINT 5012
ISN 0204      5012 FORMAT(// 6X, 'BEAM', 19X, 'AXIAL LOAD', 19X, 'SHEAR FORCE', 22X,
*           'MOMENT', 20X, 'BEAM' / 2X, 'I J I J M N', 3X, 'BUCKLING',
*           4X, 'TENSION COMPRESSION LATERAL(Y) VERTICAL(Z)', 3X,
*           'ROLL(X)', 5X, 'PITCH(Y)', 5X, 'YAW(Z)', 3X, 'I J I J M N' /
DO 2400 IJ=1,NB
ISN 0205      IF(IY(IJ) .LE. ZZ(IJ)) GO TO 5013
ISN 0206      YZHINI(IJ)=ZZ(IJ)
ISN 0208      GO TO 5014
ISN 0209      YZHIN = MIN.CROSS SECTION AREA INERTIA
C
C   5013 YZHINI(IJ)=YY(IJ)
C   CALC. FORCES AND MOMENTS
C
ISN 0210      5014 PCRFYF=4.*PI*PI*E(IJ)*YY(IJ)/(XLB(IJ)**2)
ISN 0211      PCRFZ=4.*PI*PI*E(IJ)*ZZ(IJ)/(XLB(IJ)**2)
ISN 0212      PTENS=STENS(MC(IJ))*AA(IJ)
ISN 0213      PCOMP=SCOMP(MC(IJ))*AA(IJ)
ISN 0214      SHEAR FORCES
ISN 0215      FY=.67*SHEAR(MC(IJ))*AA(IJ)
ISN 0216      FZ=FY
C
C   MOMENTS
ISN 0217      IF(XIQ(IJ).NE.0.) GO TO 400
ISN 0219      THOMX = 0.
ISN 0220      GO TO 410

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ISN 0221      400 THORX=SHEAR(MC(IJ))/XIG(IJ)
ISN 0222      410 SYIELD = ANINI(SCOMP(MC(IJ)),STENS(MC(IJ)))
ISN 0223      IF(Z1(IJ),NE.0.) GO TO 420
ISN 0225      BENDMY = 0.
ISN 0226      GO TO 430
ISN 0227      420 BENDMY=SYIELD*Y(IJ)/Z1(IJ)
ISN 0228      430 IF(Z2(IJ),NE.0.) GO TO 440
ISN 0230      BENDMZ = 0.
ISN 0231      GO TO 450
ISN 0232      440 BENDMZ=SYIELD*Z(IJ)/Z2(IJ)
C
C      CHECK BEAM END CONDITIONS.
C
ISN 0233      450 IF(PY(IJ),EQ.0.AND.PYJ(IJ),EQ.0) GO TO 100
ISN 0235      IF(PY(IJ),EQ.0.OR.PYJ(IJ),EQ.0) GO TO 110
C      PINNED-PINNED.
ISN 0237      PCRY = PCRFY/4.
ISN 0238      BENDMY = 0.
ISN 0239      FZ = 0.
ISN 0240      GO TO 120
C      FIXED-PINNED.
ISN 0241      110 PCRY = PCRFY/2.
ISN 0242      GO TO 120
C      FIXED-FIXED
ISN 0243      100 PCRY = PCRFY
ISN 0244      120 IF(PZ(IJ),EQ.0.AND.PZJ(IJ),EQ.0) GO TO 200
ISN 0246      IF(PZ(IJ),EQ.0.OR.PZJ(IJ),EQ.0) GO TO 210
C      PINNED-PINNED.
ISN 0248      PCRZ = PCRFZ/4.
ISN 0249      BENDMZ = 0.
ISN 0250      FY = 0.
ISN 0251      GO TO 220
C      FIXED-PINNED.
ISN 0252      210 PCRZ = PCRFZ/2.
ISN 0253      GO TO 220
C      FIXED-FIXED
ISN 0254      200 PCRZ = PCRFZ
ISN 0255      220 PCR(IJ) = PCRZ
ISN 0256      IF(PCRY,LT.PCRZ) PCR(IJ)=PCRY
ISN 0258      5018 PRINT 5015,(IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),PCR(IJ),PTENS,
        1 PCOMP,FY,FZ,THORX,BENDMY,BENDMZ,IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ))
ISN 0259      5015 FORMAT(1X,5I3,1P8E12.4,5I3)
ISN 0260      2400 CONTINUE
ISN 0261      5050 PRINT 5050
ISN 0262      PRINT 5051
ISN 0263      5051 FORMAT(/ / 1X, 'BEAM DEFLECTIONS' )
ISN 0264      *
        * 'ROTATION ABOUT' / 2X, 'I J M N', 2X, 'BUCKLING', 4X,
        * 'TENSION COMPRESSION F(Y)', 7X, 'F(Z)', 7X, 'BM(Z)', 6X,
        * 'BM(Y)', 5X, 'X-AXIS Y-AXIS Z-AXIS' / )
C
C      CALC. DEFLECTIONS
C
00002530
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00002580
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ISN 0265      C      AXIAL DEFLECTIONS
ISN 0266      DO 2500 IJ=1,NB
ISN 0267      SYIELD = AMIN1(SCOMP(MC(IJ)),STENS(MC(IJ)))
ISN 0268      IF(XK3(1,1,IJ).EQ.0.0) GO TO 5330
ISN 0269      XDEFB=PCR(IJ)/XK3(1,1,IJ)
ISN 0270      XDEFT=STENS(MC(IJ))*AA(IJ)/XK3(1,1,IJ)
ISN 0271      XDEFC=SCOMP(MC(IJ))*AA(IJ)/XK3(1,1,IJ)
ISN 0272      GO TO 5340
ISN 0273      5330 XDEFB = 0.0
ISN 0274      XDEFT = 0.0
ISN 0275      XDEFC = 0.0
ISN 0276      5340 CONTINUE
ISN 0277      C      DUE TO SHEAR FORCES
ISN 0278      IF(XK3(2,2,IJ).EQ.0.0) GO TO 5350
ISN 0279      YDSF=.67*SHEAR(MC(IJ))*AA(IJ)/XK3(2,2,IJ)
ISN 0280      GO TO 5360
ISN 0281      5350 YDSF = 0.0
ISN 0282      5360 IF(XK3(3,3,IJ).EQ.0.0) GO TO 5370
ISN 0283      ZDSF=.67*SHEAR(MC(IJ))*AA(IJ)/XK3(3,3,IJ)
ISN 0284      GO TO 5380
ISN 0285      5370 ZDSF = 0.0
ISN 0286      5380 CONTINUE
ISN 0287      C      DEFL. DUE TO BEND.FORCE ((K35/DEL)*FORCE)
ISN 0288      IF(XK3(2,2,IJ).EQ.0.0.OR.Z2(IJ).EQ.0.0) GO TO 5390
ISN 0289      YDMZ=4.*SYIELD*Z2(IJ)/(Z2(IJ)*XLB(IJ)*XK3(2,2,IJ))
ISN 0290      GO TO 5400
ISN 0291      5390 YDMZ = 0.0
ISN 0292      5400 IF(XK3(3,3,IJ).EQ.0.0.OR.Z1(IJ).EQ.0.0) GO TO 5410
ISN 0293      ZDMY=4.*SYIELD*Y1(IJ)/(Z1(IJ)*XLB(IJ)*XK3(3,3,IJ))
ISN 0294      GO TO 5420
ISN 0295      5410 ZDMY = 0.0
ISN 0296      5420 CONTINUE
ISN 0297      C      TORSIONAL ROTATION
ISN 0298      IF(XK3(4,4,IJ).NE.0.0.AND.XIQ(IJ).NE.0.0) GO TO 5317
ISN 0299      ROTX=0.0
ISN 0300      GO TO 5316
ISN 0301      5317 ROTX=SHEAR(MC(IJ))/XIQ(IJ)/XK3(4,4,IJ)
ISN 0302      C      BEND. ROTATION ((K33/DEL)*MOM.)
ISN 0303      5318 IF(XK3(5,5,IJ).EQ.0.0.OR.Z1(IJ).EQ.0.0) GO TO 5430
ISN 0304      ROTY=4.*SYIELD*Y1(IJ)/(Z1(IJ)*XK3(5,5,IJ))
ISN 0305      GO TO 5440
ISN 0306      5430 ROTY = 0.0
ISN 0307      5440 IF(XK3(6,6,IJ).EQ.0.0.OR.Z2(IJ).EQ.0.0) GO TO 5450
ISN 0308      ROTZ=4.*SYIELD*Z2(IJ)/(Z2(IJ)*XK3(6,6,IJ))
ISN 0309      GO TO 5460
ISN 0310      5450 ROTZ = 0.0
ISN 0311      5460 CONTINUE
ISN 0312      5316 PRINT 5319, (IJ,IG(IJ),J6(IJ),M6(IJ),NG(IJ),XDEFB,XDEFT,XDEFC,
ISN 0313      1 YDSF,ZDSF,YDMZ,ZDMY,ROTX,ROTY,ROTZ)
ISN 0314      5319 FORMAT(1X,5I3,1P10E11.3)
ISN 0315      2500 CONTINUE
ISN 0316      RETURN
ISN 0317
ISN 0318

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END

ISM 0319

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINCNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NODEDIT,ID,XREF
C DATA SET D2334PSIN AT LEVEL 006 AS OF 06/25/79
C DATA SET D2332VRI AT LEVEL 005 AS OF 01/27/78
C SUBROUTINE RSINI(IMODEL,ICASE,INSEC)
C
C IMPLICIT REAL*8(A-H,O-Z)
REAL*8 KUN, MODEL, IMODEL, KEI, KETOTL
REAL*4 XK5, XKI, XKR, ENGSYS
INTEGER*4 TITLE(40),UNIT,CASE,HEADER(24),BPL(100,3)
INTEGER*2 FL26I(150),FL26J(150),FL35I(150),FL35J(150)
INTEGER*2 NLSFLG,XUGB,NLI,IUPR,NLI,INBUFF,IG,JG,I8S,JBS
COMMON/DEIN/ XI*BAR,XF*BAR,YN*BAR,ZP*BAR,VLENZ(5,3),
1 FXAXI(900),HEX(80),HEY(80),HEZI(80),ALIFT(80),VNAXI(900),VNAXNI(900),
2 FXAXNI(900),XKSI(2700),XKI(2700),XKR(2700),NLSFLG(900),CHUG(180),
3 MVP
COMMON/DEPR/ ZOOTAP,ZOOTAP,ZOOTOAP,DLVOL(5,3),FRD(150,4),
1 FR5(150,4),SUMDFI(6,150),FINTI(6,150),VEEN(2,150)
COMMON/ENERGY/ XPCTI(80),XFETDI(6,150),XETOTOI(80),XSE(80),XDEI(80),
1 XCEI(80),XFEI(80),KEI(80),PEI(80),XETOTL,KETOTL,
2 PETOTL,SETOTL,DETOTL,CETOTL,FETOTL
COMMON/MADE/ KF126(150),KF135(150),FL26I,FL26J,FL35I,FL35J,
1 TPL(100),BPL,KPL
COMMON/DINICP/ STENS(20),SOMPI(20),SHEAR(20),EE(20),GG(20),
1 FINTI(6,150),VOLL(5),VZEROU(5),KMATR(6,4),NVCH,INBUFF(5,8)
COMMON/INPR/ NDRI,NSP
COMMON
XX(80),XY(80),XZ(80),XL(80),XM(80),
1 XNI(80),DPX(80),DPY(80),DPZ(80),DPL(80),DPH(80),DPH(80),PINI(80),
2 QIN(80),PINI(80),XI1(80),XI2(80),XI3(80),XI4(80),XI5(80),XI6(80),
5 DELI(80),POLDI(80),GOLDI(80),ROLDI(80),UOLDI(80),VOLDI(80),
6 WOLDI(80),XOLDI(80),YOLDI(80),ZOLDI(80),PINO(80),QINO(80),RINO(80),
7 PHOLD(80),THEOLD(80),PSIOLD(80),
8 XACFDI(80),YACFDI(80),XAFOLD(80),YAFOLD(80),ZAFOLDI(80),
9 XNPFDI(50),YNPFDI(50),ZNPFDI(50),XANPFO(50),YANPFO(50),ZANPFO(50),
A TKR(200),TPEN(80),IDTHALF,
B KPBEAM(4,200),KPFLAG(900),IPEN(80),KPEN,KRCONT
COMMON/NPO014/ NHP
COMMON/NPO1R8/ XNP(50),YNP(50),ZNP(50),UNPI(50),VNPI(50),MNP(50),
1 XDNP(50),YDNP(50),ZDNP(50),XACCNP(50),YACCNP(50),ZACCNP(50),
2 SBUCKR(150),PCRI(150)
COMMON/PRIA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50),
1 ZACNPF(50),
2

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00000410 1 ZACNPF(50),XIMP(80),YIMP(80),ZIMP(80),XIMPNP(50),YIMNP(50),
00000420 2 ZIMPNP(50),XIMPOL(80),YIMPOL(80),ZIMPOL(80),XIMPPL(50),
00000430 3 YIMPPL(50),ZIMPPL(50)
COMMON/OLEO/EOLEO(20),FAOI(20),EXPOLE(20),YMAXI(20),
00000440 1 YOLEOI(20),BOLEOI(20),BROLEO(20),XKEXT(20),XKCOMP(20),FCOUL(20),
00000450 2 ALPHAP,ISOLED(20),JGOLEOI(20),MGOLEOI(20),NGOLEOI(20),NOLEO
COMMON/COMALL/ CIG,150),PI(60),R(80),U(80),W(80),X(81),
00000470 1 Y(61),Z(61),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),
00000480 2 YI(61),ZI(80),XYI(60),XZI(80),YZI(80),AIJ(9),BIJ(720),
00000490 3 DRI(150),DAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80),
00000500 4 POOTI(80),GDOT(80),RDOT(80),UDOT(80),VODT(80),NDOT(80),XDOT(80),
00000510 5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
00000520 6 XACCI(80),YACC(80),ZACCI(80),AIDOT(9),
00000530 7 PHUIJ(150),THEIJ(150),SEIIJ(150),SUMPD(6,150),TITLE,
00000540 8 XLARI(40),FSPAR(40),VEEDI(3,3),DXI(81),DY(81),DZ(81),
00000550 9 DPINI(81),DQINI(81),DRINI(81),SEIJI(150),DEIJI(150),CEIK(40),
00000560 A CEIK(40),
00000570 B SBARI(40),KLUM(40),MAXNM,MAXIGS,MAXTBL,
00000580 C NM,NB,I-J,I6(150),J6(150),
00000590 D NJ(900),NM(40),IJPRI(150)
COMMON/CFFR/FSPRG(40,8),DELGI(40)
00000600 1 KKSPI(5,200),EXSPI(5,200),TSP(200),STEMP1(40),STEMP2(40),
00000610 2 STEMP3(40),STEMP4(40),STEMP5(40),KKONT
COMMON/MAPR/ ETOTTO,ENGSHY(6,200),INGSGT
00000620 1 NYBM,IJPRTI(14),IPHDP(80),NFBNH
COMMON/COMHIA/ND,NVBMN,NFBMN,NFI,NKM,NLB,NPH,NMTL,NPTS(50),
00000630 1 NYBM,IJPRTI(14),IPHDP(80),NFBNH
COMMON /MAX/ IRUPSW(150),IPENSM(80),VEEBAR(900),ZINIT(80),
00000640 DATA UNIT/21/
00000650 1 ...FIND DESIRED CASE...
C
C
00000660 10 CALL OPININHEADER,24,UNIT,IER)
IF (IER .NE. 0) STOP
00000670 CALL DATINI MODEL ,2,UNIT,IER)
00000680 CALL DATINI CASE ,8HCASE ,1,UNIT,IER)
00000690 CALL DATINI INSEC ,8HMSEC ,1,UNIT,IER)
00000700 IF ( IMODEL.EQ.IMODEL ) .AND. (CASE.EQ.ICASE)
00000710 1 CALL CLSINI(UNIT,IER)
00000720 IF (IER .NE. 0) STOP
00000730 GO TO 10
C
C
00000740 ...RETRIEVE VARIABLES...
C
C
00000750 20 CALL DATINI TIME ,8HTIME ,2,UNIT,IER)
C
C
00000760 ....INDICES....
C
C
00000770 CALL DATINI KRCONT ,8HKRCNT ,1,UNIT,IER)
00000780 CALL DATINI KPEN ,8HKPEN ,1,UNIT,IER)
00000790 CALL DATINI KKONT ,8HKKONT ,1,UNIT,IER)
00000800 CALL DATINI KPL ,8HKPL ,1,UNIT,IER)
00000810
00000820
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00000860
00000870
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00000900
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ISN 0094	CALL DATIN(YAFOLD,8HYAFOLD	,N12,UNIT,IER)	00001470
ISN 0095	CALL DATIN(ZAFOLD,8HZAFOLD	,N12,UNIT,IER)	00001480
ISN 0096	CALL DATIN(XIMP,8HXIMP	,N12,UNIT,IER)	00001490
ISN 0097	CALL DATIN(YIMP,8HYIMP	,N12,UNIT,IER)	00001500
ISN 0098	CALL DATIN(ZIMP,8HZIMP	,N12,UNIT,IER)	00001510
ISN 0099	CALL DATIN(XIMPOL,8HXIMPOL	,N12,UNIT,IER)	00001520
ISN 0100	CALL DATIN(YIMPOL,8HYIMPOL	,N12,UNIT,IER)	00001530
ISN 0101	CALL DATIN(ZIMPOL,8HZIMPOL	,N12,UNIT,IER)	00001540
ISN 0102	CALL DATIN(ZINIT,8HZINIT	,N12,UNIT,IER)	00001550
ISN 0103	CALL DATIN(PINO,8HPINO	,N12,UNIT,IER)	00001560
ISN 0104	CALL DATIN(QINO,8HQINO	,N12,UNIT,IER)	00001570
ISN 0105	CALL DATIN(RINO,8HRINO	,N12,UNIT,IER)	00001580
ISN 0106	CALL DATIN(OPIN,8HDPIN	,N12,UNIT,IER)	00001590
ISN 0107	CALL DATIN(DGIN,8HDGIN	,N12,UNIT,IER)	00001600
ISN 0108	CALL DATIN(DRIN,8HDRIN	,N12,UNIT,IER)	00001610
ISN 0109	CALL DATIN(PIN,8HPIN	,N12,UNIT,IER)	00001620
ISN 0110	CALL DATIN(QIN,8HQIN	,N12,UNIT,IER)	00001630
ISN 0111	CALL DATIN(RIN,8HRIN	,N12,UNIT,IER)	00001640
ISN 0112	CALL DATIN(KEI,8HKEI	,N12,UNIT,IER)	00001650
ISN 0113	CALL DATIN(PEI,8HPEI	,N12,UNIT,IER)	00001660
ISN 0114	CALL DATIN(XSE,8HXSE	,N12,UNIT,IER)	00001670
ISN 0115	CALL DATIN(XDE,8HXDE	,N12,UNIT,IER)	00001680
ISN 0116	CALL DATIN(XCE,8HXC	,N12,UNIT,IER)	00001690
ISN 0117	CALL DATIN(XFE,8HXFE	,N12,UNIT,IER)	00001700
ISN 0118	CALL DATIN(XETOT,8HXETOT	,N12,UNIT,IER)	00001710
ISN 0119	CALL DATIN(XPCT,8HXPCT	,N12,UNIT,IER)	00001720
ISN 0120	CALL DATIN(XETOTO,8HXETOTO	,N12,UNIT,IER)	00001730
ISN 0121	N19 = 9*2*N1		00001740
ISN 0122	CALL DATIN(BIJ,8HBIJ	,N19,UNIT,IER)	00001750
ISN 0123	CALL DATIN(IPENSW,8HIPENSW	,N1,UNIT,IER)	00001760
			00001770
			00001780
			00001790
			00001800
			00001810
			00001820
			00001830
			00001840
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			00001930
			00001940
			00001950
			00001960
			00001970
			00001980
			00001990

ISN 0124	N12 = 2*N12		
ISN 0125	CALL DATIN(XNP,8HXNP	,N12,UNIT,IER)	
ISN 0126	CALL DATIN(YNP,8HYNP	,N12,UNIT,IER)	
ISN 0127	CALL DATIN(ZNP,8HZNP	,N12,UNIT,IER)	
ISN 0128	CALL DATIN(XDNP,8HXDNP	,N12,UNIT,IER)	
ISN 0129	CALL DATIN(YDNP,8HYDNP	,N12,UNIT,IER)	
ISN 0130	CALL DATIN(ZDNP,8HZDNP	,N12,UNIT,IER)	
ISN 0131	CALL DATIN(UNP,8HUNP	,N12,UNIT,IER)	
ISN 0132	CALL DATIN(VNP,8HVNP	,N12,UNIT,IER)	
ISN 0133	CALL DATIN(WNP,8HWNP	,N12,UNIT,IER)	
ISN 0134	CALL DATIN(XACNP,8HXACNP	,N12,UNIT,IER)	
ISN 0135	CALL DATIN(YACNP,8HYACNP	,N12,UNIT,IER)	
ISN 0136	CALL DATIN(ZACNP,8HZACNP	,N12,UNIT,IER)	
ISN 0137	CALL DATIN(XACNPF,8HXACNPF	,N12,UNIT,IER)	
ISN 0138	CALL DATIN(YACNPF,8HYACNPF	,N12,UNIT,IER)	
ISN 0139	CALL DATIN(ZACNPF,8HZACNPF	,N12,UNIT,IER)	
ISN 0140	CALL DATIN(XNPF,8HXNPF	,N12,UNIT,IER)	
ISN 0141	CALL DATIN(YNPF,8HYNPF	,N12,UNIT,IER)	
ISN 0142	CALL DATIN(ZNPF,8HZNPF	,N12,UNIT,IER)	
ISN 0143	CALL DATIN(XANPF,8HXANPF	,N12,UNIT,IER)	

C C C

A-189


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ISN 0144 CALL DATIN(YANPFO,8HYANPFO ,NMP2,UNIT,IER)
ISN 0145 CALL DATIN(ZANPFO,8HZANPFO ,NMP2,UNIT,IER)
ISN 0146 CALL DATIN(XIMPMP,8HXIMPMP ,NMP2,UNIT,IER)
ISN 0147 CALL DATIN(YIMPMP,8HYIMPMP ,NMP2,UNIT,IER)
ISN 0148 CALL DATIN(ZIMPMP,8HZIMPMP ,NMP2,UNIT,IER)
ISN 0149 CALL DATIN(XIMPPL,8HXIMPPL ,NMP2,UNIT,IER)
ISN 0150 CALL DATIN(YIMPPL,8HYIMPPL ,NMP2,UNIT,IER)
ISN 0151 CALL DATIN(ZIMPPL,8HZIMPPL ,NMP2,UNIT,IER)

C
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C
ISN 0152 NB2 = 2*NB
ISN 0153 CALL DATIN(KFL35 ,8HKFL35 ,NB,UNIT,IER)
ISN 0154 CALL DATIN(KFL26 ,8HKFL26 ,NB,UNIT,IER)
ISN 0155 CALL DATIN(FL26I ,8HFL26I ,NB,UNIT,IER)
ISN 0156 CALL DATIN(FL26J ,8HFL26J ,NB,UNIT,IER)
ISN 0157 CALL DATIN(FL35I ,8HFL35I ,NB,UNIT,IER)
ISN 0158 CALL DATIN(FL35J ,8HFL35J ,NB,UNIT,IER)
ISN 0159 CALL DATIN(SEIJ ,8HSEIJ ,NB2,UNIT,IER)
ISN 0160 CALL DATIN(OEIJ ,8HDEIJ ,NB2,UNIT,IER)
ISN 0161 CALL DATIN(IRUPSH,8HIRUPSH ,NB,UNIT,IER)
ISN 0162 CALL DATIN(OPHIJ,8HOPHIJ ,NB2,UNIT,IER)
ISN 0163 CALL DATIN(PHIJ ,8HPIIJ ,NB2,UNIT,IER)
ISN 0164 CALL DATIN(THIJ ,8HTHEIJ ,NB2,UNIT,IER)
ISN 0165 CALL DATIN(PSIJ ,8HPSIJ ,NB2,UNIT,IER)
ISN 0166 CALL DATIN(SBUCKR,8HSBUCKR ,NB2,UNIT,IER)
ISN 0167 CALL DATIN(DRI ,8HDRI ,NB2,UNIT,IER)
ISN 0168 CALL DATIN(FUB ,8HFUB ,NB2,UNIT,IER)
ISN 0169 NB4 = 2*2*NB
ISN 0170 CALL DATIN(VEEN (1,1),8HVEEN ,NB4,UNIT,IER)
ISN 0171 NB12 = 2*6*NB
ISN 0172 CALL DATIN(SUDF (1,1),8HSUDF ,NB12,UNIT,IER)
ISN 0173 CALL DATIN(FINT (1,1),8HFINT ,NB12,UNIT,IER)
ISN 0174 CALL DATIN(SUDFI(1,1),8HSUDFI ,NB12,UNIT,IER)
ISN 0175 CALL DATIN(FINTI (1,1),8HFINTI ,NB12,UNIT,IER)
ISN 0176 NB18 = 2*9*NB
ISN 0177 CALL DATIN(VEEBAR,8HVEEBAR ,NB18,UNIT,IER)
ISN 0178 NB6 = 6*NB
ISN 0179 NB3 = 3*NB
ISN 0180 NB12 = 6*2*NB
ISN 0181 CALL DATIN(NI ,8HNI ,NB3,UNIT,IER)
ISN 0182 CALL DATIN(VEE ,8HVEE ,NB12,UNIT,IER)
ISN 0183 CALL DATIN(KRFLAG,8HKRFLAG ,NB6,UNIT,IER)
ISN 0184 NOL2=2*NOLEO
ISN 0185 CALL DATIN(YOLEO ,8HYOLEO ,NOL2,UNIT,IER)
ISN 0186 DO 100 K = 1,4
ISN 0187 CALL DATIN(FRD (1,K),8HFRD ,NB2,UNIT,IER)
ISN 0188 CALL DATIN(FRS (1,K),8HFRS ,NB2,UNIT,IER)
ISN 0189 100 CONTINUE
ISN 0190 NLI = NLB/2 + MOD(NLB,2)
ISN 0191 CALL DATIN(CHUG ,8HCHUG ,NLI,UNIT,IER)

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C
ISN 0192      KR2 = 2*KRCRONT
ISN 0193      CALL DATINI(TKR ,8HTKR ,KR2,UNIT,IER)
ISN 0194      KR4 = 4*KRCRONT
ISN 0195      CALL DATINI(KRBEAM(1,1),8HKRBEAM ,KR4,UNIT,IER)
ISN 0196      CALL DATINI(IPEN ,8HIPEN ,KPEN,UNIT,IER)
ISN 0197      KPEH2 = 2*KPEN
ISN 0198      CALL DATINI(TPEN ,8HTPEN ,KPEH2,UNIT,IER)
ISN 0199      KPL2=2*KPL
ISN 0200      CALL DATINI(TPL ,8HTPL ,KPL2,UNIT,IER)
ISN 0201      DO 120 K=1,3
ISN 0202      CALL DATINI(BPL(1,K),8HBPL ,KPL,UNIT,IER)
ISN 0203      120 CONTINUE
C
ISN 0204      KK2=2*KKONT
ISN 0205      CALL DATINI(TSP ,8HTSP ,KK2,UNIT,IER)
ISN 0206      KK5=5*KKONT
ISN 0207      CALL DATINI(KKSP(1,1),8HKKSP ,KK5,UNIT,IER)
ISN 0208      KK52=5*2*KKONT
ISN 0209      CALL DATINI(EXSP(1,1),8HEXSP ,KK52,UNIT,IER)
ISN 0210      NSP2 = 2*NSP
ISN 0211      NS2 = NSP/2 + MOD(NSP,2)
ISN 0212      CALL DATINI(DELG ,8HDELG ,NSP2,UNIT,IER)
ISN 0213      CALL DATINI(IFS ,8HIFS ,NS2,UNIT,IER)
ISN 0214      CALL DATINI(JBS ,8HJBS ,NS2,UNIT,IER)
ISN 0215      CALL DATINI(SBAR ,8HSBAR ,NSP2,UNIT,IER)
ISN 0216      CALL DATINI(FSPBAR ,8HFSBAR ,NSP2,UNIT,IER)
ISN 0217      CALL DATINI(FSPOP ,8HFSPOP ,NSP2,UNIT,IER)
ISN 0218      CALL DATINI(SCP ,8HSCP ,NSP2,UNIT,IER)
ISN 0219      CALL DATINI(STEMP1,8HSTEMP1 ,NSP2,UNIT,IER)
ISN 0220      CALL DATINI(STEMP2,8HSTEMP2 ,NSP2,UNIT,IER)
ISN 0221      CALL DATINI(STEMP3,8HSTEMP3 ,NSP2,UNIT,IER)
ISN 0222      CALL DATINI(STEMP4,8HSTEMP4 ,NSP2,UNIT,IER)
ISN 0223      CALL DATINI(STEMP5,8HSTEMP5 ,NSP2,UNIT,IER)
ISN 0224      CALL DATINI(INN ,8HINN ,NS2,UNIT,IER)
ISN 0225      CALL DATINI(CEIK ,8HCEIK ,NSP2,UNIT,IER)
ISN 0226      CALL DATINI(CEIKF ,8HCEIKF ,NSP2,UNIT,IER)
ISN 0227      CALL DATINI(SC ,8HSC ,NSP2,UNIT,IER)
ISN 0228      CALL DATINI(KUN ,8HKUN ,NSP2,UNIT,IER)
ISN 0229      DO 200 K=1,8
ISN 0230      CALL DATINI(FSPRNG(1,K),8HFSPRNG ,NSP2,UNIT,IER)
ISN 0231      200 CONTINUE
ISN 0232      NVCH2 = 2*NVCH
ISN 0233      CALL DATINI(VOL ,8HVOL ,NVCH2,UNIT,IER)
ISN 0234      DO 300 K = 1,3
ISN 0235      CALL DATINI(DLVOL (1,K),8HDLVOL ,NVCH2,UNIT,IER)
ISN 0236      300 CONTINUE
C
ISN 0237      CALL DATINI(XDOTAP,8HXDOTAP ,2,UNIT,IER)

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00003190

CALL DATINI YDOTAP, 8NYDOTAP ,2,UNIT,IER)
CALL DATINI ZDOTAP, 8NZDOTAP ,2,UNIT,IER)
CALL DATINI ETOTTO, 8HETOTTO ,2,UNIT,IER)
CALL DATINI XETOTL, 8HXETOTL ,2,UNIT,IER)
CALL DATINI KETOTL, 8HKETOTL ,2,UNIT,IER)
CALL DATINI PETOTL, 8HPETOTL ,2,UNIT,IER)
CALL DATINI SETOTL, 8HSETOTL ,2,UNIT,IER)
CALL DATINI DETOTL, 8HDETOTL ,2,UNIT,IER)
CALL DATINI CETOTL, 8HCETOTL ,2,UNIT,IER)
CALL DATINI FETOTL, 8HFETOTL ,2,UNIT,IER)
CALL DATINI INGSCT, 8HINGSCT ,1,UNIT,IER)
CALL CLSINI(UNIT,IER)
RETURN
END

ISN 0238
ISN 0239
ISN 0240
ISN 0241
ISN 0242
ISN 0243
ISN 0244
ISN 0245
ISN 0246
ISN 0247
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ISN 0251

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NODEDIT,10,XREF
C DATA SET D233ASOUT AT LEVEL 006 AS OF 06/25/79
C DATA SET D2332VRO AT LEVEL 005 AS OF 01/27/78
SUBROUTINE RSOUT(MODEL,CASE,MSEC)

00000010
00000020
00000030
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00000090
00000100
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00000400

IMPLICIT REAL*8(A-H,O-Z)
REAL*8 KUN, MODEL, KEI, KETOTL
REAL*4 XK5, XK1, XKR, ENGSY
INTEGER*4 TITLE(40),UNIT,CASE,BPL(100,3)
INTEGER*2 FL26I(150),FL26J(150),FL35I(150)
INTEGER*2 NLSFLG,CHUG,NL,IJPR,MN,INBUFF,IG,JG,IJS,JBS
COMMON/DEIN/ XNBAR,XPBAR,YNBAR,YPBAR,ZNBAR,ZPBAR,VOLENZ(5,3),
1 FXAXI(900),HEX(80),HYBI(80),HEZ(80),ALIFT(80),VMAXI(900),VMAXNI(900),
2 FXAXNI(900),XKSI(2700),XKI(2700),XKR(2700),NLSFLG(900),CHUG(180),
3 MYP
COMMON/DEPR/ XDOTAP,YDOTAP,ZDOTAP,DLVOL(5,3),FRD(150,4),
1 FR5(150,4),SUMDFI(6,150),FINTI(6,150),VEEN(2,150)
COMMON/ENERGY/ XPTCI(80),XETOTI(80),XETOTOI(80),XSE(80),XDEI(80),
1 XCEI(80),XFEI(80),KEI(80),PEI(80),XETOTL,KETOTL,
2 PETOTL,SETOTL,DETOTL,CETOTL,FETOTL
COMMON/MADE/ KFI26I(150),KFI35I(150),FL26I,FL26J,FL35I,FL35J,
1 TPL(100),BPL,KPL
COMMON/DINICP/ STENS(20),SHEAR(20),EE(20),GG(20),
1 FINTI(6,150),VOL(5),VZERO(5),KMATR(6,4),NVCH,INBUFF(5,8)
COMMON/INPR/ NDRI,NSP
COMMON
COMMON
1 XNI(80),DPX(80),DPY(80),DPZ(80),DPL(80),DPHI(80),DPN(80),PINI(80),
2 QIN(80),PINI(80),XII(80),XII(80),XII(80),XII(80),XII(80),XII(80),
5 DELI(80),POLDI(80),ROLDI(80),ROLDI(80),UOLDI(80),VOLDI(80),
6 WOLDI(80),XOLDI(80),YOLDI(80),ZOLDI(80),PINO(80),QINO(80),RINO(80),
7 PHIOLD(80),THEOLD(80),PSIOLD(80),
8 XACFDI(80),YACFDI(80),ZACFDI(80),XAFOLD(80),YAFOLD(80),ZAFOLD(80),
9 XNPFDI(50),YNPFDI(50),ZNPFDI(50),XANPFOI(50),YANPFOI(50),ZANPFOI(50),
A TKR(200),TPENI(80),DTHALF,
B KRBEAM(4,200),KRFLAG(900),IPENI(80),KPEN,KRCONT
COMMON/NP0014/ NNP
COMMON/NP01R8/ XNP(50),YNP(50),ZNP(50),UNP(50),VNP(50),MNP(50),
1 XDNPI(50),YDNPI(50),ZDNPI(50),XACNPI(50),YACNPI(50),ZACNPI(50),
2 SBUCXR(150),PCRI(150)
COMMON/PRHA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50),
1 XN

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ISN 0019	1 ZACNPF(50),XIMP(80),YIMP(80),ZIMP(80),XIMP(50),YIMP(50),	0000410
	2 ZIMP(50),XIMP(80),YIMP(80),ZIMP(80),XIMP(50),	0000420
	3 YIMP(50),ZIMP(80)	0000430
	COMMON/OLEO/EOLEO(20),FAO(20),EXPOLE(20),YMAX(20),	0000440
	1 YOLEO(20),BOLEO(20),BOLEO(20),XKEXT(20),XKCOMP(20),FCOUL(20),	0000450
	2 ALPHAP,IGOLEO(20),JGOLEO(20),NGOLEO(20),NGOLEO(20),NOLEO	0000460
	COMMON/COMALL/ C(6,150),PI(80),Q(80),R(80),U(80),V(80),W(80),X(81),	0000470
	1 Y(81),Z(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),	0000480
	2 YI(80),ZI(80),XYI(80),XZI(80),YZI(80),AIJ(9),BIJ(720),	0000490
	3 DRI(150),OAI(720),VEE(900),MGT(80),PHI(80),THETA(80),PSI(80),	0000500
	4 PDOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),	0000510
	5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,	0000520
	6 XACC(80),YACC(80),ZACC(80),AIDOT(9),	0000530
	7 PHIJ(150),THEIJ(150),PSIJ(150),SUMPF(6,150),TITLE,	0000540
	8 XLSAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),	0000550
	9 OPIN(81),OQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),	0000560
	A CEIK(40),	0000570
	B SBAR(40),KUN(40),MAXNM,MAXIGS,MAXTBL,	0000580
	C NM,NB,I,J,IG(150),JG(150),	0000590
	D NI(900),NNI(40),IJPR(150)	0000600
ISN 0021	COMMON/CFPR/FSPRNG(40,8),DELG(40)	0000610
ISN 0022	COMMON/MACF/IBS(40),FSPOI(40),SCP(40),JBS(40),	0000620
	1 KSP(5,200),EXSPI(5,200),TSPI(200),STEMP(40),STEMP2(40),	0000630
	2 STEMP3(40),STEMP4(40),STEMP5(40),KKONT	0000640
ISN 0023	COMMON/MAPR/ ETOTTO, ENGSNY(6,200), INGSCT	0000650
ISN 0024	COMMON/COMI4/ND,NVBHM,NFBHM,NMI,NKM,NLB,NPH,NMTL,NPTS(50),	0000660
	1 NVBH,IJPR(14),IPHDPI(80),NFBH	0000670
ISN 0025	COMMON /MAX/ IRUPSH(150), IPENSH(80), VEEBAR(900), ZINIT(80),	0000680
	1 DPHIJ(150), FUB(150)	0000690
ISN 0026	DATA UNIT/21/	0000700
		0000710
		0000720
		0000730
		0000740
ISN 0027	CALL OPNOUT(UNIT)	0000750
ISN 0028	CALL DATOUT(MODEL ,8HMODEL ,2,UNIT,IER)	0000760
ISN 0029	CALL DATOUT(CASE ,8HCASE ,1,UNIT,IER)	0000770
ISN 0030	CALL DATOUT(MSEC ,8HSEC ,1,UNIT,IER)	0000780
ISN 0031	CALL DATOUT(TIME ,8HTIME ,2,UNIT,IER)	0000790
		0000800
	...INDICES...	0000810
ISN 0032	CALL DATOUT(KRCNT,8HKRCNT ,1,UNIT,IER)	0000820
ISN 0033	CALL DATOUT(KPEN ,8HKPEN ,1,UNIT,IER)	0000830
ISN 0034	CALL DATOUT(KKONT ,8HKKONT ,1,UNIT,IER)	0000840
ISN 0035	CALL DATOUT(KPL ,8HKPL ,1,UNIT,IER)	0000850
		0000860
	...ARRAYS...	0000870
		0000880
		0000890
ISN 0036	NM2 = 24NM	0000900
ISN 0037	CALL DATOUT(P ,8HP ,NM2,UNIT,IER)	0000910
ISN 0038	CALL DATOUT(Q ,8HQ ,NM2,UNIT,IER)	0000920
ISN 0039	CALL DATOUT(R ,8HR ,NM2,UNIT,IER)	0000930
ISN 0040	CALL DATOUT(U ,8HU ,NM2,UNIT,IER)	0000940

ISN 0041	CALL DATOUT(V	,SHV	,NM2,UNIT,IER)	00000940
ISN 0042	CALL DATOUT(W	,SHW	,NM2,UNIT,IER)	00000950
ISN 0043	CALL DATOUT(X	,SHX	,NM2,UNIT,IER)	00000960
ISN 0044	CALL DATOUT(Y	,SHY	,NM2,UNIT,IER)	00000970
ISN 0045	CALL DATOUT(Z	,SHZ	,NM2,UNIT,IER)	00000980
ISN 0046	CALL DATOUT(PHI	,SHPHI	,NM2,UNIT,IER)	00000990
ISN 0047	CALL DATOUT(THETA	,SHTHETA	,NM2,UNIT,IER)	00001000
ISN 0048	CALL DATOUT(PSI	,SHPSI	,NM2,UNIT,IER)	00001010
ISN 0049	CALL DATOUT(PDOT	,SHPDOT	,NM2,UNIT,IER)	00001020
ISN 0050	CALL DATOUT(QDOT	,SHQDOT	,NM2,UNIT,IER)	00001030
ISN 0051	CALL DATOUT(RDOT	,SHRDOT	,NM2,UNIT,IER)	00001040
ISN 0052	CALL DATOUT(UDOT	,SHUDOT	,NM2,UNIT,IER)	00001050
ISN 0053	CALL DATOUT(VDOT	,SHVDOT	,NM2,UNIT,IER)	00001060
ISN 0054	CALL DATOUT(WDOT	,SHWDOT	,NM2,UNIT,IER)	00001070
ISN 0055	CALL DATOUT(XDOT	,SHXDOT	,NM2,UNIT,IER)	00001080
ISN 0056	CALL DATOUT(YDOT	,SHYDOT	,NM2,UNIT,IER)	00001090
ISN 0057	CALL DATOUT(ZDOT	,SHZDOT	,NM2,UNIT,IER)	00001100
ISN 0058	CALL DATOUT(PHIDOT	,SHPHIDOT	,NM2,UNIT,IER)	00001110
ISN 0059	CALL DATOUT(THEDOT	,SHTHEDOT	,NM2,UNIT,IER)	00001120
ISN 0060	CALL DATOUT(PSIDOT	,SHPSIDOT	,NM2,UNIT,IER)	00001130
ISN 0061	CALL DATOUT(POLD	,SHPOL	,NM2,UNIT,IER)	00001140
ISN 0062	CALL DATOUT(OLD	,SHQOLD	,NM2,UNIT,IER)	00001150
ISN 0063	CALL DATOUT(ROLD	,SHROLD	,NM2,UNIT,IER)	00001160
ISN 0064	CALL DATOUT(UOLD	,SHUOLD	,NM2,UNIT,IER)	00001170
ISN 0065	CALL DATOUT(VOLD	,SHVOLD	,NM2,UNIT,IER)	00001180
ISN 0066	CALL DATOUT(WOLD	,SHWOLD	,NM2,UNIT,IER)	00001190
ISN 0067	CALL DATOUT(XOLD	,SHXOLD	,NM2,UNIT,IER)	00001200
ISN 0068	CALL DATOUT(ZOLD	,SHZOLD	,NM2,UNIT,IER)	00001210
ISN 0069	CALL DATOUT(PHOLD	,SHPHOLD	,NM2,UNIT,IER)	00001230
ISN 0070	CALL DATOUT(THOLD	,SHTHOLD	,NM2,UNIT,IER)	00001240
ISN 0071	CALL DATOUT(PSIOLD	,SHPSIOLD	,NM2,UNIT,IER)	00001250
ISN 0072	CALL DATOUT(OLD	,SHDX	,NM2,UNIT,IER)	00001260
ISN 0073	CALL DATOUT(DX	,SHDY	,NM2,UNIT,IER)	00001270
ISN 0074	CALL DATOUT(DY	,SHDZ	,NM2,UNIT,IER)	00001280
ISN 0075	CALL DATOUT(DZ	,SHXACC	,NM2,UNIT,IER)	00001290
ISN 0076	CALL DATOUT(YACC	,SHYACC	,NM2,UNIT,IER)	00001300
ISN 0077	CALL DATOUT(XACC	,SHZACC	,NM2,UNIT,IER)	00001310
ISN 0078	CALL DATOUT(ZACC	,SHXACF	,NM2,UNIT,IER)	00001320
ISN 0079	CALL DATOUT(YACF	,SHYACF	,NM2,UNIT,IER)	00001330
ISN 0080	CALL DATOUT(XACF	,SHZACF	,NM2,UNIT,IER)	00001340
ISN 0081	CALL DATOUT(ZACF	,SHXACFD	,NM2,UNIT,IER)	00001350
ISN 0082	CALL DATOUT(YACFD	,SHYACFD	,NM2,UNIT,IER)	00001360
ISN 0083	CALL DATOUT(XACFD	,SHZACFD	,NM2,UNIT,IER)	00001370
ISN 0084	CALL DATOUT(ZAFOLD	,SHXAFOLD	,NM2,UNIT,IER)	00001380
ISN 0085	CALL DATOUT(YAFOLD	,SHYAFOLD	,NM2,UNIT,IER)	00001390
ISN 0086	CALL DATOUT(XAFOLD	,SHZAFOLD	,NM2,UNIT,IER)	00001400
ISN 0087	CALL DATOUT(ZIMP	,SHXIMP	,NM2,UNIT,IER)	00001410
ISN 0088	CALL DATOUT(YIMP	,SHYIMP	,NM2,UNIT,IER)	00001420
ISN 0089	CALL DATOUT(XIMP	,SHZIMP	,NM2,UNIT,IER)	00001430
ISN 0090	CALL DATOUT(ZIMPOL	,SHXIMPOL	,NM2,UNIT,IER)	00001440
ISN 0091	CALL DATOUT(YIMPOL	,SHYIMPOL	,NM2,UNIT,IER)	00001450
ISN 0092	CALL DATOUT(XIMPOL	,SHZIMPOL	,NM2,UNIT,IER)	00001460
ISN 0093	CALL DATOUT(ZIMPOL	,SHZIMPOL	,NM2,UNIT,IER)	00001460

ISN 0094	CALL DATOUT(ZINIT ,8HZINIT	,NM2,UNIT,IER)	00001470
ISN 0095	CALL DATOUT(PINO ,8HPINO	,NM2,UNIT,IER)	00001480
ISN 0096	CALL DATOUT(QINO ,8HQINO	,NM2,UNIT,IER)	00001490
ISN 0097	CALL DATOUT(IRINO ,8HRINO	,NM2,UNIT,IER)	00001500
ISN 0098	CALL DATOUT(OPIN ,8HOPIN	,NM2,UNIT,IER)	00001510
ISN 0099	CALL DATOUT(DQIN ,8HDQIN	,NM2,UNIT,IER)	00001520
ISN 0100	CALL DATOUT(DQIN ,8HDQIN	,NM2,UNIT,IER)	00001530
ISN 0101	CALL DATOUT(PIN ,8HPIN	,NM2,UNIT,IER)	00001540
ISN 0102	CALL DATOUT(QIN ,8HQIN	,NM2,UNIT,IER)	00001550
ISN 0103	CALL DATOUT(IRIN ,8HRIN	,NM2,UNIT,IER)	00001560
ISN 0104	CALL DATOUT(KEI ,8HKEI	,NM2,UNIT,IER)	00001570
ISN 0105	CALL DATOUT(PEI ,8HPEI	,NM2,UNIT,IER)	00001580
ISN 0106	CALL DATOUT(XSE ,8HXSE	,NM2,UNIT,IER)	00001590
ISN 0107	CALL DATOUT(XDE ,8HXDE	,NM2,UNIT,IER)	00001600
ISN 0108	CALL DATOUT(XCE ,8HXCE	,NM2,UNIT,IER)	00001610
ISN 0109	CALL DATOUT(XFE ,8HXFE	,NM2,UNIT,IER)	00001620
ISN 0110	CALL DATOUT(XETOT ,8HXETOT	,NM2,UNIT,IER)	00001630
ISN 0111	CALL DATOUT(XPCT ,8HXPCT	,NM2,UNIT,IER)	00001640
ISN 0112	CALL DATOUT(XETOTO ,8HXETOTO	,NM2,UNIT,IER)	00001650
ISN 0113	NM9 = 9*2*MM		00001660
ISN 0114	CALL DATOUT(BIJ ,8HBIJ	,NM9,UNIT,IER)	00001670
ISN 0115	CALL DATOUT(IPENSM ,8HIPENSM	,NM1,UNIT,IER)	00001680
			00001690
			00001700
			00001710
			00001720
			00001730
			00001740
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			00001920
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			00001940
			00001950
			00001960
			00001970
			00001980
			00001990

C C

ISN 0116	NMP2 = 2*MM		
ISN 0117	CALL DATOUT(XNP ,8HXP	,NMP2,UNIT,IER)	
ISN 0118	CALL DATOUT(YNP ,8HYNP	,NMP2,UNIT,IER)	
ISN 0119	CALL DATOUT(ZNP ,8HZNP	,NMP2,UNIT,IER)	
ISN 0120	CALL DATOUT(XDNP ,8HXDNP	,NMP2,UNIT,IER)	
ISN 0121	CALL DATOUT(YDNP ,8HYDNP	,NMP2,UNIT,IER)	
ISN 0122	CALL DATOUT(ZDNP ,8HZDNP	,NMP2,UNIT,IER)	
ISN 0123	CALL DATOUT(XNP ,8HXP	,NMP2,UNIT,IER)	
ISN 0124	CALL DATOUT(YNP ,8HYNP	,NMP2,UNIT,IER)	
ISN 0125	CALL DATOUT(ZNP ,8HZNP	,NMP2,UNIT,IER)	
ISN 0126	CALL DATOUT(XACNP ,8HXACNP	,NMP2,UNIT,IER)	
ISN 0127	CALL DATOUT(YACNP ,8HYACNP	,NMP2,UNIT,IER)	
ISN 0128	CALL DATOUT(ZACNP ,8HZACNP	,NMP2,UNIT,IER)	
ISN 0129	CALL DATOUT(XACNP ,8HXACNP	,NMP2,UNIT,IER)	
ISN 0130	CALL DATOUT(YACNP ,8HYACNP	,NMP2,UNIT,IER)	
ISN 0131	CALL DATOUT(ZACNP ,8HZACNP	,NMP2,UNIT,IER)	
ISN 0132	CALL DATOUT(XNPFD ,8HXNPFD	,NMP2,UNIT,IER)	
ISN 0133	CALL DATOUT(YNPFD ,8HYNPFD	,NMP2,UNIT,IER)	
ISN 0134	CALL DATOUT(ZNPFD ,8HZNPFD	,NMP2,UNIT,IER)	
ISN 0135	CALL DATOUT(XANPFO ,8XANPFO	,NMP2,UNIT,IER)	
ISN 0136	CALL DATOUT(YANPFO ,8YANPFO	,NMP2,UNIT,IER)	
ISN 0137	CALL DATOUT(ZANPFO ,8ZANPFO	,NMP2,UNIT,IER)	
ISN 0138	CALL DATOUT(XIMPNP ,8XIMPNP	,NMP2,UNIT,IER)	
ISN 0139	CALL DATOUT(YIMPNP ,8YIMPNP	,NMP2,UNIT,IER)	
ISN 0140	CALL DATOUT(ZIMPNP ,8ZIMPNP	,NMP2,UNIT,IER)	
ISN 0141	CALL DATOUT(XIMPPL ,8XIMPPL	,NMP2,UNIT,IER)	
ISN 0142	CALL DATOUT(YIMPPL ,8YIMPPL	,NMP2,UNIT,IER)	
ISN 0143	CALL DATOUT(ZIMPPL ,8ZIMPPL	,NMP2,UNIT,IER)	

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C
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C
ISN 0144      NB2 = 2*NB
ISN 0145      CALL DATOUT(KFL35 ,8HKFL35 ,NB,UNIT,IER)
ISN 0146      CALL DATOUT(KFL26 ,8HKFL26 ,NB,UNIT,IER)
ISN 0147      CALL DATOUT(FL261 ,8HFL261 ,NB,UNIT,IER)
ISN 0148      CALL DATOUT(FL26J ,8HFL26J ,NB,UNIT,IER)
ISN 0149      CALL DATOUT(FL35I ,8HFL35I ,NB,UNIT,IER)
ISN 0150      CALL DATOUT(FK35J ,8HFL35J ,NB,UNIT,IER)
ISN 0151      CALL DATOUT(SEIJ ,8HSEIJ ,NB2,UNIT,IER)
ISN 0152      CALL DATOUT(DEIJ ,8HDEIJ ,NB2,UNIT,IER)
ISN 0153      CALL DATOUT(IRUPSM,8HIRUPSM ,NB,UNIT,IER)
ISN 0154      CALL DATOUT(OPHIJ,8HOPHIJ ,NB2,UNIT,IER)
ISN 0155      CALL DATOUT(PHIJ ,8HPHIJ ,NB2,UNIT,IER)
ISN 0156      CALL DATOUT(THIJ ,8HTHEIJ ,NB2,UNIT,IER)
ISN 0157      CALL DATOUT(PSIJ ,8HPSIJ ,NB2,UNIT,IER)
ISN 0158      CALL DATOUT(SBUCKR,8HSBUCKR ,NB2,UNIT,IER)
ISN 0159      CALL DATOUT(DRI ,8HDRI ,NB2,UNIT,IER)
ISN 0160      CALL DATOUT(FUB ,8HFUB ,NB2,UNIT,IER)
ISN 0161      NB4 = 2*2*NB
ISN 0162      CALL DATOUT(VEEN (1,1),8HVEEN ,NB4,UNIT,IER)
ISN 0163      NB12 = 2*6*NB
ISN 0164      CALL DATOUT(SUMDF (1,1),8HSUMDF ,NB12,UNIT,IER)
ISN 0165      CALL DATOUT(FINT (1,1),8HFINT ,NB12,UNIT,IER)
ISN 0166      CALL DATOUT(SUMDFI(1,1),8HSUMDFI ,NB12,UNIT,IER)
ISN 0167      CALL DATOUT(FINTI (1,1),8HFINTI ,NB12,UNIT,IER)
ISN 0168      NB18 = 2*9*NB
ISN 0169      CALL DATOUT(VEEBAR,8HVEEBAR ,NB18,UNIT,IER)
ISN 0170      NB3 = 3*NB
ISN 0171      NB6 = 6*NB
ISN 0172      NB12 = 6*2*NB
ISN 0173      CALL DATOUT(NI ,8HNI ,NB3,UNIT,IER)
ISN 0174      CALL DATOUT(VEE ,8HVEE ,NB12,UNIT,IER)
ISN 0175      CALL DATOUT(KRFLAG,8HKRFLAG ,NB6,UNIT,IER)
ISN 0176      NOL2=2*NOL2
ISN 0177      CALL DATOUT(YOLEO ,8HYOLEO ,NOL2,UNIT,IER)
ISN 0178      DO 100 K = 1,4
ISN 0179          CALL DATOUT(FRD (1,K),8HFRD ,NB2,UNIT,IER)
ISN 0180          CALL DATOUT(FRS (1,K),8HFRS ,NB2,UNIT,IER)
ISN 0181      100 CONTINUE
ISN 0182      NLI = NLB/2 + MOD(NLB,2)
ISN 0183      CALL DATOUT(CHUG ,8HCHUG ,NLI,UNIT,IER)

C
C
C
ISN 0184      KR2 = 2*KRCNT
ISN 0185      CALL DATOUT(TKR ,8HTKR ,KR2,UNIT,IER)
ISN 0186      KR4 = 4*KRCNT
ISN 0187      CALL DATOUT(KRBEAM(1,1),8HKRBEAM ,KR4,UNIT,IER)
ISN 0188      CALL DATOUT(IPEN ,8HIPEN ,KPN,UNIT,IER)
ISN 0189      KPN2 = 2*KPN
ISN 0190      CALL DATOUT(IPEN ,8HTPEN ,KPN2,UNIT,IER)

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ISN 0191      KPL2=2*KPL
ISN 0192      CALL DATOUT(TPL ,8HTPL ,KPL2,UNIT,IER)
ISN 0193      DO 120 K=1,3
ISN 0194      CALL DATOUT(BPL(1,K),8HBPL ,KPL,UNIT,IER)
ISN 0195      120 CONTINUE
C
C
ISN 0196      KK2=2*KKONT
ISN 0197      CALL DATOUT(TSP ,8HTSP ,KK2,UNIT,IER)
ISN 0198      KK5=5*KKONT
ISN 0199      CALL DATOUT(KKSP(1,1),8HKKSP ,KK5,UNIT,IER)
ISN 0200      KK52=5*2*KKONT
ISN 0201      CALL DATOUT(EXSP(1,1),8HEXSP ,KK52,UNIT,IER)
ISN 0202      NSP2 = 2*NSP
ISN 0203      NS2 = NSP/2 + MOD(NSP,2)
ISN 0204      CALL DATOUT(DELG ,8HDELG ,NSP2,UNIT,IER)
ISN 0205      CALL DATOUT(IFS ,8HIFS ,NS2,UNIT,IER)
ISN 0206      CALL DATOUT(JBS ,8HJBS ,NS2,UNIT,IER)
ISN 0207      CALL DATOUT(SBAR ,8HSBAR ,NSP2,UNIT,IER)
ISN 0208      CALL DATOUT(FSPBAR,8HFSBAR ,NSP2,UNIT,IER)
ISN 0209      CALL DATOUT(FSPOP ,8HFSPOP ,NSP2,UNIT,IER)
ISN 0210      CALL DATOUT(SCP ,8HSCP ,NSP2,UNIT,IER)
ISN 0211      CALL DATOUT(STEMP1,8HSTEMP1 ,NSP2,UNIT,IER)
ISN 0212      CALL DATOUT(STEMP2,8HSTEMP2 ,NSP2,UNIT,IER)
ISN 0213      CALL DATOUT(STEMP3,8HSTEMP3 ,NSP2,UNIT,IER)
ISN 0214      CALL DATOUT(STEMP4,8HSTEMP4 ,NSP2,UNIT,IER)
ISN 0215      CALL DATOUT(STEMP5,8HSTEMP5 ,NSP2,UNIT,IER)
ISN 0216      CALL DATOUT(NN ,8HNN ,NS2,UNIT,IER)
ISN 0217      CALL DATOUT(CEIK ,8HCEIK ,NSP2,UNIT,IER)
ISN 0218      CALL DATOUT(CEIKF ,8HCEIKF ,NSP2,UNIT,IER)
ISN 0219      CALL DATOUT(SC ,8HSC ,NSP2,UNIT,IER)
ISN 0220      CALL DATOUT(KUN ,8HKUN ,NSP2,UNIT,IER)
ISN 0221      DO 200 K=1,8
ISN 0222      CALL DATOUT(FSPRG(1,K),8HFSPRG ,NSP2,UNIT,IER)
ISN 0223      200 CONTINUE
ISN 0224      NVCH2 = 2*NVCH
ISN 0225      CALL DATOUT(VOL ,8HVOL ,NVCH2,UNIT,IER)
ISN 0226      DO 300 K = 1,3
ISN 0227      CALL DATOUT(DLVOL (1,K),8HDLVOL ,NVCH2,UNIT,IER)
ISN 0228      300 CONTINUE
C
C
ISN 0229      CALL DATOUT(XDOTAP,8HXDOTAP ,2,UNIT,IER)
ISN 0230      CALL DATOUT(YDOTAP,8HYDOTAP ,2,UNIT,IER)
ISN 0231      CALL DATOUT(ZDOTAP,8HZDOTAP ,2,UNIT,IER)
ISN 0232      CALL DATOUT(ETOTTO,8HETOTTO ,2,UNIT,IER)
ISN 0233      CALL DATOUT(XETOTL,8HXETOTL ,2,UNIT,IER)
ISN 0234      CALL DATOUT(XETOTL,8HXETOTL ,2,UNIT,IER)
ISN 0235      CALL DATOUT(PETOTL,8HPETOTL ,2,UNIT,IER)
ISN 0236      CALL DATOUT(SETOTL,8HSETOTL ,2,UNIT,IER)
ISN 0237      CALL DATOUT(DETOTL,8HDETOTL ,2,UNIT,IER)

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PAGE 007

00003060
00003070
00003080
00003090
00003100
00003110

CALL DATOUT(IGCTOTL,SHCTOTL ,2,UNIT,IER)
CALL DATOUT(FETOTL,SHFETOTL ,2,UNIT,IER)
CALL DATOUT(INGSET,SHINGSET ,1,UNIT,IER)
CALL CLSOUT(UNIT)
RETURN
END

ISN 0236
ISN 0239
ISN 0240
ISN 0241
ISN 0242
ISN 0243

A-199

LEVEL 21.8 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.43.23

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*

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
DATA SET D2334SHX AT LEVEL 002 AS OF 05/17/76
SUBROUTINE SHELLXDARRAY,KEY,N)

ISM 0002	C	IMPLICIT REAL*8(A-H,O-Z)	00000010
ISM 0003	C	INTEGER*2 N	00000015
ISM 0004	C		00000020
	C		00000025
	C		00000030
	C		00000040
	C		00000050
	C		00000060
	C		00000070
	C		00000080
	C		00000090
	C		00000100
	C		00000110
	C		00000120
	C		00000130
	C		00000140
	C		00000150
	C		00000160
	C		00000170
	C		00000180
	C		00000190
	C		00000200
	C		00000210
	C		00000220
	C		00000230
	C		00000240
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	C		00000290
	C		00000300
	C		00000310
	C		00000320
	C		00000330
	C		00000340
	C		00000350
	C		00000360
	C		00000370
	C		00000380

10 K = IFIRST - 1
DO 20 I=IFIRST, N
K = K + 1
IF(KEY(K)) 20,20,40
20 CONTINUE

DO 30 I=1, N
30 KEY(I) = -KEY(I)
RETURN

40 IFIRST = K
TEMP = DARRAY(K)
60 TO 60

50 DARRAY(K) = DARRAY(IK)
K = IK

60 IK = KEY(K)
KEY(K) = -IK

IK MUST BE COMPARED WITH IFIRST.
IF(IK - IFIRST) 50,70,50

A-200

PAGE 002

00000390
00000400
00000410
00000420

C 70 DARRAY(K) = TEMP
60 TO 10
END

ISN 0023
ISN 0024
ISN 0025

A-201

LEVEL 21.6 (JUN 74)

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NODEIT,ID,XREF
C DATA SET D2334SHM AT LEVEL 002 AS OF 07/19/78

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A-202

COOKING - COOK

624

6211 FOLMOT (2(52,53), 5E10.0)

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SUPPLEMENTARY
INFORMATION



SUPPLEMENTARY

INFORMATION

AD-4055898

ERRATA SHEET

Report No. FAA-RD-77-189, I

PROGRAM "KRASH" THEORY

1. Delete complete Appendix A, Program Listing, and replace with enclosed Appendix A (Revised), Program Listing, pages A-2 through A-202.
2. The enclosed change (yellow sheet) to the listing, Subroutine 'INPUT', is necessary if it is desired to model more than one oleo strut. Refer to Page A-130.

Released September 28, 1979

LEVEL 21.0 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.03.20

PROGRAM LISTING

LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,

SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
 C DATA SET D2334SS AT LEVEL 001 AS OF 06/26/79
 C DATA SET D2334MAIN AT LEVEL 011 AS OF 06/25/79
 C DATA SET D2332GMN AT LEVEL 002 AS OF 05/02/78
 C DATA SET D2332FMN AT LEVEL 002 AS OF 02/09/78

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ISN 0002 IMPLICIT REAL*8 (A-H,O-Z)
ISN 0003 REAL*8 KUN, CASEIN, CASOUT, MINDT
ISN 0004 REAL*4 ENGSHY(6,200),PERCNT(6),ETIME(200)
ISN 0005 INTEGER*4 TITLE(40),STOP,RUNIN,RUNOUT,BPL(100,3)
ISN 0006 INTEGER*2 NL,N3,IJPR,NM,IBS,JBS,IG,JG,IEER,IESE,IEPSE,IEDE,IEPDE
ISN 0007 INTEGER*2 IECE,IEPCE,IEFE,IEPFE,IEDEV,IETOT
ISN 0008 INTEGER*2 MG(150),NG(150),INP(50),MNP(50)
ISN 0009 INTEGER*2 FL26I(150),FL26J(150),FL35I(150),FL35J(150)
ISN 0010 INTEGER*2 NMEP,NMFP,NBFP,NBOP,NSEP,NDRP,NSTP,NENP,
  * JMAS(50,10),JNODE(50,8),JBMF(50,4),JBD(50,4),
  * JBSI(50,6),JSPP(50,4),JENG(50,3),JDRI(10),
  * NMEN,NMEW,NBEM,NBOM,NSEM,NDRM,NSTM,NENM,NPRINT
  DIMENSION DEV(200)
  DIMENSION N3(150,6),
  1 VEE2(6,150)
  COMMON/INPR/ NDRI,NSP
  COMMON/MADE/KFL26(150),KFL35(150),FL26I,FL26J,FL35I,FL35J,
  1 TPL(100),BPL,KPL
  COMMON/MACF/ IBS(40),FSP(40),SCP(40),JBS(40),
  1 KKSPL5,200,EXSP(5,200),TSP(200),STEP1(40),STEP2(40),
  2 STEMP3(40),STEMP4(40),STEMP5(40),KKONT
  COMMON/MACFIN/ THAX,IPRINT
  COMMON/MAPR/ ETOT0,ENGSHY,INGSCT
  COMMON/MAPRI/ DEV,ETIME,IEER,IESE,IEPSE,IEDE,IEPDE,IECE,IEPCE,
  1 IEFE,IEPFE,IEDEV,IETOT
  COMMON/NP0014/ NNP
  COMMON/NP0012/ MG,NG,INP,MNP
  COMMON/PRMA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50),
  1 ZACNPF(50),XIMP(80),YIMP(80),ZIMP(80),XIMPNP(50),YIMPNP(50),
  2 ZIMPNP(50),XIMPOL(80),YIMPOL(80),ZIMPOL(80),XIMPPL(50),
  3 YIMPPL(50),ZIMPPL(50)
  COMMON
  1 XN(80),DPX(80),DPY(80),DPZ(80),DPL(80),DPH(80),DPN(80),PIN(80),
  2 QIN(80),RIN(80),XII(80),XII(80),XII(80),XII(80),XII(80),XII(80),
  5 DELI(80),POLD(80),GOLD(80),ROLD(80),UOLD(80),VOLD(80),
  6 HOLD(80),XOLD(80),YOLD(80),ZOLD(80),PINO(80),QINO(80),RINO(80),
  
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APPENDIX A (REVISED)


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C      4.      SAME AS 2 ONLY INCLUDE SYMMETRICAL CONSTRAINTS IN DE.
C      00000930
C      00000940
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C      00001450

      REMIND NECESSARY UNITS IF PLOTS ARE REQUESTED
      IF(INEP.GT. 0) REMIND 1
      IF(INNP.GT. 0) REMIND 2
      IF(INBP.GT. 0) REMIND 3
      IF(INOP.GT. 0) REMIND 4
      IF(INSEP.GT. 0) REMIND 5
      IF(INDRP.GT. 0) REMIND 9
      IF(INNP.GT. 0) REMIND 11
      REMIND 10
      IF(INSTP.GT. 0) REMIND 13

C      SET PLOT COUNTERS TO ZERO
C      MLEN = 0
C      NLEN = 0
C      NBFM = 0
C      NBDW = 0
C      NSEN = 0
C      NDRM = 0
C      NSTH = 0
C      NENM = 0
C      NPRINT = 0

C      SET ENERGY ERROR MESSAGE INDICES TO ZERO
C      IEER=0
C      IETOT=0
C      IESE=0
C      IEPSE=0
C      IEDE=0
C      IEPDE=0
C      IECE=0
C      IEPCE=0
C      IEFE=0
C      IEPFE=0
C      IEDEV=0
C      SYMFLG = 0.
C      PUNMOD = 0.
C      IF(RUNMOD.EQ.1.) SYMFLG = 1.
C      IF(RUNMOD.EQ.3.) PUNMOD = 1.
C      IF(RUNMOD.EQ.4.) SYMFLG = 2.
C      IF(RUNMOD.EQ.2.) CALL GENMOD
C      CALL INPRINT
C      DT2 = 2.0*DELTAT
C      DTHALF = .5*DELTAT
C      DO 130 I = 1,NH
C      XI(I) = YI(I)*ZI(I)-YZI(I)*YZI(I)
C      XI2(I) = XZI(I)*ZI(I)+XZI(I)*YZI(I)

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ISN 0097      XI3(I) = XYI(I)*YZI(I)+YI(I)*XZI(I)
ISN 0098      XI4(I) = XI(I)*YZI(I)+XZI(I)*XYI(I)
ISN 0099      XI5(I) = XI(I)*ZI(I)-XZI(I)*XYI(I)
ISN 0100      XI6(I) = XI(I)*YI(I)-XYI(I)*XZI(I)
ISN 0101      130 DELXI = 1.0/(XI(I)*XI(I)-XYI(I)*XZI(I)-XZI(I)*XI(I))
ISN 0102      DO 154 I=1,200
C     COUNTERS FOR RUPTURE AND YIELD SUMMARY ARE SET TO ZERO
      TKRII)=0.
      DO 154 J=1,4
      KRBEAM(J,I)=0.
154 CONTINUE
      DO 155 I=1,200
      TSP(I)=0.
      DO 155 J=1,5
      EXSP(J,I)=0.
      KKSP(J,I)=0.
155 CONTINUE
      IF (RUNIN.EQ.0) GO TO 5
      CALL RC
      CALL RSIN(CASEIN,RUNIN,MSECIN)
      PRINT 5000,CASEIN,RUNIN,MSECIN
      CALL DOAIJ
      INGOLD = INGSC
      GO TO 270
5 CONTINUE
5000 FORMAT(1H0,2X,'***DATA MANAGEMENT RESTART ROUTINES INVOKED***'
1 / 10X,'REQUESTED CASE TITLE - ',A8
2 / 10X,'REQUESTED RUN NUMBER - ',I10
3 / 10X,'REQUESTED RESTART TIME - ',I10 / 1H0)
      INGSC = 0
      INGOLD = 0
      KRCONT = 0
      KPEN=0
      KKONT=0
      KPL=0
C (26)
C ZERO ARRAYS
      TIME = 0.0
      NM9 = 9*MM
      DO 140 I = 1,NM9
140 BIJ(I) = 0.0
      DO 150 I = 1,NM
      DX(I) = 0.0
      DY(I) = 0.0
      DZ(I) = 0.0
      XX(I) = 0.0
      XY(I) = 0.0
      XZ(I) = 0.0
      XL(I) = 0.0
      XM(I) = 0.0
      XN(I) = 0.0
      XIMP(I)=0.
      YIMP(I)=0.

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ISN 0145      ZINP(I)=0.
ISN 0146      DPX(I) = 0.0
ISN 0147      DPT(I) = 0.0
ISN 0148      DPZ(I) = 0.0
ISN 0149      DPL(I) = 0.0
ISN 0150      DPH(I) = 0.0
ISN 0151      DPN(I) = 0.0
ISN 0152      DPTN(I) = 0.0
ISN 0153      DQIN(I) = 0.0
ISN 0154      DRIN(I) = 0.0
ISN 0155      XACC(I)=0.0
ISN 0156      YACC(I)=0.0
ISN 0157      ZACC(I)=0.0
ISN 0158      150 CONTINUE
ISN 0159      DO 156 I=1,600
ISN 0160      KREFLAG(I)=0
ISN 0161      156 CONTINUE
ISN 0162      DO 157 I=1,NNP
ISN 0163      XINPNI(I)=0.
ISN 0164      YINPNI(I)=0.
ISN 0165      ZINPNI(I)=0.
ISN 0166      802 FORMAT(1X, 'MAIN', 4E15.6)
ISN 0167      157 CONTINUE
ISN 0168      DO 152 IKH=1,NSP
ISN 0169      IBS(IKH) = 0
ISN 0170      NN(IKH) = 0
ISN 0171      SC(IKH) = 0.0
ISN 0172      CEIK(IKH) = 0.0
ISN 0173      CEIKF(IKH) = 0.
ISN 0174      SBAR(IKH) = 0.
ISN 0175      KUN(IKH) = 0.
ISN 0176      FSPBAR(IKH) = 0.0
ISN 0177      C      EXTERNAL SPRING SUPPLY TERMS 3/79
ISN 0178      FSPOP(IKH)=0.
ISN 0179      SCP(IKH)=0.
ISN 0180      JBS(IKH)=0
ISN 0181      STEMP1(IKH)=0.
ISN 0182      STEMP2(IKH)=0.
ISN 0183      STEMP3(IKH)=0.
ISN 0184      STEMP4(IKH)=0.
ISN 0185      STEMP5(IKH)=0.
ISN 0186      152 CONTINUE
ISN 0187      DO 160 IJ = 1,NB
ISN 0188      SEIJ(IJ) = 0.0
ISN 0189      DEIJ(IJ) = 0.0
ISN 0190      KFL26(IJ) = 0
ISN 0191      KFL35(IJ) = 0
ISN 0192      FL26I(IJ)=0
ISN 0193      FL35I(IJ)=0
ISN 0194      FL35J(IJ)=0
ISN 0195      DO 160 L = 1,6
ISN 0196      SUMDF(L,IJ) = 0.0

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ISN 0197      N3(I,J,L) = 0
ISN 0198      160 VEE2(L,IJ) = 0.0
ISN 0199      DO 165 J = 1,3
ISN 0200      DO 165 K = 1,3
ISN 0201      165 VEEOD(J,K) = 0.0
              C DO INITIAL CONDITIONS
              CALL IC
ISN 0202      C DO ALL THE (AIJ) INTO DIJ
              CALL DOAIJ
ISN 0203      CALL DERIV
ISN 0204      CALL PRINT
ISN 0205      NPRINT = 1
ISN 0206      IPC = 0
ISN 0207      DO 200 I = 1,NM
ISN 0208      C PRESET OLD VALUES
              PINO(I) = 0.0
              QINO(I) = 0.0
              RINO(I) = 0.0
ISN 0209      XOLD(I) = X(I)
ISN 0210      YOLD(I) = Y(I)
ISN 0211      ZOLD(I) = Z(I)
ISN 0212      PHIOLD(I) = PHI(I)
ISN 0213      THEOLD(I) = THETA(I)
ISN 0214      PSOLD(I) = PSI(I)
ISN 0215      QOLD(I) = Q(I)
ISN 0216      ROLD(I) = R(I)
ISN 0217      UOLD(I) = U(I)
ISN 0218      VOLD(I) = V(I)
ISN 0219      WOLD(I) = W(I)
ISN 0220      XAFOLD(I) = XACF(I)
ISN 0221      YAFOLD(I) = YACF(I)
ISN 0222      ZAFOLD(I) = ZACF(I)
ISN 0223      XIMPOLD(I) = XIMPI(I)
ISN 0224      YIMPOLD(I) = YIMPI(I)
ISN 0225      ZIMPOLD(I) = ZIMPI(I)
ISN 0226      C DO 1ST STEP EULER
              OPIN(I) = DELTAT*P(I)
              OQIN(I) = DELTAT*Q(I)
              ORIN(I) = DELTAT*R(I)
              PIN(I) = DPIN(I)
              QIN(I) = DQIN(I)
              RIN(I) = DRIN(I)
              P(I) = P(I)+DELTAT*PDOT(I)
              Q(I) = Q(I)+DELTAT*QDOT(I)
              R(I) = R(I)+DELTAT*RDOT(I)
              U(I) = U(I)+DELTAT*UDOT(I)
              V(I) = V(I)+DELTAT*VDOT(I)
              W(I) = W(I)+DELTAT*WDOT(I)
              XACFI(I) = XACF(I)+DELTAT*XACFD(I)
              YACFI(I) = YACF(I)+DELTAT*YACFD(I)
              ZACFI(I) = ZACF(I)+DELTAT*ZACFD(I)
              XIMPI(I) = XIMP(I)+DELTAT*XACFI(I)
ISN 0227      XIMP(I) = XIMP(I)+DELTAT*XACFI(I)
ISN 0228      YIMP(I) = YIMP(I)+DELTAT*YACFI(I)
ISN 0229      ZIMP(I) = ZIMP(I)+DELTAT*ZACFI(I)
ISN 0230      OPIN(I) = DELTAT*P(I)
ISN 0231      OQIN(I) = DELTAT*Q(I)
ISN 0232      ORIN(I) = DELTAT*R(I)
ISN 0233      PIN(I) = DPIN(I)
ISN 0234      QIN(I) = DQIN(I)
ISN 0235      RIN(I) = DRIN(I)
ISN 0236      P(I) = P(I)+DELTAT*PDOT(I)
ISN 0237      Q(I) = Q(I)+DELTAT*QDOT(I)
ISN 0238      R(I) = R(I)+DELTAT*RDOT(I)
ISN 0239      U(I) = U(I)+DELTAT*UDOT(I)
ISN 0240      V(I) = V(I)+DELTAT*VDOT(I)
ISN 0241      W(I) = W(I)+DELTAT*WDOT(I)
ISN 0242      XACFI(I) = XACF(I)+DELTAT*XACFD(I)
ISN 0243      YACFI(I) = YACF(I)+DELTAT*YACFD(I)
ISN 0244      ZACFI(I) = ZACF(I)+DELTAT*ZACFD(I)
ISN 0245      XIMP(I) = XIMP(I)+DELTAT*XACFI(I)

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ISN 0246 YIMP(I)=YIMP(I)+DELTAT*YACF(I)
ISN 0247 ZIMP(I)=ZIMP(I)+DELTAT*ZACF(I)
ISN 0248 DX(I) = DELTAT*XDOT(I)
ISN 0249 X(I) = X(I)+DX(I)
ISN 0250 DY(I) = DELTAT*YDOT(I)
ISN 0251 Y(I) = Y(I)+DY(I)
ISN 0252 DZ(I) = DELTAT*ZDOT(I)
ISN 0253 Z(I) = Z(I)+DZ(I)
ISN 0254 PHI(I) = PHI(I) + DELTAT*PHIDOT(I)
ISN 0255 THETA(I) = THETA(I) + DELTAT*THETADOT(I)
ISN 0256 PSI(I) = PSI(I) + DELTAT*PSIDOT(I)
ISN 0257
200 CONTINUE
ISN 0258 IF(INP.EQ.0) GO TO 100
ISN 0259 DO 210 J=1,NNP
ISN 0260 XANPFO(J)=XACNPF(J)
ISN 0261 YANPFO(J)=YACNPF(J)
ISN 0262 ZANPFO(J)=ZACNPF(J)
ISN 0263 XINPPL(J)=XIMPNP(J)
ISN 0264 YINPPL(J)=YIMPNP(J)
ISN 0265 ZINPPL(J)=ZIMPNP(J)
ISN 0266 XACNPF(J)=XACNPF(J)+DELTAT*XNPF(J)
ISN 0267 YACNPF(J)=YACNPF(J)+DELTAT*YNPF(J)
ISN 0268 ZACNPF(J)=ZACNPF(J)+DELTAT*ZNPF(J)
ISN 0269 XIMPNP(J)=XIMPNP(J)+DELTAT*XACNPF(J)
ISN 0270 YIMPNP(J)=YIMPNP(J)+DELTAT*YACNPF(J)
ISN 0271 ZIMPNP(J)=ZIMPNP(J)+DELTAT*ZACNPF(J)
ISN 0272
210 CONTINUE
ISN 0273 190 TIME = TIME+DT2-DELTAT
ISN 0274 IPC = IPC+1
ISN 0275 CALL DERIV
ISN 0276 IF(IPC-IPRINT) 310,260,260
ISN 0277
260 TIME = TIME+1000 + .5
ISN 0278 IF (MSCOUT(1).LE.0 .OR. MSCOUT(1).GT.TIME) GO TO 270
ISN 0279 CALL RSCOUT(CASOUT,RUNOUT,TIME)
ISN 0280 PRINT 4000, MSCOUT(1), TIME, TIME, CASOUT, RUNOUT
ISN 0281 DO 265 I=1,4
ISN 0282 MSCOUT(I) = MSCOUT(I+1)
ISN 0283
265 MSCOUT(5) = 0
ISN 0284
4000 FORMAT(1H0,2X,'***DATA MANAGEMENT CHECKPOINT ROUTINES INVOKED***'
ISN 0285 1 / 10X,'REQUESTED TIME - ',I10 / 10X,' ACTUAL TIME - ',I10,00003440
ISN 0286 2 / 10X,' REAL TIME - ',I10E10.4 / 10X,' CASE TITLE - ',A8
ISN 0287 3 / 10X,' RUN NO. - ',I10 / 1H0)
ISN 0288
270 CALL PRINT
ISN 0289 NPRINT = 1
ISN 0290 IPC = 0
ISN 0291
310 CONTINUE
ISN 0292 C PREDICT, MOVE DOWN, AND DO DELTA'S
ISN 0293 280 DO 300 I = 1,MM
ISN 0294 T = PINO(I)+DT2*P(I)
ISN 0295 PINO(I) = PIN(I)
ISN 0296 PIN(I) = T
ISN 0297 OPIN(I) = PIN(I)-PINO(I)
ISN 0298 T = QINO(I)+DT2*Q(I)
ISN 0299
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00003090
00003100
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ISM 0297 QINO(I) = QIN(I)
ISM 0298 QIN(I) = T
ISM 0299 QQIN(I) = QIN(I)-QINO(I)
ISM 0300 T = RINO(I)+DT2*R(I)
ISM 0301 RINO(I) = RINI(I)
ISM 0302 RINI(I) = T
ISM 0303 ORIN(I) = RIN(I)-RINO(I)
ISM 0304 T = XOLD(I)+DT2*XDOT(I)
ISM 0305 XOLD(I) = X(I)
ISM 0306 X(I) = T
ISM 0307 DX(I) = X(I)-XOLD(I)
ISM 0308 T = YOLD(I)+DT2*YDOT(I)
ISM 0309 YOLD(I) = Y(I)
ISM 0310 Y(I) = T
ISM 0311 DY(I) = Y(I)-YOLD(I)
ISM 0312 T = ZOLD(I)+DT2*ZDOT(I)
ISM 0313 ZOLD(I) = Z(I)
ISM 0314 Z(I) = T
ISM 0315 DZ(I) = Z(I)-ZOLD(I)
ISM 0316 T = PHIOLD(I)+DT2*PHIDOT(I)
ISM 0317 PHIOLD(I) = PHI(I)
ISM 0318 PHI(I) = T
ISM 0319 T = THEOLD(I)+DT2*THEDOT(I)
ISM 0320 THEOLD(I) = THETA(I)
ISM 0321 THETA(I) = T
ISM 0322 T = PSOLD(I)+DT2*PSIDOT(I)
ISM 0323 PSOLD(I) = PSI(I)
ISM 0324 PSI(I) = T
ISM 0325 T = POLD(I)+DT2*PODOT(I)
ISM 0326 POLD(I) = P(I)
ISM 0327 P(I) = T
ISM 0328 T = QOLD(I)+DT2*QDOT(I)
ISM 0329 QOLD(I) = Q(I)
ISM 0330 Q(I) = T
ISM 0331 T = ROLD(I)+DT2*RDOT(I)
ISM 0332 ROLD(I) = R(I)
ISM 0333 R(I) = T
ISM 0334 T = UOLD(I)+DT2*UDOT(I)
ISM 0335 UOLD(I) = U(I)
ISM 0336 U(I) = T
ISM 0337 T = VOLD(I)+DT2*VDOT(I)
ISM 0338 VOLD(I) = V(I)
ISM 0339 V(I) = T
ISM 0340 T = WOLD(I)+DT2*WDOT(I)
ISM 0341 WOLD(I) = W(I)
ISM 0342 W(I) = T
ISM 0343 T = XAFOLD(I)+DT2*XACFD(I)
ISM 0344 XAFOLD(I) = XACF(I)
ISM 0345 XACF(I) = T
ISM 0346 T = XIMPOL(I)+DT2*XACF(I)
ISM 0347 XIMPOL(I) = XIMP(I)
ISM 0348 XIMP(I) = T
ISM 0349 T = YAFOLD(I)+DT2*YACFD(I)

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ISN 0350      YAFOLD(I)=YACF(I)
ISN 0351      YACF(I)=T
ISN 0352      T=YIMPOL(I)+DT2*YACF(I)
ISN 0353      YIMPOL(I)=YIMP(I)
ISN 0354      YIMP(I)=T
ISN 0355      T=ZAFOLD(I)+DT2*ZACFD(I)
ISN 0356      ZAFOLD(I)=ZACF(I)
ISN 0357      ZACF(I)=T
ISN 0358      T=ZIMPOL(I)+DT2*ZACF(I)
ISN 0359      ZIMPOL(I)=ZIMP(I)
ISN 0360      ZIMP(I)=T
ISN 0361      800 FORMAT(/'MAIN',2X,'I=',I5.2X,'ZAFOLD=',E15.6,2X,'ZACFD ',E15.6,
ISN 0362      1 2X,'ZACF ',E15.6,2X,'ZIMP ',E15.6,2X,'ZIMPOL=',E15.6/)
ISN 0363      801 FORMAT(/6X,'J=',I5.2X,'ZANPFO=',E15.6,2X,'ZNPFD ',E15.6,2X,
ISN 0364      1 'ZACNPF=',E15.6,2X,'ZIMPNP=',E15.6,2X,'ZIMPPL=',E15.6/)
ISN 0365      300 CONTINUE
ISN 0366      IF(1NPF.EQ.0) GO TO 400
ISN 0367      DO 410 J=1,NPF
ISN 0368      T=XANPFO(J)+DT2*XNPFD(J)
ISN 0369      XANPFO(J)=XACNPF(J)
ISN 0370      XACNPF(J)=T
ISN 0371      T=XIMPPL(J)+DT2*XACNPF(J)
ISN 0372      XIMPPL(J)=XIMPNP(J)
ISN 0373      XIMPNP(J)=T
ISN 0374      T=YANPFO(J)+DT2*YNPFD(J)
ISN 0375      YANPFO(J)=YACNPF(J)
ISN 0376      YACNPF(J)=T
ISN 0377      T=YIMPPL(J)+DT2*YACNPF(J)
ISN 0378      YIMPPL(J)=YIMPNP(J)
ISN 0379      YIMPNP(J)=T
ISN 0380      T=ZANPFO(J)+DT2*ZNPFD(J)
ISN 0381      ZANPFO(J)=ZACNPF(J)
ISN 0382      ZACNPF(J)=T
ISN 0383      T=ZIMPPL(J)+DT2*ZACNPF(J)
ISN 0384      ZIMPPL(J)=ZIMPNP(J)
ISN 0385      ZIMPNP(J)=T
ISN 0386      410 CONTINUE
ISN 0387      400 CONTINUE
ISN 0388      IF(IEER.NE.1) GO TO 420
ISN 0389      PRINT 7100
ISN 0390      7100 FORMAT(1H1 // 1X,'TERMINATION DUE TO ENERGY ERROR MESSAGE')
ISN 0391      7201 IF(IESE.NE.1) GO TO 7202
ISN 0392      PRINT 7301
ISN 0393      7301 FORMAT(/ 1X,'26. IESE=1 TOTAL STRAIN ENERGY IS NEGATIVE')
ISN 0394      7202 IF(IEPSE.NE.1) GO TO 7203
ISN 0395      PRINT 7302
ISN 0396      7302 FORMAT(/ 1X,'27. IEPSE=1 ELEMENT STRAIN ENERGY EXCEEDS NTOL2',
ISN 0397      * , VALUE')
ISN 0398      7203 IF(IEDE.NE.1) GO TO 7204
ISN 0399      PRINT 7303
ISN 0400      7303 FORMAT(/ 1X,'28. IEDE=1 TOTAL DAMPING ENERGY IS NEGATIVE')
ISN 0401      7204 IF(IEPDE.NE.1) GO TO 7205
ISN 0402      PRINT 7304
ISN 0403
ISN 0405

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ISN 0406 7304 FORMAT(/ 1X,'29. IEPDE=1 ELEMENT DAMPING ENERGY EXCEEDS NTOL2',
* , VALUE')
ISN 0407 7205 IF(IECE.NE.1) GO TO 7206
ISN 0409 PRINT 7305
ISN 0410 7305 FORMAT(/ 1X,'30. IECE=1 TOTAL CRUSHING ENERGY IS NEGATIVE')
ISN 0411 7206 IF(IEPCE.NE.1) GO TO 7207
ISN 0413 PRINT 7306
ISN 0414 7306 FORMAT(/ 1X,'31. IEPCE=1 MASS CRUSHING ENERGY EXCEEDS NTOL2',
* , VALUE')
ISN 0415 7207 IF(IEFE.NE.1) GO TO 7208
ISN 0417 PRINT 7307
ISN 0418 7307 FORMAT(/ 1X,'32. IEFE=1 TOTAL FRICTION ENERGY IS NEGATIVE')
ISN 0419 7208 IF(IEPFE.NE.1) GO TO 7209
ISN 0421 PRINT 7308
ISN 0422 7308 FORMAT(/ 1X,'33. IEPFE=1 MASS FRICTION ENERGY EXCEEDS NTOL2',
* , VALUE')
ISN 0423 7209 IF(IEDEV.NE.1) GO TO 7210
ISN 0425 PRINT 7309
ISN 0426 7309 FORMAT(/ 1X,'34. IEDEV=1 MASS DEVIATION EXCEEDS NTOL3 VALUE')
ISN 0427 7210 IF(IETOT.NE.1) GO TO 7211
ISN 0429 PRINT 7310
ISN 0430 7310 FORMAT(/ 1X,'35. IETOT=1 TOTAL ENERGY CHANGE EXCEEDS NTOL1',
* , VALUE')
ISN 0431 7211 GO TO 500
ISN 0432 420 IF(TIME-THAX) 190,190,500
ISN 0433 500 IF(KRCONT.LE.0) GO TO 4500
ISN 0435 PRINT 2000
ISN 0436 2000 FORMAT(1H1//6X,'SUMMARY OF INTERNAL BEAM YIELDING',
1 'AND RUPTURE'//18X,'BEAM',13X,'BEAM DIRECTION FOR',2X,
2 'TENSION(+) OR',4X,'TIE',6X,'IJ',3X,'I',3X,'J',3X,'M',3X,'N',
3 3X,'YIELD',6X,'RUPTURE',2X,'COMPRESSION(-)')
DO 3500 JJ=1,KRCONT
IJ = KRBEAM(1,JJ)
PRINT 3000,TKR(JJ),KRBEAM(1,JJ),IG(IJ),JG(IJ),MG(IJ),NG(IJ),
1 KRBEAM(2,JJ),KRBEAM(3,JJ),KRBEAM(4,JJ)
3500 CONTINUE
ISN 0440 3000 FORMAT(1X,F9.6,3X,I3,4(2X,I2),5X,I1,11X,I1,10X,I2)
ISN 0441 4500 IF(KKONT.LE.0) GO TO 5600
ISN 0444 PRINT 2500
ISN 0445 2500 FORMAT(1H1//6X,'SUMMARY OF EXTERNAL SPRING LOADING AND UNLOADING',
1 // 10X,'TYPES:1=INITIAL LOADING 2=MAX. LOADING 3=UNLOAD TO ZERO
2 FORCE 4=INITIATION OF RELOAD'//10X,'NOTE:SPRING RELOADS AT ZERO
3 FORCE(SEQ.1,2,3,4) OR AT FINITE FORCE VALUE(SEQ.1,2,4),
4 // 10X,'NOTE:INITIAL DEFLECTION IS FIRST IMPACT IF NYPE=1,
5 OTHERWISE IT IS POINT AT WHICH RELOADING OCCUR FOR NYPE=4'
6 //1X,'TIME(SEC)',2X,'MASS',3X,'NODE',2X,'DIRECTION',
7 2X,'TYPE',3X,'INITIAL',9X,'MAXIMUM',15X,'UNLOADED'
8 / 13X,'NO.',4X,'NO.',3X,'L=1,2,3,4X,'NO.',2X,
9'DEFLECTION',3X,'FORCE',1X,'&OR',1X,'DEFLECT',1X,'DEFLECT',
A 2X,'&',1X,'FORCE')
DO 3600 JJ=1,KKONT
PRINT 3100,TSP(JJ),KKSPI(1,JJ),KKSPI(2,JJ),KKSPI(3,JJ),KKSPI(4,JJ),
1 EXSPI(1,JJ),EXSPI(2,JJ),EXSPI(3,JJ),EXSPI(4,JJ),EXSPI(5,JJ)

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ISN 0448 3600 CONTINUE
ISN 0449 3100 FORMAT(1X,F9.6,3X,3(I2,5X),2X,I2,3X,F8.4,2X,E10.2,2(I2X,F8.4),2X,
1 E10.2)

C
C SUMMARY TABLE FOR PLASTIC HINGE
C
ISN 0450 5600 IF(KPL.LE.0) GO TO 5500
ISN 0451 PRINT 5610
ISN 0452 5610 FORMAT(//,1X,'SUMMARY OF PLASTIC HINGE FORMATIONS')
ISN 0453 PRINT 5620
ISN 0454 5620 FORMAT(/,17X,'BEAM',9X,'BEAM END',/4X,'TIME',5X,
ISN 0455 1 'IJ I J M N',3X,'MASS NO. DIRECTION')
ISN 0456 DO 5630 K=1,KPL
ISN 0457 TIMEPL=TPL(K)
ISN 0458 IJ=BPL(K,1)
ISN 0459 I=IG(IJ)
ISN 0460 J=JG(IJ)
ISN 0461 M=MG(IJ)
ISN 0462 N=NG(IJ)
ISN 0463 MAXPB=BPL(K,3)
ISN 0464 NOIREC=BPL(K,2)
ISN 0465 PRINT 5640,TIMEPL,IJ,I,J,M,N,MAXPB,NOIREC
ISN 0466 5640 FORMAT(1X,F9.6,2X,5I3,5X,I3,9X,I2)
ISN 0467 5630 CONTINUE
ISN 0468 5500 IF (KPB.LE.0) GO TO 6000
ISN 0470 PRINT 5501
ISN 0471 5501 FORMAT(1H,7X,'CONTROL VOLUME PENETRATIONS' //)
ISN 0472 5502 PRINT 5502
ISN 0473 5502 FORMAT(1H,13X,'TIME',10X,'MASS' /)
ISN 0474 PRINT 5503,(TPEN(K),IPEN(K),K=1,KPB)
ISN 0475 5503 FORMAT(1H,10X,F10.5,110)
C****PRINT ENERGY SUMMARY
ISN 0476 6000 PRINT 9
ISN 0477 9 FORMAT(1H1 // 1X,'SUMMARY OF ENERGY DISTRIBUTION' ///)
ISN 0478 PRINT 10
ISN 0479 10 FORMAT(10X,'PERCENT',2X,'TOTAL',14X,'OF',4(I6X,'OF'),15X,'OF',11X,
1 10X,'MAXIMUM',3X,'TOTAL',14X,'OF',4(I6X,'OF'),15X,'OF',11X,
2 'ENERGY',2X,'SYSTEM',3X,'KINETIC',2X,'CURRENT',1X,
3 'POTENTIAL',1X,'CURRENT',2X,'STRAIN',3X,'CURRENT',2X,
4 'DAMPING',2X,'CURRENT',1X,'CRUSHING',2X,'CURRENT',1X,
5 'FRICTION',1X,'CURRENT' / 2X,'TIME',3X,'DEVIATION',1X,'ENERGY',
6 5(3X,'ENERGY',4X,'TOTAL'),3X,'ENERGY',3X,'TOTAL' /)
C DTP = IPRINT*DELTAT
C TIME = -DTP
ISN 0480 INGO = INGO + 1
ISN 0481 DO 20 I = INGO,INGSC
C TIME = TIME+DTP
C ITIME = TIME*1000 + .5
C IF (ITIME .LT. MSECIN) GO TO 20
ETOT = 0.0
DO 30 J = 1,6
ISN 0482 30 ETOT = ETOT+ENGSHY(J,I)
ISN 0483
ISN 0484 PCTT0 = ETOT/ETOTTO
ISN 0485

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DO 40 J = 1,6
40 PERCNT(J) = ENGSHY(J,I)/ETOT
PRINT 60, ETIME(I),DEV(I),PCTT0,((ENGSHY(J,I),PERCNT(J),J=1,6)
60 FORMAT(1X,F6.5,2X,F9.6,2PF7.2,6(1PE11.3,2PF7.2))
20 CONTINUE
TNAX=TIME
CALL PREPLT(TPRINT,N1,N1P,NB,NBP,NDRI,MSECIN)
GO TO 1
1000 CONTINUE
STOP
END

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ISN 0486
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LEVEL 21.8 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.03.31

LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

COMPILER OPTIONS - NAME= MAIN,OPT=82,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,IO,XREF

C DATA SET D2334ACCEL AT LEVEL 005 AS OF 06/25/79

C SUBROUTINE ACCELTHASDEX,X1,YC,ZC,A1,A2,A3,TIME,NPTSP,NPTS)

C REVISED 10-13-77

C IMPLICIT REAL*8 (A-H,O-Z)

C COMMON/INAC/ ACCEL(300),TIM(300),INDEX(50,2),JAY(50,2),KOUNT

C COMMON/INDEAC/ NACC

C ISAV = 1

C TT = TIME

C 6105 DO 6100 I=ISAV,NACC

C I1 = I

C 6200 FORMAT(2I5)

C IF(INDEX(I,1).EQ.MASDEX) GO TO 6101

C 6100 CONTINUE

C RETURN

C 6101 ISAV = I1 + 1

C JSTRT = JAY(I1,1)

C NPTS = JAY(I1,2)

C NPTSP=NPTSP+NPTS

C JSTOP=NPTS

C K=NPTSP+1

C 6102 K = K+1

C 6201 FORMAT(5I5)

C IF(TT.GE.TIM(K-1).AND.TT.LT.TIM(K)) GO TO 6103

C IF(K.NE.JSTOP) GO TO 6102

C IREF=K

C NPTSP=NPTS

C GO TO 6104

C 6103 IREF = K-1

C NPTSP=NPTS

C 6104 CALL INTERP(IREF,TT,ACOUT)

C IDER = INDEX(I,2)

C GO TO (6111,6112,6113,6114,6115,6116),IDER

C PP2NT 6106,IDER

C 6106 FORMAT(1X,'1. IDER OUT OF RANGE,VALUE = ',I2)

C RETURN

C 6111 X1 = ACOUT

C GO TO 6107

C 6112 YC = ACOUT

C GO TO 6107

C 6113

C 6114

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ISN 0042
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ISN 0049
ISN 0051
ISN 0052

6113 ZC = ACOUT
60 TO 6107
6114 A1 = ACOUT
60 TO 6107
6115 A2 = ACOUT
60 TO 6107
6116 A3 = ACOUT
6107 IF(ISAV.GT.NACC) RETURN
60 TO 6105
END

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

COMPILER OPTIONS	- NAME=	MAIN,OPT=02,LINECNT=55,SIZE=0600K,
C	SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NODEDIT,ID,XREF	
C	DATA SET D2334CFORC AT LEVEL 004 AS OF 06/25/79	00000010
C	DATA SET D2332VCF AT LEVEL 001 AS OF 01/27/78	00000020
C	DATA SET D2332VCFOR AT LEVEL 001 AS OF 09/06/77	00000030
C	DATA SET D2332CF AT LEVEL 009 AS OF 09/02/77	00000040
	SUBROUTINE CFORCE	00000050
C	IMPLICIT REAL*8 (A-H,O-Z)	00000060
	REAL*8 KUN	00000070
	INTEGER*4 TITLE(40)	00000080
	INTEGER*2 NL,NL,IBS,JBS	00000090
	INTEGER*2 MTEMP(40)	00000100
	INTEGER*2 IJPR,IG,JG	00000110
	INTEGER*2 II(40),KK(40),MM(40),INP(50),MNP(50),MG(150),NG(150)	00000120
	DIMENSION VAI(3),VADOT(3),PBAR(3),XLNGTH(3),IISP(3),XXLBAR(3),	00000130
	1 FSP(3,3),XVOC(3,3),C4(3),C5(3),S(3),SDOT(3),PL(3,3)	00000140
	DIMENSION DPORIN(4),DXYZ(3),DXYZPR(3),TERM(6)	00000150
	DIMENSION XVOCSL(3,3),DVC3(3)	00000160
	DIMENSION FSPB(3,3),FSPF(3,3),XVOCB(3,3),XVOCF(3,3),TERMF(6)	00000170
	DIMENSION DVC(3),DVC1(3),DVC2(3),DVC3(3),C5SL(3),C5SLT(3),	00000180
	1 VEEDT(3),VEEC3(3),VEEC3(3)	00000190
	DIMENSION TT(3),XXC(6),RTERM(6)	00000200
	DIMENSION RXI(50),RY(50),RZ(50),XNPDP(50),YNPDP(50),ZNPDP(50)	00000210
	DIMENSION LSTEST(3)	00000220
	DIMENSION ETERM(3),ETB(3),ETF(3)	00000230
	COMMON/CFIC/ SINBET,COSBET,ABETA(9)	00000240
	COMMON/CFIR/ SIFL(40),SAFL(40),SBFL(40),SFFL(40),XXEFL(40)	00000250
	COMMON/CFPR/ FSPRNG(40,8),DELGI(40)	00000260
	COMMON/INCF/ SAI(40),SBI(40),SFI(40),SI(40),XMI(40),XKE(40),	00000270
	1 XNAXI(40),FSPOF(40),FSPOI(40),6FLEX(40),CDAMP(40),PLOMT	00000280
	COMMON/INPR/ NDRI,NSP	00000290
	COMMON/INCFIC/ BETA	00000300
	COMMON/INIDCP/ YDPI(80)	00000310
	COMMON/MACF/IBSI(40),FSPOI(40),SCP(40),JBS(40),	00000320
	1 KKSPL(5,200),EXSP(5,200),TSP(200),STEMP1(40),STEMP2(40),	00000330
	2 STEMP3(40),STEMP4(40),STEMP5(40),KKONT	00000340
	COMMON/MACFIN/ THAX,IPRINT	00000350
	COMMON/MCFIII/ SYHFLG	00000360
	COMMON/NP0012/ MG,NG,INP,MNP	00000370
	COMMON/NP0112/ II,KK,MM	00000380
	COMMON/NP0014/ NNP	00000390
	COMMON/NP0018/ RX,RY,RZ	00000400


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ISN 0033      COMMON/MP02R6/ XNPDP, YNPDP, ZNPDP
ISN 0034      COMMON/CONALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),
1 Y(81),Z(81),AI(9),AJ(9),AK(9),AL(9),AM(9),AN(9),AO(9),AP(9),AQ(9),
2 YI(80),ZI(80),XI(80),YI(80),ZI(80),YI(80),ZI(80),YI(80),ZI(80),
3 DRI(150),DAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80),
4 PDI(80),QDI(80),RDI(80),UDI(80),VDI(80),WDI(80),XDI(80),
5 YDI(80),ZDI(80),PHI(80),THETA(80),PSI(80),TIME,DELTA,
6 XAC(80),YAC(80),ZAC(80),AIDOT(9),
7 PHII(150),THEII(150),PSII(150),SUMDF(6,150),TITLE,
8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9 DPIN(81),DQIN(81),ORIN(81),SEIJ(150),DEIJ(150),CEIK(40),
A CEIK(40),
B SBAR(40),KUN(40),MAXM,MAXIGS,MAXTBL,
C NF,NB,I,J,IG(150),JG(150),
D NI(900),NN(40),IJPR(150)
EQUIVALENCE (C4(1),DXYZ(1)),(C5(1),DXYZPR(1))
SIGN(X1,X2) = DSIGN(X1,X2)
SORT(X) = DSORT(X)
AMAXI(X,Y) = DMAXI(X,Y)
ABS(X) = DABS(X)
ONE = 1.
VA(1) = X(I)
VA(2) = Y(I)
VA(3) = Z(I)
VADOT(1) = XDOT(I)
VADOT(2) = YDOT(I)
VADOT(3) = ZDOT(I)
PSAR(1) = P(I)
PSAR(2) = Q(I)
PSAR(3) = R(I)

C      DETERMINE WHAT NODE POINTS M MUST BE ANALYZED FOR THIS
C      MASS POINT I.
C      COUNT = 0
C      DO 10 IKM=1,NSP
C      C ZERO GROUND DEFL. AT TIME = 0.
C      IF (TIME.NE.0.) GO TO 25
C      DELG(IKM) = 0.
C      25 IF (I.NE.II(IKM)) GO TO 10
C      IF (KOUNT.NE.0) GO TO 11
C      KOUNT = 1
C      MTEMP(KOUNT) = MM(IKM)
C      GO TO 10
C      11 DO 13 JJ=1,KOUNT
C      IF (MTEMP(JJ).EQ.MM(IKM)) GO TO 10
C      13 CONTINUE
C      KOUNT = KOUNT+1
C      MTEMP(KOUNT) = MM(IKM)
C      10 CONTINUE

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ISN 0161

911 CONTINUE
910 CONTINUE
C LOOP 6
C CALCULATE VC3, C4, C5 IN GROUND AND SLOPE AXES
DVR1 = AI(1)*RRX+AI(4)*RRY+AI(7)*RRZ
DVR2 = AI(3)*RRX+AI(6)*RRY+AI(9)*RRZ
DVR3 = AIDOT(1)*RRX+AIDOT(4)*RRY+AIDOT(7)*RRZ
DVR4 = AIDOT(3)*RRX+AIDOT(6)*RRY+AIDOT(9)*RRZ
DO 920 K = 1,3
IF (IISP(K)) 925,920,925
925 ISUB1 = 3*(K-2)
DVC1(K) = AI(ISUB1) * XXLBAR(K)
ISUB3 = 3*(K)
DVC3(K) = AI(ISUB3) * XXLBAR(K)
DVC5(K) = SINBET * DVC1(K) + COSBET * DVC3(K)
VC1 = VA(1) + DVC1(K)+DVR1
VC3 = VA(3) + DVC3(K)+DVR3
VCSL3 = SINBET * VC1 + COSBET * VC3
DVC01 = AIDOT(ISUB1) * XXLBAR(K)
DVC03 = AIDOT(ISUB3) * XXLBAR(K)
DVC503 = SINBET * DVC01 + COSBET * DVC03
VCD1 = VADOT(1) + DVC01+DVRD1
VCD3 = VADOT(3) + DVC03+DVRD3
VCS03 = SINBET * VCD1 + COSBET * VCD3
VEEC3(K) = VC3
VEEC5(K) = VCSL3
IF (DVC3(K)) 927,926,927
926 C4(K) = 0.
C5(K) = 0.
GO TO 928
927 C4(K) = VC3/DVC3(K)
C5(K) = (DVC3(K) * VCD3 - VC3 * DVC03)/(DVC3(K) * DVC3(K))
928 IF (DVC5(K)) 930,929,930
929 C4SL(K) = 0.
C5SL(K) = 0.
GO TO 920
930 C4SL(K) = VCSL3/DVC5(K)
C5SL(K) = (DVC5(K) * VCSL3 - VCSL3 * DVC503)/(DVC5(K) * DVC5(K))
920 CONTINUE
C LOOP H
C CALCULATE X COORD OF SPRING INTERSECTION PT TO SEE IF LEVEL OR
SLOPE IS USED.
DO 30 K = 1,3
IF (IISP(K)) 35,30,35
35 IF (VEEC3(K)) 36,36,40
36 IF (VEEC5(K)) 30,30,40
40 VCINT(K) = VA(1) + DVC1(K) * (1-C4(K))+DVR1
IF(DVC3(K).LE.0.) VCINT(K) = 1000.D0
THIS TAKES CARE OF HORIZONTAL AND UPWARD POINTING SPRINGS
ISUB = 3*(K-1)
BARL = XXLBAR(K)
SUM = 0.0
SUMD = 0.0

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ISN 0162
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ISN 0166

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ISN 0206
ISN 0207
ISN 0208
ISN 0209
ISN 0210
ISN 0211

C LOOP J1 CALCULATE ALL DVC & DVCDOOT IN GROUND SYSTEM
DO 50 J=1,3
  ISUB = ISUB + 1
  DVC(J) = AI(ISUB) * BARL
  DVCDOOT(J) = AIDOT(ISUB) * BARL
50 CONTINUE
C LOOP J2 CALCULATE DVC & DVCDOOT IN SLOPE AXES IF APPROPRIATE. FORM
C
  SUM & SUMD FOR SK & SKOOT.
  DO 52 J=1,3
    IF (BETA) 54,56,54
  54 IF (VCINT(K)) 56,54,58
  58 SUM1 = 0.
  SUM2 = 0.
  JSUB = 3*(J-1)
  DO 53 L=1,3
    JSUB = JSUB + 1
    SUM1 = SUM1 + ABETA(JSUB) * DVC(L)
    SUM2 = SUM2 + ABETA(JSUB) * DVCDOOT(L)
  53 CONTINUE
  DVEEC = SUM1
  DVEECD = SUM2
  C4BAR = C4SL(K)
  C5BAR = C5SL(K)
  LSTEST(K) = 1.
  GO TO 59
  56 DVEEC = DVC(J)
  DVEECD = DVCDOOT(J)
  C4BAR = C4(K)
  C5BAR = C5(K)
  LSTEST(K) = 0
  59 DVP = C4BAR * DVEEC
  DDP = C4BAR * DVEECD + C5BAR * DVEEC
  SUM = SUM + DVP * DVP
  SUMD = SUMD + DVP * DDP
52 CONTINUE
SK = SQR(SUM)
S(K) = SK
SDOT(K) = SUMD/SK
C GET LENGTH
DO 822 IKM=1,NSP
  IF(I.EQ.II(IKM).AND.K.EQ.KK(IKM).AND.M.EQ.MM(IKM)) GO TO 824
822 CONTINUE
824 SC(IKM) = SK
  IF(BARL) 55,60,60
  55 T = -BARL-SK*DELG(IKM)
  T = -T
  GO TO 65
  60 T = BARL-SK*DELG(IKM)
  65 XLNGTHIK = T
30 CONTINUE
  PL(1,1) = -SDOT(1)*SIGN(ONE,XXLBAR(1))
  PL(2,2) = -SDOT(2)*SIGN(ONE,XXLBAR(2))
  PL(3,3) = -SDOT(3)*SIGN(ONE,XXLBAR(3))
0002000
0002010
0002020
0002030
0002040
0002050
0002060
0002070
0002080
0002090
0002100
0002110
0002120
0002130
0002140
0002150
0002160
0002170
0002180
0002190
0002200
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0002240
0002250
0002260
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0002470
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0002490
0002500
0002510
0002520

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ISN 0212      PL(1,1) = 0.
ISN 0213      PL(2,2) = 0.
ISN 0214      PL(3,3) = 0.
ISN 0215      PL(2,1) = PBAR(3)*XLNGTH(1)
ISN 0216      PL(3,1) = -PBAR(2)*XLNGTH(1)
ISN 0217      PL(1,2) = -PBAR(3)*XLNGTH(2)
ISN 0218      PL(3,2) = PBAR(1)*XLNGTH(2)
ISN 0219      PL(1,3) = PBAR(2)*XLNGTH(3)
ISN 0220      PL(2,3) = -PBAR(1)*XLNGTH(3)
ISN 0221      IF(M.EQ.0) GO TO 76
ISN 0223      TT(1) = -PBAR(3)*RRY+PBAR(2)*RRZ
ISN 0224      TT(2) = PBAR(3)*RRX-PBAR(1)*RRZ
ISN 0225      TT(3) = -PBAR(2)*RRX+PBAR(1)*RRY
ISN 0226      DO 77 K=1,3
ISN 0227      DO 78 JJ=1,3
ISN 0228      PL(JJ,K) = PL(JJ,K)+TT(JJ)
ISN 0229      78 CONTINUE
ISN 0230      77 CONTINUE
C LOOP K
ISN 0231      76 DO 75 JJ = 1,3
ISN 0232      ISUB = JJ-3
ISN 0233      VAD = VADOT(JJ)
C LOOP L
ISN 0234      DO 80 K = 1,3
ISN 0235      IF(IISP(K)) 85,80,85
ISN 0236      85 IF(VEEC3(K)) 81,81,90
ISN 0237      81 IF(VEEC3(K)) 80,80,90
ISN 0238      90 SUM = 0.0
C LOOP H
ISN 0239      DO 95 L = 1,3
ISN 0240      ISUB = ISUB+3
ISN 0241      95 SUM = SUM+AI(ISUB)*PL(L,K)
ISN 0242      VEEDOT(JJ,K) = VAD+SUM
ISN 0243      80 CONTINUE
ISN 0244      75 CONTINUE
C CALCULATE CONTACT POINT VELOCITIES ON SLOPE.
ISN 0245      IF (BETA) 98,96,98
ISN 0246      98 DO 101 K=1,3
ISN 0247      IF (VCINT(K)) 101,101,94
ISN 0248      94 DO 97 J=1,3
ISN 0249      SUM = 0.
ISN 0250      JSUB = 3*(J-1)
ISN 0251      DO 99 L=1,3
ISN 0252      JSUB = JSUB + 1
ISN 0253      SUM = SUM + ABETA(JSUB) * VEEDOT(L,K)
ISN 0254      99 CONTINUE
ISN 0255      VEEDT(J) = SUM
ISN 0256      97 CONTINUE
ISN 0257      DO 102 JJ=1,3
ISN 0258      VEEDOT(JJ,K) = VEEDT(JJ)
ISN 0259      102 CONTINUE
ISN 0260      101 CONTINUE
C LOOP N

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ISN 0261      % DO 105 K = 1,3
ISN 0262      IF(IISPI(K)) 110,105,110
ISN 0263      110 IF(VEEC3(K)) 111,111,115
ISN 0264      111 IF(VEEC3(K)) 105,105,115
ISN 0265      115 SK = 5(K)

C
C GET SPRING NUMBER TO USE INPUT DATA SUBSCRIPTED BY IKM.
C
C DO 1002 IKM=1,NSP
C   IF(I.EQ.II(IKM).AND.K.EQ.KK(IKM).AND.M.EQ.MM(IKM)) GO TO 1003
C   1002 CONTINUE
C   1003 SC(IKM) = SK
C
C CALCULATION OF FSPO.
C
C   IF(SDOT(K).LT.0.) GO TO 140
C   IF(SK.LT.SBAR(IKM)) GO TO 140
C
C LOADING PATH.
C
C   IF(IFS(IKM).NE.0) GO TO 125
C   IF(SK.GT.SFFL(IKM)) GO TO 130
C
C NORMAL FSPO CALCULATIONS FOR LOADING CASE.
C
C   FSPO = FSPOF(IKM)
C   IF(SK.GE.SBFL(IKM)) GO TO 150
C   IF(SK.GE.SAFL(IKM)) GO TO 148
C   FSPO = FSPOI(IKM)
C   IF(SK.GE.SIFL(IKM)) GO TO 150
C   FSPO = FSPO*SK/SIFL(IKM)
C   GO TO 150
C   148 FSPO = FSPOI(IKM)+(SK-SAFL(IKM))*(FSPO-FSPOI(IKM))/
C     1 (SBFL(IKM)-SAFL(IKM))
C   GO TO 150
C
C FSPO CALCULATIONS ON BOTTOMING SPRING.
C
C   130 IBS(IKM) = 1
C   125 FSPO = FSPOF(IKM)+XKEFL(IKM)*(SK-SFFL(IKM))
C   150 FSPBAR(IKM) = FSPO
C   SBAR(IKM) = SK
C   NN(IKM) = 0
C   GO TO 155
C
C UNLOADING AND RELOADING PATHS.
C
C   140 IF(NN(IKM).NE.0) GO TO 135
C   IF(IFS(IKM).EQ.0) GO TO 145
C
C UNLOADING AND RELOADING ON BOTTOMING SPRING.
C
C   KUN(IKM) = XKE(IKM)

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15N 0302      GO TO 146
C
C  NORMAL UNLOADING AND RELOADING.
C
145 IF(SK.LE.SAFL(IKM)) GO TO 147
KUN(IKM) = (FSPO(IKM)-FSPO(IKM))/(SB(IKM)-SA(IKM))
IF(KUN(IKM).LT.(FSPBAR(IKM)/SBAR(IKM))) GO TO 147
GO TO 146
147 KUN(IKM) = FSPO(IKM)/SI(IKM)
146 NK(IKM) = 1
135 FSPO = FSPBAR(IKM)-(SBAR(IKM)-SK)*KUN(IKM)
155 FSPO=CDAMP(IKM)*SDOT(K)
IF(SDOT(K).LT. 0) FSPO=0.
FSPO=FSPO+FSPO
C  NOW IF FSPO IS NEGATIVE, SET IT EQUAL TO ZERO
IF(FSPO.LT.0.) FSPO=0.
FSPOF5=10.*AMAX1(FSPOF(IKM),FSPOI(IKM))
CUTOFF FORCE=10*MAX OF FSPOF,FSPOI
IF(FSPO.GT.FSPOF5) FSPO=FSPOF5
IF(SDOT(K).LT.0.) GO TO 1020
JBS=1 INITIAL LOADING OCCURS
JBS=2 MAX. LOAD AND/OR DEFLECTION OCCUR
JBS=3 UNLOAD TO ZERO FORCE
JBS=4 RELOAD OCCURS
JBS=5 MAX. LOAD DUE TO DAMPING OCCURS
IF(JBS(IKM).EQ.5) GO TO 1040
INITIAL LOADING SUMMARY
IF(JBS(IKM).EQ.2) GO TO 1030
IF(SCPI(IKM).GT.0.0 .AND.FSPO.NE.0.) GO TO 1012
IF(SCPI(IKM).GT.0.) GO TO 1030
IF(SC(IKM).LE.0.) GO TO 1030
IF (JBS(IKM).GT.0) GO TO 1009
KKONT=KKONT+1
TSPI(KKONT)=TIME
EXSP(1,KKONT)=SK
STEP(1,IKM)=SK
KKSP(1,KKONT)=II(IKM)
KKSP(2,KKONT)=HH(IKM)
KKSP(3,KKONT)=KK(IKM)
KKSP(4,KKONT)=1
1009 IF(JBS(IKM).GT.3) GO TO 1008
JBS(IKM)=1
GO TO 1040
1008 IF(FSPO.GT.0.0 .AND.SK.GT.SCPI(IKM)) GO TO 1031
GO TO 1040
C  MAXIMUM LOADING SUMMARY
1012 IF(JBS(IKM).EQ.3) GO TO 1030
IF(FSPO(IKM).LT.FSPO) GO TO 1040
IF(JBS(IKM).EQ.4) JBS(IKM)=5
IF(JBS(IKM).EQ.1) JBS(IKM)=5
1010 IF(JBS(IKM).EQ.2) GO TO 1040
KKONT=KKONT+1
TSPI(KKONT)=TIME
00003590
00003600
00003610
00003620
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00003970
00003980
00003990
00004000
00004010
00004020
00004030
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00004090
00004100
00004110

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ISN 0362      EXSPI1,KKONT)=STEMP1(IKH)
ISN 0363      EXSPI2,KKONT)=FSPOI(IKH)
ISN 0364      EXSPI3,KKONT)=SCP(IKH)
ISN 0365      EXSPI4,KKONT)=STEMP3(IKH)
ISN 0366      EXSPI5,KKONT)=STEMP2(IKH)
ISN 0367      STEMP4(IKH)=FSPOI(IKH)
ISN 0368      STEMP5(IKH)=SCP(IKH)
ISN 0369      KKSPI1,KKONT)=II(IKH)
ISN 0370      KKSPI2,KKONT)=MM(IKH)
ISN 0371      KKSPI3,KKONT)=KK(IKH)
ISN 0372      KKSPI4,KKONT)=2
ISN 0373      IF(FSPD.EQ.0.) GO TO 1013
ISN 0375      IF(JBS(IKH).NE.5) GO TO 1013
ISN 0377      GO TO 1040
ISN 0378      1013 JBS(IKH)=2
ISN 0379      GO TO 1040
ISN 0380      C      UNLOADING SUMMARY
ISN 0381      1020 IF(FSPOI(IKH).GT.FSPO .AND.FSPO.NE.0.0 .AND.SK.LT.SCP(IKH))
ISN 0382      1 GO TO 1010
ISN 0383      IF(FSPO.NE.0.) GO TO 1040
ISN 0384      IF(FSPOI(IKH).LT.FSPO) GO TO 1040
ISN 0385      IF(JBS(IKH).EQ.3) GO TO 1040
ISN 0386      KKONT=KKONT+1
ISN 0387      TSPI(KKONT)=TIME
ISN 0388      EXSPI1,KKONT)=STEMP1(IKH)
ISN 0389      EXSPI2,KKONT)=STEMP4(IKH)
ISN 0390      EXSPI3,KKONT)=STEMP5(IKH)
ISN 0391      EXSPI4,KKONT)=SK
ISN 0392      EXSPI5,KKONT)=FSPO
ISN 0393      STEMP2(IKH)=FSPO
ISN 0394      STEMP3(IKH)=SK
ISN 0395      KKSPI1,KKONT)=II(IKH)
ISN 0396      KKSPI2,KKONT)=MM(IKH)
ISN 0397      KKSPI3,KKONT)=KK(IKH)
ISN 0398      KKSPI4,KKONT)=3
ISN 0399      JBS(IKH)=3
ISN 0400      GO TO 1040
ISN 0401      C      RELOADING SUMMARY
ISN 0402      1030 IF(JBS(IKH).EQ.2 .AND.FSPOI(IKH).NE.0.0 .AND.FSPO.GT.FSPOI(IKH))
ISN 0403      1 GO TO 1031
ISN 0404      IF(JBS(IKH).EQ.1) GO TO 1040
ISN 0405      IF(JBS(IKH).EQ.4) GO TO 1040
ISN 0406      IF(SK.LT.STEMP3(IKH)) GO TO 1040
ISN 0407      IF(FSPOI(IKH).NE.0.0 .AND.FSPO.LE.FSPOI(IKH)) GO TO 1040
ISN 0408      1031 KKONT=KKONT+1
ISN 0409      TSPI(KKONT)=TIME
ISN 0410      EXSPI1,KKONT)=SK
ISN 0411      EXSPI2,KKONT)=STEMP4(IKH)
ISN 0412      EXSPI3,KKONT)=STEMP5(IKH)
ISN 0413      IF(JBS(IKH).EQ.2) GO TO 1032
ISN 0414      EXSPI4,KKONT)=STEMP3(IKH)
ISN 0415      EXSPI5,KKONT)=STEMP2(IKH)
ISN 0416      GO TO 1033
ISN 0417
ISN 0418
ISN 0419
ISN 0420
ISN 0421
ISN 0422
00004120
00004130
00004140
00004150
00004160
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00004600
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00004620
00004630
00004640

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ISN 0423      1032 EXSPI(4,KKONT)=SK
ISN 0424      EXSPI(5,KKONT)=FSPO
ISN 0425      STEMP2(IKM)=FSPO
ISN 0426      STEMP3(IKM)=SK
ISN 0427      1033 STEMP1(IKM)=SK
ISN 0428      KKSPI(1,KKONT)=II(IKM)
ISN 0429      KKSPI(2,KKONT)=HH(IKM)
ISN 0430      KKSPI(3,KKONT)=KK(IKM)
ISN 0431      KKSPI(4,KKONT)=4
ISN 0432      JBS(IKM)=4
ISN 0433      1040 SCPI(IKM)=SK
ISN 0434      FSPOP(IKM)=FSPO
ISN 0435      OLDEL6 = DELG(IKM)
ISN 0436      DELG(IKM) = FSPO*GFLEX(IKM)
ISN 0437      DELG(IKM) = AMAX1(OLDEL6,DELG(IKM))
ISN 0438      FSPRNG(IKM,1) = FSPO
ISN 0439      FSPRNG(IKM,8)=FSPO
ISN 0440      FFLOW = XMAX(IKM)
ISN 0441      IF(TIME-GE.PLOMT) FFLOW=0.
ISN 0443      C CHECK TO SEE IF SPRING IS ON SLOPE OR BETA = 0.
ISN 0444      IF(VCINT(K)) 191,191,180
ISN 0446      180 IF(BETA.EQ.0.) GO TO 191
ISN 0447      C GET 3 COMPONENTS OF FSPO IN GROUND AXES
ISN 0448      XVOC(1,K) = AI(3*K-2)*FSPO
ISN 0449      XVOC(2,K) = AI(3*K-1)*FSPO
ISN 0450      XVOC(3,K) = AI(3*K)*FSPO
ISN 0451      XVOC(1,K) = XVOC(1,K)*SIGNONE,XXLBAR(K))
ISN 0452      XVOC(2,K) = XVOC(2,K)*SIGNONE,XXLBAR(K))
ISN 0453      XVOC(3,K) = XVOC(3,K)*SIGNONE,XXLBAR(K))
ISN 0454      C CONVERT TO SLOPE AXES,GETTING Z COMPONENT ONLY
ISN 0455      XVOCSL(3,K) = SINBET*XVOC(1,K)+COSBET*XVOC(3,K)
ISN 0456      C CALCULATE X AND Y COMPONENTS IN SLOPE AXES FROM GROUND FRICTION
ISN 0457      C AND VELOCITY DIRECTION
ISN 0458      V1 = VEEDOT(1,K)
ISN 0459      V2 = VEEDOT(2,K)
ISN 0460      VBB = SQRT(V1*V1+V2*V2)
ISN 0461      IF(VBB) 183,183,182
ISN 0462      183 VX=0.
ISN 0463      GO TO 184
ISN 0464      182 VX = XMU(IKM)*XVOCSL(3,K)/VBB+FFLOW/VBB
ISN 0465      184 XVOCSL(1,K) = VX*VEEDOT(1,K)
ISN 0466      XVOCSL(2,K) = VX*VEEDOT(2,K)
ISN 0467      IF(SYMFLE.NE.0.AND.YDP(1).EQ.0.) XVOCSL(2,K) = 0.
ISN 0468      FSPRNG(IKM,2) = XVOCSL(1,K)
ISN 0469      FSPRNG(IKM,3) = XVOCSL(2,K)
ISN 0470      FSPRNG(IKM,4) = XVOCSL(3,K)
ISN 0471      C NOW TRANSFORM BACK TO GROUND AXES TO REJOIN BASIC CODING
ISN 0472      C FROM HERE ON SEPARATE LOADS NORMAL TO SURFACE AND FRICTION LOADS
ISN 0473      C TO CALCULATE CRUSHING ENERGY AND FRICTION ENERGY
ISN 0474      181 XVOCB(1,K) = SINBET*XVOCSL(3,K)
ISN 0475      XVOCB(2,K) = 0.
ISN 0476      XVOCB(3,K) = COSBET*XVOCSL(3,K)

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ISN 0470      XVOCF(1,K) = COSBET*XVOCSL(1,K)
ISN 0471      XVOCF(2,K) = XVOCSL(2,K)
ISN 0472      XVOCF(3,K) = -SINBET*XVOCSL(1,K)
ISN 0473      GO TO 210

C (15A)
ISN 0474      191 VX = AI(3*K)*FSP0
ISN 0475      VX = VX*SIGNONE,XXLBAR(K))
ISN 0476      XVOC(3,K) = VX
ISN 0477      V1 = VEEDOT(1,K)
ISN 0478      V2 = VEEDOT(2,K)
ISN 0479      VBB = SQRT(V1*V1+V2*V2)
ISN 0480      IF(VBB) 201,201,200
ISN 0481      201 VX=0.
ISN 0482      GO TO 202
ISN 0483      200 VX = XMU(IKM)*VX/VBB+FPLOW/VBB
ISN 0484      202 XVOCB(1,K) = 0.
ISN 0485      XVOCB(2,K) = 0.
ISN 0486      XVOCB(3,K) = XVOC(3,K)
ISN 0487      XVOCF(3,K) = 0.
ISN 0488      XVOCF(1,K) = VX*VEEDOT(1,K)
ISN 0489      XVOCF(2,K) = VX*VEEDOT(2,K)
ISN 0490      IF(SYHFLG.NE.0.AND.YDPI(I).EQ.0.) XVOCF(2,K) = 0.
ISN 0491      FSPRG(IKM,2) = XVOCF(1,K)
ISN 0492      FSPRG(IKM,3) = XVOCF(2,K)
ISN 0493      FSPRG(IKM,4) = XVOCB(3,K)
ISN 0494      210 IF(BARL) 355,360,360
ISN 0495      355 T = -BARL-SK*DELG(IKM)
ISN 0496      T = -T
ISN 0497      GO TO 365
ISN 0498      360 T = BARL-SK*DELG(IKM)
ISN 0499      365 XLNGTH(K) = T
ISN 0500      IS = 0
ISN 0501      C LOOP Q
ISN 0502      DO 220 J = 1,3
ISN 0503      SUMB = 0.
ISN 0504      SUMF = 0.
ISN 0505      C LOOP R
ISN 0506      DO 230 L = 1,3
ISN 0507      IS = IS+1
ISN 0508      SUMB = SUMB-AI(IS)*XVOCB(L,K)
ISN 0509      230 SUMF = SUMF-AI(IS)*XVOCF(L,K)
ISN 0510      FSPB(J,K) = SUMB
ISN 0511      FSPF(J,K) = SUMF
ISN 0512      FSP(J,K) = SUMB+SUMF
ISN 0513      FSPRG(IKM,(J+4)) = FSP(J,K)
ISN 0514      220 CONTINUE
ISN 0515      C END OF LOOP N
ISN 0516      105 CONTINUE
ISN 0517      C CRASH FORCES
ISN 0518      DO 240 J = 1,3
ISN 0519      SUM = 0.0
ISN 0520      DO 250 K = 1,3
ISN 0521      250 SUM = SUM+FSP(J,K)
ISN 0522      00005180
ISN 0523      00005190
ISN 0524      00005200
ISN 0525      00005210
ISN 0526      00005220
ISN 0527      00005230
ISN 0528      00005240
ISN 0529      00005250
ISN 0530      00005260
ISN 0531      00005270
ISN 0532      00005280
ISN 0533      00005290
ISN 0534      00005300
ISN 0535      00005310
ISN 0536      00005320
ISN 0537      00005330
ISN 0538      00005340
ISN 0539      00005350
ISN 0540      00005360
ISN 0541      00005370
ISN 0542      00005380
ISN 0543      00005390
ISN 0544      00005400
ISN 0545      00005410
ISN 0546      00005420
ISN 0547      00005430
ISN 0548      00005440
ISN 0549      00005450
ISN 0550      00005460
ISN 0551      00005470
ISN 0552      00005480
ISN 0553      00005490
ISN 0554      00005500
ISN 0555      00005510
ISN 0556      00005520
ISN 0557      00005530
ISN 0558      00005540
ISN 0559      00005550
ISN 0560      00005560
ISN 0561      00005570
ISN 0562      00005580
ISN 0563      00005590
ISN 0564      00005600
ISN 0565      00005610
ISN 0566      00005620
ISN 0567      00005630
ISN 0568      00005640
ISN 0569      00005650
ISN 0570      00005660
ISN 0571      00005670
ISN 0572      00005680
ISN 0573      00005690
ISN 0574      00005700
ISN 0575      00005700

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ISN 0519
ISN 0520
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ISN 0559
ISN 0560

XXC(J) = SUM
240 CONTINUE
C DXYZ(1) = DX(I)
C DXYZ(2) = DY(I)
C DXYZ(3) = DZ(I)
C DXYZ(1) = VADOT(1)*DELTA
C DXYZ(2) = VADOT(2)*DELTA
C DXYZ(3) = VADOT(3)*DELTA
C DQRIN(1) = DQIN(I)
C DQRIN(2) = DRIN(I)
C DQRIN(3) = DPIN(I)
C DQRIN(4) = DQIN(I)
C DQRIN(1) = PBAR(2)*DELTA
C DQRIN(2) = PBAR(3)*DELTA
C DQRIN(3) = PBAR(1)*DELTA
C DQRIN(4) = PBAR(2)*DELTA
C TERM(1) = FSPB(3,1)*(XLNGTH(1)+RRX)
C TERM(2) = FSPB(1,2)*(XLNGTH(2)+RRY)
C TERM(3) = FSPB(2,3)*(XLNGTH(3)+RRZ)
C TERM(4) = FSPB(2,1)*(XLNGTH(1)+RRX)
C TERM(5) = FSPB(3,2)*(XLNGTH(2)+RRY)
C TERM(6) = FSPB(1,3)*(XLNGTH(3)+RRZ)
C TERM(1) = FSPF(3,1)*(XLNGTH(1)+RRX)
C TERM(2) = FSPF(1,2)*(XLNGTH(2)+RRY)
C TERM(3) = FSPF(2,3)*(XLNGTH(3)+RRZ)
C TERM(4) = FSPF(2,1)*(XLNGTH(1)+RRX)
C TERM(5) = FSPF(3,2)*(XLNGTH(2)+RRY)
C TERM(6) = FSPF(1,3)*(XLNGTH(3)+RRZ)
C CRASH MOMENTS
C XXC(4) = TERM(5)+TERM(5)-TERM(3)-TERM(3)
C XXC(5) = TERM(6)+TERM(6)-TERM(1)-TERM(1)
C XXC(6) = TERM(4)+TERM(4)-TERM(2)-TERM(2)
C IF(M.EQ.0) GO TO 2001
C IF WE ARE AT A NODE POINT, WE MUST CALCULATE ADDITIONAL
C MOMENT CONTRIBUTIONS TO XXC(4-6).
C
C RTERM(1) = RRX*(FSPB(3,2)+FSPB(3,3))
C RTERM(2) = RRY*(FSPB(1,1)+FSPB(1,3))
C RTERM(3) = RRZ*(FSPB(2,1)+FSPB(2,2))
C RTERM(4) = RRX*(FSPB(2,2)+FSPB(2,3))
C RTERM(5) = RRY*(FSPB(3,1)+FSPB(3,3))
C RTERM(6) = RRZ*(FSPB(1,1)+FSPB(1,2))
C RTERM(1) = RRX*(FSPF(3,2)+FSPF(3,3))
C RTERM(2) = RRY*(FSPF(1,1)+FSPF(1,3))
C RTERM(3) = RRZ*(FSPF(2,1)+FSPF(2,2))
C RTERM(4) = RRX*(FSPF(2,2)+FSPF(2,3))
C RTERM(5) = RRY*(FSPF(3,1)+FSPF(3,3))
C RTERM(6) = RRZ*(FSPF(1,1)+FSPF(1,2))
C XXC(4) = XXC(4)+RTERM(5)+RTERM(5)-RTERM(3)-RTERM(3)
C XXC(5) = XXC(5)+RTERM(6)+RTERM(6)-RTERM(1)-RTERM(1)
C XXC(6) = XXC(6)+RTERM(4)+RTERM(4)-RTERM(2)-RTERM(2)
C ETERM(1) = RRY*DQRIN(2)-RRZ*DQRIN(1)

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ISN 0561      ETERM(2) = RRZ*DPQRINI(3)-RRY*DPQRINI(2)
ISN 0562      ETERM(3) = RRX*DPQRINI(1)-RRY*DPQRINI(3)
ISN 0563      ETB(1) = DPQRINI(1)*(RRY*FSPB(3,1)-RRZ*FSPB(2,1))
ISN 0564      ETB(2) = DPQRINI(1)*(RRZ*FSPB(1,2)-RRX*FSPB(3,2))
ISN 0565      ETB(3) = DPQRINI(2)*(RRX*FSPB(2,3)-RRY*FSPB(1,3))
ISN 0566      ETF(1) = DPQRINI(3)*(RRY*FSPF(3,1)-RRZ*FSPF(2,1))
ISN 0567      ETF(2) = DPQRINI(1)*(RRZ*FSPF(1,2)-RRX*FSPF(3,2))
ISN 0568      ETF(3) = DPQRINI(2)*(RRX*FSPF(2,3)-RRY*FSPF(1,3))

C
C      FOR SYMMETRICAL CASE,CENTERLINE MASSES,FORCE Y,L,N LOADS TO ZERO
C
C      2001 IF(SYMLG.EQ.0.OR.YDP(I).NE.0.) GO TO 2010
C          XXC(2) = 0.
C          XXC(4) = 0.
C          XXC(6) = 0.
C          IF(M.EQ.0.OR.SYMLG.EQ.2.) GO TO 2010
C          DO 2002 JJ=1,NNP
C              IF(I.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 2004
C          2002 CONTINUE
C          2004 IF(YNPD(JJ).EQ.0.) GO TO 2010
C
C          C      IF WE HAVE A SYMMETRIC CASE,CL MASS,AND NON-CL NODE POINT,
C          C      WE MUST DOUBLE X,Z AND M LOADS ON MASS I DUE TO THE EXTERNAL
C          C      SPRING ON THE OPPOSITE SIDE NODE POINT.
C
C          XXC(1) = 2.*XXC(1)
C          XXC(3) = 2.*XXC(3)
C          XXC(5) = 2.*XXC(5)
C
C      C      WE ARE STILL IN AN M (NODE POINT) LOOP. NOW SUM UP ALL THE
C      C      EXTERNAL SPRING FORCES AND MOMENTS ACTING AT MASS I DUE TO
C      C      EACH OF THE KOUNT NODE POINTS M.
C
C      2010 DO 2020 J=1,6
C          XC(J) = XC(J)+XXC(J)
C      2020 CONTINUE
C      CALL MATVEC(AI,DXYZ,DXYZPR,1)
C      DO 260 K = 1,3
C          IF(IISP(K).EQ.0) GO TO 260
C          SUM = 0.
C          SUMF = 0.
C          DO 270 J = 1,3
C              SUM = SUM-FSPB(J,K)*DXYZPR(J)
C              SUMF = SUMF-FSPF(J,K)*DXYZPR(J)
C          270 CONTINUE
C          SUM1 = TERM(K)*DPQRINI(K)-TERM(K+3)*DPQRINI(K+1)
C          SUMF1 = TERM(K)*DPQRINI(K)-TERM(K+3)*DPQRINI(K+1)
C          DO 2050 IKM=1,NSP
C              IF(I.EQ.II(IKM).AND.K.EQ.KK(IKM).AND.M.EQ.MM(IKM)) GO TO 2060
C          2050 CONTINUE
C          2060 IF(M.EQ.0) GO TO 2030
C              SUM1 = SUM1+FSPB(K,K)*ETERM(K)-ETB(K)
C              SUMF1 = SUMF1+FSPF(K,K)*ETERM(K)-ETF(K)

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00006690
00006700
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00006740
00006750
00006760

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ISN 0608      2030 CEIK(IKM) = CEIK(IKM)+SUM+SUM1
ISN 0609      CEIKF(IKM) = CEIKF(IKM)+SUMF+SUMF1
C
C      FOR A SYMMETRICAL MODEL WE MUST ADD CE AND FE CONTRIBUTIONS
C      FROM THE OPPOSITE SPRINGS THAT ARE NOT INPUT EXPLICITLY.
C
      IF(SYMF LG.NE.1.) GO TO 260
      IF(M.EQ.0.AND.YDP(I).EQ.0.) GO TO 260
      IF(M.EQ.0) GO TO 3000
      IF(YDP(I).EQ.0.AND.YNPD(JJ).EQ.0.) GO TO 260
3000 CEIK(IKM) = CEIK(IKM)+SUM+SUM1
      CEIKF(IKM) = CEIKF(IKM)+SUMF+SUMF1
260 CONTINUE
20 CONTINUE
20 RETURN
END
ISN 0610
ISN 0612
ISN 0614
ISN 0616
ISN 0618
ISN 0619
ISN 0620
ISN 0621
ISN 0622
ISN 0623
00006770
00006780
00006790
00006800
00006810
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00006830
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00006890
00006900
00006910
00006920

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

```
COMPILER OPTIONS - NAME= MAIN.OPT=02.LINECNT=55.SIZE=0600K.
```

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0000000110
000000020
000000030
000000040
000000060
000000070
000000080
000000090
000000100
000000110
000000120
000000130
000000140
000000150
000000160
000000170
000000180
000000190
000000200
000000210
000000220
000000230
000000240
000000250
000000260
000000270
000000280
000000290
000000300
000000310
000000320
000000330
000000340
000000350
000000360
000000370
000000380
000000390
000000400

SUBROUTINE DATIN(X,NAME,NMDS,UNIT,ERROR)
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C
C RETRIEVES VARIABLE AND ASSOCIATED VALUES FROM STORAGE
C
C ARG$ : X - STORAGE LOCATION WHERE VALUES RETRIEVED ARE
C          TO BE STORED
C          NAME - LITERAL NAME OF VARIABLE TO BE RETRIEVED
C                (8 CHAR MAX)
C          NMDS - NUMBER OF VALUES TO RETURN
C          UNIT - UNIT WHERE MASTER DATA SET IS MOUNTED
C          ERROR - FLAG; ERROR FLAG
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C
C INTEGER XI(1),TEMP(4),RECORD(250),ERROR,UNIT,ENDI
C DOUBLE PRECISION NAME,DURTY,START,BLANK,END
C EQUIVALENCE (DURTY,TEMP(1)),(NMDS,TEMP(4))
C DATA LRECL/250,/START/'**START#'/,BLANK/'
C      1 END/'*END*END'/', JNDS/-1/, ENDI/'*END'/'
C
C ...GET VARIABLE NAME AND NUMBER OF VALUES...
C
C ERROR = 0
C IF (JNDS .GT. 0) GO TO 5
C PRINT 6000
C ERROR = 22
C RETURN
C
C DO 20 I = 1,3
C   IF (JNDS .LT. LRECL) GO TO 10
C   READ (UNIT,END=99) RECORD
C   JNDS = 0
C   10 JNDS = JNDS +1
C   20 TEMPI = RECORD(JNDS)
C
C ...CHECK IF END OF DATA...
C

```



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ISN 0072
ISN 0073
ISN 0074
ISN 0075
ISN 0077
ISN 0078
ISN 0079
ISN 0080
ISN 0081
ISN 0082

C ...POSITION TO END OF DATA SET...
C
C
C      ENTRY CLSIN(UNIT,ERROR)
C      JMS = -1
C      ERROR = 0
C      200 IF (RECORD(LRECL) .EQ. END1) RETURN
C      READ (UNIT,END=299) RECORD
C      GO TO 200
C      299 CONTINUE
C      ERROR = 30
C      PRINT 5000
C      RETURN
C
C ...FORMATS...
C
C      1000 FORMAT(1H0,10X,'11. ***** - END OF DATA REACHED AT',
C      1 ' VARIABLE ',A9,'****')
C      3000 FORMAT(1H0,10X,'12. ***** - END OF FILE REACHED AT',
C      1 ' VARIABLE ',A9,'****')
C      4000 FORMAT(1H0,10X,'13. ***** - END OF FILE REACHED TRYING TO',
C      1 ' OPEN DATA SET FOR READING****')
C      5000 FORMAT(1H0,10X,'14. ***** - EOF TRYING TO CLOSE DATA SET',
C      1 ' AFTER READING****')
C      6000 FORMAT(1H0,10X,'15. ***** - CANNOT READ DATA WITHOUT',
C      1 ' FIRST OPENING DESIRED DATA SET****')
C      END
ISN 0083
ISN 0084
ISN 0085
ISN 0086
ISN 0087
ISN 0088

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00000940
00000950
00000960
00000970
00000980
00000990
00001000
00001010
00001020
00001030
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LEVEL 21.0 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.04.17

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
C SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
C DATA SET D2334DAOUT AT LEVEL 008 AS OF 03/23/79
C DATA SET D2332ZDATO AT LEVEL 007 AS OF 07/19/78
C INCREASE NUMBER OF BACKSPACES TO 5. 3-20-79 MJL
SUBROUTINE DATOUT(X,NAME,NMDS,UNIT,ERROR)
DIMENSION X(1),TEMP(4),RECORD(250)
INTEGER X,UNIT,ERROR,TEMP,RECORD
DOUBLE PRECISION NAME,DUMMY
EQUIVALENCE (DUMMY,TEMP(1)),(JMDS,TEMP(4))
DATA LRECL/250/, JMDS/-1/
C ...WRITE VARIABLE DEFINITION DATA...

IF (JMDS.GT. 0) GO TO 10

PRINT 1000

ERROR = 42

RETURN

10 IF (NMDS.LT. 1000000) GO TO 15

PRINT 2000,NMDS

ERROR = 47

RETURN

15 DUMMY = NAME

TEMP(3) = NMDS

ERROR = 0

DO 30 I = 1,3

IF (JMDS.LT. LRECL) GO TO 20

WRITE (UNIT) RECORD

JMDS = 0

20 JMDS = JMDS +1

RECORD(JMDS) = TEMP(I)

30 IF (NMDS.LE. 0) RETURN

...WRITE VARIABLE VALUES...

C

C

DO 60 I = 1,NMDS

IF (JMDS.LT. LRECL) GO TO 50

WRITE (UNIT) RECORD

JMDS = 0

50 JMDS = JMDS +1

RECORD(JMDS) = X(I)

60 RETURN

C

ISN 0002
ISN 0003
ISN 0004
ISN 0005
ISN 0006
ISN 0007

ISN 0008
ISN 0009
ISN 0010
ISN 0011
ISN 0012
ISN 0013
ISN 0014
ISN 0015
ISN 0016
ISN 0017
ISN 0018
ISN 0019
ISN 0020
ISN 0021
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ISN 0037
ISN 0038
ISN 0039
ISN 0040

```

C      ...WRITING HEADER INFORMATION...
C
C      ENTRY OPNOUT(UNIT)
C      INTEGER DSN(1),DATE(5)
C      INTEGER ACCORD(22) /22*0/
C      INTEGER HEAD(3)/'**ST','ART','END'/
C
C      ...FIND LAST RECORD WRITTEN...
C
C      100 READ (UNIT,END=105)
C      GO TO 100
C      105 CONTINUE
C
C      TAPE IS BACKSPACED TWICE TO POSITION TAPE HEAD AT BEGINNING
C      OF LAST RECORD.
C
C      DO 106 J=1,2
C      BACKSPACE UNIT
C      106 CONTINUE
C
C      LAST RECORD IS READ AGAIN, TO POSITION TAPE FOR NEXT WRITE,
C      WHICH WILL DESTROY EOF TAPE MARK.
C
C      READ(21) RECORD
C
C      ...WRITE HEADER...
C
C      DO 107 I=1,22
C      107 ACCORD(I) = 0
C      RECORD(1) = HEAD(1)
C      RECORD(2) = HEAD(2)
C      CALL CDATE(1,0)
C      RECORD(3) = 24
C      RECORD(4) = DATE(1)
C      RECORD(5) = DATE(2)
C      CALL JOBAC(ACCORD)
C      DO 110 I = 1,22
C      JMODS = I + 5
C      110 RECORD(JMODS) = ACCORD(I)
C      RETURN
C
C      ...WRITE CLOSING INFORMATION...
C
C      ENTRY CLSOUT(UNIT)
C      IF (JMODS .LT. LRECL) GO TO 200
C      WRITE (UNIT) RECORD
C      JMODS = 0
C      200 JMODS = JMODS + 1
C      DO 210 I = JMODS, LRECL

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ISN 0039
ISN 0039
ISN 0040
ISN 0041

ISN 0042
ISN 0043
ISN 0044

ISN 0045
ISN 0046
ISN 0047

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ISN 0069      210  RECORD(I) = HEAD(3)
ISN 0070      WRITE (UNIT) RECORD
C
C      TAPE FILE IS ENDED, THEN BACKSPACED TWICE TO POSITION
C      TAPE HEAD TO BEGINNING OF LAST RECORD. THAT RECORD IS
C      THEN READ, AND NEXT READ WILL ENCOUNTER EOF.
C
      END FILE UNIT
      DO 215 J=1,2
      BACKSPACE UNIT
215 CONTINUE
      READ(21) RECORD
      JNDS = -1
      RETURN
1000 FORMAT(1H0,10X,'16. ****ERROR - MUST OPEN DATA SET BEFORE',
           1  'WRITING DATA OUT****')
2000 FORMAT(1H0,10X,'17. **WARNING - REQUESTED STORING ',I9,
           1  ' VALUES. STORE FAILED**')
      END
ISN 0071
ISN 0072
ISN 0073
ISN 0074
ISN 0075
ISN 0076
ISN 0077
ISN 0078
ISN 0079
ISN 0080

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00094
00095
00096
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00100
00101
00102
00103
00104
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00109
00110
00111
00112

```


LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF

DATA SET D2332VDE AT LEVEL 009 AS OF 02/09/78

DELTA VB/DELTA TAT VERSION

REAL#8 KEIUTL,KEI
REAL#8 KIN-KB(6)

REAL#8 PX,M1,MZ,M
REAL#6 YK5.YKT.YK

INTEGERS#4 TITLE#4

```
INTEGER*2 NLSFIG,
          FL2011
```

INTEGER*2 MG(150)

D(9), AIAIJT(9), A

NO DIMENSION XVOL(6,

DIMENSION RX(50),

DIMENSION XDNP(50

DIMENSION XNPOLD(

VEEBAR(

DFJ(6),

FMAX(900), HE, (80

HVP

COMMON/DEIR/ PLM2

COMMON/DEPR/ XDOT

COMMON/DEINPR/ AA

100

ISN 0031	1 XIB(150),Z1(150),Z2(150),MC(150),XJ(150),SF26(150),SF35(150), 2 SF26J(150),SF35J(150),PY,PZ,PJ,NSC,NPIN COMMON/ENERGY/ XPC(80),XETOT(80),XETOTD(80),XSE(80),XDE(80), 1 XCE(80),XFE(80),KEI(80),PEI(80),XETOTL,KETOTL, 2 PETOTL,SETOTL,DETOTL,CETOTL,FETOTL COMMON/MADE/KFL26(150),KFL35(150),FL26J,FL35J,FL35J, 1 TPL(100),BPL,KPL COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),EE(20),GG(20), 1 FINT(6,150),VOL(5),VZERO(5),KMATRI(6,4),NVCH,INBUFF(5,8) COMMON/INDEAC/ NACC COMMON/INIDCP/ YDP(80) COMMON/INPR/ NDRI,NSP COMMON 1 XN(80),DPX(80),DPY(80),DPZ(80),DPL(80),DPH(80),DPN(80),PIN(80), 2 QIN(80),PIN(80),XII(80),XIZ(80),XIX(80),XIA(80),XIS(80),XIG(80), 5 DELI(80),POLD(80),QOLD(80),ROLD(80),UOLD(80),VOLD(80), 6 MOLD(80),XOLD(80),YOLD(80),ZOLD(80),PINO(80),QINO(80),RINO(80), 7 PHOLD(80),THEOLD(80),PSIOLD(80), 8 XACFD(80),YACFD(80),ZACFD(80),XAFOLD(80),YAFOLD(80),ZAFOLD(80), 9 XNPF(50),YNPF(50),ZNPFD(50),XANPFO(50),YANPFO(50),ZANPFO(50), A KRB(200),TPEN(80),OTHALF, B KRB(4,200),KRF(900),IPEN(80),KPEN,KRCONT COMMON/MCFII/ SYMFLG COMMON/MP0012/ MG,NG,INP,MNP COMMON/MP0012/ II,KK,MM COMMON/MP0014/ NNP COMMON/MP0008/ RX,RY,RZ COMMON/MP0018/ XNP,YNP,ZNP,UNP,VNP,MNP,XONP,ZONP, 1 XACCNP,YACCNP,ZACCNP,SBUCKR(150),PCR(150) COMMON/DEIC/ WTOT,CLTEST(150) COMMON/OLEO/OLEO(20),FAO(20),FAA(20),EXPOL(20),YMAX(20), 1 YOLEO(20),BOLEO(20),BROLEO(20),XKEXT(20),XKCOMP(20),FCOUL(20), 2 ALPHAP,IGOLEO(20),JGOLEO(20),NGOLEO(20),NGOLEO(20),NOLEO COMMON/PRHA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50), 1 ZACNPF(50),XIMP(80),YIMP(80),ZIMP(80),XIMPNI(50),YIMPNI(50), 2 ZIMPNI(50),XIMPOL(80),YIMPOL(80),ZIMPOL(80),XIMPNI(50), 3 YIMPNI(50),ZIMPNI(50) COMMON/IRDE/ PFIL COMMON/UB/ OB(150),IUB(150),NUB COMMON/COMALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(80), 1 Y(80),Z(80),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80), 2 YI(80),ZI(80),YI(80),XI(80),YI(80),YI(80),YI(80),YI(80), 3 DRI(150),OAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80), 4 PROOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),XDOT(80), 5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTA, 6 XACC(80),YACC(80),ZACC(80),AIDOT(9), 7 PHIIJ(150),THEIJ(150),PSIIJ(150),SUMPF(6,150),TITLE, 8 XIBARI(40),FSPARI(40),VEEDOT(3,3),DX(81),DY(81),DZ(81), 9 DPMI(81),DQINI(81),DRINI(81),SEIJ(150),DEIJ(150),CEIK(40), A CEIKF(40), B SBARI(40),KUN(40),MAXMI,MAXIGS,MAXTBL, C NM,NB,I,J,IG(150),JG(150), D NI(900),NM(40),IJPR(150)	00000410 00000420 00000430 00000440 00000450 00000460 00000470 00000480 00000490 00000500 00000510 00000520 00000530 00000540 00000550 00000560 00000570 00000580 00000590 00000600 00000610 00000620 00000630 00000640 00000650 00000660 00000670 00000680 00000690 00000700 00000710 00000720 00000730 00000740 00000750 00000760 00000770 00000780 00000790 00000800 00000810 00000820 00000830 00000840 00000850 00000860 00000870 00000880 00000890 00000900 00000910 00000920 00000930
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1      COMMON /MAX/ IRUPSM(150),IPENSM(80),VEEBAR(900),ZINIT(60),
1      DPHIJ(150),FUB(150)
COMMON /VARIANT/ MINDT,DT2,TPRINT,EL,EU,RATMIN,RATMAX,IPC,IVAR
COMMON /MACFIN/ THAX,IPRINT
EQUIVALENCE (S1,SINCOS(1)),(C1,SINCOS(2)),(S2,SINCOS(3)),
1      (C2,SINCOS(4)),(S3,SINCOS(5)),(C3,SINCOS(6))
SQRT(X) = DSQRT(X)
SIN(X) = DSIN(X)
COS(X) = DCOS(X)
SIGN(X1,X2) = DSIGN(X1,X2)
ABS(X) = DABS(X)
AMAX1(X,Y) = DMAX1(X,Y)
ATAN2(Y,X) = DATAN2(Y,X)
TANH(X) = DTANH(X)
ONE = 1.
TT = .2
ET = .8
S = DELTAT
PI2 = 3.1415926535897932400/2.
ERR = 0.
IF (TIME.NE.0.0) GO TO 60
DO 70 IJ = 1,NB
PHIJ(IJ) = 0.
DPHIJ(IJ) = 0.
VEEN(1,IJ) = 0.
VEEN(2,IJ) = 0.
DO 71 K=1,6
71 SURDFI(K,IJ) = 0.
70 IRUPSM(IJ) = 0
DO 72 I=1,NM
XSE(I) = 0.
XOE(I) = 0.
72 IPENSM(I)=0
NB9 = 9*NB
DO 74 I = 1,NB9
VEEBAR(I) = 0.
74 CONTINUE
C DO ALL THE (AI)((AJ))
60 DO 10 I = 1,NM
ARG = PHIJ(I)
S1 = SIN(ARG)
C1 = COS(ARG)
ARG = THETA(I)
S2 = SIN(ARG)
C2 = COS(ARG)
ARG = PSI(I)
S3 = SIN(ARG)
C3 = COS(ARG)
DO 40 J = 1,6
T = SINCOS(J)
IF (T) 45,40,50
45 T = -T
50 IF (T-I.E-10) 55,40,40

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ISN 0101      55 SINCO5(J) = 0.0
ISN 0102      40 CONTINUE
ISN 0103      C
ISN 0104      J = 9*(I-1)
ISN 0105      C MOVE AI S TO OLD AI S
ISN 0106      DO 4 J1 = 1,9
ISN 0107      4 OAI(J+J1) = BIJ(J+J1)
ISN 0108      S1S2 = S1*S2
ISN 0109      C1S2 = C1*S2
ISN 0110      AI(1) = C2*C3
ISN 0111      BIJ(J+1) = AI(1)
ISN 0112      AI(2) = C2*S3
ISN 0113      BIJ(J+2) = AI(2)
ISN 0114      AI(3) = -S2
ISN 0115      BIJ(J+3) = AI(3)
ISN 0116      AI(4) = -C1*S3+S1S2*C3
ISN 0117      BIJ(J+4) = AI(4)
ISN 0118      AI(5) = C1*C3+S1S2*S3
ISN 0119      BIJ(J+5) = AI(5)
ISN 0120      AI(6) = S1*C2
ISN 0121      BIJ(J+6) = AI(6)
ISN 0122      AI(7) = S1*S3+C1S2*C3
ISN 0123      BIJ(J+7) = AI(7)
ISN 0124      AI(8) = -S1*C3+C1S2*S3
ISN 0125      BIJ(J+8) = AI(8)
ISN 0126      AI(9) = C1*C2
ISN 0127      BIJ(J+9) = AI(9)
ISN 0128      C (27)
ISN 0129      PP = P(I)
ISN 0130      QQ = Q(I)
ISN 0131      RR = R(I)
ISN 0132      UU = U(I)
ISN 0133      VV = V(I)
ISN 0134      WW = W(I)
ISN 0135      XDOT(I) = AI(1)*UU+AI(6)*VV+AI(7)*WW
ISN 0136      YDOT(I) = AI(2)*UU+AI(5)*VV+AI(8)*WW
ISN 0137      ZDOT(I) = AI(3)*UU+AI(6)*VV+AI(9)*WW
ISN 0138      C (28), (29)
ISN 0139      CS = S1/C2
ISN 0140      CC = C1/C2
ISN 0141      PHIDOT(I) = PP+QQ*CS*S2+RR*CC*S2
ISN 0142      THEDOT(I) = QQ*C1-RR*S1
ISN 0143      PSIDOT(I) = QQ*CS+RR*CC
ISN 0144      C DO AIDOT NOW
ISN 0145      T = PSIDOT(I)*C2
ISN 0146      T1 = THEDOT(I)*S1-T*C1
ISN 0147      T2 = THEDOT(I)*C1+T*S1
ISN 0148      T3 = PHIDOT(I)-PSIDOT(I)*S2
ISN 0149      CIJ(J+1) = -BIJ(J+4)*T1-BIJ(J+7)*T2
ISN 0150      CIJ(J+4) = BIJ(J+1)*T1+BIJ(J+7)*T3
ISN 0151      CIJ(J+7) = BIJ(J+1)*T2-BIJ(J+4)*T3
ISN 0152      CIJ(J+2) = -BIJ(J+5)*T1-BIJ(J+8)*T2
ISN 0153      CIJ(J+5) = BIJ(J+2)*T1+BIJ(J+8)*T3
ISN 0154      00001470
ISN 0155      00001480
ISN 0156      00001490
ISN 0157      00001500
ISN 0158      00001510
ISN 0159      00001520
ISN 0160      00001530
ISN 0161      00001540
ISN 0162      00001550
ISN 0163      00001560
ISN 0164      00001570
ISN 0165      00001580
ISN 0166      00001590
ISN 0167      00001600
ISN 0168      00001610
ISN 0169      00001620
ISN 0170      00001630
ISN 0171      00001640
ISN 0172      00001650
ISN 0173      00001660
ISN 0174      00001670
ISN 0175      00001680
ISN 0176      00001690
ISN 0177      00001700
ISN 0178      00001710
ISN 0179      00001720
ISN 0180      00001730
ISN 0181      00001740
ISN 0182      00001750
ISN 0183      00001760
ISN 0184      00001770
ISN 0185      00001780
ISN 0186      00001790
ISN 0187      00001800
ISN 0188      00001810
ISN 0189      00001820
ISN 0190      00001830
ISN 0191      00001840
ISN 0192      00001850
ISN 0193      00001860
ISN 0194      00001870
ISN 0195      00001880
ISN 0196      00001890
ISN 0197      00001900
ISN 0198      00001910
ISN 0199      00001920
ISN 0200      00001930
ISN 0201      00001940
ISN 0202      00001950
ISN 0203      00001960
ISN 0204      00001970
ISN 0205      00001980
ISN 0206      00001990

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ISN 0149      CIJ(J+6) = BIJ(J+2)*T2-BIJ(J+5)*T3
ISN 0150      CIJ(J+3) = -BIJ(J+6)*T1-BIJ(J+9)*T2
ISN 0151      CIJ(J+6) = BIJ(J+3)*T1+BIJ(J+9)*T3
ISN 0152      CIJ(J+9) = BIJ(J+3)*T2-BIJ(J+6)*T3
ISN 0153      10 CONTINUE

C
C      THE FOLLOWING CODING GETS THE VEHICLE C.G. TRANSLATIONAL
C      VELOCITY IN GROUND AXES BY EQUATING THE VEHICLE LINEAR
C      MOMENTUM WITH THE SUM OF THE MOMENTA OF ALL THE INDIVIDUAL
C      LUMPED MASSES.
C
ISN 0154      SUMMXD = 0.
ISN 0155      SUMMYD = 0.
ISN 0156      SUMMZD = 0.
ISN 0157      SUMM = 0.
ISN 0158      DO 12 I=1,NM
ISN 0159          SUMM = SUMM+MGT(I)
ISN 0160          SUMMXD = SUMMXD+MGT(I)*XDOT(I)
ISN 0161          SUMMYD = SUMMYD+MGT(I)*YDOT(I)
ISN 0162          SUMMZD = SUMMZD+MGT(I)*ZDOT(I)

C
C      FOR A SYMMETRICAL MODEL WE MUST ADD THE MOMENTUM CONTRIBUTIONS
C      FROM THE OPPOSITE MASSES THAT ARE NOT INPUT EXPLICITLY.
C
ISN 0163      IF(SYMLG.NE.1.OR.YDPI(I).EQ.0.) GO TO 12
ISN 0164          SUMM = SUMM+MGT(I)
ISN 0165          SUMMXD = SUMMXD+MGT(I)*XDOT(I)
ISN 0166          SUMMYD = SUMMYD+MGT(I)*YDOT(I)
ISN 0167          SUMMZD = SUMMZD+MGT(I)*ZDOT(I)
ISN 0168          SUMMXD = SUMMXD+MGT(I)*XDOT(I)
ISN 0169          SUMMYD = SUMMYD+MGT(I)*YDOT(I)
ISN 0170          SUMMZD = SUMMZD+MGT(I)*ZDOT(I)
ISN 0171      12 CONTINUE
ISN 0172          XDOTAP = SUMMXD/SUMM
ISN 0173          YDOTAP = SUMMYD/SUMM
ISN 0174          ZDOTAP = SUMMZD/SUMM

C
C      FOR THE MAIN INTERNAL BEAM LOOP (DO 1000), WE NEED XNP(J),
C      DXNP(J), AND UNP(J) FOR THE NODE POINTS.
C
ISN 0175      IF(INNP.EQ.0) GO TO 16
ISN 0176      DO 14 J=1,NNP
ISN 0177          XNPOLD(J) = XNP(J)
ISN 0178          YNPOLD(J) = YNP(J)
ISN 0179          ZNPOLD(J) = ZNP(J)
ISN 0180          I = INP(J)
ISN 0181          IS = 9*(I-1)
ISN 0182          DO 15 KS=1,9
ISN 0183              IS = IS+1
ISN 0184              AI(KS) = BIJ(IS)
ISN 0185          15 CONTINUE
ISN 0186              TX = AI(1)*RXI(J)+AI(4)*RY(J)+AI(7)*RZ(J)
ISN 0187              TY = AI(2)*RXI(J)+AI(5)*RY(J)+AI(8)*RZ(J)
ISN 0188              TZ = AI(3)*RXI(J)+AI(6)*RY(J)+AI(9)*RZ(J)
ISN 0189              XNP(J) = X(I)+TX
ISN 0190              YNP(J) = Y(I)+TY
ISN 0191              ZNP(J) = Z(I)+TZ
ISN 0192          14 CONTINUE
ISN 0193      16 CONTINUE
ISN 0194      10 CONTINUE
ISN 0195      1000 CONTINUE
ISN 0196      STOP
ISN 0197      END

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ISN 0190      ZNP(J) = Z(I)*TZ
ISN 0191      DXNP(J) = XNP(J)-XNPOLD(J)
ISN 0192      DYNP(J) = YNP(J)-YNPOLD(J)
ISN 0193      DZNP(J) = ZNP(J)-ZNPOLD(J)
ISN 0194      OMCXY = -R(I)*RY(J)+Q(I)*RZ(J)
ISN 0195      OMCYX = R(I)*RX(J)-P(I)*RZ(J)
ISN 0196      OMCZ = -Q(I)*RX(J)+P(I)*RY(J)
ISN 0197      UNP(J) = U(I)*OMCRY
ISN 0198      VNP(J) = V(I)*OMCRY
ISN 0199      WNP(J) = W(I)*OMCRZ
ISN 0200      IF(TIME.NE.0.) GO TO 14
ISN 0201      DXNP(J) = 0.
ISN 0202      DYNP(J) = 0.
ISN 0203      DZNP(J) = 0.
ISN 0204      DZNP(J) = 0.
ISN 0205      14 CONTINUE

C
C      ZERO OUT BEAM FORCES ON MASSES.
C
C      16 DO 18 I=1,N
ISN 0206      XX(I) = 0.
ISN 0207      XY(I) = 0.
ISN 0208      XZ(I) = 0.
ISN 0209      XL(I) = 0.
ISN 0210      XM(I) = 0.
ISN 0211      XN(I) = 0.
ISN 0212      18 CONTINUE
ISN 0213      ILAST = 0
ISN 0214

C
C      DO 1000 IS MAIN DO LOOP TO GET TOTAL INTERNAL FORCES AND MOMENTS
C
C      DO 1000 IJ = 1,NB
ISN 0215      IJK = 6*(IJ-1)
ISN 0216      IF(IRUPSM(IJ).NE.0) GO TO 1000
ISN 0217      I = IG(IJ)
ISN 0218      J = JG(IJ)
ISN 0219      M = MG(IJ)
ISN 0220      N = NG(IJ)
ISN 0221      20 IF(I-ILAST) 20,30,20
ISN 0222      20 ILAST = I
ISN 0223      IS = 9*(I-1)
ISN 0224      DO 320 KS = 1,9
ISN 0225      IS = IS+1
ISN 0226      AIDOT(KS) = CIJ(IS)
ISN 0227      320 AIJKS = BIJ(IS)
ISN 0228
ISN 0229      C      NOW GET AJ.
ISN 0230      30 IS = 9*(J-1)
ISN 0231      DO 3201 KS=1,9
ISN 0232      IS = IS+1
ISN 0233      IF(J.EQ.0) GO TO 3202
ISN 0234      AJIKS = BIJ(IS)
ISN 0235

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ISN 0236      GO TO 3201
ISN 0237      3202 AJ(KS) = AI(KS)
ISN 0238      IF(KS.EQ.2.OR.KS.EQ.4.OR.KS.EQ.6.OR.KS.EQ.8) AJ(KS) = -AJ(KS)
ISN 0240      3201 CONTINUE
C
C      IF J.EQ.0, WE HAVE A SYMMETRICAL MODEL IN WHICH BEAM IJ
C      CONNECTS NODE POINT (I,M) TO AN IMAGINARY POINT (J,N=0)
C      LOCATED SYMMETRICALLY ACROSS THE AIRPLANE PLANE OF SYMMETRY
C      (X-Z PLANE). FOR THESE TRANSVERSE BEAMS, THE CONDITIONS AT (J,N)
C      ARE DEDUCED FROM THE STATE AT (I,M). J IS CHANGED TO 81 BECAUSE
C      THE IBM 360-91 WILL NOT ACCEPT A ZERO SUBSCRIPTED VECTOR.
C
C      IF(J.NE.0) GO TO 3300
C      J = 81
C      IF(M.NE.0) GO TO 3301
C
C      IF M.EQ.0, THERE IS NO NODE POINT AT I.
C
C      3302 DX(MDI) = DX(I)
C      DY(MDI) = DY(I)
C      DZ(MDI) = DZ(I)
C      X(MDI) = X(I)
C      Y(MDI) = Y(I)
C      Z(MDI) = Z(I)
C      U(MDI) = U(I)
C      V(MDI) = V(I)
C      W(MDI) = W(I)
C      PI = P(I)
C      QI = Q(I)
C      RI = R(I)
C      GO TO 3303
C
C      THIS LOOP GETS NODE POINT NUMBER JI KNOWING I AND M.
C
C      3301 DO 3305 JI=1,MNP
C      IF(I.EQ.INP(JI).AND.M.EQ.MNP(JI)) GO TO 3306
C      3305 CONTINUE
C      3306 DY(MDI) = DXNP(JI)
C      DZ(MDI) = DZNP(JI)
C      X(MDI) = XNP(JI)
C      Y(MDI) = YNP(JI)
C      Z(MDI) = ZNP(JI)
C      U(MDI) = UNP(JI)
C      V(MDI) = VNP(JI)
C      W(MDI) = WNP(JI)
C      PI = P(I)
C      QI = Q(I)
C      RI = R(I)
C      3303 IF(J.NE.81) GO TO 3310
C
C      IF J.EQ.81, WE HAVE A SYMMETRICAL MODEL. NOW CALCULATE
C      CONDITIONS AT J,N BASED ON KNOWLEDGE OF STATE AT I,M.

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ISN 0277	DXH00J = DXH00I	00003590
ISN 0278	OYH00J = -OYH00I	00003600
ISN 0279	DZH00J = DZH00I	00003610
ISN 0280	XPH00J = XPH00I	00003620
ISN 0281	YH00J = -YH00I	00003630
ISN 0282	ZH00J = ZH00I	00003640
ISN 0283	OPIN(J) = -OPIN(I)	00003650
ISN 0284	OQIN(J) = OQIN(I)	00003660
ISN 0285	ORIN(J) = -ORIN(I)	00003670
ISN 0286	UH00J = UH00I	00003680
ISN 0287	VH00J = -VH00I	00003690
ISN 0288	WH00J = WH00I	00003700
ISN 0289	PJ = -PI	00003710
ISN 0290	QJ = QI	00003720
ISN 0291	RJ = -RI	00003730
ISN 0292	GO TO 3320	00003740
ISN 0293	3300 IF(M.EQ.0) GO TO 3302	00003750
ISN 0294	GO TO 3301	00003760
ISN 0295	3310 IF(N.NE.0) GO TO 3311	00003770
ISN 0296		00003780
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		00004440
		00004450
		00004460
		00004470
		00004480
		00004490
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		00004690
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		00004950
		00004960


```

ISN 0326      RJ = R(J)
C
C
C ALL OF THE ABOVE PATHS LEAD TO HERE. WE NOW HAVE POSITIONS
C (XMOD,ETC.) AND INCREMENTAL CHANGES IN POSITIONS (DXMOD,ETC.)
C FOR BOTH ENDS OF BEAM IJ.
C
ISN 0327      3320 XIJ = XMODJ-XMODI
ISN 0328      YIJ = YMODJ-YMODI
ISN 0329      ZIJ = ZMODJ-ZMODI
C
C CALCULATE AIJ. FIRST UPDATE PHIJJ, THEIJ, PSIIJ.
C
C
C PHIJJ(IJ) = PHIJJ(IJ) + DPHIIJ(IJ)
C IF(XIJ.EQ.0.AND.YIJ.EQ.0.) GO TO 3330
C PSIIJ(IJ) = ATAN2(YIJ,XIJ)
C GO TO 3340
C
C 3330 PSIIJ(IJ) = 0.
C 3340 THEIJ(IJ) = -ATAN2(ZIJ,SQRT(XIJ*XIJ+YIJ*YIJ))
C
C ZERO OUT VERY SMALL SIN AND COS TERMS.
C
C
C ARG = PHIJJ(IJ)
C S1 = SIN(ARG)
C C1 = COS(ARG)
C ARG = THEIJ(IJ)
C S2 = SIN(ARG)
C C2 = COS(ARG)
C ARG = PSIIJ(IJ)
C S3 = SIN(ARG)
C C3 = COS(ARG)
C DO 3392 J1 = 1,6
C T = SIN(COS(J1))
C IF(T) 3394,3392,3398
C 3394 T = -T
C 3398 IF(T-1.E-10) 3396,3392,3392
C 3396 SIN(COS(J1)) = 0.0
C 3392 CONTINUE
C
C S1S2 = S1*S2
C C1S2 = C1*S2
C AIJ(1) = C2*C3
C AIJ(2) = C2*S3
C AIJ(3) = -S2
C AIJ(4) = -C1*S3 + S1S2*C3
C AIJ(5) = C1*C3 + S1S2*S3
C AIJ(6) = S1*C2
C AIJ(7) = S1*S3 + C1S2*C3
C AIJ(8) = -S1*C3 + C1S2*S3
C AIJ(9) = C1*C2
C
C CALCULATE CURRENT BEAM LENGTH XXLB.
C
C
C XXLB = SQRT(XIJ*XIJ+YIJ*YIJ+ZIJ*ZIJ)
C

```


C CALCULATE AIJTAJ AND AIJTAI. FILL TEMP WITH EITHER AJ OR AI.

ISN 0365
ISN 0366
ISN 0367
ISN 0369
ISN 0370
ISN 0371
ISN 0372
ISN 0373
ISN 0374
ISN 0375
ISN 0376
ISN 0377
ISN 0378
ISN 0379
ISN 0380
ISN 0381
ISN 0383
ISN 0384
ISN 0385
ISN 0386
ISN 0387
ISN 0388

```

DO 6000 I3=1,2
DO 6010 I4=1,9
IF(13.EQ.2) GO TO 6020
TEMP(I4) = AJ(I4)
GO TO 6010
6020 TEMP(I4) = AI(I4)
6010 CONTINUE
L2 = 0
DO 6030 K2=1,3
DO 6040 J2=1,3
L2 = L2+1
SUMH(L2) = 0.
DO 6050 I2=1,3
SUMH(L2) = SUMH(L2) + AIJ(3*(J2-1)+I2)*TEMP(3*(K2-1)+I2)
6050 CONTINUE
IF(13.EQ.2) GO TO 6060
AIJTAJ(L2) = SUMH(L2)
GO TO 6040
6060 AIJTAI(L2) = SUMH(L2)
6040 CONTINUE
6030 CONTINUE
6000 CONTINUE

```

00004650
00004660
00004670
00004680
00004690
00004700
00004710
00004720
00004730
00004740
00004750
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00004990
00005000
00005010
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00005070
00005080
00005090
00005100
00005110
00005120
00005130
00005140
00005150
00005160
00005170

C CALCULATE VELOCITIES AND INCREMENTAL DEFLECTIONS AT J,N
C AND I,M IN BEAM AXES.

ISN 0389
ISN 0390
ISN 0391
ISN 0392
ISN 0393
ISN 0394
ISN 0395
ISN 0396
ISN 0397
ISN 0398
ISN 0399
ISN 0400
ISN 0401
ISN 0402
ISN 0403
ISN 0404
ISN 0405
ISN 0406
ISN 0407
ISN 0408
ISN 0409
ISN 0410
ISN 0411
ISN 0412

```

VJ(1) = AIJTAJ(1)*VHODJ+AIJTAJ(4)*VHODJ+AIJTAJ(7)*VHODJ
VJ(2) = AIJTAJ(2)*VHODJ+AIJTAJ(5)*VHODJ+AIJTAJ(8)*VHODJ
VJ(3) = AIJTAJ(3)*VHODJ+AIJTAJ(6)*VHODJ+AIJTAJ(9)*VHODJ
VJ(4) = AIJTAJ(1)*PJ+AIJTAJ(4)*QJ+AIJTAJ(7)*RJ
VJ(5) = AIJTAJ(2)*PJ+AIJTAJ(5)*QJ+AIJTAJ(8)*RJ
VJ(6) = AIJTAJ(3)*PJ+AIJTAJ(6)*QJ+AIJTAJ(9)*RJ
VI(1) = AIJTAI(1)*VHODI+AIJTAI(4)*VHODI+AIJTAI(7)*VHODI
VI(2) = AIJTAI(2)*VHODI+AIJTAI(5)*VHODI+AIJTAI(8)*VHODI
VI(3) = AIJTAI(3)*VHODI+AIJTAI(6)*VHODI+AIJTAI(9)*VHODI
VI(4) = AIJTAI(1)*PI+AIJTAI(4)*QI+AIJTAI(7)*RI
VI(5) = AIJTAI(2)*PI+AIJTAI(5)*QI+AIJTAI(8)*RI
VI(6) = AIJTAI(3)*PI+AIJTAI(6)*QI+AIJTAI(9)*RI
DJ(1) = AIJ(1)*VHODJ + AIJ(2)*VHODJ + AIJ(3)*VHODJ
DJ(2) = AIJ(4)*VHODJ + AIJ(5)*VHODJ + AIJ(6)*VHODJ
DJ(3) = AIJ(7)*VHODJ + AIJ(8)*VHODJ + AIJ(9)*VHODJ
DI(1) = AIJ(1)*VHODI + AIJ(2)*VHODI + AIJ(3)*VHODI
DI(2) = AIJ(4)*VHODI + AIJ(5)*VHODI + AIJ(6)*VHODI
DI(3) = AIJ(7)*VHODI + AIJ(8)*VHODI + AIJ(9)*VHODI
DJ(4) = AIJTAJ(1)*VHODJ+AIJTAJ(4)*VHODJ+AIJTAJ(7)*VHODJ
DJ(5) = AIJTAJ(2)*VHODJ+AIJTAJ(5)*VHODJ+AIJTAJ(8)*VHODJ
DJ(6) = AIJTAJ(3)*VHODJ+AIJTAJ(6)*VHODJ+AIJTAJ(9)*VHODJ
DI(4) = AIJTAI(1)*VHODI+AIJTAI(4)*VHODI+AIJTAI(7)*VHODI
DI(5) = AIJTAI(2)*VHODI+AIJTAI(5)*VHODI+AIJTAI(8)*VHODI
DI(6) = AIJTAI(3)*VHODI+AIJTAI(6)*VHODI+AIJTAI(9)*VHODI

```

```

C      CALCULATE VELOCITIES AND RELATIVE INCREMENTAL DEFLECTIONS (J-I) AND
C      SURS (J+I) FOR INTERNAL FORCE CALCULATIONS. VEEN(1 AND 2) ARE
C      USED FOR OUTPUT ONLY.
C
      DO 6100 J2=1,9
      IF(J2.GT.6) GO TO 6110
      DI(J2) = DJ(J2) - DI(J2)
      VEL(J2) = VJ(J2) - VI(J2)
      GO TO 6100
6110 DI(J2) = DJ(J2-3) + DI(J2-3)
      IF(J2.NE.7) VEEN(J2-7,IJ) = VEEN(J2-7,IJ)+DI(J2)
      VEL(J2) = VJ(J2-3) + VI(J2-3)
6100 CONTINUE
      DPHIL(IJ) = D(7)/2.
C
C      MARCH 1977 INTERNAL FORCE CODING
C
      DO 150 K = 1,6
      I,K = I,K+1
C
C      NOW LETS GET A KR IF A TABLE EXISTS
C      FIRST DETERMINE WHICH TABLE WE WANT
C
      ITN = NLSFLG(IJK)
      IF(ITN.EQ.0) GO TO 144
      IF(K.EQ.1.OR.K.EQ.4) GO TO 191
      IF(K.EQ.2.OR.K.EQ.6) GO TO 192
      IF(K.EQ.3) GO TO 191
      KPR = KFL35(IJ)
      GO TO 193
192 IF(KFL26(IJ).EQ.0) GO TO 191
      KPR = KFL26(IJ)
      GO TO 193
191 KPR = K
C
C      KPR IS THE TABLE NUMBER (1-6) FOR CURRENT IJK
C
C193 MYSUB = IJK-KPR
      ITN = NLSFLG(MYSUB)
      IF(K.NE.1.OR.IJUB(IJ).EQ.0) GO TO 200
      AXK=ABS(VEE(MYSUB))-DB(IJ)
      IF(AXK.LT.0.) AXK=0.
      IF((VEE(MYSUB).LT.0.AND.IJUB(IJ).GT.0).OR.
      1 (VEE(MYSUB).GT.0.AND.IJUB(IJ).LT.0)) AXK=0.
      GO TO 201
200 AXK = ABS(VEE(MYSUB))
201 PTR = CHUG(ITN)
      IF(AXK.LT.XKR(PTR)) GO TO 110
      IF(AXK.GT.XKR(PTR+1)) GO TO 120
      140 KR(K) = XKS(PTR)*AXK+XKI(PTR)
C
C      CALCULATE STUFF FOR YIELDING AND RUPTURE SUMMARY TABLES,
C      (YIELDING ONLY HERE).

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ISN 0413
ISN 0414
ISN 0416
ISN 0417
ISN 0418
ISN 0419
ISN 0420
ISN 0422
ISN 0423
ISN 0424

ISN 0425
ISN 0426

ISN 0427
ISN 0428
ISN 0430
ISN 0432
ISN 0434
ISN 0436
ISN 0437
ISN 0438
ISN 0440
ISN 0441
ISN 0442

ISN 0443
ISN 0444
ISN 0445
ISN 0447
ISN 0448
ISN 0450
ISN 0452
ISN 0453
ISN 0454
ISN 0455
ISN 0457
ISN 0459

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ISN 0460      C      IF(KRFLAG(IJK).NE.0) GO TO 141
ISN 0462      IF(KR(K).EQ.1.) GO TO 141
ISN 0464      KRCONT = KRCONT+1
ISN 0465      TKR(KRCONT) = TIME
ISN 0466      KRBEAM(1,KRCONT) = IJ
ISN 0467      KRBEAM(2,KRCONT) = K
ISN 0468      KRFLAG(IJK) = 1
ISN 0469      GO TO 141

C*****CHUG DOWN
ISN 0470      110 PTR = PTR-1
ISN 0471      IF(AXK.LT.XKR(PTR)) GO TO 110
ISN 0473      130 CHUG(ITN) = PTR
ISN 0474      GO TO 140

C*****CHUG UP
ISN 0475      120 PTR = PTR+1
ISN 0476      IF(AXK.GT.XKR(PTR+1)) GO TO 120
ISN 0478      GO TO 130
ISN 0479      144 KR(K) = 1
ISN 0480      GO TO 150

C      C      AFTER ALL THIS CHUGGING,140 CALCULATES KR.
C      C      NOTE THAT 130 SAVED LOCATION IN TABLE NO. ITN FOR THE
C      C      STARTING POINT AT THE NEXT TIME CUT.
C      C
ISN 0481      141 IF(K.EQ.1.OR.K.EQ.4) GO TO 150
ISN 0483      IF(K.EQ.2.OR.K.EQ.6) GO TO 142
ISN 0485      IF(KR(K).NE.1.AND.KFL35(IJ).EQ.0) KFL35(IJ) = K
ISN 0487      GO TO 150
ISN 0488      142 IF(KR(K).NE.1.AND.KFL26(IJ).EQ.0) KFL26(IJ) = K

C      C      THIS LOOP SETS KFL35 TO EITHER 3 OR 5,WHICHEVER KR TABLE
C      C      GOES NONLINEAR FIRST. FROM THEN ON,KR WILL BE READ FROM
C      C      THAT TABLE WHETHER K=3 OR 5. THE SAME GOES FOR KFL26.
C      C
ISN 0490      150 CONTINUE

C      C      SET KR=1. FOR UNLOADING AND RELOADING.
C      C
ISN 0491      IJL = 6*(IJ-1)
ISN 0492      DO 7000 L = 1,6
ISN 0493      IJL = IJL + 1
ISN 0494      A = D(L)

C      C      CORRECT Y AND Z DEFLECTIONS BY REMOVING ROTATION COMPONENT.
C      C      SEE ALSO LABEL 632.
C      C
ISN 0495      IF(L.EQ.2) A=A-XXLB*D(9)/2.
ISN 0497      IF(L.EQ.3) A=A+XXLB*D(8)/2.
ISN 0499      B = A + VEE(IJL)
ISN 0500      IF(A.GE.0.0.AND.B.GE.0.0.OR.A.LT.0.0.AND.B.LT.0.0) GO TO 7010

C      C      SIGNS ARE NOT THE SAME (UNLOADING)

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ISN 0502      C      IF(NI(IJL).NE.0) GO TO 7020
ISN 0504      NI(IJL) = 1
ISN 0505      VEEBAR(IJL) = ABS(VEE(IJL))
ISN 0506      GO TO 7020
ISN 0507      7010 IF(ABS(VEE(IJL)).LT.VEEBAR(IJL)) GO TO 7020

ISN 0509      C      LOADING PATH, USE KR FROM ABOVE.
ISN 0510      C
ISN 0511      NI(IJL) = 0
ISN 0512      GO TO 7000
ISN 0513      7020 KR(L) = 1.
ISN 0514      7000 CONTINUE
ISN 0515      IF(KR(5).NE.KR(3)) KR(5) = KR(3)
              IF(KR(6).NE.KR(2)) KR(6) = KR(2)

ISN 0517      C      LETS GET THE STIFFNESSES.
ISN 0518      C
ISN 0519      ISTART = 36*(IJ-1)
ISN 0520      XK11 = XK(ISTART + 1)
ISN 0521      XK22 = XK(ISTART + 8)
ISN 0522      XK26 = XK(ISTART + 12)
ISN 0523      XK33 = XK(ISTART + 15)
ISN 0524      XK35 = XK(ISTART + 17)
ISN 0525      XK44 = XK(ISTART + 22)
              XK55 = XK(ISTART + 29)
              XK66 = XK(ISTART + 36)

ISN 0526      C      CORRECT STIFFNESSES FOR CURRENT BEAM LENGTH.
ISN 0527      C
ISN 0528      C      XLB IS CURRENT LENGTH, XLB(IJ) IS ORIGINAL LENGTH.
ISN 0529      C
ISN 0530      XLBAT1 = XLB(IJ)/XXLB
ISN 0531      XLBAT2 = XLBAT1*XLBAT1
ISN 0532      XLBAT3 = XLBAT1*XLBAT2
ISN 0533      XK11SR=XK11
ISN 0534      XK44SR=XK44
ISN 0535      XK55SR=XK55
ISN 0536      XK66SR=XK66
ISN 0537      XK22SR=XK22
ISN 0538      XK33SR=XK33
ISN 0539      XK26SR=XK26
ISN 0540      XK35SR=XK35
              IF(MOLEQ.EQ.0) GO TO 4080
              DO 4081 JJ=1,MOLEQ
              IF(IGOLEO(JJ).EQ.IG(IJ).AND. JGOLEO(JJ).EQ.JG(IJ).AND.MGOLEO(JJ)
              1 .EQ.MG(IJ).AND.MGOLEO(JJ).EQ.MG(IJ)) GO TO 4083
              4081 CONTINUE
              GO TO 4080
              4083 XX55SR=XX55*SQRT(XLBAT1)
              XX66SR=XX66*SQRT(XLBAT1)
              XX22SR=XX22*SQRT(XLBAT3)
              XX33SR=XX33*SQRT(XLBAT3)
              XX26SR=XX26*SQRT(XLBAT2)

ISN 0542      ISN 0542
ISN 0543      ISN 0543
ISN 0544      ISN 0544
ISN 0545      ISN 0545
ISN 0546      ISN 0546
ISN 0547      ISN 0547
ISN 0548      ISN 0548

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ISN 0549      XK35SR=XK35*SQRT(XLRAT2)
ISN 0550      XK55=XK55*XLRAT1
ISN 0551      XK66=XK66*XLRAT1
ISN 0552      XK22=XK22*XLRAT3
ISN 0553      XK33=XK33*XLRAT3
ISN 0554      XK26=XK26*XLRAT2
ISN 0555      XK35=XK35*XLRAT2
ISN 0556      4080 CONTINUE

C
C   CALCULATE INCREMENTAL STRAIN FORCES DFJ AND DAMPING FORCES FDJ
C   AT J,N IN BEAM AXES.
C
ISN 0557      DFJ(1) = XK11*D(1)
ISN 0558      FDJ(1) = XK11SR*VEL(1)
ISN 0559      IF(IJUB(IJ).EQ.0) GO TO 202
ISN 0560      FDJ(1) = 0.
ISN 0561      IJ1 = 6*(IJ-1)+1
ISN 0562      IF(ABS(VEE(IJ1)+D(1)).GE.DB(IJ)) GO TO 202
ISN 0563      DFJ(1) = 0.
ISN 0564      202 DFJ(4) = XK44*D(4)
ISN 0565      FDJ(4) = XK44SR*VEL(4)
ISN 0566      202 DFJ(4) = XK44*D(4)
ISN 0567      FDJ(4) = XK44SR*VEL(4)

C
C   CALCULATE 2,6 LOADS.
C
ISN 0568      IF(PZ(IJ).EQ.0.AND.PZJ(IJ).EQ.0) GO TO 204
ISN 0569      IJPIN=0
ISN 0570      IF(PZ(IJ).NE.0.AND.ABS(SUMDF(6,IJ)).GE.PLM26(IJ)) GO TO 810
ISN 0571      IF(PZJ(IJ).NE.0.AND.ABS(SUMDF(6,IJ)).GE.PLM26J(IJ)) GO TO 812
ISN 0572      GO TO 204
ISN 0573      810 IF(PLM26(IJ).EQ.0.OR.FL26I(IJ).NE.0) GO TO 814
ISN 0574      812 IF(PLM26J(IJ).EQ.0.OR.FL26J(IJ).NE.0) GO TO 816
ISN 0575      FIRST TIME THRU FOR PLASTIC HINGE FORMATION SAVE DATA
ISN 0576      FOR SUMMARY TABLE. I END OF BEAM,6 DIRECTION
C
C
ISN 0577      FL26I(IJ)=1
ISN 0578      KPL=KPL+1
ISN 0579      TPL(KPL)=TIME
ISN 0580      BPL(KPL,1)=IJ
ISN 0581      BPL(KPL,2)=6
ISN 0582      IF(SUMDF(6,IJ).LT.0.) BPL(KPL,2)=-6
ISN 0583      BPL(KPL,3)=IG(IJ)
ISN 0584      814 IF(PZJ(IJ).NE.0.AND.ABS(SUMDF(6,IJ)).GE.PLM26J(IJ)) GO TO 816
ISN 0585      816 IJPIN=1
ISN 0586      812 IF(PLM26J(IJ).EQ.0.OR.FL26J(IJ).NE.0) GO TO 816
ISN 0587      FIRST TIME THRU FOR PLASTIC HINGE FORMATION.
ISN 0588      SAVE DATA FOR SUMMARY TABLE. J END OF BEAM,6 DIRECTION
ISN 0589      C
ISN 0590      C
ISN 0591      C
ISN 0592      FL26J(IJ)=1
ISN 0593      KPL=KPL+1
ISN 0594      TPL(KPL)=TIME
ISN 0595      BPL(KPL,1)=IJ

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ISN 0596      BPL(KPL,2)=6
ISN 0597      IF(SUMDF(6,IJ).LT.0.) BPL(KPL,2)=-6
ISN 0599      BPL(KPL,3)=JG(IJ)
ISN 0600      818 IF(IJPIN.EQ.1) GO TO 206
C
C PINNED AT J ONLY.
C
ISN 0602      DFJ(2) = XK22/4*DI(2)+XK26/2*DI(6)
ISN 0603      FDJ(2) = XK22SR/4*VEL(2)+XK26SR/2*VI(6)
ISN 0604      DFJ(6) = 0.
ISN 0605      FDJ(6) = 0.
ISN 0606      GO TO 210
C
C PINNED AT I ONLY.
C
ISN 0607      208 DFJ(2) = XK22/4*DI(2) + XK26/2*DI(6)
ISN 0608      FDJ(2) = XK22SR/4*VEL(2) + XK26SR/2*VJ(6)
ISN 0609      DFJ(6) = XK26/2*DI(2) + XK66*3/4*DI(6)
ISN 0610      FDJ(6) = XK26SR/2*VEL(2) + XK66SR*3/4*VJ(6)
ISN 0611      GO TO 210
C
C PINNED AT I AND J.
C
ISN 0612      206 DFJ(2) = 0.
ISN 0613      FDJ(2) = 0.
ISN 0614      DFJ(6) = 0.
ISN 0615      FDJ(6) = 0.
ISN 0616      GO TO 210
C
C FIXED AT I AND J. (NORMAL CASE)
C
ISN 0617      204 DFJ(2) = XK22*DI(2) + XK26*DI(9)
ISN 0618      FDJ(2) = XK22SR*VEL(2) + XK26SR*VEL(9)
ISN 0619      DFJ(6) = XK66*(DI(6)+3.*DI(9))/4. + XK26*DI(2)
ISN 0620      FDJ(6) = XK66SR*(VEL(6)+3.*VEL(9))/4. + XK26SR*VEL(2)
C
C CALCULATE 3,5 LOADS.
C
ISN 0621      210 IF(PY(IJ).EQ.0.AND.PY(IJ).EQ.0) GO TO 214
ISN 0623      IJPIN=0
ISN 0624      IF(PY(IJ).NE.0.AND.ABS(SUMDF(5,IJ)).GE.PLM35(IJ)) GO TO 820
ISN 0626      IF(PY(IJ).NE.0.AND.ABS(SUMDF(5,IJ)).GE.PLM35(IJ)) GO TO 822
ISN 0628      GO TO 214
ISN 0629      820 IF(PLM35(IJ).EQ.0.OR.FL35I(IJ).NE.0) GO TO 824
C
C FIRST TIME THRU FOR PLASTIC HINGE FORMATION.SAVE DATA
C FOR SUMMARY TABLE. I END OF BEAM,5 DIRECTION
C
ISN 0631      FL35I(IJ)=1
ISN 0632      KPL=KPL+1
ISN 0633      TPL(KPL)=TIME
ISN 0634      BPL(KPL,1)=IJ
ISN 0635      BPL(KPL,2)=5

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ISN 0636      IF(SUMDF(5,IJ).LT.0.) BPL(KPL,2)=-5
ISN 0638      BPL(KPL,3)=IG(IJ)
ISN 0639      824 IF(PYJ(IJ).NE.0.AND.ABS(SUMDF(5,IJ)).GE.PLM35J(IJ)) GO TO 826
ISN 0641      GO TO 218
ISN 0642      826 IJPIN=1
ISN 0643      822 IF(PLM35J(IJ).EQ.0.OR.FL35J(IJ).NE.0) GO TO 828
C
ISN 0645      C FIRST TIME THRU FOR PLASTIC HINGE FORMATION.
ISN 0646      C SAVE DATA FOR SUMMARY TABLE. J END OF BEAM,5 DIRECTION
ISN 0647      C
ISN 0648      FL35J(IJ)=1
ISN 0649      KPL=KPL+1
ISN 0650      TPL(KPL)=TIME
ISN 0651      BPL(KPL,1)=IJ
ISN 0652      BPL(KPL,2)=5
ISN 0653      IF(SUMDF(5,IJ).LT.0) BPL(KPL,2)=-5
C
ISN 0655      828 IF(IJPIN.EQ.1) GO TO 216
ISN 0656      C PINNED AT J ONLY.
ISN 0657      C
ISN 0658      C
ISN 0659      C
ISN 0660      DFJ(3) = XK33/4*D(3)+XK35/2*DI(5)
ISN 0661      FDJ(3) = XK33SR/4*VEL(3)+XK35SR/2*VI(5)
ISN 0662      DFJ(5) = 0.
ISN 0663      FDJ(5) = 0.
ISN 0664      GO TO 220
C
ISN 0665      C PINNED AT I AND J.
ISN 0666      C
ISN 0667      C
ISN 0668      C
ISN 0669      C
ISN 0670      216 DFJ(3) = XK33/4*D(3) + XK35/2*DI(5)
ISN 0671      FDJ(3) = XK33SR/4*VEL(3) + XK35SR/2*VI(5)
ISN 0672      DFJ(5) = XK35/2*D(3) + XK55*3/4*DJ(5)
ISN 0673      FDJ(5) = XK35SR/2*VEL(3) + XK55SR*3/4*VJ(5)
GO TO 220
C
ISN 0670      C FIXED AT I AND J. (NORMAL CASE)
ISN 0671      C
ISN 0672      C
ISN 0673      C
ISN 0674      214 DFJ(3) = XK33*D(3) + XK35*D(8)
ISN 0675      FDJ(3) = XK33SR*VEL(3) + XK35SR*VEL(8)
ISN 0676      DFJ(5) = XK55*(D(5)+3.*D(8))/4. + XK35*D(3)
ISN 0677      FDJ(5) = XK55SR*(VEL(5)+3.*VEL(8))/4. + XK35SR*VEL(3)
C
ISN 0678      C MULTIPLY DFJ'S BY KR'S.
ISN 0679      C
ISN 0680      C
ISN 0681      C
ISN 0682      C
ISN 0683      C
ISN 0684      C
ISN 0685      C
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ISN 1000      C

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ISN 0675      DFJ(J2) = KR(J2)*DFJ(J2)
ISN 0676      7030 CONTINUE
C
C  MULTIPLY FDJ'S BY DAMPING CONSTANTS.
C
      222 DO 6130 J2=1,6
            IF(J2.EQ.1.OR.J2.EQ.4) GO TO 6132
            IF(J2.EQ.2.OR.J2.EQ.6) GO TO 6134
            CON = 0.5*(C(3,IJ)+C(5,IJ))
            GO TO 6136
        6134 CON = 0.5*(C(2,IJ)+C(6,IJ))
        6136 FDJ(J2) = CON*FDJ(J2)
ISN 0683      GO TO 6130
ISN 0684      6130 CONTINUE
ISN 0685      6132 FDJ(J2) = C(J2,IJ)*FDJ(J2)
ISN 0686      6130 CONTINUE
ISN 0687      6130 CONTINUE
ISN 0688      6130 CONTINUE
ISN 0689      6130 CONTINUE
ISN 0690      6130 CONTINUE
C
C  CALCULATE INCREMENTAL FORCES AT I,M USING
C  STATIC BALANCE EQUATIONS. DAMPING FORCES ARE TOTAL.
C
      DO 6120 J2=1,6
            DFI(J2) = -DFJ(J2)
            FDI(J2) = -FDJ(J2)
        6120 CONTINUE
ISN 0691      DFI(5) = DFI(5) + XXLB*DFI(3)
ISN 0692      DFI(6) = DFI(6) - XXLB*DFI(2)
ISN 0693      FDI(5) = FDI(5) + XXLB*FDI(3)
ISN 0694      FDI(6) = FDI(6) - XXLB*FDI(2)
ISN 0695      FDI(5) = FDI(5) + XXLB*FDI(3)
ISN 0696      FDI(6) = FDI(6) - XXLB*FDI(2)
ISN 0697      FDI(5) = FDI(5) + XXLB*FDI(3)
ISN 0698      FDI(6) = FDI(6) - XXLB*FDI(2)
C
C  NOW SUM OVER TIME TO GET CURRENT TOTAL
C  FORCES AT I,M AND J,N. STILL IN BEAM AXES.
C
      IJK1 = 6*(IJ-1) + 1
      DO 630 K=1,6
            IF(K.NE.1.OR.IJUB(IJ).EQ.0) GO TO 602
            IF(TIME.EQ.0.) FUB(IJ) = 0.
            FUB(IJ) = FUB(IJ) + DFJ(K)
        630 CONTINUE
C
C  CHECK FOR UNSYMMETRICAL BEAMS.
C
      IF(K.NE.1.OR.IJUB(IJ).EQ.0) GO TO 602
      IF(TIME.EQ.0.) FUB(IJ) = 0.
      FUB(IJ) = FUB(IJ) + DFJ(K)
C
C  FUB(IJ) IS THE TOTAL AXIAL LOAD FOR UNSYMMETRICAL BEAMS
C  WITHOUT ANY RESTRICTIONS ON + OR -. NOW ZERO OUT SUMDF
C  IF REQUIRED. SUMDF IS USED IN SUBSEQUENT CALC'S AND PRINT.
C
      A = DI(K)
      B = VEE(IJK1) + A
      IF((B.LT.0.AND.IJUB(IJ).GT.0).OR.
         1 (B.GT.0.AND.IJUB(IJ).LT.0)) GO TO 606
      IF((FUB(IJ).LE.0.AND.IJUB(IJ).LT.0).OR.
         1 (FUB(IJ).GE.0.AND.IJUB(IJ).GT.0)) GO TO 604
      606 SUMDF(IK,IJ) = 0.
ISN 0706      A = DI(K)
ISN 0707      B = VEE(IJK1) + A
ISN 0708      IF((B.LT.0.AND.IJUB(IJ).GT.0).OR.
            1 (B.GT.0.AND.IJUB(IJ).LT.0)) GO TO 606
ISN 0710      IF((FUB(IJ).LE.0.AND.IJUB(IJ).LT.0).OR.
            1 (FUB(IJ).GE.0.AND.IJUB(IJ).GT.0)) GO TO 604
ISN 0712      606 SUMDF(IK,IJ) = 0.

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ISN 0713 SUMDFI(K,IJ) = 0.
ISN 0714 GO TO 600
ISN 0715 604 SUMDF(K,IJ) = FUB(IJ)
ISN 0716 SUMDFI(K,IJ) = -FUB(IJ)
ISN 0717 GO TO 600
ISN 0718 602 SUMDF(K,IJ) = SUMDF(K,IJ) + DFJ(K)
ISN 0719 SUMDFI(K,IJ) = SUMDFI(K,IJ) + DFJ(K)
ISN 0720 600 FSJ(K) = SUMDF(K,IJ)
ISN 0721 FSI(K) = SUMDFI(K,IJ)
ISN 0722 FINT(K,IJ) = FSJ(K) + FDJ(K)
ISN 0723 FINTI(K,IJ) = FSI(K) + FDI(K)
C
C REDO AXIAL LOAD CALCULATIONS FOR LANDING GEAR OLEO MODULES
C STRAIN FORCES ARE DUE TO AIR CURVE,DAMPING FORCES ARE DUE
C TO HYDRAULIC DAMPING & FRICTION
C
IF(INOLEO.EQ.0 .OR.K.NE.1) GO TO 630
DO 700 JJ=1,NOLEO
IF(I.EQ.IGOLEO(JJ).AND.J.EQ.JGOLEO(JJ).AND.M.EQ.MGOLEO(JJ)
1 .AND.N.EQ.NGOLEO(JJ)) GO TO 702
700 CONTINUE
ISN 0724 700 GO TO 630
ISN 0725 702 YOLEO(JJ)=YOLEO(JJ)-D(1)
ISN 0726 YOLEO=-VEL(1)
ISN 0727 FA=FAO(JJ)*(EOLEO(JJ)/(EOLEO(JJ)-YOLEO(JJ)))*EXPOLE(JJ)-FAA(JJ)
ISN 0728 BDAHP=BOLEO(JJ)
ISN 0729 IF(YDOLEO.LT.0) BDAMP=BROLEO(JJ)
ISN 0730 FH=BDAMP*YDOLEO*ABS(YDOLEO)
ISN 0731 ARGU=YDOLEO/ALPHAP
ISN 0732 FC=FCOUL(JJ)*TANH(ARGU)
ISN 0733 FCOMP=(YOLEO(JJ)-YHAX(JJ))*XKCOMP(JJ)
ISN 0734 IF(FCOMP.LT.0.) FCOMP=0.
ISN 0735 FEXT=YOLEO(JJ)*XKEXT(JJ)
ISN 0736 IF(FEXT.GT.0.) FEXT=0.
ISN 0737 FOLEO=FA+FH+FC+FEXT+FCOMP
ISN 0738 SUMDFI(K,IJ)=FA+FCOMP+FEXT
ISN 0739 SUMDF(K,IJ)=SUMDFI(K,IJ)
ISN 0740 FSI(K)=SUMDFI(K,IJ)
ISN 0741 FDI(K)=FH+FC
ISN 0742 FDJ(K)=-FDI(K)
ISN 0743 FINT(K,IJ)=FSJ(K)+FDJ(K)
ISN 0744 FINTI(K,IJ)=FSI(K)+FDI(K)
ISN 0745 630 CONTINUE
C
C STRESS CALCULATIONS
C
ISN 0756 IF(INSCEQ.0) GO TO 633
C
C Z1,Z2,X1Q AND SYIELD DATA STORED IN SMALL ARRAYS,REFERENCED BY
C NJ,WHICH VARIES FROM 1 TO NS. OTHER DATA STORED IN LARGE ARRAYS
C FOR BEAM DATA,REFERENCED BY IJ,WHICH VARIES FROM 1 TO NB.
C

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C C DETERMINE MAXIMUM BENDING MOMENTS ABOUT Y AND Z AXES.
C C THESE COULD OCCUR AT EITHER END OF BEAM (I OR J).
C C SHEAR FORCES AND AXIAL LOAD AND TORSION ARE CONSTANT ALONG BEAM.
C

501 FX = FINT(1,IJ)
    FY = FINT(2,IJ)
    FZ = FINT(3,IJ)
    PX = FINT(4,IJ)
    MYJ = FINT(5,IJ)
    MZJ = MYJ-XXLB*FZ
    MZI = MZJ+XXLB*FY
    MY = MYJ
    MZ = MZJ
    IF(PCR(IJ).NE.0.) GO TO 510
    SBUCKR(IJ) = 0.
    GO TO 512
510 SBUCKR(IJ)=FINT(1,IJ)/PCR(IJ)
512 IF(ABS(MYI).GT.ABS(MYJ)) MY = MYI
    IF(ABS(MZI).GT.ABS(MZJ)) MZ = MZI
C
C CALCULATE AXIAL STRESSES (SX) AND SHEAR STRESSES (SS)
C C FOR PLANE ELEMENTS LOCATED AT TOP,BOTTOM,RIGHT AND LEFT
C C SIDES OF BEAM.
C
C IF YY(IJ),ZZ(IJ)=0 SMXY,SMXZ BLOW UP CODE TO BYPASS
C IF (YY(IJ).NE.0.) GO TO 502
    SMXY =0.0
    GO TO 507
502 SMXY = MY*Z1(IJ)/YY(IJ)
507 IF(ZZ(IJ).NE.0.) GO TO 503
    SMXZ =0.0
    GO TO 504
503 SMXZ = MZ*Z2(IJ)/ZZ(IJ)
504 SSHX = MX*XIG(IJ)
    IF (AA(IJ).NE.0.0) GO TO 505
    SSFY =0.0
    SSFZ =0.0
    SXFX =0.0
    GO TO 506
505 SSFY = FY/AA(IJ)*1.5
    SSFZ = FZ/AA(IJ)*1.5
    SXFX = FX/AA(IJ)
C
C TOP (1)
C
506 SAX(1) = SXFX-SXMY
    SS(1) = SSHX+SSFY
C
C BOTTOM (2)
C
    SAX(2) = SXFX+SXMY
C
    ISN 0758
    ISN 0759
    ISN 0760
    ISN 0761
    ISN 0762
    ISN 0763
    ISN 0764
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ISN 0800      C      SS(2) =--SSMX+SSFY
ISN 0801      C      LEFT (3)
ISN 0802      C      SAX(3) = SXFX+SMXZ
ISN 0803      C      SS(3) = SSMX-SSFZ
ISN 0804      C      RIGHT (4)
ISN 0805      C      SAX(4) = SXFX-SMXZ
ISN 0806      C      SS(4) =--SSMX-SSFZ
ISN 0807      C      NOW, FOR EACH OF THE FOUR LOCATIONS, CALCULATE MAXIMUM SHEAR
ISN 0808      C      STRESS (SSM) AND PRINCIPAL STRESSES (S1,S2). USE THESE TO
ISN 0809      C      FORM RATIOS OF ACTUAL STRESS/FAILURE STRESS FOR TWO FAILURE
ISN 0810      C      CRITERIA. THE TWO CRITERIA USED ARE MAXIMUM SHEAR THEORY AND
ISN 0811      C      THEORY OF CONSTANT ENERGY OF DISTORTION. REFER TO ROARK, P. 94, 29.
ISN 0812      C      DO 653 IS=1,4
ISN 0813      C      SYIELD = STENS(MC(IJ))
ISN 0814      C      IF(SAX(IS).LT.0.) SYIELD=SCOMP(MC(IJ))
ISN 0815      C      SSM = SQRT(.25*SAX(IS)*SAX(IS)+SS(IS)*SS(IS))
ISN 0816      C      S1 = .5*SAX(IS)+SSM
ISN 0817      C      S2 = .5*SAX(IS)-SSM
ISN 0818      C      SP = SQRT(S1*S1+S2*S2-S1*S2)
ISN 0819      C      FRSI(IJ,IS) = SSM/SHEAR(MC(IJ))
ISN 0820      C      FRDI(IJ,IS) = SP/SYIELD
ISN 0821      C      653 CONTINUE
ISN 0822      C      C*****COMPUTE THE ENERGY HERE BUT ADD IT AFTER 230 (NO RUPTURE)
ISN 0823      C      633 SUMSEI = 0.0
ISN 0824      C      SUMDEI = 0.0
ISN 0825      C      SUMSEJ = 0.0
ISN 0826      C      SUMDEJ = 0.0
ISN 0827      C      SUMSE = 0.0
ISN 0828      C      SUMDE = 0.0
ISN 0829      C      C*****DON'T USE AN IJ IF IT'S A DRI ELEMENT
ISN 0830      C      IF(IJPR(IJ).NE.0) GO TO 632
ISN 0831      C      DO 631 K = 1,6
ISN 0832      C      SUMSEI = SUMSEI + FSI(K)*DI(K)
ISN 0833      C      SUMDEI = SUMDEI + FDI(K)*DI(K)
ISN 0834      C      SUMSEJ = SUMSEJ + FSJ(K)*DJ(K)
ISN 0835      C      SUMDEJ = SUMDEJ + FDJ(K)*DJ(K)
ISN 0836      C      SUMSE = SUMSEI + SUMSEJ
ISN 0837      C      SUMDE = SUMDEI + SUMDEJ
ISN 0838      C      631 CONTINUE
ISN 0839      C      C UPDATE DEFLECTIONS AND CHECK FOR RUPTURE. FIRST CORRECT Y AND Z
ISN 0840      C      C DEFLECTIONS BY REMOVING COMPONENTS DUE TO ROTATION OF MASSES.
ISN 0841      C      632 D(2) = D(2) - XXLB*D(9)/2.
ISN 0842      C      D(3) = D(3) + XXLB*D(8)/2.
ISN 0843      C      IJL = 6*(IJ-1)
ISN 0844      C      DO 230 L = 1,6

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ISN 0836 IJL = IJL+1
ISN 0837 T = VEE(IJL)+D(L)
ISN 0838 TF=INT(L,IJ)
ISN 0839 FEE(IJL)=TF
ISN 0840 VEE(IJL) = T
ISN 0841 IF(T) 240,250,250
ISN 0842 240 IF(ABS(T)-VMAXN(IJL)) 251,260,260
ISN 0843 250 IF(T-VMAX(IJL)) 251,260,260
ISN 0844 260 IRUPSH(IJ)=1
ISN 0845 IF(T) 252,253,253
ISN 0846 252 PRINT 1040,IJ,L,VEE(IJL),VMAXN(IJL),TIME
ISN 0847 NDIR=-1
ISN 0848 1040 FORMAT(IH1,'NEG.DIRECTION RUPTURE'//IX,'BEAM',2X,'DIRECTION',3X,
1 'MAGNITUDE',6X,'ALLOWABLE',6X,'TIME'//IX,IS,5X,IS,1P3E15.6)
GO TO 256
ISN 0849 253 PRINT 1050,IJ,L,VEE(IJL),VMAX(IJL),TIME
ISN 0850 NDIR=1
ISN 0851 1050 FORMAT(IH1,'POS.DIRECTION RUPTURE'//IX,'BEAM',2X,'DIRECTION',3X,
ISN 0852 1 'MAGNITUDE',6X,'ALLOWABLE',6X,'TIME'//IX,IS,5X,IS,1P3E15.6)
GO TO 256
ISN 0853 251 IF(TF) 274,271,271
ISN 0854 274 IF(ABS(TF)-FMAXN(IJL)) 230,255,255
ISN 0855 271 IF(TF-FMAX(IJL)) 230,255,255
ISN 0856 255 IRUPSH(IJ)=1
ISN 0857 IF(TF) 272,273,273
ISN 0858 272 PRINT 1040,IJ,L,FEE(IJL),FMAXN(IJL),TIME
ISN 0859 NDIR=-1
ISN 0860 GO TO 256
ISN 0861 273 PRINT 1050,IJ,L,FEE(IJL),FMAX(IJL),TIME
ISN 0862 NDIR=1
ISN 0863 C
C
C CALCULATE STUFF FOR YIELDING AND RUPTURE SUMMARY TABLE,
C (RUPTURE ONLY HERE).
C
ISN 0864 256 KRCONT = KRCONT+1
ISN 0865 TKR(KRCONT) = TIME
ISN 0866 KRBEAM(1,KRCONT) = IJ
ISN 0867 KRBEAM(3,KRCONT) = L
ISN 0868 KRBEAM(4,KRCONT)=NDIR
ISN 0869 GO TO 1000
ISN 0870 230 CONTINUE
ISN 0871 SEIJ(IJ) = SEIJ(IJ)+SUMSEI
ISN 0872 DEIJ(IJ) = DEIJ(IJ)+SUMDEI
C
C SUM OVER BOTH TIME AND BEAMS.
C
ISN 0873 XSE(I) = XSE(I) + SUMSEI
ISN 0874 XDE(I) = XDE(I) + SUMDEI
ISN 0875 IF(IJ.NE.81) GO TO 280
C
C FOR TRANSVERSE BEAMS, ADD ENERGY AT J=81 END OF BEAM TO I MASS.
C
ISN 0877 XSE(I) = XSE(I) + SUMSEJ

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ISN 0878 XDE(I) = XDE(I) + SUMDEJ
ISN 0879 GO TO 282
ISN 0880 280 XSE(J) = XSE(J) + SUMSEJ
ISN 0881 XDE(J) = XDE(J) + SUMDEJ
C
C FOR A SYMMETRICAL MODEL WE MUST ADD SE AND DE CONTRIBUTIONS
C FROM THE OPPOSITE BEAMS THAT ARE NOT INPUT EXPLICITLY. WE
C DO NOT DO THIS FOR TRANSVERSE BEAMS OR THOSE ON THE
C AIRPLANE CL.
C
ISN 0882 282 IF(SYMF LG.NE.1.OR.J.EQ.81.OR.CLTEST(IJ).EQ.1.) GO TO 238
ISN 0884 SEIJ(IJ) = SEIJ(IJ)+SUMSE
ISN 0885 DEIJ(IJ) = DEIJ(IJ)+SUMDE
ISN 0886 XSE(I) = XSE(I) + SUMSEI
ISN 0887 XSE(J) = XSE(J) + SUMSEJ
ISN 0888 XDE(I) = XDE(I) + SUMDEI
ISN 0889 XDE(J) = XDE(J) + SUMDEJ
ISN 0890 238 IF (IJPRI(IJ).NE.0) DRI(IJ) = -6.5500*VEE(6*(IJ-1)+1)
C
C NOW ADD FSI AND FDI AND CALL IT FSI. SAME AT J. WE NO
C LONGER NEED SEPARATE STRAIN AND DAMPING FORCES.
C
DO 270 J2=1,6
FSI(J2) = FSI(J2) + FDI(J2)
FSJ(J2) = FSJ(J2) + FDJ(J2)
270 CONTINUE
C
C CONVERT BEAM FORCES TO MASS AXES AND REVERSE SIGNS TO GET
C FORCES ACTING ON MASSES. USE TRANSPOSE OF AIJTAJ OR AIJTAI.
C
IF (IJPRI(IJ).NE.0) GO TO 6210
T1 = -FSI(1)
T2 = -FSI(2)
T3 = -FSI(3)
FSI(1) = AIJTAI(1)*T1+AIJTAI(2)*T2+AIJTAI(3)*T3
FSI(2) = AIJTAI(4)*T1+AIJTAI(5)*T2+AIJTAI(6)*T3
FSI(3) = AIJTAI(7)*T1+AIJTAI(8)*T2+AIJTAI(9)*T3
T1 = -FSI(4)
T2 = -FSI(5)
T3 = -FSI(6)
FSI(4) = AIJTAI(1)*T1+AIJTAI(2)*T2+AIJTAI(3)*T3
FSI(5) = AIJTAI(4)*T1+AIJTAI(5)*T2+AIJTAI(6)*T3
FSI(6) = AIJTAI(7)*T1+AIJTAI(8)*T2+AIJTAI(9)*T3
6210 IF(J.EQ.81) GO TO 6200
T1 = -FSJ(1)
T2 = -FSJ(2)
T3 = -FSJ(3)
FSJ(1) = AIJTAJ(1)*T1+AIJTAJ(2)*T2+AIJTAJ(3)*T3
FSJ(2) = AIJTAJ(4)*T1+AIJTAJ(5)*T2+AIJTAJ(6)*T3
FSJ(3) = AIJTAJ(7)*T1+AIJTAJ(8)*T2+AIJTAJ(9)*T3
T1 = -FSJ(4)
T2 = -FSJ(5)
T3 = -FSJ(6)

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ISN 0921      FSJ(4) = AIJTAJ(1)*T1+AIJTAJ(2)*T2+AIJTAJ(3)*T3
ISN 0922      FSJ(5) = AIJTAJ(4)*T1+AIJTAJ(5)*T2+AIJTAJ(6)*T3
ISN 0923      FSJ(6) = AIJTAJ(7)*T1+AIJTAJ(8)*T2+AIJTAJ(9)*T3
ISN 0924      6200 CONTINUE
C
C      TO GET THE BEAM MOMENTS AT MASS J, WE MUST ACCOUNT FOR THE
C      MOMENTS DUE TO THE BEAM FORCES AT NODE POINT (J,N), WHICH
C      IS OFFSET FROM MASS J BY THE VECTOR (RX,RY,RZ). THESE VECTOR
C      ELEMENTS ARE SUBSCRIPTED BY NODE POINT, FROM 1 TO NNP, AND
C      ARE IN MASS J AXES.
C
ISN 0925      IF(N.EQ.0.OR.J.EQ.81) GO TO 3410
C
C      MOMENTS AT J, MASS J AXES.
C
ISN 0927      FSJ(4) = FSJ(4) + FSJ(3)*RY(JJ) - FSJ(2)*RZ(JJ)
ISN 0928      FSJ(5) = FSJ(5) - FSJ(3)*RX(JJ) + FSJ(1)*RZ(JJ)
ISN 0929      FSJ(6) = FSJ(6) + FSJ(2)*RX(JJ) - FSJ(1)*RY(JJ)
ISN 0930      3410 CONTINUE
C
C      MOMENTS AT I, MASS I AXES. SKIP FOR DRI ELEMENTS.
C
ISN 0931      IF(IJPR(IJ).NE.0) GO TO 264
ISN 0932      IF(M.EQ.0) GO TO 266
ISN 0933      FSI(4) = FSI(4) + FSI(3)*RY(JI) - FSI(2)*RZ(JI)
ISN 0934      FSI(5) = FSI(5) - FSI(3)*RX(JI) + FSI(1)*RZ(JI)
ISN 0935      FSI(6) = FSI(6) + FSI(2)*RX(JI) - FSI(1)*RY(JI)
ISN 0936      GO TO 266
ISN 0937      264 DO 265 JJJ=1,6
ISN 0938      FSI(JJJ) = 0.
ISN 0939      265 CONTINUE
ISN 0940
ISN 0941      C
C      FOR SYMFLG = 1., WE LATER DOUBLE ALL XZ AND M INTERNAL
C      AND DAMPING LOADS ACTING ON A MASS ON THE AIRPLANE
C      PLANE OF SYMMETRY. SINCE WE DO THIS FOR ALL BEAMS,
C      HERE WE MUST HALVE THE LOADS FOR BEAMS THAT LIE
C      ENTIRELY IN THE PLANE OF SYMMETRY, SINCE THESE LOADS
C      SHOULD NOT BE DOUBLED. CLTEST(IJ) IS NE ZERO FOR THIS
C      CONDITION.
C
ISN 0942      266 CONTINUE
ISN 0943      IF(SYMFLG.NE.1.OR.CLTEST(IJ).EQ.0.) GO TO 5001
ISN 0944      DO 5002 JJJ=1,6
ISN 0945      FSJ(JJJ) = FSJ(JJJ)/2.
ISN 0946      FSI(JJJ) = FSI(JJJ)/2.
ISN 0947      5002 CONTINUE
ISN 0948
C
C      NOW SUM FORCES AT MASSES I AND J. SUMMING OVER BEAMS.
C
ISN 0949      5001 XX(I) = XX(I) + FSI(1)
ISN 0950      XY(I) = XY(I) + FSI(2)
ISN 0951      XZ(I) = XZ(I) + FSI(3)
ISN 0952      XL(I) = XL(I) + FSI(4)

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ISN 0953      XM(I) = XM(I) + FS(I,5)
ISN 0954      XN(I) = XN(I) + FS(I,6)
ISN 0955      IF(J.EQ.81) GO TO 1000
ISN 0957      XX(J) = XX(J) + FSJ(1)
ISN 0958      XY(J) = XY(J) + FSJ(2)
ISN 0959      XZ(J) = XZ(J) + FSJ(3)
ISN 0960      XL(J) = XL(J) + FSJ(4)
ISN 0961      XM(J) = XM(J) + FSJ(5)
ISN 0962      XN(J) = XN(J) + FSJ(6)
ISN 0963      1000 CONTINUE
C
C      END OF MAIN INTERNAL BEAM IJ LOOP.
C
      IS=9*(MVP-1)
      DO 1010 KS=1,9
      IS=IS+1
      1010 AP(KS)=BIJ(IS)
C FINISH COMPUTING DERIVATIVES
C      SET COUNTER=0 FOR ACCEL PULSE
      NPTSP=0
      NPTS=0
      DO 2000 I = 1,NH
      IS = 9*(I-1)
      DO 330 KS = 1,9
      IS = IS+1
      AIDOT(KS) = CIJ(IS)
      330 AI(KS) = BIJ(IS)
C DO CRASH FORCES
      DO 460 JI=1,6
      XC(JI) = 0.
      460 CONTINUE
      DO 340 IKM=1,NSP
      IF(I.EQ.II(IKM)) GO TO 400
      340 CONTINUE
      400 CALL CFORCE
      C (20),(23),(24)
      440 XA = MGT(I)-ALIFT(I)*MTOT
      SX = XX(I)+XA*AI(3)+XC(1)
      SY = XY(I)+XA*AI(6)+XC(2)
      SZ = XZ(I)+XA*AI(9)+XC(3)
      SL = XL(I)+XC(4)
      SM = XM(I)+XC(5)
      SN = XN(I)+XC(6)
C
C      IF WE HAVE A SYMMETRIC CASE (SYMFLG.NE.0) AND THE MASS WE ARE
C      CONSIDERING IS ON THE AIRPLANE CENTERLINE (YDI(I)=0), THEN WE
C      MUST CORRECT THE TOTAL FORCES AND MOMENTS TO ACCOUNT FOR THE
C      BEAMS ON THE OTHER SIDE, NOT CALCULATED, THAT CONNECT TO THIS MASS.
C
      IF(SYMFLG.EQ.0.OR.YDI(I).NE.0.) GO TO 1011
      SY = 0.
      SL = 0.
ISN 0992
ISN 0994
ISN 0995

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ISN 0996      SN = 0.
ISN 0997      IF(SYMFLEQ.2.) GO TO 1011
ISN 0999      SX = SX+XX(I)
ISN 1000      SZ = SZ+XZ(I)
ISN 1001      SM = SM+XM(I)
ISN 1002      C GEY P,Q,R,U,V,W
ISN 1003      1011 PP = P(I)
ISN 1004      QQ = Q(I)
ISN 1005      RR = R(I)
ISN 1006      UU = U(I)
ISN 1007      VV = V(I)
ISN 1008      WW = W(I)
ISN 1009      C MASS
ISN 1010      ZH=366.0/MST(I)
ISN 1011      IF(ETIME.NE.0.) GO TO 343
ISN 1012      XACF(I) = XACC(I)
ISN 1013      YACF(I) = YACC(I)
ISN 1014      ZACF(I) = ZACC(I)
ISN 1015      C TEMP CALCS
ISN 1016      XACF(I)=0.
ISN 1017      YACF(I)=0.
ISN 1018      ZACF(I)=0.
ISN 1019      C (25)
ISN 1020      343 UDOTI = UDOT(I)
ISN 1021      VDOTI = VDOT(I)
ISN 1022      WDOTI = WDOT(I)
ISN 1023      UDOT(I)=SX*ZH-QQ*MM+RR*VV
ISN 1024      VDOT(I)=SY*ZH-PP*UU+QQ*UU
ISN 1025      WDOT(I)=SZ*ZH-PP*VV+QQ*UU
ISN 1026      IF(INACC.EQ.0) GO TO 341
ISN 1027      CALL ACCELT(I,UDOT(I),VDOT(I),WDOT(I),PDOT(I),QDOT(I),RDOT(I),
ISN 1028      ITIME,NPTSP,NPTS)
ISN 1029      NPTSP=NPTS
ISN 1030      341 XACC(I)=(UDOT(I)+QQ*MM-RR*VV)/366.
ISN 1031      YACC(I)=(VDOT(I)+RR*UU-PP*MM)/366.
ISN 1032      ZACC(I)=(WDOT(I)+PP*VV-QQ*UU)/366.
ISN 1033      XACFDI = XACFD(I)
ISN 1034      YACFDI = YACFD(I)
ISN 1035      ZACFDI = ZACFD(I)
ISN 1036      IF(PFIL.EQ.0.) GO TO 344
ISN 1037      XACFDI = (XACC(I)-XACF(I))/PFIL
ISN 1038      YACFDI = (YACC(I)-YACF(I))/PFIL
ISN 1039      ZACFDI = (ZACC(I)-ZACF(I))/PFIL
ISN 1040      60 TO 345
ISN 1041      344 XACFDI = 0.
ISN 1042      YACFDI = 0.
ISN 1043      ZACFDI = 0.
ISN 1044      C (26)
ISN 1045      345 T1 = -XZI(I)*PP-YZI(I)*QQ+ZI(I)*RR+HEZ(I)
ISN 1046      T2 = XI(I)*PP-XZI(I)*QQ-XZI(I)*RR+HEX(I)
ISN 1047      T3 = -XYI(I)*PP+YI(I)*QQ-YZI(I)*RR+HEY(I)
ISN 1048      SL = SL-QQ*T1+RR*T3
ISN 1049      SM = SM-RR*T2+PP*T1

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00012600
00012610
00012620
00012630
00012640
00012650
00012660
00012670
00012680
00012690
00012700
00012710
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00012730
00012740
00012750
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00012780
00012790
00012800
00012810
00012820
00012830
00012840
00012850
00012860
00012870
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00012890
00012900
00012910
00012920
00012930
00012940
00012950
00012960
00012970
00012980
00012990
00013000
00013010
00013020
00013030
00013040
00013050
00013060
00013070
00013080
00013090
00013100
00013110
00013120

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ISN 1047 C (25) SN = SN-PP*T3+QQ*T2
ISN 1048 DEL = DEL(I)
ISN 1049 POOT(I) = POOT(I)
ISN 1050 POOT(I) = DEL*(SL*XI1(I)+SM*XI2(I)+SN*XI3(I))
ISN 1051 QOOT(I) = QOOT(I)
ISN 1052 QOOT(I) = DEL*(SL*XI2(I)+SM*XI5(I)+SN*XI4(I))
ISN 1053 RROOT(I) = RROOT(I)
ISN 1054 RROOT(I) = DEL*(SL*XI3(I)+SM*XI4(I)+SN*XI6(I))

C
C FOR A SYMMETRICAL CASE, CONSTRAIN THE ACCELERATIONS OF THE
C CENTERLINE MASSES.
C
IF(SYMFLEQ.0.0.OR.YDP(I).NE.0.) GO TO 342
VROOT(I) = 0.
PROOT(I) = 0.
RROOT(I) = 0.
342 XROOT(I) = XROOT(I)
YROOT(I) = YROOT(I)
ZROOT(I) = ZROOT(I)
PHROOT(I) = PHROOT(I)
THROOT(I) = THROOT(I)
PSDOTT(I) = PSDOTT(I)
IF(TIME) 1900,1900,300

C
C ...VARIABLE INTEGRATION ADDED 11/09/77 DHS...
C
300 UP = UI(I)
UI(I) = TT*U(I)+ET*(VOLD(I)+DHALF*(UDOT(I)+UDOTT(I))
ERR = AMAX1(ERR,
1(ABS(UDOT(I)-UDOTT(I)*DELTA)/
2 AMAX1(ABS(VOLD(I))+ABS(U(I)-VOLD(I)),1.D-06))

C
C VP = V(I)
V(I) = TT*V(I)+ET*(VOLD(I)+DHALF*(VDOT(I)+VDOTT(I))
ERR = AMAX1(ERR,
1(ABS(VDOT(I)-VDOTT(I)*DELTA)/
2 AMAX1(ABS(VOLD(I))+ABS(V(I)-VOLD(I)),1.D-06))

C
C WP = W(I)
W(I) = TT*W(I)+ET*(WOLD(I)+DHALF*(WDOT(I)+WDOTT(I))
ERR = AMAX1(ERR,
1(ABS(WDOT(I)-WDOTT(I)*DELTA)/
2 AMAX1(ABS(WOLD(I))+ABS(W(I)-WOLD(I)),1.D-06))

C
C PP = P(I)
P(I) = TT*P(I)+ET*(POLD(I)+DHALF*(PDOT(I)+PDOTT(I))
ERR = AMAX1(ERR,
1(ABS(PDOT(I)-PDOTT(I)*DELTA)/
2 AMAX1(ABS(POLD(I))+ABS(P(I)-POLD(I)),1.D-06))

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C
C
ISN 1079      QP = Q(I)
ISN 1080      Q(I) = TT*Q(I)+ET*(QOLD(I)+DTHALF*(QOOT(I)+QOOTI))
ISN 1081      ERR = AMAX1(ERR,
1(ABS(QOOT(I)-QOOTI)*DELTA)/
2      AMAX1(ABS(QOLD(I)+ABS(Q(I)-QOLD(I)),1.D-06))
C
C
ISN 1082      RP = R(I)
ISN 1083      R(I) = TT*(R(I)+ET*(ROLD(I)+DTHALF*(RDOT(I)+RDOTI))
ISN 1084      ERR = AMAX1(ERR,
1(ABS(RDOT(I)-RDOTI)*DELTA)/
2      AMAX1(ABS(ROLD(I)+ABS(R(I)-ROLD(I)),1.D-06))
C
C
C      CHANGE ERR DEFINITION FOR ENERGY BASED VARIABLE DT SCHEME.
C
C
ISN 1085      IF(IVAR.EQ.2) ERR=DEVMAX*THAX/TIME
ISN 1087      X(I) = TT*(X(I)+ET*(XOLD(I)+DTHALF*(XDOT(I)+XDOTI))
ISN 1088      Y(I) = TT*(Y(I)+ET*(YOLD(I)+DTHALF*(YDOT(I)+YDOTI))
ISN 1089      Z(I) = TT*(Z(I)+ET*(ZOLD(I)+DTHALF*(ZDOT(I)+ZDOTI))
ISN 1090      PHI(I) = TT*(PHI(I)+ET*(PHIOLD(I)+DTHALF*(PHIDOT(I)+PHIDOTI))
ISN 1091      THETA(I) = TT*(THETA(I)+ET*(THEOLD(I)+DTHALF*(THEDOT(I)+THEDOTI))
ISN 1092      PSI(I) = TT*(PSI(I)+ET*(PSIOLD(I)+DTHALF*(PSIDOT(I)+PSIDOTI))
ISN 1093      PINI(I) = TT*(PINI(I)+ET*(PINOLD(I)+DTHALF*(PINI(I)+POLD(I)))
ISN 1094      QINI(I) = TT*(QINI(I)+ET*(QINOLD(I)+DTHALF*(QI(I)+QOLD(I)))
ISN 1095      RINI(I) = TT*(RINI(I)+ET*(RINOLD(I)+DTHALF*(RI(I)+ROLD(I)))
C
C
C      XACI ETC ARE MASS IMPULSE CALCS 2-5-79
C
ISN 1096      XACI=XACF(I)
ISN 1097      YACI=YACF(I)
ISN 1098      ZACI=ZACF(I)
ISN 1099      XACF(I) = TT*XACF(I)+ET*(XAFOLD(I)+DTHALF*(XACFD(I)+XACFDI))
ISN 1100      YACF(I) = TT*YACF(I)+ET*(YAFOLD(I)+DTHALF*(YACFD(I)+YACFDI))
ISN 1101      ZACF(I) = TT*ZACF(I)+ET*(ZAFOLD(I)+DTHALF*(ZACFD(I)+ZACFDI))
ISN 1102      XIMP(I)=TT*XIMP(I)+ET*(XIMPOLD(I)+DTHALF*(XACF(I)+XACI))
ISN 1103      YIMP(I)=TT*YIMP(I)+ET*(YIMPOLD(I)+DTHALF*(YACF(I)+YACI))
ISN 1104      ZIMP(I)=TT*ZIMP(I)+ET*(ZIMPOLD(I)+DTHALF*(ZACF(I)+ZACI))
ISN 1105      IF ((IPENSN(I).NE.0).OR.(I.EQ.MVP).OR.(MVP.EQ.0)) GO TO 1900
C
C
C      CONTROL VOLUME PENETRATION CALCULATIONS
C
ISN 1107      TP1=X(I)-X(MVP)
ISN 1108      TP2=Y(I)-Y(MVP)
ISN 1109      TP3=Z(I)-Z(MVP)
ISN 1110      XPI=AP(1)*TP1+AP(2)*TP2+AP(3)*TP3
ISN 1111      YPI=AP(4)*TP1+AP(5)*TP2+AP(6)*TP3
ISN 1112      ZPI=AP(7)*TP1+AP(8)*TP2+AP(9)*TP3
ISN 1113      IF ((-XNBAR.GT.XPI).OR.(XPI.GT.XPBAR)) GO TO 1900
ISN 1115      IF ((-YNBAR.GT.YPI).OR.(YPI.GT.YPBAR)) GO TO 1900
ISN 1117      IF ((-ZNBAR.GT.ZPI).OR.(ZPI.GT.ZPBAR)) GO TO 1900
ISN 1119      KPEN=KPEN+1

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ISN 1120 IPEN(KPEN)=I
ISN 1121 IPEN(KPEN)=TIME
ISN 1122 IPENSH(I)=1
ISN 1123 PRINT 1080, I, TIME
ISN 1124 1080 FORMAT(1H0, ' CONTROL VOLUME PENETRATED BY MASS ', I2, ' ', TIME=,
          1 F10.5)
C
C ZERO XCE AND XFE FOR ALL I'S PRIOR TO ENERGY CALCS BELOW.
C
ISN 1125 1900 XCE(I) = 0.
ISN 1126 XFE(I) = 0.
ISN 1127 2000 CONTINUE
ISN 1128 IF(NNP.EQ.0) GO TO 2008

C NOW CALCULATE THE VELOCITIES AND ACCELERATIONS OF THE NODE
C POINTS. THESE ARE USED ONLY FOR OUTPUT DATA.
C
DO 4000 J=1,NNP
  I = INP(J)
  OMCRX = -R(I)*RY(J)+Q(I)*RZ(J)
  OMCRY = R(I)*RX(J)-P(I)*RY(J)
  OMCZ = -Q(I)*RX(J)+P(I)*RY(J)
  OMCCRZ = -R(I)*OMCRY+Q(I)*OMCRZ
  OMCCRZ = R(I)*OMCRX-P(I)*OMCRZ
  UNP(J) = U(I)+OMCRX
  VNP(J) = V(I)+OMCRY
  WNP(J) = W(I)+OMCRZ
  IS = 9*(I-1)
  DO 4010 KS=1,9
    IS = IS+1
    AI(KS) = BIJ(IS)
  4010 CONTINUE
  TX = AI(1)*RX(J)+AI(4)*RY(J)+AI(7)*RZ(J)
  TY = AI(2)*RX(J)+AI(5)*RY(J)+AI(8)*RZ(J)
  TZ = AI(3)*RX(J)+AI(6)*RY(J)+AI(9)*RZ(J)
  XNP(J) = X(I)+TX
  YNP(J) = Y(I)+TY
  ZNP(J) = Z(I)+TZ
  XDNPJ(J) = AI(1)*UNP(J)+AI(4)*VNP(J)+AI(7)*WNP(J)
  YDNPJ(J) = AI(2)*UNP(J)+AI(5)*VNP(J)+AI(8)*WNP(J)
  ZDNPJ(J) = AI(3)*UNP(J)+AI(6)*VNP(J)+AI(9)*WNP(J)
  ACX = -RDOT(I)*RY(J)+QDOT(I)*RZ(J)
  ACY = -QDOT(I)*RX(J)-PDOT(I)*RY(J)
  ACZ = -QDOT(I)*RX(J)+PDOT(I)*RY(J)
  YACCNPJ(J) = XACC(I)+(ACX+OMCCRZ)/386.
  XACCNPJ(J) = YACC(I)+(ACY+OMCCRZ)/386.
  ZACCNPJ(J) = ZACC(I)+(ACZ+OMCCRZ)/386.
  IF(TIME.NE.0.) GO TO 4020
  XACNPF(J) = XACCNPJ(J)
  YACNPF(J) = YACCNPJ(J)
  ZACNPF(J) = ZACCNPJ(J)
  4020 XNPF(J) = XNPF(J)

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ISN 1167      YNPFDJ = YNPF(J)
ISN 1168      ZNPFJ = ZNPF(J)
ISN 1169      IF (PFIL.EQ.0.) GO TO 4030
ISN 1170      YNPF(J) = (XACNPF(J)-XACNPF(J))/PFIL
ISN 1171      YNPF(J) = (YACNPF(J)-YACNPF(J))/PFIL
ISN 1172      ZNPF(J) = (ZACNPF(J)-ZACNPF(J))/PFIL
ISN 1173      GO TO 4050
ISN 1174      4030 XNPF(J) = 0.
ISN 1175      YNPF(J) = 0.
ISN 1176      ZNPF(J) = 0.
ISN 1177      4050 IF (TIME) 4000,4000,4040
ISN 1178      XACNPI,XIMNPI ETC ARE MASS NODE POINT IMPULSE CALCS 2-5-79
C
C
C
ISN 1179      4040 XACNPI=XACNPF(J)
ISN 1180      YACNPI=YACNPF(J)
ISN 1181      ZACNPI=ZACNPF(J)
ISN 1182      XACNPF(J)=TT*XACNPF(J)+ET*(XANPFO(J)+DTHALF*(XNPF(J)+XNPF(J)))
ISN 1183      YACNPF(J)=TT*YACNPF(J)+ET*(YANPFO(J)+DTHALF*(YNPF(J)+YNPF(J)))
ISN 1184      ZACNPF(J)=TT*ZACNPF(J)+ET*(ZANPFO(J)+DTHALF*(ZNPF(J)+ZNPF(J)))
ISN 1185      XIMNPF(J)=TT*XIMNPF(J)+ET*(XIMNPL(J)+DTHALF*(XACNPF(J)
1 +XACNPI))
ISN 1186      YIMNPF(J)=TT*YIMNPF(J)+ET*(YIMNPL(J)+DTHALF*(YACNPF(J)
1 +YACNPI))
ISN 1187      ZIMNPF(J)=TT*ZIMNPF(J)+ET*(ZIMNPL(J)+DTHALF*(ZACNPF(J)
1 +ZACNPI))
ISN 1188      4000 CONTINUE
C
C
C
ISN 1189      2008 CONTINUE
ISN 1190      IF (IVAR.EQ.0) GO TO 2010
ISN 1191      IF (TIME) 2010,2010,2015
ISN 1192      2015 DELTA = 0.
ISN 1193      DT2 = 2. * DELTA
ISN 1194      IF (ERR.LT.EL) DELTA = RATHAX
ISN 1195      IF (ERR.GT.EU) .AND. (DELTA.GT. MINDT)) DELTA = RATHIN
ISN 1196      IF ((DELTA.EQ.0.) .AND. (IPC.EQ.1)) DELTA = 1.0
ISN 1197      IF (DELTA.EQ.0.) GO TO 2010
ISN 1198      IF (IPC.NE.1.) GO TO 2019
ISN 1199      TREL = DMOD(TIME+DELTA,TPRINT)
ISN 1200      TLEFT = TPRINT - TREL
ISN 1201      MPTSP = (TLEFT/DELTA) + .5
ISN 1202      DELT1 = TLEFT / MPTSP
ISN 1203      IPRINI = MPTSP + IPC + 1
ISN 1204      GO TO 2018
ISN 1205      2019 MPTS = IPRINT - IPC
ISN 1206      IF ((MPTS.EQ.0) .OR. (MPTS.EQ.1)) GO TO 2010
ISN 1207      TREL = DMOD(TIME+DELTA,TPRINT)
ISN 1208      TLEFT = TPRINT - TREL
ISN 1209      MPTSP = ((MPTS-1)/DELTA) + .5
ISN 1210      DELT1 = TLEFT / MPTSP
ISN 1211      IPRINI = IPC + MPTSP + 1
ISN 1212      DTX = DELT1 - DELTA
ISN 1213
ISN 1214
ISN 1215
ISN 1216
ISN 1217
ISN 1218
ISN 1219

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ISN 1220 IF (DTX.EQ.0.) GO TO 2010
ISN 1221 TIME1 = TIME
ISN 1222 DT2 = DELTAT + DELT1
ISN 1223 DELTAT = DELT1
ISN 1224 DTHALF = .5 * DELTAT
ISN 1225 IPRINT = IPRINT1
ISN 1226

ISN 1227 2010 DO 2011 IKM=1,NSP
ISN 1228 I = II(IKM)
ISN 1229 XCE(I) = XCE(I) + CEIK(IKM)
ISN 1230 XFE(I) = XFE(I) + CEIKF(IKM)
ISN 1231 2011 CONTINUE

C
C ENERGY CALCULATIONS BY MASS. CEIK AND CEIKF ALREADY SUMMED OVER
C TIME. NOW SUM OVER SPRINGS FOR GIVEN MASS.
C
ISN 1232 SET ZINIT(I)=Z(I) AT TIME=0
ISN 1233
ISN 1234 IF (TIME.NE.0.) GO TO 2012
ISN 1235 DO 2014 I=1,NM
ISN 1236 ZINIT(I)=Z(I)
ISN 1237 2012 CONTINUE
ISN 1238 2012 XETOTL = 0.
ISN 1239 KEYOTL = 0.
ISN 1240 PETOTL = 0.
ISN 1241 SETOTL = 0.
ISN 1242 DETOTL = 0.
ISN 1243 CETOTL = 0.
ISN 1244 FEOTL = 0.
ISN 1245 DEVHAX = 0.
ISN 1246 DO 2016 I = 1,NM
ISN 1247 C*****DON'T USE AN I IF IT'S = TO A J OF A DRI I,J PAIR
ISN 1248 DO 2017 IJ = 1,NB
ISN 1249 IF (IJPR(IJ).EQ.0) GO TO 2017
ISN 1250 IF (I.NE.JB(IJ)) GO TO 2017
ISN 1251 PEI(I) = 0.0
ISN 1252 KEI(I) = 0.0
ISN 1253 GO TO 2020
ISN 1254 2017 CONTINUE
ISN 1255 PEI(I) = -WGT(I)*Z(I)+ALIFT(I)*WTOT*(Z(I)-ZINIT(I))
ISN 1256 KEI(I) = .5*(WGT(I)*U(I)*U(I)+V(I)*V(I)+W(I)*W(I))/386.0
1 *P(I)*(PI)*XI(I)+Q(I)*XY(I)+R(I)*XZI(I)
2 *Q(I)*(PI)*XY(I)+Q(I)*YI(I)+R(I)*YZI(I)
3 *R(I)*(PI)*XZI(I)+Q(I)*YZI(I)+R(I)*ZI(I)

C
C FOR A SYMMETRICAL MODEL WE MUST ADD KE AND PE CONTRIBUTIONS
C FROM THE OPPOSITE MASSES THAT ARE NOT INPUT EXPLICITLY.
C
ISN 1257 IF (SYMFLG.NE.1.OR.YDP(I).EQ.0.) GO TO 2020
ISN 1258 PEI(I) = 2.*PEI(I)
ISN 1259 KEI(I) = 2.*KEI(I)
ISN 1260 2020 XETOT(I) = KEI(I)+PEI(I)+XSE(I)+XDE(I)+XCE(I)+XFE(I)
ISN 1261

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00015260
00015270
00015280
00015290
00015300
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00015370
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00015390
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00015670
00015680
00015690
00015700
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00015720
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00015740
00015750
00015760
00015770

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C C SUM OVER MASSES TO CHECK WITH OTHER ENERGY PRINT.
C
ISN 1262 KETOTL = KETOTL + KEI(I)
ISN 1263 PETOTL = PETOTL + PEI(I)
ISN 1264 SETOTL = SETOTL + XSE(I)
ISN 1265 DETOTL = DETOTL + XDE(I)
ISN 1266 CETOTL = CETOTL + XCE(I)
ISN 1267 FETOTL = FETOTL + XFE(I)
ISN 1268 KETOTL = KETOTL + XFE(I)
ISN 1269 IF(TIME.NE.0.) GO TO 2024
ISN 1270 KETOTO(I) = KETOTO(I)
ISN 1271 KETOTO(I) = KETOTO(I)
ISN 1272 2024 IF(XETOTO(I).NE.0) GO TO 2022
ISN 1273 XPC(I) = 100.
ISN 1274 GO TO 2030
ISN 1275 2022 XPC(I) = XETOTO(I)/XETOTO(I)*100.
ISN 1276 2030 DEV = ABS(XPC(I)-100.)
ISN 1277 DEVMAX = AMAX1(DEVMAX,DEV)
ISN 1278 2016 CONTINUE
ISN 1279
C C VOLUME CHANGE CALCULATIONS
C
ISN 1280 IF(NVCH) 2001,2001,2002
ISN 1281 2002 FLIP = 0.
ISN 1282 DO 2003 MI=1,NVCH
ISN 1283 VOL(MI) = 1.
ISN 1284 DO 2004 I=1,6
ISN 1285 SUMX = 0.
ISN 1286 SUMY = 0.
ISN 1287 SUMZ = 0.
C
C EACH ROW OF KMATR CONTAINS THE FOUR CORNER NUMBERS FOR THE
C APPROPRIATE SIDE OF THE CUBE
C
C EACH ROW OF INBUFF CONTAINS THE ACTUAL MASS NUMBERS FOR THE
C EIGHT CORNERS OF THE VOLUME
C
DO 2005 J=1,4
K = KMATR(I,J)
L = INBUFF(MI,K)
C
FOR A SYMMETRICAL MODEL THE MASS NUMBER L MAY BE 0, SO WE USE
THE MASS NUMBER FOR CORNER (K-1) AND CHANGE THE SIGN OF THE Y
COORDINATE. SEE PG. 1-66 OF LR27699, KRAH USERS MANUAL.
C
IF(L.NE.0) GO TO 2100
L = INBUFF(MI,K-1)
Y(L) = -Y(L)
FLIP = 1.
2100 SUMX = SUMX + X(L)
SUMY = SUMY + Y(L)
SUMZ = SUMZ + Z(L)
IF(FLIP.NE.1.) GO TO 2005
Y(L) = -Y(L)
C
ISN 1291
ISN 1292
ISN 1293
ISN 1294
ISN 1295
ISN 1296
ISN 1297
ISN 1298
ISN 1299
ISN 1301
00015780
00015790
00015800
00015810
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00015870
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00015970
00015980
00015990
00016000
00016010
00016020
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00016070
00016080
00016090
00016100
00016110
00016120
00016130
00016140
00016150
00016160
00016170
00016180
00016190
00016200
00016210
00016220
00016230
00016240
00016250
00016260
00016270
00016280
00016290
00016300

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ISN 1302      FLIP = 0.
ISN 1303      2005 CONTINUE
ISN 1304      XVOL(I,1) = SUMX/4.D0
ISN 1305      XVOL(I,2) = SUMY/4.D0
ISN 1306      XVOL(I,3) = SUMZ/4.D0
ISN 1307      2004 CONTINUE
C             NOW WE HAVE THE XYZ COORDINATES OF THE CENTERS OF THE SIX
C             SIDES OF VOLUME M
DO 2006 I=1,3
  SUM = 0.
DO 2007 J=1,3
  DXVOL = XVOL(2*I,J) - XVOL(2*I-1,J)
  SUM = SUM + DXVOL*DXVOL
2007 CONTINUE
  VOLLEN(MI,I) = SQRT(SUM)
  DLVOL(MI,I) = VOLLEN(MI,I)-VOLLEN(MI,I)
  VOL(MI) = VOL(MI)*VOLLEN(MI,I)
2006 CONTINUE
2003 CONTINUE
2001 RETURN
      END

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00016310
00016320
00016330
00016340
00016350
00016360
00016370
00016380
00016390
00016400
00016410
00016420
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00016440
00016450
00016460
00016470
00016480
00016490
00016500
00016510

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LEVEL 21.8 (JUN 74)

LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

A-68


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C NM,NB,I,J,IG(150),JG(150),
D NI(900),NN(40),L,PR(150)
EQUIVALENCE (XTHOLD(1,1),XYZIJJ(1,1),XTHOLD(1,2),XYZIJJ(1,1))
EQUIVALENCE (S1,SINCOS(1)),(C1,SINCOS(2)),(S2,SINCOS(3))
EQUIVALENCE (C2,SINCOS(4)),(S3,SINCOS(5)),(C3,SINCOS(6))
EQUIVALENCE (XK(1),XK3(1,1,1))
SIN(X) = DSIN(X)
COS(X) = DCOS(X)
SQRT(X) = DSQRT(X)
ATAN2(Y,X) = DATAN2(Y,X)
PI = 3.1415926535897932400
IOLD=0
DO 1100 I = 1,NM
  ARG=PHIDP(I)
  S1=SIN(ARG)
  C1=COS(ARG)
  ARG=THEDP(I)
  S2=SIN(ARG)
  C2=COS(ARG)
  ARG=PSIDP(I)
  S3=SIN(ARG)
  C3=COS(ARG)
  DO 1085 J = 1,6
    T=SINCOS(J)
    IF (T) 1070,1085,1075
  1070 T=-T
  1075 IF(T-I.E-10) 1080,1085,1085
  1080 SINCOS(J)=0.
  1085 CONTINUE
  J=9*(I-1)
C MOVE AI'S TO OLD AI'S
DO 1090 J2 = 1,9
  1090 OAI(J+J2)=BIJ(J+J2)
  S1S2=S1*S2
  C1S2=C1*S2
  BIJ(J+1)=C2*C3
  BIJ(J+2)=C2*S3
  BIJ(J+3)=-S2
  BIJ(J+4)=-C1*S3+S1S2*C3
  BIJ(J+5)=C1*C3+S1S2*S3
  BIJ(J+6)=S1*C2
  BIJ(J+7)=S1*S3+C1S2*C3
  BIJ(J+8)=-S1*C3+C1S2*S3
  BIJ(J+9)=C1*C2
1100 CONTINUE
PRINT 2021
2021 FORMAT(/ 1X,'BEAM UNCOUPLED,UNDAMPED FREQUENCIES (CPS)', /
1 2X,'I',2X,'J',2X,'M',2X,'N',
2 5X,'(1)',9X,'(2)',9X,'(3)',9X,'(4)',9X,
3 '(5)',9X,'(6)')
C
DO 1010 IJ = 1,NB
  I = IG(IJ)

```

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00000410
00000420
00000430
00000440
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00000460
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00000750
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00000770
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00000810
00000820
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00000870
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00000890
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00000920
00000930

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ISN 0023
ISN 0024
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ISN 0064
ISN 0065
ISN 0066

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ISN 0067
ISN 0068

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ISM 0069      J = J6(IJ)
ISM 0070      M = M6(IJ)
ISM 0071      N = N6(IJ)
ISM 0072      IF(J.NE.0) GO TO 3300
ISM 0073      J = 61
ISM 0074      IF(M.NE.0) GO TO 3301
ISM 0075      C
C
C IF J.EQ.0, WE HAVE A SYMMETRICAL MODEL IN WHICH BEAM IJ
C CONNECTS NODE POINT (I,M) TO AN IMAGINARY POINT (J,N=0)
C LOCATED SYMMETRICALLY ACROSS THE AIRPLANE PLANE OF SYMMETRY
C (X-Z PLANE). FOR THESE TRANSVERSE BEAMS, THE CONDITIONS AT (J,N)
C ARE DEDUCED FROM THE STATE AT (I,M). J IS CHANGED TO 61 BECAUSE
C THE IBM 360-91 WILL NOT ACCEPT A ZERO SUBSCRIPTED VECTOR.
C
C IF M.EQ.0, THERE IS NO NODE POINT AT I.
C
C 3302 XMODI = -XDP(I)
C      YMODI = -YDP(I)
C      ZMODI = -ZDP(I)
C      GO TO 3303
C
C THIS LOOP GETS NODE POINT NUMBER JI KNOWING I AND M.
C
C 3301 DO 3305 JI=1,NNP
C      IF(I.EQ.INP(JI).AND.M.EQ.MNP(JI)) GO TO 3306
C 3305 CONTINUE
C 3306 XMODI = -XNPDPI(JI)
C      YMODI = -YNPDPI(JI)
C      ZMODI = -ZNPDPI(JI)
C 3303 IF(J.NE.61) GO TO 3310
C
C IF J.EQ.61, WE HAVE A SYMMETRICAL MODEL. NOW CALCULATE
C CONDITIONS AT J,M BASED ON KNOWLEDGE OF STATE AT I,M.
C
C      XMODJ = XMODI
C      YMODJ = YMODI
C      ZMODJ = ZMODI
C      GO TO 3320
C 3300 IF(M.EQ.0) GO TO 3302
C      GO TO 3301
C 3310 IF(N.NE.0) GO TO 3311
C
C IF N.EQ.0, THERE IS NO NODE POINT AT J.
C
C      XMODJ = -XDP(J)
C      YMODJ = -YDP(J)
C      ZMODJ = -ZDP(J)
C      GO TO 3320
C
C THIS LOOP GETS NODE POINT NUMBER JJ KNOWING J AND N.
C
C 3311 DO 3312 JJ=1,NNP
C      IF(J.EQ.INP(JJ).AND.N.EQ.MNP(JJ)) GO TO 3313

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00001080
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00001100
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00001120
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00001190
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ISN 0106      3312 CONTINUE
ISN 0107      3313 XMODJ = -XNPDPI(JJ)
ISN 0108      YMODJ = -YNPDPI(JJ)
ISN 0109      ZMODJ = -ZNPDP(JJ)

C
C
C      ALL OF THE ABOVE PATHS LEAD TO HERE. WE NOW HAVE POSITIONS
C      (XMOD,ETC.) OF BOTH ENDS OF BEAM IJ.
C
      3320 XIJ = XMODJ-XMODI
      YIJ = YMODJ-YMODI
      ZIJ = ZMODJ-ZMODI
C
C CALCULATE AIJ. FIRST CALCULATE PHIJJ, THEIJ, PSIIJ.
C
      PHIJJ(IJ) = 0.
      IF(XIJ.EQ.0.AND.YIJ.EQ.0.) GO TO 3330
      PSIIJ(IJ) = ATAN2(YIJ,XIJ)
      GO TO 3340
      3330 PSIIJ(IJ) = 0.
      3340 THEIJ(IJ) = -ATAN2(ZIJ,SQRT(XIJ*XIJ+YIJ*YIJ))
C
C ZERO OUT VERY SMALL SIN AND COS TERMS.
C
      ARG = PHIJJ(IJ)
      S1 = SIN(ARG)
      C1 = COS(ARG)
      ARG = THEIJ(IJ)
      S2 = SIN(ARG)
      C2 = COS(ARG)
      ARG = PSIIJ(IJ)
      S3 = SIN(ARG)
      C3 = COS(ARG)
      DO 3392 J1 = 1,6
      T = SIN(COS(J1))
      IF(T) 3394,3392,3398
      3394 T = -T
      3398 IF(T-1.E-10) 3396,3392,3392
      3396 SIN(COS(J1)) = 0.0
      3392 CONTINUE
      S1S2 = S1*S2
      C1S2 = C1*S2
      AIJ(1) = C2*C3
      AIJ(2) = C2*S3
      AIJ(3) = -S2
      AIJ(4) = -C1*S3 + S1S2*C3
      AIJ(5) = C1*C3 + S1S2*S3
      AIJ(6) = S1*C2
      AIJ(7) = S1*S3 + C1S2*C3
      AIJ(8) = -S1*C3 + C1S2*S3
      AIJ(9) = C1*C2
      J2 = 9*(IJ-1)
      CBIJ = CBAR(IJ)
      IF ((IOLD.NE.0).AND.(I.EQ.IOLD)) GO TO 1120

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00001480
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0002000
0002010

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ISN 0151 IS=9*(I-1)
ISN 0152 DO 1110 J2 = 1,9
ISN 0153 IS=IS+1
ISN 0154 1110 AI(J2)=BIJ(IS)
ISN 0155 1120 IOLD=I
ISN 0156 IF(J.NE.01) GO TO 1121

C
C IF J=01, WE HAVE A SYMMETRICAL MODEL AND MUST CALCULATE AJ BASED
C ON AI RATHER THAN EULER ANGLES FOR MASS J, WHICH DOESN'T EXIST.
C
DO 1123 J2=1,9
AJ(J2) = AI(J2)
1123 CONTINUE
AJ(2) = -AJ(2)
AJ(4) = -AJ(4)
AJ(6) = -AJ(6)
AJ(8) = -AJ(8)
GO TO 1122
1121 IS=9*(J-1)
DO 1125 J2 = 1,9
IS=IS+1
1125 AJ(J2) = BIJ(IS)

C
C CALCULATE AIJTAJ AND AIJTAI. FILL TEMP WITH EITHER AJ OR AI.
C
1122 DO 6000 I3=1,2
DO 6010 I4=1,9
IF(I3.EQ.2) GO TO 6020
TEMP(I4) = AJ(I4)
GO TO 6010
6020 TEMP(I4) = AI(I4)
6010 CONTINUE
L2 = 0
DO 6030 K2=1,3
DO 6040 J2=1,3
L2 = L2+1
SUMM(L2) = 0.
DO 6050 I2=1,3
SUMM(L2) = SUMM(L2) + AIJ(3*(J2-1)+I2)*TEMP(3*(K2-1)+I2)
6050 CONTINUE
IF(I3.EQ.2) GO TO 6060
AIJTAJ(L2) = SUMM(L2)
GO TO 6040
6060 AIJTAI(L2) = SUMM(L2)
6040 CONTINUE
6030 CONTINUE
6000 CONTINUE

C
C COMPUTE BEAM FREQUENCY AND DAMPING CONSTANTS.
C
KKS=I
DO 1312 KS = 1,2
IF (KS.EQ.2.AND..J.NE.01) KKS=J

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ISN 0151
ISN 0152
ISN 0153
ISN 0154
ISN 0155
ISN 0156

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ISN 0188
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ISN 0200
ISN 0201
ISN 0202
ISN 0203
ISN 0204
ISN 0205
ISN 0206

XTHOLD(1,KS)=XI(KKS)
XTHOLD(2,KS)=XI(KKS)
XTHOLD(3,KS)=XI(KKS)
XTHOLD(4,KS)=XI(KKS)
XTHOLD(5,KS)=XI(KKS)
XTHOLD(6,KS)=XI(KKS)
XTHOLD(7,KS)=XI(KKS)
XTHOLD(8,KS)=XI(KKS)
XTHOLD(9,KS)=XI(KKS)

1312

C MASS I AND J INERTIAS ARE IN XYZIJI AND XYZIJJ WHICH ARE
C EQUIVALENT TO XTHOLD. NOW TRANSFORM BOTH TO BEAM IJ AXES
C BY PREMULTIPLYING BY AIJTAI(OR AIJTAJ) AND POSTMULTIPLYING
C BY THE TRANSPOSE OF SAME. XII AND XIJ ARE DIAGONAL ELEMENTS
C OF RESULTING INERTIA MATRIX FOR MASS I AND J, IN BEAM AXES.
C

ISN 0207
ISN 0208
ISN 0209
ISN 0210
ISN 0211
ISN 0212
ISN 0213
ISN 0214
ISN 0215
ISN 0216
ISN 0217
ISN 0218
ISN 0219
ISN 0220
ISN 0221
ISN 0222
ISN 0223
ISN 0224
ISN 0225
ISN 0226
ISN 0227
ISN 0228
ISN 0229
ISN 0230

ABT1=XVZIJ(1)*AIJTAI(1)+XVZIJ(4)*AIJTAI(4)+XVZIJ(7)*AIJTAI(7)
ABT2=XVZIJ(2)*AIJTAI(1)+XVZIJ(5)*AIJTAI(4)+XVZIJ(8)*AIJTAI(7)
ABT3=XVZIJ(3)*AIJTAI(1)+XVZIJ(6)*AIJTAI(4)+XVZIJ(9)*AIJTAI(7)
ABT4=XVZIJ(1)*AIJTAI(2)+XVZIJ(4)*AIJTAI(5)+XVZIJ(7)*AIJTAI(8)
ABT5=XVZIJ(2)*AIJTAI(2)+XVZIJ(5)*AIJTAI(5)+XVZIJ(8)*AIJTAI(8)
ABT6=XVZIJ(3)*AIJTAI(2)+XVZIJ(6)*AIJTAI(5)+XVZIJ(9)*AIJTAI(8)
ABT7=XVZIJ(1)*AIJTAI(3)+XVZIJ(4)*AIJTAI(6)+XVZIJ(7)*AIJTAI(9)
ABT8=XVZIJ(2)*AIJTAI(3)+XVZIJ(5)*AIJTAI(6)+XVZIJ(8)*AIJTAI(9)
ABT9=XVZIJ(3)*AIJTAI(3)+XVZIJ(6)*AIJTAI(6)+XVZIJ(9)*AIJTAI(9)
XXIJ(1) = AIJTAI(1)*ABT1+AIJTAI(4)*ABT2+AIJTAI(7)*ABT3
XXIJ(2) = AIJTAI(2)*ABT4+AIJTAI(5)*ABT5+AIJTAI(8)*ABT6
XXIJ(3) = AIJTAI(3)*ABT7+AIJTAI(6)*ABT8+AIJTAI(9)*ABT9
ABT1=XVZIJ(1)*AIJTAJ(1)+XVZIJ(4)*AIJTAJ(4)+XVZIJ(7)*AIJTAJ(7)
ABT2=XVZIJ(2)*AIJTAJ(1)+XVZIJ(5)*AIJTAJ(4)+XVZIJ(8)*AIJTAJ(7)
ABT3=XVZIJ(3)*AIJTAJ(1)+XVZIJ(6)*AIJTAJ(4)+XVZIJ(9)*AIJTAJ(7)
ABT4=XVZIJ(1)*AIJTAJ(2)+XVZIJ(4)*AIJTAJ(5)+XVZIJ(7)*AIJTAJ(8)
ABT5=XVZIJ(2)*AIJTAJ(2)+XVZIJ(5)*AIJTAJ(5)+XVZIJ(8)*AIJTAJ(8)
ABT6=XVZIJ(3)*AIJTAJ(2)+XVZIJ(6)*AIJTAJ(5)+XVZIJ(9)*AIJTAJ(8)
ABT7=XVZIJ(1)*AIJTAJ(3)+XVZIJ(4)*AIJTAJ(6)+XVZIJ(7)*AIJTAJ(9)
ABT8=XVZIJ(2)*AIJTAJ(3)+XVZIJ(5)*AIJTAJ(6)+XVZIJ(8)*AIJTAJ(9)
ABT9=XVZIJ(3)*AIJTAJ(3)+XVZIJ(6)*AIJTAJ(6)+XVZIJ(9)*AIJTAJ(9)
XXIJ(1) = AIJTAJ(1)*ABT1+AIJTAJ(4)*ABT2+AIJTAJ(7)*ABT3
XXIJ(2) = AIJTAJ(2)*ABT4+AIJTAJ(5)*ABT5+AIJTAJ(8)*ABT6
XXIJ(3) = AIJTAJ(3)*ABT7+AIJTAJ(6)*ABT8+AIJTAJ(9)*ABT9

C NOW CALCULATE EQUIVALENT MASS AND FREQUENCY. FINALLY,
C DAMPING CONSTANT = CBIIJ/PI/FREQ. THIS IS USED IN DERIV.
C

ISN 0231
ISN 0232
ISN 0233
ISN 0234
ISN 0235
ISN 0236
ISN 0237
ISN 0238
ISN 0239
ISN 0240

DO 1032 K=1,3
IF(J.NE.81) GO TO 1034
XMAS(K) = WGT(I)/2./366.
XMAS(K+3) = XXII(K)/2.
GO TO 1036
1034 XMAS(K) = WGT(I)*WGT(J)/(WGT(I)+WGT(J))/366.
XMAS(K+3) = XXII(K)*XXIJ(K)/(XXII(K)+XXIJ(K))
1036 FREQ(K) = SQRT(XK3(K,K,IJ)/XMAS(K))/2/PI
IF(FREQ(K).NE.0.) GO TO 1400

00002550
00002560
00002570
00002580
00002590
00002600
00002610
00002620
00002630
00002640
00002650
00002660
00002670
00002680
00002690
00002700
00002710
00002720
00002730
00002740
00002750
00002760
00002770
00002780
00002790
00002800
00002810
00002820
00002830
00002840
00002850
00002860
00002870
00002880
00002890
00002900
00002910
00002920
00002930
00002940
00002950
00002960
00002970
00002980
00002990
00003000
00003010
00003020
00003030
00003040
00003050
00003060
00003070

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ISN 0242      C(K,IJ) = 0.
ISN 0243      GO TO 1410
ISN 0244      1400 C(K,IJ) = CBIJ/PI/FREQ(K)
ISN 0245      1410 FREQ(K+3) = SQRT(XK3(K+3,K+3,IJ)/XMAS(K+3))/2/PI
ISN 0246      IF(FREQ(K+3).NE.0.) GO TO 1420
ISN 0247      C(K+3,IJ) = 0.
ISN 0248      GO TO 1032
ISN 0249      1420 C(K+3,IJ) = CBIJ/PI/FREQ(K+3)
ISN 0250      1032 CONTINUE
ISN 0251      PRINT 1030,IJ,IG(IJ),JG(IJ),NG(IJ),NG(IJ), (FREQ(K),K=1,6)
ISN 0252      1030 FORMAT(1X,5I3,1P6E12.4)
ISN 0253      1010 CONTINUE
ISN 0254      PRINT 1021
ISN 0255      1021 FORMAT(/ 1X, 'DAMPING TERMS (LB/IN/SEC, TRANSLATIONS (1)-(3) AND LB-
ISN 0256      1IN-SEC, ROTATIONS (4)-(6))' / 2X, 'IJ', 2X, 'I', 2X, 'J', 2X, 'M', 2X, 'N',
ISN 0257      2 7X, '(1)', 12X,
ISN 0258      3 '(2)', 12X, '(3)', 12X, '(4)', 12X, '(5)', 12X, '(6)')
ISN 0259      PRINT 1022,(IJ,IG(IJ),JG(IJ),NG(IJ),NG(IJ),
ISN 0260      1 (C(K,IJ),K=1,6),IJ=1,NB)
ISN 0261      1022 FORMAT(1X,5I3,1P6E15.5)
ISN 0262      PRINT 2053
ISN 0263      2053 FORMAT(/ 1X, 'EULER ANGLES, BEAM IJ TO AIRPLANE (RADIAN)')
ISN 0264      PRINT 2301
ISN 0265      2301 FORMAT(2X, 'IJ I J M N', 4X, 'THEIJO(IJ)', 5X, 'PSIIJO(IJ)')
ISN 0266      PRINT 2300,(IJ,IG(IJ),JG(IJ),NG(IJ),NG(IJ),
ISN 0267      1 THEIJO(IJ),PSIIJO(IJ),IJ=1,NB)
ISN 0268      2300 FORMAT (1X,5I3,1P2E15.5)
ISN 0269      RETURN
ISN 0270      END

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LEVEL 21.8 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.16.02

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
DATA SET D2334ECHO AT LEVEL 002 AS OF 07/20/78

ISN 0002	C	SUBROUTINE ECHO	00000010
ISN 0003	C	DIMENSION CARD (20)	00000020
ISN 0004	C		00000030
ISN 0005	C		00000040
ISN 0006	C		00000050
			00000060
			00000070
			00000080
			00000090
			00000100
			00000110
			00000120
			00000130
			00000140
			00000150
			00000160
			00000170
			00000180
			00000190
			00000200
			00000210
			00000220
			00000230
			00000240
			00000250
			00000260
			00000270
			00000280
			00000290

LEVEL 21.8 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.16.06

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
C SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
DATA SET 02334EULER AT LEVEL 001 AS OF 03/24/76

SUBROUTINE EULER(A,PHI,THETA,PSI)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(9)
SIN(X) = DSIN(X)
COS(X) = DCOS(X)
S1 = SIN(PHI)
C1 = COS(PHI)
S2 = SIN(THETA)
C2 = COS(THETA)
S3 = SIN(PSI)
C3 = COS(PSI)
A(1) = C2*C3
A(2) = C2*S3
A(3) = -S2
A(4) = -C1*S3+S1*S2*C3
A(5) = C1*C3+S1*S2*S3
A(6) = S1*C2
A(7) = S1*S3+C1*S2*C3
A(8) = -S1*C3+C1*S2*S3
A(9) = C1*C2
RETURN
END

ISN 0002
ISN 0003
ISN 0004
ISN 0005
ISN 0006
ISN 0007
ISN 0008
ISN 0009
ISN 0010
ISN 0011
ISN 0012
ISN 0013
ISN 0014
ISN 0015
ISN 0016
ISN 0017
ISN 0018
ISN 0019
ISN 0020
ISN 0021
ISN 0022
ISN 0023

00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000210
00000220

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINCNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
C DATA SET D2334FSHEL AT LEVEL 002 AS OF 05/17/78

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00000011
00000015
00000020
00000025
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120
00000130
00000140
00000150
00000160
00000170
00000180
00000190
00000200
00000210
00000220
00000230
00000240
00000250
00000260
00000270
00000280
00000290
00000300
00000310
00000320
00000330
00000340
00000350
00000360
00000370
00000380
00000390

SUBROUTINE FSHELL(ARRAY,KEY,N)
IMPLICIT REAL*8(A-H,O-Z)
INTEGER*2 N

C THIS IS A FORTRAN SUBROUTINE FOR SORTING AN INDEPENDENT ARRAY OF
C SIZE N INTO ASCENDING ORDER(ALGEBRAICALLY LEAST FIRST), AND
C PROVIDING A 'KEY' ARRAY WHICH WILL ALLOW SUBROUTINE SHELLX TO
C RETURN DEPENDENT ARRAYS TO THEIR ORIGINAL CORRESPONDENCE WITH THE
C INDEPENDENT ARRAY.
C
C DIMENSION ARRAY(1),KEY(1)
C
C ESTABLISH THE INITIAL CONDITION OF THE KEY ARRAY.
C
C DO 10 I=1, N
C 10 KEY(I) = I
C
C ESTABLISH THE INITIAL CONDITION FOR M, M IS THE CURRENT NUMBER
C OF SUBSETS INTO WHICH IARRAY HAS BEEN PARTITIONED.
C
C M = N
C
C REDUCE M, WHEN THE ALGORITHM PROCEEDS WITH THE REDUCED M, THE
C EFFECT IS A MERGE OF THE OLD SUBSETS INTO ABOUT HALF AS MANY
C NEW. INITIALLY, IARRAY IS PARTITIONED INTO ABOUT N/2 SUBSETS,
C EACH OF WHICH CONTAINS 2 ELEMENTS, WITH THE EXCEPTION THAT ONE
C SUBSET WILL CONTAIN 3 ELEMENTS IF N IS ODD. IT IS RECOMMENDED
C THAT A SAMPLE PROBLEM BE WORKED BY HAND TO UNDERSTAND THE
C MECHANISM OF THE PARTITIONING.
C
C 20 M = M / 2
C
C TEST THE REDUCED M. IF M IS ZERO, THE ENTIRE IARRAY HAS BEEN
C SORTED, AND CONTROL IS RETURNED TO THE CALLING PROGRAM.
C
C IF(M) 30,30,40
C 30 RETURN
C
C SET K=N-M. THE ELEMENTS IN IARRAY FROM IARRAY(1) TO IARRAY(K)

```

```

C      WILL BE USED AS 'BASE' ELEMENTS FOR COMPARISONS. THAT IS,
C      IARRAY(I) WILL BE COMPARED WITH IARRAY(I+M). THUS, ALL
C      ELEMENTS IN IARRAY WILL ENTER THE COMPARISON SEQUENCE.
C
ISN 0012      40 K = N - M
ISN 0013      DO 70 J=1, K
C
C      SINCE THE INDEX ADDRESSING THE 'BASE' ELEMENT MAY BE MODIFIED
C      'BACKWARDS' BY THE FOLLOWING CODE, SET I=J AND USE I FOR
C      THE 'BASE' INDEX. THIS PRESERVES THE CORRECT VALUE OF J FOR THE
C      NEXT 'BASE'.
C      I = J
C
C      II IS CREATED TO REFERENCE THE NEXT HIGHEST ELEMENT IN THE
C      CURRENT SUBSET, WHICH IS TO BE COMPARED WITH IARRAY(I).
C
ISN 0015      50 II = I + M
C
C      COMPARE ARRAY(I) WITH ARRAY(II)
C      IF(ARRAY(I) - ARRAY(II)) 70,70,60
C
C      60 TIMBO = ARRAY(I)
C      ARRAY(II) = ARRAY(II)
C      ARRAY(II) = TIMBO
C      TIMBO = KEY(I)
C      KEY(I) = KEY(II)
C      KEY(II) = TIMBO
C
C      I = I - M
C      IF(I) 70,70,50
C
C      THE ELEMENT IS PROPERLY PLACED IN ITS SUBSET. EXAMINE THE NEXT
C      'BASE' ELEMENT.
C      70 CONTINUE
C
C      ALL OF THE M SUBSETS HAVE BEEN SORTED
C      GO TO 20
C      END
ISN 0025
ISN 0026
ISN 0027

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ISN 0031  COMMON/MACF/IBS(40),FSPDP(40),SCP(40),JBS(40),
1  KXSPI(5,200),EXSPI(5,200),TSP(200),STEMP1(40),STEMP2(40),
2  STEMP3(40),STEMP4(40),STEMP5(40),KKONT
COMMON/INDEAC/ NACC
ISN 0032  COMMON/INIC/ XDPI(80),ZDPI(80),PHIDPI(80),PSIDP(80),
1  THEDPI(80),PPR,QPR,RPR,XGIN,ZGIN,PHIPR,PSIPR,THEPR,
2  XGDOT,YGDOT,ZGDOT
COMMON/INIDCP/ YDP(80)
ISN 0033  COMMON/INPR/ NDIR,NSP
COMMON/INCFIC/ BETA
ISN 0034  COMMON/MACFIN/ THAX,IPRINT
ISN 0035  COMMON/CORNEW/ DAHPC,RUNMOD,RUNMOD
ISN 0036  COMMON/NO014/ NNP
ISN 0037  COMMON/NO012/ MS,MS,INP,INP
ISN 0038  COMMON/NO012/ II,KK,MH
ISN 0039  COMMON/NO0212/ MS,NQ,IJVM,IJFM,IJVM,IJFM
ISN 0040  COMMON/NO0212/ XNPD,ZNPD
ISN 0041  COMMON/OLEO/OLEO(20),FAO(20),FAA(20),EXPOLE(20),YMAX(20),
ISN 0042  1  YOLEO(20),BOLEO(20),BROLEO(20),XXEXT(20),XKCOMPI(20),FCOUL(20),
2  ALPHAP,IGOLEO(20),JGOLEO(20),NGOLEO(20),NGOLEO(20),NGOLEO
COMMON/CORALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),
1  Y(81),Z(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),
2  YI(80),ZI(80),XVI(80),XZI(80),YXI(80),AXI(9),BIJ(720),
3  DRI(150),OAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80),
4  PDOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),
5  YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
6  XACCI(80),YACCI(80),ZACCI(80),AIDOT(9),
7  PHILJ(150),THEIJ(150),PSIIJ(150),SUMDF(6,150),TITLE,
8  XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9  DPINI(81),DQINI(81),DRINI(81),SEIJ(150),DEIJ(150),CEIK(40),
A  CEIK(40),
B  SBAR(40),KUN(40),MAXNM,MAXIGS,MAXTBL,
C  NY,NB,I,J,IG(150),JG(150),
D  NI(900),NN(40),IJPR(150)
COMMON/CORR8/ 6
ISN 0046  COMMON/UB/ DB(150),IJB(150),NJB
ISN 0047  COMMON/STUFF/ NEMI(80),NEMIJ(150),NFOLD,NBOLD
ISN 0048  COMMON/CORR4/ KR ,LDP ,LDP1
ISN 0049  COMMON/CORR4/ND,NVBHN,NFBHN,NHT,NKH,NLB,
1  NPH ,NMTL ,NPTS ,NVBN ,IJPRT ,IPHDP,NFBM
ISN 0050  1  COMMON/CORR12/ IQ ,JQ ,LQ ,NPQ ,INBUF ,
1  NKMVEC,IJSVE
COMMON/INAC/ACCEL(300),TIM(300),INDEX(50,2),JAY(50,2),KOUNT
ISN 0051  EQUIVALENCE (XK(1),XK3(1,1,1))
ISN 0052  EQUIVALENCE (VMAX(1),VMAX2(1,1)),(FMAX(1),FMAX2(1))
ISN 0053  EQUIVALENCE (VMAXN(1),VMAX3(1,1)),(FMAXN(1),FMAX3(1))
ISN 0054  EQUIVALENCE (VMAXN(1),VMAX3(1,1)),(FMAXN(1),FMAX3(1))
ISN 0055  EQUIVALENCE (MASSNO(1),INDEX(1,1)),(DIR(1),INDEX(1,2))
ISN 0056  DO 1 I=1,NP
ISN 0057  NEWI(I) = 0
ISN 0058  1  CONTINUE
ISN 0059  NPHEN = NY
ISN 0060  NFOLD = NY
ISN 0061  NNPOLD = NNP
ISN 0062  NNPOLD = NNP

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ISN 0063      C      CARDS 0100
ISN 0064      C      DO 10 I=1,NM
ISN 0065      C      IF(YDP(I).EQ.0.) GO TO 10
ISN 0066      C      NPNEW = NPNEW+1
ISN 0067      C      NEWI(I) = NPNEW
ISN 0068      C      NGT(NPNEW) = NGT(I)
ISN 0069      C      XDP(NPNEW) = XDP(I)
ISN 0070      C      YDP(NPNEW) = -YDP(I)
ISN 0071      C      ZDP(NPNEW) = ZDP(I)
ISN 0072      C      XI(NPNEW) = XI(I)
ISN 0073      C      YI(NPNEW) = YI(I)
ISN 0074      C      ZI(NPNEW) = ZI(I)
ISN 0075      C      10 CONTINUE
ISN 0076      C      NM = NPNEW
ISN 0077      C      CARDS 0200
ISN 0078      C      IF(NP.EQ.0) GO TO 2000
ISN 0079      C      DO 2001 I=1,NM
ISN 0080      C      NPNP(I) = 0
ISN 0081      C      2001 CONTINUE
ISN 0082      C      DO 2002 JJ=1,NP
ISN 0083      C      NEWNP(JJ) = 0
ISN 0084      C      I = INP(JJ)
ISN 0085      C      NPNP(I) = NPNP(I)+1
ISN 0086      C      2002 CONTINUE
ISN 0087      C      NPNP(I) CONTAINS THE NUMBER OF NODE POINTS ATTACHED TO
ISN 0088      C      MASS I, FOR ANY MASSES THAT HAVE NODE POINTS.
ISN 0089      C      NPNEW = NP
ISN 0090      C      DO 2010 JJ=1,NP
ISN 0091      C      I = INP(JJ)
ISN 0092      C      M = FRIP(JJ)
ISN 0093      C      IF(NEWI(I).EQ.0.AND.YNPDP(JJ).EQ.0.) GO TO 2010
ISN 0094      C      NEWNP(JJ) = NPNEW
ISN 0095      C      XNPDP(NPNEW) = XNPDP(JJ)
ISN 0096      C      YNPDP(NPNEW) = -YNPDP(JJ)
ISN 0097      C      ZNPDP(NPNEW) = ZNPDP(JJ)
ISN 0098      C      IF(NEWI(I).NE.0) GO TO 2020
ISN 0099      C      THIS IS CENTERLINE MASS WITH OFF-CENTER NODE POINT.
ISN 0100      C      NPNP(I) = NPNP(I)+1
ISN 0101      C      INP(NPNEW) = I
ISN 0102      C      FRIP(NPNEW) = NPNP(I)
ISN 0103      C      GO TO 2010
ISN 0104      C      THIS IS OFF-CENTER MASS.
ISN 0105      C
ISN 0106      C
ISN 0107      C
ISN 0108      C
ISN 0109      C
ISN 0110      C
ISN 0111      C
ISN 0112      C
ISN 0113      C
ISN 0114      C
ISN 0115      C
ISN 0116      C
ISN 0117      C
ISN 0118      C
ISN 0119      C
ISN 0120      C
ISN 0121      C
ISN 0122      C
ISN 0123      C
ISN 0124      C
ISN 0125      C
ISN 0126      C
ISN 0127      C
ISN 0128      C
ISN 0129      C
ISN 0130      C
ISN 0131      C
ISN 0132      C
ISN 0133      C
ISN 0134      C
ISN 0135      C
ISN 0136      C
ISN 0137      C
ISN 0138      C
ISN 0139      C
ISN 0140      C
ISN 0141      C
ISN 0142      C
ISN 0143      C
ISN 0144      C
ISN 0145      C
ISN 0146      C

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```

2020 INP(NSPNEW) = NEWI(I)
2010 CONTINUE
NMP = NMPNEW
C
C CARDS 0300
2000 IF(NSP.EQ.0) GO TO 41
NSPNEW = NSP
DO 30 J=1,NSP
I = II(J)
K = KK(J)
M = MM(J)
IF(M.EQ.0) GO TO 2003
DO 2004 JJ=1,NMP
IF(I.EQ.INP(JJ).AND.M.EQ.NMP(JJ)) GO TO 2005
2004 CONTINUE
2005 IF(NEWI(I).EQ.0.AND.YNPD(JJ).EQ.0.) GO TO 30
GO TO 2006
2003 IF(NEWI(I).EQ.0) GO TO 30
2006 NSPNEW = NSPNEW+1
KK(NSPNEW) = K
MM(NSPNEW) = M
IF(M.EQ.0) GO TO 2007
IF(NEWI(I).NE.0) GO TO 2007
II(NSPNEW) = I
MM(NSPNEW) = NMP(NEWI(JJ))
2007 XLBAR(NSPNEW) = XLBAR(J)
IF(K.EQ.2) XLBAR(NSPNEW) = -XLBAR(NSPNEW)
XMI(NSPNEW) = XMI(J)
XKE(NSPNEW) = XKE(J)
XMAX(NSPNEW) = XMAX(J)
GFLEX(NSPNEW) = GFLEX(J)
C
C CARDS 0400
SI(NSPNEW) = SI(J)
SA(NSPNEW) = SA(J)
SB(NSPNEW) = SB(J)
SF(NSPNEW) = SF(J)
FSPOI(NSPNEW) = FSPOI(J)
FSPOF(NSPNEW) = FSPOF(J)
CDAMP(NSPNEW)=CDAMP(J)
FSPOP(NSPNEW)=FSPOP(J)
SCPI(NSPNEW) =SCPI(J)
STEMP1(NSPNEW)=STEMP1(J)
STEMP2(NSPNEW)=STEMP2(J)
STEMP3(NSPNEW)=STEMP3(J)
STEMP4(NSPNEW)=STEMP4(J)
STEMP5(NSPNEW)=STEMP5(J)
30 CONTINUE
NSP = NSPNEW

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1500 0159

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ISN 0159      41 CONTINUE
C
C      CARDS 0500
C
      IF(NB.EQ.0) GO TO 101
      DO 99 I=1,NB
      NEWI(I) = 0
      99 CONTINUE
      NBNEW = NB
      NGOLD = NB
      DO 50 K=1,NB
      I = IG(K)
      J = JG(K)
      M = MG(K)
      N = NG(K)
      IF(M.EQ.0) GO TO 70
      DO 71 JJ=1, NNOLD
      IF(I.NE. INP(JJ).OR. M.NE. MNP(JJ)) GO TO 71
      IF(YNP(JJ).EQ.0.0) GO TO 72
      GO TO 51
      71 CONTINUE
      PRINT 2030
      2030 FORMAT(5X, '3. DATA ERROR IN GENMOD AT 2030')
      STOP
      70 IF(YDP(I).NE.0.0) GO TO 51
      72 IF(N.EQ.0) GO TO 73
      DO 74 JJ=1, NNOLD
      IF(J.NE. INP(JJ).OR. N.NE. MNP(JJ)) GO TO 74
      IF(YNP(JJ).EQ.0.0) GO TO 50
      GO TO 90
      74 CONTINUE
      PRINT 2040
      2040 FORMAT(5X, '4. DATA ERROR IN GENMOD AT 2040')
      STOP
      73 IF(YDP(J).EQ.0.0) GO TO 50
      GO TO 90
      51 IF(J.NE.0) GO TO 90
      JG(K) = NEWI(I)
      NG(K) = M
      GO TO 50
C
C      FOR ALL OTHER SITUATIONS, WE MUST ADD NEW BEAMS TO MODEL.
C
C      90 NBNEW = NBNEW+1
C      NEWI(K) = NBNEW
C      IF(YDP(I).EQ.0.0.OR. YDP(J).EQ.0.) GO TO 52
C
C      BOTH I AND J MASSES OFF AIRPLANE X-Z PLANE.
C
      IG(NBNEW) = NEWI(I)
      JG(NBNEW) = NEWI(J)
      MG(NBNEW) = M
      NG(NBNEW) = N
ISN 0206
ISN 0207
ISN 0208

ISN 0210
ISN 0211
ISN 0212
ISN 0213

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ISN 0214      GO TO 80
ISN 0215      52 ITEST = 0
ISN 0216      IF(YOPI).EQ.0.) GO TO 53
C
C      MASS I IS OFF X-Z PLANE, J IS ON.
C      GET NODE POINT NUMBER JN FOR MASS J.
C
ISN 0218      IF(N.NE.0) GO TO 55
ISN 0220      MS(NBNEW) = 0
ISN 0221      GO TO 57
ISN 0222      55 DO 54 JN=1,NNP
ISN 0223      IF(INP(JN).EQ.J.AND.MNP(JN).EQ.N) GO TO 56
ISN 0225      54 CONTINUE
ISN 0226      MS(NBNEW) = N
ISN 0227      IF(NENP(JN).EQ.0) GO TO 57
ISN 0229      MS(NBNEW) = MNP(NENP(JN))
ISN 0230      57 MS(NBNEW) = M
ISN 0231      IG(NBNEW) = J
ISN 0232      JG(NBNEW) = NEWI(I)
ISN 0233      GO TO 80
ISN 0234      53 IF(YOPI).EQ.0.) GO TO 59
C
C      MASS I IS ON X-Z PLANE, J IS OFF.
C      GET NODE POINT NUMBER JM FOR MASS I.
C
ISN 0236      60 IF(M.NE.0) GO TO 61
ISN 0238      MS(NBNEW) = 0
ISN 0239      GO TO 62
ISN 0240      61 DO 63 JM=1,NNP
ISN 0241      IF(INP(JM).EQ.I.AND.MNP(JM).EQ.M) GO TO 64
ISN 0243      63 CONTINUE
ISN 0244      64 MS(NBNEW) = M
ISN 0245      IF(NENP(JM).EQ.0) GO TO 62
ISN 0247      MS(NBNEW) = MNP(NENP(JM))
ISN 0248      62 IF(ITEST.NE.0) GO TO 58
ISN 0250      MS(NBNEW) = N
ISN 0251      IG(NBNEW) = I
ISN 0252      JG(NBNEW) = NEWI(J)
ISN 0253      GO TO 80
C
C      BOTH MASSES I AND J ARE ON X-Z PLANE.
C
ISN 0254      59 ITEST = 1
ISN 0255      IG(NBNEW) = I
ISN 0256      JG(NBNEW) = J
ISN 0257      GO TO 60
ISN 0258      58 IF(N.NE.0) GO TO 150
ISN 0260      MS(NBNEW) = 0
ISN 0261      GO TO 80
ISN 0262      150 DO 151 JN=1,NNP
ISN 0263      IF(INP(JN).EQ.J.AND.MNP(JN).EQ.N) GO TO 152
ISN 0265      151 CONTINUE
ISN 0266      152 MS(NBNEW) = N

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ISN 0267      IF(NBNEW(JN).EQ.0) GO TO 80
ISN 0269      NG(NBNEW) = NNP(NBNEW(JN))

C
C
C      ALL ABOVE STUFF GETS I,J,M AND N FOR NEW BEAM.
C      NOW SET ITS PARAMETERS EQUAL TO THOSE FOR ITS TWIN.
C
ISN 0270      80 MC(NBNEW) = MC(K)
ISN 0271      AA(NBNEW) = AA(K)
ISN 0272      YY(NBNEW) = YY(K)
ISN 0273      ZZ(NBNEW) = ZZ(K)
ISN 0274      XJ(NBNEW) = XJ(K)
ISN 0275      ZI(NBNEW) = ZI(K)
ISN 0276      Z2(NBNEW) = Z2(K)
ISN 0277      XIQ(NBNEW)=XIQ(K)
ISN 0278      PY(NBNEW) = PY(K)
ISN 0279      PJ(NBNEW)=PJ(K)
ISN 0280      PZ(NBNEW) = PZ(K)
ISN 0281      PJ(NBNEW)=PJ(K)
ISN 0282      SF26(NBNEW)=SF26(K)
ISN 0283      SF35(NBNEW)=SF35(K)
ISN 0284      SF26J(NBNEW)=SF26J(K)
ISN 0285      SF35J(NBNEW)=SF35J(K)
ISN 0286      CBAR(NBNEW) = CBAR(K)
ISN 0287      IJPR(NBNEW) = 0
ISN 0288      IJUB(NBNEW)=IJUB(K)
ISN 0289      DB(NBNEW)=DB(K)
ISN 0290      50 CONTINUE
ISN 0291      NB = NBNEW
ISN 0292      101 CONTINUE

C
C      CARDS 0601 AND UP
C
ISN 0293      IF(ND.EQ.0) GO TO 102
ISN 0295      CDUM = .01
ISN 0296      IF(DAMP.NE.0.) CDUM = DAMPC
ISN 0298      ND = 0
ISN 0299      DO 103 IJ=1,NB
ISN 0300      IF(CBAR(IJ).EQ.CDUM) GO TO 103
ISN 0302      ND = ND+1
ISN 0303      103 CONTINUE
ISN 0304      102 CONTINUE
ISN 0305      IF(NOLEO.EQ.0.) GO TO 709
ISN 0307      NOLEON=NOLEO
ISN 0308      DO 701 J=1,NOLEO
ISN 0309      DO 702 IJ=1,NBOLD
ISN 0310      IF(IGOLEO(IJ).EQ. IG(IJ).AND.JGOLEO(IJ).EQ. JG(IJ).AND.MGOLEO(IJ)
1.EQ.MG(IJ).AND. NGOLEO(J).EQ.NG(IJ)) GO TO 703
ISN 0312      702 CONTINUE
ISN 0313      703 IF(NEWIJ(IJ).EQ.0) GO TO 701
ISN 0315      JI=NEWIJ(IJ)
ISN 0316      NOLEON=NOLEON+1
ISN 0317      IGOLEO(NOLEON)=IG(JI)
ISN 0318      JGOLEO(NOLEON)=JG(JI)

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[illegible]

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NORI = NORINA
340 CONTINUE
C
C CARDS 1200
C IF(NVCH.EQ.0) GO TO 360
C SET EVEN NUMBERED CORNER MASS NUMBERS EQUAL TO NEW MASSES
C ACROSS FROM ODD NUMBERED CORNER MASSES.
C
DO 300 I=1,NVCH
DO 370 K=2,6,2
INBUFF(I,K) = NEMI(INBUFF(I,K-1))
370 CONTINUE
380 CONTINUE
360 CONTINUE
C
C CARDS 1300
C IF(NVBM.EQ.0) GO TO 450
NVBMM = NVBM
DO 410 JI=1,NVBM
IF(JG(IJVM(JI)).EQ.0) JG(IJVM(JI)) = NEMI(IG(IJVM(JI)))
I = IG(IJVM(JI))
J = JG(IJVM(JI))
M = MG(IJVM(JI))
N = NG(IJVM(JI))
DO 420 IJ=1,NBOLD
IF(I.EQ.IG(IJ).AND..J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
1 GO TO 430
420 CONTINUE
430 IF(NEMI(IJ).EQ.0) GO TO 410
NVBMN = NVBMM+1
IJVM(NVBMN) = NEMI(IJ)
DO 440 L=1,6
VMAX2(L,NEMI(IJ)) = VMAX2(L,IJ)
440 CONTINUE
410 CONTINUE
NVBM = NVBMM
450 CONTINUE
IF(NVBMN.EQ.0) GO TO 460
NVBMN=NVBMM
DO 461 JI=1,NVBMN
IF(JG(IJVMN(JI)).EQ.0) JG(IJVMN(JI))=NEMI(IG(IJVMN(JI)))
I=IG(IJVMN(JI))
J=JG(IJVMN(JI))
M=MG(IJVMN(JI))
N=NG(IJVMN(JI))
DO 462 IJ=1,NBOLD
IF (I.EQ.IG(IJ).AND..J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
1 GO TO 463
462 CONTINUE
463 IF(NEMI(IJ).EQ.0) GO TO 461
460 CONTINUE
461 CONTINUE

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ISN 0444 NVBMNM=NVBMM+1
ISN 0445 IJVM(NVBMM)=NEWIJ(IJ)
ISN 0446 DO 465 L=1,6
ISN 0447 VMAX3(L,NEWIJ(IJ))=VMAX3(L,IJ)
ISN 0448
ISN 0449 465 CONTINUE
ISN 0450 461 CONTINUE
ISN 0451 NVBMN=NVBMM
ISN 0452 460 CONTINUE
ISN 0453 IF(NFBM.EQ.0) GO TO 400
ISN 0454 NFBMM=NFBM
ISN 0455 DO 451 JI=1,NFBM
ISN 0456 IF(JG(IJFM(JI)).EQ.0) JG(IJFM(JI)) = NEWI(IG(IJFM(JI)))
ISN 0457 I = IG(IJFM(JI))
ISN 0458 J = JG(IJFM(JI))
ISN 0459 M = MG(IJFM(JI))
ISN 0460 N = NG(IJFM(JI))
ISN 0461 DO 452 IJ=1,NBOLD
ISN 0462 IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).
ISN 0463 1AND.N.EQ.NG(IJ)) GO TO 453
ISN 0465 452 CONTINUE
ISN 0466 453 IF(NEWIJ(IJ).EQ.0) GO TO 451
ISN 0468 NFBMM=NFBMM+1
ISN 0469 IJFM(NFBMM) = NEWIJ(IJ)
ISN 0470 DO 455 L=1,6
ISN 0471 FMAX2(L,NEWIJ(IJ))=FMAX2(L,IJ)
ISN 0472 455 CONTINUE
ISN 0473 451 CONTINUE
ISN 0474 NFBM=NFBMM
ISN 0475 400 CONTINUE
ISN 0476 IF(NFBM.EQ.0) GO TO 470
ISN 0478 NFBMM=NFBM
ISN 0479 DO 471 JI=1,NFBM
ISN 0480 IF(JG(IJFM(JI)).EQ.0) JG(IJFM(JI))=NEWI(IG(IJFM(JI)))
ISN 0482 I=IG(IJFM(JI))
ISN 0483 J=JG(IJFM(JI))
ISN 0484 M=MG(IJFM(JI))
ISN 0485 N=NG(IJFM(JI))
ISN 0486 DO 472 IJ=1,NBOLD
ISN 0487 IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
ISN 0489 1 GO TO 473
ISN 0490 472 CONTINUE
ISN 0491 473 IF(NEWIJ(IJ).EQ.0) GO TO 471
ISN 0492 NFBMM=NFBMM+1
ISN 0493 IJFM(NFBMM)=NEWIJ(IJ)
ISN 0494 DO 475 L=1,6
ISN 0495 FMAX3(L,NEWIJ(IJ))=FMAX3(L,IJ)
ISN 0496 475 CONTINUE
ISN 0497 471 CONTINUE
ISN 0498 NFBM=NFBMM
ISN 0499 470 CONTINUE
ISN 0500 LL=0
ISN 0501 L=KOUNT

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C

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ISN 0502 IF(NACC.EQ.0) GO TO 490
ISN 0504 NACNEW=NACC
ISN 0505 DO 476 K=1,NACC
ISN 0506 I=MASSNO(K)
ISN 0507 IF(NEWI(I).EQ.0) GO TO 491
ISN 0509 NACNEW=NACNEW+1
ISN 0510 IN=NEWI(I)
ISN 0511 MASSNO(NACNEW)=IN
ISN 0512 DIR(NACNEW)=DIR(K)
ISN 0513 NPTS(NACNEW)=NPTS(K)
ISN 0514 JAY(NACNEW,1)=NACNEW
ISN 0515 JJ=NPTS(K)
ISN 0516 DO 477 JK=1,JJ
ISN 0517 L=L+1
ISN 0518 LL=LL+1
ISN 0519 TIM(L)=TIM(LL)
ISN 0520 ACCEL(L)=ACCEL(LL)
ISN 0521 477 CONTINUE
ISN 0522 KOUNT=KOUNT+NPTS(K)
ISN 0523 IF(KOUNT.GT.300) GO TO 478
ISN 0525 491 CONTINUE
ISN 0526 NACC=NACNEW
ISN 0527 476 CONTINUE
ISN 0528 GO TO 490
ISN 0529 478 PRINT 479,NACC,KOUNT
ISN 0530 479 FORMAT(1X,'7.ERROR IN ACCEL TIME DATA INPUT'/1X,'NUMACL,KOUNT=',
1 215)
ISN 0531 490 CONTINUE
C
C CARDS 1400
ISN 0532 IF(NHI.EQ.0) GO TO 500
ISN 0534 NHINEM = NHI
ISN 0535 DO 510 K=1,NHI
ISN 0536 I = INBUF(K)
ISN 0537 IF(NEWI(I).EQ.0) GO TO 510
ISN 0539 NHINEM = NHINEM+1
ISN 0540 IN = NEWI(I)
ISN 0541 INBUF(NHINEM) = IN
ISN 0542 ALIFT(IN) = ALIFT(I)
ISN 0543 HEX(IN) = HEX(I)
ISN 0544 HEY(IN) = HEY(I)
ISN 0545 HEZ(IN) = HEZ(I)
ISN 0546 XYI(IN) = XYI(I)
ISN 0547 YZI(IN) = YZI(I)
ISN 0548 XZI(IN) = XZI(I)
ISN 0549 NHI = NHINEM
ISN 0550 510 CONTINUE
ISN 0551 500 CONTINUE
C
C CARDS 1500
ISN 0552 IF(NPH.EQ.0) GO TO 530
ISN 0554 NPHNEW = NPH

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ISN 0555	DO 540 J=1,NPH	00006240
ISN 0556	I = IPHDP(J)	00006250
ISN 0557	IF(NEWI(I).EQ.0) GO TO 540	00006260
ISN 0559	NPHNEW = NPHNEW+1	00006270
ISN 0560	IN = NEWI(I)	00006280
ISN 0561	PHDP(IN) = -PHDP(I)	00006290
ISN 0562	THEDP(IN) = THEDP(I)	00006300
ISN 0563	PSIDP(IN) = -PSIDP(I)	00006310
ISN 0564	IPHDP(NPHNEW) = IN	00006320
ISN 0565	540 CONTINUE	00006330
ISN 0566	NPH = NPHNEW	00006340
	C	00006350
	C	00006360
	C	00006370
	C	00006380
ISN 0567	DO 570 IJ=1,NBOLD	00006390
ISN 0568	IF(NEWI(IJ).EQ.0) GO TO 570	00006400
ISN 0570	IJN = NEWI(IJ)	00006410
ISN 0571	PHIJ(IJN) = -PHIJ(IJ)	00006420
ISN 0572	THEIJ(IJN) = THEIJ(IJ)	00006430
ISN 0573	PSIIJ(IJN) = -PSIIJ(IJ)	00006440
ISN 0574	570 CONTINUE	00006450
ISN 0575	530 CONTINUE	00006460
	C	00006470
	C	00006480
	C	00006490
ISN 0576	IF(NKM.EQ.0) GO TO 600	00006500
ISN 0578	NKMNEW = NKM	00006510
ISN 0579	DO 610 IJ=1,NBOLD	00006520
ISN 0580	IF(NKMVEC(IJ).EQ.0.OR.NEWI(IJ).EQ.0) GO TO 610	00006530
ISN 0582	NKMNEW = NKMNEW+1	00006540
ISN 0583	IJN = NEWI(IJ)	00006550
ISN 0584	NKMVEC(IJN) = 1	00006560
ISN 0585	DO 620 K=1,6	00006570
ISN 0586	DO 620 L=1,6	00006580
ISN 0587	XX3(L,K,IJN) = XX3(L,K,IJ)	00006590
ISN 0588	620 CONTINUE	00006600
ISN 0589	610 CONTINUE	00006610
ISN 0590	NKM = NKMNEW	00006620
ISN 0591	CONTINUE	00006630
ISN 0592	IF(PUNMOD.EQ.0) GO TO 700	00006640
ISN 0594	IPUNCH = 7	00006650
	C	00006660
	C	00006670
	C	00006680
	C	00006690
ISN 0595	WRITE(IPUNCH,1000) TITLE	00006700
	C	00006710
	C	00006720
ISN 0596	WRITE(IPUNCH,1010) NM,NSP,NB,NLB,NS,HVP,NVCH,NDR1,NPL,NACC,NVBH,	00006730
	1 NHI,NPH,ND	00006740
	C	00006750
	C	00006760

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ISN 0597      C      WRITE(IPUNCH,1020) IPRINT,DELTAT,TMAX,PILOTT,RUNMOD,NKM
ISN 0598      C      CARD 0005
ISN 0599      C      LINE = 005
ISN 0599      C      WRITE(IPUNCH,1030) XGDOT,YGDOT,ZGDOT,LINE
ISN 0600      C      CARD 0006
ISN 0601      C      LINE = 006
ISN 0601      C      WRITE(IPUNCH,1030) PPR,QPR,RPR,LINE
ISN 0602      C      CARD 0007
ISN 0603      C      LINE = 007
ISN 0603      C      WRITE(IPUNCH,1040) PHIPR,THEPR,PSIPR,XGIN,ZGIN,BETA,LINE
ISN 0604      C      CARDS 0100
ISN 0605      C      LINE = 101
ISN 0605      C      DO 900 I=1,NM
ISN 0606      C      WRITE(IPUNCH,1050) WGT(I),XDP(I),YDP(I),ZDP(I),XI(I),YI(I),ZI(I),
ISN 0607      C      1 LINE
ISN 0607      C      LINE = LINE+1
ISN 0608      C      900 CONTINUE
ISN 0609      C      CARDS 0200
ISN 0610      C      IF(NNP.EQ.0) GO TO 904
ISN 0611      C      LINE = 201
ISN 0612      C      WRITE(IPUNCH,1055) (MNP(I),INP(I),XNPDP(I),YNPDP(I),ZNPDP(I),
ISN 0613      C      1 I=1,NNP),LINE
ISN 0614      C      CARDS 0300
ISN 0615      C      904 LINE = 301
ISN 0615      C      DO 905 J=1,NSP
ISN 0616      C      WRITE(IPUNCH,1060) MM(J),II(J),KK(J),XLBAR(J),XMU(J),XKE(J),
ISN 0617      C      1 XMAX(J),LINE
ISN 0617      C      LINE = LINE+1
ISN 0617      C      905 CONTINUE
ISN 0618      C      CARDS 0400
ISN 0619      C      LINE = 401
ISN 0620      C      DO 910 J=1,NSP
ISN 0621      C      WRITE(IPUNCH,1040) SI(J),SA(J),SB(J),SF(J),FSPDI(J),FSPDF(J),
ISN 0622      C      1 LINE
ISN 0622      C      LINE = LINE+1
ISN 0622      C      910 CONTINUE
ISN 0622      C      CARDS 0500
ISN 0622      C

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ISN 0623      LINE = 501
ISN 0624      DO 915 I=1,NB
ISN 0625      WRITE(IPUNCH,1070) MG(I),IG(I),NG(I),JG(I),E(I),AA(I),G(I),
                1 YY(I),ZZ(I),PY(I),PZ(I),LINE
ISN 0626      LINE = LINE+1
ISN 0627      915 CONTINUE
                C
                C CARD 0600
                C
                C WRITE(IPUNCH,1080) DAMPC
                C
                C CARDS 0601 AND UP
                C
                C
                C LINE = 601
                C DO 920 IJ=1,NB
ISN 0629      WRITE(IPUNCH,1090) MG(IJ),IG(IJ),NG(IJ),JG(IJ),CBAR(IJ),LINE
ISN 0630      LINE = LINE+1
ISN 0631      920 CONTINUE
ISN 0632      C
ISN 0633      C CARDS 0700
                C
                C
                C CARDS 0800
                C
                C
                C CARDS 1000
                C
                C
                C CARD 1100
                C
                C
                C CARDS 1101 AND UP
                C
                C
                C CARDS 1200
                C
                C
                C CARDS 1300
                C
                C
                C CARDS 1400
                C
                C
                C CARDS 1500
                C
                C
                C CARDS 1600
                C
                C
                C CARDS 1700,1800
                C
                C
                C CARDS 2000
                C

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ISN 0640
ISN 0641
ISN 0642
ISN 0643
ISN 0644
ISN 0645
ISN 0646

C
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CARDS 2100

1000 FORMAT(20A4)
1010 FORMAT(14I5,7X,'003')
1020 FORMAT(110,1P3E10,3,20X,F5.1,I5,7X,'004')
1030 FORMAT(1P3E10,3,46X,I4)
1040 FORMAT(1P6E10,3,16X,I4)
1050 FORMAT(1P7E10,3,6X,I4)
1055 FORMAT(2I5,1P3E10,3,36X,I4)
1060 FORMAT(3I5,1P4E10,3,21X,I4)
1070 FORMAT(2(I2,I3),1P5E10,3,215,6X,I4)
1080 FORMAT(1P5E10,3,67X,'600')
1090 FORMAT(4I5,1P5E10,3,46X,I4)
700 RETURN
END

LEVEL 21.8 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.16.41

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LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,

SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,LD,XREF

C DATA SET D2334IC AT LEVEL 003 AS OF 06/25/79

C DATA SET D2332NIC AT LEVEL 007 AS OF 12/01/77

C DATA SET D2332NIC AT LEVEL 005 AS OF 11/04/77

C DATA SET D2332MIC AT LEVEL 002 AS OF 09/02/77

C SUBROUTINE IC

ISN 0002 C IMPLICIT REAL*8 (A-H,O-Z)

ISN 0003 REAL*8 KUN

ISN 0004 REAL*4 CLTEST

ISN 0005 INTEGER*4 PY(150),PZ(150),PVJ(150),PZJ(150)

ISN 0006 INTEGER*4 TITLE(40)

ISN 0007 INTEGER*2 NI,NN

ISN 0008 INTEGER*2 INBUFF

ISN 0009 INTEGER*2 IJPR,IG,JG

ISN 0010 INTEGER*2 II(40),KK(40),MM(40),NG(150),INP(50),MNP(50)

ISN 0011 DIMENSION XMPR(3),ABARPR(3,3),ANGDPR(3,3),DPR(3,3),AIDPI(3,3),

ISN 0012 1 AIC(3,3),ADPR(3,3),VJPI(80,3),APR(3,3),VJPI(3,3),XV(3)

ISN 0013 DIMENSION XK3(6,6,150),YZMINI(150)

ISN 0014 DIMENSION RX(50),RY(50),RZ(50),XNPDP(50),YNPDP(50),ZNPDP(50)

ISN 0015 DIMENSION XNP(50),YNP(50),ZNP(50),XDNPI(50),YDNPI(50),ZDNPI(50)

ISN 0016 DIMENSION UNP(50),VNP(50),MNP(50),XACCN(50),YACCN(50),ZACCN(50)

ISN 0017 DIMENSION IMDRI(80)

ISN 0018 COMMON/DEINPR/ AA(150),E(150),YY(150),ZZ(150),XIQ(150),

1 XLB(150),ZL(150),Z2(150),MC(150),XJ(150),SF26(150),SF35(150),

2 SF26J(150),SF35J(150),PY,PZ,PYJ,PZJ,NSC,NPIN

COMMON/CFIC/ SINBET,COSBET,ABETA(9)

COMMON/DINCP/ STENS(20),SCOMP(20),SHEAR(20),EE(20),GG(20),

1 FINI(6,150),VOL(5),VZERO(5),KMATRI(6,4),NVCH,INBUFF(5,8)

COMMON/INIC/ XDP(80),ZDP(80),PHIDP(80),PSIDP(80),

1 THEDP(80),PPR,QPR,RPR,XGIN,ZGIN,PHIPR,PSIPR,THEPR,

2 XGDOT,YGDOT,ZGDOT

COMMON/INIDCP/ YDP(80)

COMMON/INCFIC/ BETA

COMMON/INPR/ MDRI,NSP

COMMON/MCFII/ SYHFLG

COMMON/NP0012/ MG,NG,INP,MNP

COMMON/NP0112/ II,KK,MM

COMMON/NP0014/ NRP

COMMON/NP00R8/ RX,RY,RZ

COMMON/NP01R8/ XNP,YNP,UNP,VNP,MNP,XDNP,YDNP,ZDNP,

1 XACCNP,YACCNP,ZACCNP,SBUCKR(150),PCR(150)

ISN 0022

ISN 0023

ISN 0024

ISN 0025

ISN 0026

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ISN 0029

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LOCKHEED-CALIFORNIA CO BURBANK

GENERAL AVIATION AIRPLANE STRUCTURAL CRASHWORTHINESS USER'S MAN--ETC(U)

FEB 78 M A GAMON

DOT-FA75WA-3707

UNCLASSIFIED

LR-28307-VOL-1

FAA/RD-77/189-VOL-1

NL

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AD A
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ISN 0031      COMMON/NP02R6/ XNPDP, YNPDP, ZNPDP
ISN 0032      COMMON/OLEO/ EOLEO(20), FAO(20), EXPOLE(20), YMAX(20),
1 YOLEO(20), BOLEO(20), BROLEO(20), XKEXT(20), XKCOMP(20), FCOUL(20),
2 ALPHAP, IGOLEO(20), JGOLEO(20), MGOLEO(20), NGOLEO(20), NOLEO
ISN 0033      COMMON/DEIC/ WTOT, CLTEST(150)
ISN 0034      COMMON/COMALL/ C(6,150), P(80), Q(80), R(80), S(80), T(80), U(80), V(80), W(80), X(81),
1 Y(81), Z(81), AI(9), AJ(9), AK(9), AL(9), AM(9), AN(9), AO(9), AP(9), AQ(9), AR(9), AS(9), AT(9), AU(9), AV(9),
2 YI(80), ZI(80), XZI(80), YZI(80), ZZI(80), AIJ(9), BIJ(720),
3 DRI(150), OAI(720), VEE(900), WGT(80), PHI(80), THETA(80), PSI(80),
4 PDOT(80), QDOT(80), RDOT(80), UDOT(80), VDOT(80), WDOT(80), XDOT(80),
5 YDOT(80), ZDOT(80), PHIDOT(80), THEDOT(80), PSIDOT(80), TIME, DELTAT,
6 XACC(80), YACC(80), ZACC(80), AIDOT(9),
7 PHII(150), THEIJ(150), PSII(150), SUMDF(6,150), YITLE,
8 XLBAR(40), FSPBAR(40), VEEDOT(3,3), DX(81), DY(81), DZ(81),
9 DPIN(81), DQIN(81), DRIN(81), SEIJ(150), DEIJ(150), CEIK(40),
A CEIKF(40),
B SBARI(40), KUNI(40), MAXNM, MAXIGS, MAXTBL,
C NM, NB, I, J, IG(150), JG(150),
D NI(900), NN(40), IJFR(150)
ISN 0035      COMMON/IPIC/ NIC
ISN 0036      EQUIVALENCE (PPR,XMPR(1)), (QPR,XMPR(2)), (RPR,XMPR(3)),
1 (PHIDPR,ANGOPR(1)), (THEDPR,ANGOPR(2)), (PSIDPR,ANGOPR(3))
EQUIVALENCE (XK(1),XK3(1,1,1))
ISN 0037      SIN(X) = DSIN(X)
ISN 0038      COS(X) = DCOS(X)
ISN 0039      SQR(X) = DSQR(X)
ISN 0040      ARSIN(X) = DARSIN(X)
ISN 0041      ATAN2(Y,X) = DATAN2(Y,X)
ISN 0042      AMINI(X,Y) = DMINI(X,Y)
ISN 0043      ABS(X)=DABS(X)
ISN 0044      WTOT = 0.0
ISN 0045      PI = 3.1415926535897932400
ISN 0046      PI2 = PI/2.
ISN 0047      PIN = -PI
ISN 0048      PI2N = -PI2
ISN 0049      BETAR = BETA*PI/180.
ISN 0050      SINBET = DSIN(BETAR)
ISN 0051      COSBET = DCOS(BETAR)
ISN 0052      ABETA(1) = COSBET
ISN 0053      ABETA(2) = 0.
ISN 0054      ABETA(3) = -SINBET
ISN 0055      ABETA(4) = 0.
ISN 0056      ABETA(5) = 1.
ISN 0057      ABETA(6) = 0.
ISN 0058      ABETA(7) = SINBET
ISN 0059      ABETA(8) = 0.
ISN 0060      ABETA(9) = COSBET
ISN 0061      KHATRI(1,1) = 3
ISN 0062      KHATRI(1,2) = 4
ISN 0063      KHATRI(1,3) = 7
ISN 0064      KHATRI(1,4) = 8
ISN 0065      KHATRI(2,1) = 1
ISN 0066      KHATRI(2,2) = 2
ISN 0067

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ISN 0124 XGDP = XGDP+NGT(I)*XDPI(I)
ISN 0125 YGDP = YGDP-NGT(I)*YDPI(I)
ISN 0126 ZGDP = ZGDP+NGT(I)*ZDPI(I)
ISN 0127 2020 CONTINUE
ISN 0128 XGDP = XGDP/MTOT
ISN 0129 YGDP = YGDP/MTOT
ISN 0130 ZGDP = ZGDP/MTOT
ISN 0131 PRINT 2013
ISN 0132 PRINT 2012,XGDP,YGDP,ZGDP
ISN 0133 2012 FORMAT(1X,'X (FS) = ',1PE12.5 /
ISN 0134 1X,'Y (BL) = ',1PE12.5 /
1X,'Z (WL) = ',1PE12.5)
C APRIME AND ABAPRIME (3)
CALL EULER(APR,PHIPR,THEPR,PSIPR)
S1 = SIN(PHIPR)
C1 = COS(PHIPR)
S2 = SIN(THEPR)
C2 = COS(THEPR)
C NOW ABAPRIME (4)
ABAPR(1,1) = 1.0
ABAPR(2,1) = 0.0
ABAPR(3,1) = 0.0
ABAPR(1,2) = S1*S2/C2
ABAPR(2,2) = C1
ABAPR(3,2) = S1/C2
ABAPR(1,3) = C1*S2/C2
ABAPR(2,3) = -S1
ABAPR(3,3) = C1/C2
C ANGLE DOT PRIMES (6)
CALL MATVEC(ABAPR,XMPR,ANGDPR,0)
C D PRIME (7)
DPR(1,1) = 0.0
DPR(1,2) = THEPR*S1-PSIDPR*C1*C2
DPR(1,3) = THEPR*C1+PSIDPR*S1*C2
DPR(2,1) = -DPR(1,2)
DPR(2,2) = 0.0
DPR(2,3) = -PHIDPR+PSIDPR*S2
DPR(3,1) = -DPR(1,3)
DPR(3,2) = -DPR(2,3)
DPR(3,3) = 0.0
C A DOT PRIME (8)
CALL MATMUL(APR,DPR,ADPR)
ZCMMAX = 0.0
ZSLMAX = 0.
DO 2040 I = 1,NM
CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
CALL MATMUL(APR,AIDP,AIC)
THETA(I) = -ARSIN(AIC(3,1))
IF(THEPR.GT.PI2.AND.THEPR.LE.PI) THETA(I)=PI-THETA(I)
IF(THEPR.LT.PI2.AND.THEPR.GE.PI) THETA(I)=PI+THETA(I)
CT = 1./COS(THETA(I))
PHI(I) = ARSIN(AIC(3,2)*CT)

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ISN 0172      PSI(I) = ARSIN(AIC(2,1)*CT)
ISN 0173      VJP(I,1) = XGDP-YDP(I)
ISN 0174      VJP(I,2) = YGDP-YDP(I)
ISN 0175      VJP(I,3) = ZGDP-ZDP(I)
ISN 0176      2040 CONTINUE
C
C      CALCULATE VECTOR COMPONENTS FROM MASS I TO NODE POINT M
C      FOR ALL NNP NODE POINTS.
C
      IF(NNP.EQ.0) GO TO 2051
      DO 3000 JJ=1,NNP
      I = INP(JJ)
      T1 = XDP(I)-XNPDOP(JJ)
      T2 = YDP(I)-YNPDOP(JJ)
      T3 = ZDP(I)-ZNPDOP(JJ)
C
C      THESE ARE IN (-) AIRPLANE AXES.  CONVERT TO BODY AXES BY
C      MULTIPLYING BY AIDP TRANSPOSE.  THIS NORMALLY IS UNITY.
C
      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
      RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
      RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
      RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
      3000 CONTINUE
C
C      DETERMINE LOWEST SPRING.
C
      2051 DO 2050 IKM=1,NSP
      I = II(IKM)
      K = KK(IKM)
      M = MM(IKM)
      IF(M.NE.0) GO TO 2052
      RRX = 0.
      RRY = 0.
      RRZ = 0.
      GO TO 2054
      2052 DO 2056 JJ=1,NNP
      IF(I.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 2058
      2056 CONTINUE
      2058 RRX = RX(JJ)
      RRY = RY(JJ)
      RRZ = RZ(JJ)
      2054 CONTINUE
C
C      EQUATIONS (1-122) FOR AI.
C
      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
      CALL MATMUL(APR,AIDP,AIC)
      DVR1 = AIC(1,1)*RRX+AIC(1,2)*RRY+AIC(1,3)*RRZ
      DVR3 = AIC(3,1)*RRX+AIC(3,2)*RRY+AIC(3,3)*RRZ
      VC = AIC(3,K)*XLBAR(IKM)+DVR3
      VCX = AIC(1,K)*XLBAR(IKM)+DVR1
      DO 2062 L=1,3
ISN 0184      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0185      RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
ISN 0186      RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
ISN 0187      RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
ISN 0188      3000 CONTINUE
C
C      DETERMINE LOWEST SPRING.
C
      2051 DO 2050 IKM=1,NSP
      I = II(IKM)
      K = KK(IKM)
      M = MM(IKM)
      IF(M.NE.0) GO TO 2052
      RRX = 0.
      RRY = 0.
      RRZ = 0.
      GO TO 2054
      2052 DO 2056 JJ=1,NNP
      IF(I.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 2058
      2056 CONTINUE
      2058 RRX = RX(JJ)
      RRY = RY(JJ)
      RRZ = RZ(JJ)
      2054 CONTINUE
C
C      EQUATIONS (1-122) FOR AI.
C
      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
      CALL MATMUL(APR,AIDP,AIC)
      DVR1 = AIC(1,1)*RRX+AIC(1,2)*RRY+AIC(1,3)*RRZ
      DVR3 = AIC(3,1)*RRX+AIC(3,2)*RRY+AIC(3,3)*RRZ
      VC = AIC(3,K)*XLBAR(IKM)+DVR3
      VCX = AIC(1,K)*XLBAR(IKM)+DVR1
      DO 2062 L=1,3
ISN 0189      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0190      RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
ISN 0191      RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
ISN 0192      RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
ISN 0193      3000 CONTINUE
ISN 0194      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0195      RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
ISN 0196      RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
ISN 0197      RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
ISN 0198      3000 CONTINUE
ISN 0199      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0200      RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
ISN 0201      RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
ISN 0202      RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
ISN 0203      3000 CONTINUE
ISN 0204      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0205      RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
ISN 0206      RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
ISN 0207      RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
ISN 0208      3000 CONTINUE
ISN 0209      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0210      RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
ISN 0211      RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
ISN 0212      RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
ISN 0213      3000 CONTINUE

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ISN 0214 VC = VC*APR(3,L)*VJP(I,L)
ISN 0215 VCX = VCX*APR(1,L)*VJP(I,L)
ISN 0216 2062 CONTINUE
ISN 0217 ZSL = VCX*SINBET+VC*COSEBET
ISN 0218 IF(VC-ZCHAX) 2064,2064,2066
ISN 0219 2066 ZCHAX = VC
ISN 0220 2064 IF(ZSL-ZSLMAX) 2050,2050,2068
ISN 0221 2068 ZSLMAX = ZSL
ISN 0222 2050 CONTINUE
ISN 0223 PRINT 2014
ISN 0224 2014 FORMAT( / 1X, 'VEHICLE INERTIAS (IN-LB-SEC**2)')
ISN 0225 XIG = 0
ISN 0226 YIG = 0
ISN 0227 ZIG = 0
ISN 0228 DO 2015 I=1,NM
ISN 0229 IF(IMORI(I).NE.0) GO TO 2015
ISN 0230 XARM = XDP(I) - XGDP
ISN 0231 YARM = YDP(I) - YGDP
ISN 0232 ZARM = ZDP(I) - ZGDP
ISN 0233 GOODY1 = MGT(I)*(YARM*YARM+ZARM*ZARM)/386.
ISN 0234 GOODY2 = MGT(I)*(XARM*XARM+ZARM*ZARM)/386.
ISN 0235 GOODY3 = MGT(I)*(XARM*XARM+YARM*YARM)/386.
ISN 0236 XIG = XIG+XI(I)+GOODY1
ISN 0237 YIG = YIG+YI(I)+GOODY2
ISN 0238 ZIG = ZIG+ZI(I)+GOODY3
ISN 0239 IF(SYMF LG.NE.1.OR.YDP(I).EQ.0.) GO TO 2015
ISN 0240 XIG = XIG+XI(I)+GOODY1
ISN 0241 YIG = YIG+YI(I)+GOODY2
ISN 0242 ZIG = ZIG+ZI(I)+GOODY3
ISN 0243 2015 CONTINUE
ISN 0244 PRINT 2016,XIG,YIG,ZIG
ISN 0245 2016 FORMAT(1X,'I(XX) = ',IPEL1.5 / 1X,'I(YY) = ',IPEL1.5 / 1X,
ISN 0247 1,'I(ZZ) = ',IPEL1.5)
ISN 0248 ZSL = -ZSLMAX-.001
ISN 0249 ZG = -ZCMAX-.001
ISN 0250 IF(BETA) 2101,2101,2102
ISN 0251 2101 XG = 0.
ISN 0252 GO TO 2220
ISN 0253 2102 IF(BETA-90.) 2103,2104,2103
ISN 0254 2104 XG = ZSL
ISN 0255 GO TO 2220
ISN 0256 2103 ZSLG = -ZSL/COSEBET
ISN 0257 DELZ = -ZG-ZSLG+ZGIN
ISN 0258 XG = DELZ/TANBET
ISN 0259 2220 PRINT 2105
ISN 0260 2105 FORMAT( / 1X, 'VEHICLE CG INITIAL GROUND COORDINATES' /
1 1X, 'XCG IS THE DISTANCE FROM SLOPE/GROUND INTERSECTION TO VEHICLE
2 CG,+FORWARD' /
3 1X, 'ZCG IS THE DISTANCE FROM GROUND PLANE TO VEHICLE CG,+DOWN')
ISN 0261 DELXG = XG-XGIN
ISN 0262 DELZG = ZG-ZGIN
ISN 0263 PRINT 2091,DELXG,DELZG
ISN 0264 2091 FORMAT(1X,'XCG = ',IPEL12.5 / 1X,'ZCG = ',IPEL12.5)
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0003000
0003010
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ISN 0265      DO 2022 IJ=1,NB
ISN 0266      I = IG(IJ)
ISN 0267      J = JG(IJ)
ISN 0268      M = MG(IJ)
ISN 0269      N = NG(IJ)
ISN 0270      IF(M.EQ.0) GO TO 5020
ISN 0271      DO 5010 JI=1,NNP
ISN 0272      IF(I.EQ.INP(JI)).AND.M.EQ.MNP(JI)) GO TO 5020
ISN 0273      5010 CONTINUE
ISN 0274      5020 IF(N.EQ.0) GO TO 5030
ISN 0275      DO 5040 JJ=1,NNP
ISN 0276      IF(J.EQ.INP(JJ)).AND.N.EQ.NNP(JJ)) GO TO 5030
ISN 0277      5040 CONTINUE
ISN 0281      C
ISN 0282      C THE FOLLOWING CODE GETS CLTEST(IJ),WHICH IS 1 IF BEAM IJ
ISN 0283      C LIES ENTIRELY IN THE CENTER PLANE OF THE AIRPLANE.THIS
ISN 0285      C IS USED IN DERIV FOR A NUMBER OF TESTS.
ISN 0286      C
ISN 0287      5030 CLTEST(IJ) = 0.
ISN 0288      IF(SYMF16.NE.1.) GO TO 2022
ISN 0289      IF(YDP(I).NE.0.OR.YDP(J).NE.0.) GO TO 2022
ISN 0290      C BOTH MASSES ON CENTERLINE.
ISN 0291      C
ISN 0292      IF(M.EQ.0.AND.N.EQ.0) GO TO 5000
ISN 0293      IF(M.EQ.0) GO TO 5001
ISN 0294      IF(N.EQ.0) GO TO 5002
ISN 0295      IF(YNPDP(JI).EQ.0.AND.YNPDP(JJ).EQ.0.) GO TO 5000
ISN 0296      GO TO 2022
ISN 0297      5001 IF(YNPDP(JJ).EQ.0.) GO TO 5000
ISN 0298      GO TO 2022
ISN 0299      5002 IF(YNPDP(JI).EQ.0.) GO TO 5000
ISN 0300      GO TO 2022
ISN 0301      5000 CLTEST(IJ) = 1.
ISN 0302      2022 CONTINUE
ISN 0303      C
ISN 0304      C LOOPE
ISN 0305      C
ISN 0306      2150 DO 2090 I = 1,NM
ISN 0307      CALL EULER(AIDP,PHIDP(I),THEODP(I),PSIDP(I))
ISN 0308      CALL MATMUL(APR,AIDP,AIC)
ISN 0309      VIP(1) = VJP(I,1)
ISN 0310      VIP(2) = VJP(I,2)
ISN 0311      VIP(3) = VJP(I,3)
ISN 0312      C (14)
ISN 0313      CALL MATVEC(APR,VIP,XV,0)
ISN 0314      XV(1) = XV(1)+XG-XGIN
ISN 0315      XV(3) = XV(3)+ZG-ZGIN
ISN 0316      X(I) = XV(1)
ISN 0317      Y(I) = XV(2)
ISN 0318      Z(I) = XV(3)
ISN 0319      C (15)
ISN 0320      CALL MATVEC(ADPR,VIP,XV,0)
ISN 0321      00003060
ISN 0322      00003070
ISN 0323      00003080
ISN 0324      00003090
ISN 0325      00003100
ISN 0326      00003110
ISN 0327      00003120
ISN 0328      00003130
ISN 0329      00003140
ISN 0330      00003150
ISN 0331      00003160
ISN 0332      00003170
ISN 0333      00003180
ISN 0334      00003190
ISN 0335      00003200
ISN 0336      00003210
ISN 0337      00003220
ISN 0338      00003230
ISN 0339      00003240
ISN 0340      00003250
ISN 0341      00003260
ISN 0342      00003270
ISN 0343      00003280
ISN 0344      00003290
ISN 0345      00003300
ISN 0346      00003310
ISN 0347      00003320
ISN 0348      00003330
ISN 0349      00003340
ISN 0350      00003350
ISN 0351      00003360
ISN 0352      00003370
ISN 0353      00003380
ISN 0354      00003390
ISN 0355      00003400
ISN 0356      00003410
ISN 0357      00003420
ISN 0358      00003430
ISN 0359      00003440
ISN 0360      00003450
ISN 0361      00003460
ISN 0362      00003470
ISN 0363      00003480
ISN 0364      00003490
ISN 0365      00003500
ISN 0366      00003510
ISN 0367      00003520
ISN 0368      00003530
ISN 0369      00003540
ISN 0370      00003550
ISN 0371      00003560
ISN 0372      00003570
ISN 0373      00003580

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ISN 0317      XV(1) = XV(1)+XGDOT
ISN 0318      XV(2) = XV(2)+YGDOT
ISN 0319      XV(3) = XV(3)+ZGDOT
ISN 0320      XDOT(I) = XV(1)
ISN 0321      YDOT(I) = XV(2)
ISN 0322      ZDOT(I) = XV(3)

C (16)
ISN 0323      CALL MATVEC(AIC,XV,VIP,1)
ISN 0324      UI = VIP(1)
ISN 0325      VI = VIP(2)
ISN 0326      WI = VIP(3)

C (17)
ISN 0327      CALL MATVEC(AIDP,XMPR,VIP,1)
ISN 0328      PI = VIP(1)
ISN 0329      QI = VIP(2)
ISN 0330      RI = VIP(3)

C AIBAR (18)
ISN 0331      S1 = SIN(PI(I))
ISN 0332      C1 = COS(PI(I))
ISN 0333      S2 = SIN(THETA(I))
ISN 0334      C2 = COS(THETA(I))
ISN 0335      ABARPR(1,2) = S1*S2/C2
ISN 0336      ABARPR(2,2) = C1
ISN 0337      ABARPR(3,2) = S1/C2
ISN 0338      ABARPR(1,3) = C1*S2/C2
ISN 0339      ABARPR(2,3) = -S1
ISN 0340      ABARPR(3,3) = C1/C2

C (19)
ISN 0341      CALL MATVEC(ABARPR,VIP,XV,0)
ISN 0342      PHIDOT(I) = XV(1)
ISN 0343      THEDOT(I) = XV(2)
ISN 0344      PSIDOT(I) = XV(3)

C END LOOP C
ISN 0345      2090 CONTINUE
ISN 0346      IF(MNP.EQ.0) GO TO 4000
ISN 0347      DO 4010 JJ=1,MNP
ISN 0348      I = INP(JJ)
ISN 0349      CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
ISN 0350      CALL MATMUL(APR,AIDP,AIC)
ISN 0351      TX = AIC(1,1)*RX(I,JJ)+AIC(1,2)*RY(JJ)+AIC(1,3)*RZ(JJ)
ISN 0352      TY = AIC(2,1)*RX(I,JJ)+AIC(2,2)*RY(JJ)+AIC(2,3)*RZ(JJ)
ISN 0353      TZ = AIC(3,1)*RX(I,JJ)+AIC(3,2)*RY(JJ)+AIC(3,3)*RZ(JJ)
ISN 0354      XNP(JJ) = X(I)+TX
ISN 0355      YNP(JJ) = Y(I)+TY
ISN 0356      ZNP(JJ) = Z(I)+TZ
ISN 0357      4010 CONTINUE
ISN 0358      4000 CONTINUE
ISN 0359      IF(NOLEO.EQ.0) GO TO 4020
ISN 0360      DO 4022 J=1,NOLEO
ISN 0361      YOLEO(J)=0.
ISN 0362      4024 YNEW=-FAOI(J)*(EOLEO(J)/EOLEO(J)-YOLEO(J))*EXPOLE(J)
ISN 0363      YNEW=YNEW+FAA(J)/XEXT(J)
ISN 0364      ERR=ABS(YNEW-YOLEO(J))
ISN 0365
ISN 0366

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ISN 0367      YOLED(J)=YNEW
ISN 0368      IF(ERR.LT.0.0001) GO TO 4022
ISN 0370      GO TO 4024
ISN 0371      4022 CONTINUE
C
C      YOLED = AXIAL COMPRESSION DISTANCE OF STRUT MEASURED FROM THE
C      FULLY EXTENDED POSITION
C
ISN 0372      4020 IF(NIC.LE.0) RETURN
C
C      COMPUTE PREL. UNCOUPLED LOADS AND DEFLECTIONS
C
C      PRINT 5011
ISN 0374      5011 FORMAT(/ / 1X, 'BEAM LOADS')
ISN 0375      PRINT 5012
ISN 0376      5012 FORMAT(/ / 6X, 'BEAM', 19X, 'AXIAL LOAD', 19X, 'SHEAR FORCE', 22X,
ISN 0377      *      'MOMENT', 20X, 'BEAM' / 2X, 'I J I J M N', 3X, 'BUCKLING',
C      *      6X, 'TENSION COMPRESSION LATERAL(Y) VERTICAL(Z)', 3X,
C      *      'ROLL(X)', 5X, 'PITCH(Y)', 5X, 'YAW(Z)', 3X, 'I J I J M N' /
C      DO 2400 IJ=1,NB
ISN 0378      IF(Y(IJ).LE.ZZ(IJ)) GO TO 5013
ISN 0379      YZMIN(IJ)=ZZ(IJ)
ISN 0380      GO TO 5014
ISN 0381      5013 YZMIN(IJ)=YY(IJ)
ISN 0382      GO TO 5014
ISN 0383      5013 YZMIN(IJ)=YY(IJ)
C      YZMIN = MIN.CROSS SECTION AREA INERTIA
C      CALC. FORCES AND MOMENTS
C      AXIAL FORCES
ISN 0384      5014 PCRFY=4.*PI*PI*(IJ)*YY(IJ)/(XLB(IJ)**2)
ISN 0385      PCRFZ=4.*PI*PI*(IJ)*ZZ(IJ)/(XLB(IJ)**2)
ISN 0386      PTENS=STENS(MC(IJ))*AA(IJ)
ISN 0387      PCOMP=SCOMP(MC(IJ))*AA(IJ)
C      SHEAR FORCES
ISN 0388      FY=.67*SHEAR(MC(IJ))*AA(IJ)
ISN 0389      FZ=FY
C      MOMENTS
ISN 0390      IF(XIQ(IJ).NE.0.) GO TO 400
ISN 0391      THOMX = 0.
ISN 0392      GO TO 410
ISN 0393      400 THOMX=SHEAR(MC(IJ))/XIQ(IJ)
ISN 0394      410 SYIELD = AMINI(SCOMP(MC(IJ)),STENS(MC(IJ)))
ISN 0395      IF(ZI(IJ).NE.0.) GO TO 420
ISN 0396      BENDHY = 0.
ISN 0397      GO TO 430
ISN 0398      420 BENDHY=SYIELD*YY(IJ)/ZI(IJ)
ISN 0399      430 IF(Z2(IJ).NE.0.) GO TO 440
ISN 0400      BENDHZ = 0.
ISN 0401      GO TO 450
ISN 0402      440 BENDHZ=SYIELD*ZZ(IJ)/Z2(IJ)
ISN 0403      GO TO 450
ISN 0404      450 IF(PY(IJ).EQ.0.AND.PYJ(IJ).EQ.0) GO TO 100
ISN 0405      IF(PY(IJ).EQ.0.OR.PYJ(IJ).EQ.0) GO TO 110
C      CHECK BEAM END CONDITIONS.
C
ISN 0406      450 IF(PY(IJ).EQ.0.AND.PYJ(IJ).EQ.0) GO TO 100
ISN 0408      IF(PY(IJ).EQ.0.OR.PYJ(IJ).EQ.0) GO TO 110

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ISN 0410      C PINNED-PINNED.
ISN 0411      PCRY = PCRFY/4.
ISN 0412      BENDMY = 0.
ISN 0413      FZ = 0.
ISN 0414      GO TO 120
ISN 0415      C FIXED-PINNED.
ISN 0416      110 PCRY = PCRFY/2.
ISN 0417      GO TO 120
ISN 0418      C FIXED-FIXED
ISN 0419      100 PCRY = PCRFY
ISN 0420      120 IF(PZ(IJ)).EQ.0.AND.PZ(IJ).EQ.0) GO TO 200
ISN 0421      IF(PZ(IJ)).EQ.0.OR.PZ(IJ).EQ.0) GO TO 210
ISN 0422      C PINNED-PINNED.
ISN 0423      PCRZ = PCRFZ/4.
ISN 0424      BENDMZ = 0.
ISN 0425      FY = 0.
ISN 0426      GO TO 220
ISN 0427      C FIXED-PINNED.
ISN 0428      210 PCRZ = PCRFZ/2.
ISN 0429      GO TO 220
ISN 0430      C FIXED-FIXED
ISN 0431      200 PCRZ = PCRFZ
ISN 0432      220 PCR(IJ) = PCRZ
ISN 0433      IF(PCRY.LT.PCRZ) PCR(IJ)=PCRY
ISN 0434      5018 PRINT 5015,(IJ,IG(IJ),JG(IJ),NG(IJ),PCR(IJ),PTENS,
ISN 0435      1 PCOMP,FY,FZ,THOMX,BENDMY,BENDMZ,IJ,IG(IJ),JG(IJ),NG(IJ))
ISN 0436      5015 FORMAT(1X,5I3,1P8E12.4,5I3)
ISN 0437      2400 CONTINUE
ISN 0438      PRINT 5050
ISN 0439      5050 FORMAT(// 1X,'BEAM DEFLECTIONS')
ISN 0440      5051 PRINT 5051
ISN 0441      * 'ROTATION ABOUT' / 2X,'IJ I J M N',2X,'BUCKLING',4X,
ISN 0442      * 'TENSION COMPRESSION F(Y)',7X,'F(Z)',7X,'BM(Z)',6X,
ISN 0443      * 'BM(Y)',5X,'X-AXIS Y-AXIS Z-AXIS' / )
ISN 0444      C CALC.DEFLECTIONS
ISN 0445      C
ISN 0446      C AXIAL DEFLECTIONS
ISN 0447      C
ISN 0448      DO 2500 IJ=1,NB
ISN 0449      SYIELD = AMINI(SCOMP(MC(IJ)),STENS(MC(IJ)))
ISN 0450      IF(XK3(1,1,IJ).EQ.0.0) GO TO 5330
ISN 0451      XDEFB = PCR(IJ)/XK3(1,1,IJ)
ISN 0452      XDEF = STENS(MC(IJ))*AA(IJ)/XK3(1,1,IJ)
ISN 0453      XDEFC = SCOMP(MC(IJ))*AA(IJ)/XK3(1,1,IJ)
ISN 0454      GO TO 5340
ISN 0455      5330 XDEFB = 0.0
ISN 0456      XDEF = 0.0
ISN 0457      XDEFC = 0.0
ISN 0458      5340 CONTINUE
ISN 0459      C DUE TO SHEAR FORCES
ISN 0460      IF(XK3(2,2,IJ).EQ.0.0) GO TO 5350

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ISN 0452      YDSF=.67*SHEAR(MC(IJ))*AA(IJ)/XK3(2,2,IJ)
ISN 0453      GO TO 5360
ISN 0454      5350 YDSF = 0.0
ISN 0455      5360 IF(XK3(3,3,IJ).EQ.0.0) GO TO 5370
ISN 0456      ZDSF=.67*SHEAR(MC(IJ))*AA(IJ)/XK3(3,3,IJ)
ISN 0457      GO TO 5380
ISN 0458      5370 ZDSF = 0.0
ISN 0459      5380 CONTINUE
ISN 0460      C
ISN 0461      DEFL. DUE TO BEND.FORCE ((K55/DEL)*FORCE)
ISN 0462      IF(XK3(2,2,IJ).EQ.0.0.OR.Z2(IJ).EQ.0.0) GO TO 5390
ISN 0463      YDMZ=4.*SYIELD*Z2(IJ)/(Z2(IJ)*XLB(IJ)*XK3(2,2,IJ))
ISN 0464      GO TO 5400
ISN 0465      5390 YDMZ = 0.0
ISN 0466      5400 IF(XK3(3,3,IJ).EQ.0.0.OR.Z1(IJ).EQ.0.0) GO TO 5410
ISN 0467      ZDMY=4.*SYIELD*Y1(IJ)/(Z1(IJ)*XLB(IJ)*XK3(3,3,IJ))
ISN 0468      GO TO 5420
ISN 0469      5410 ZDMY = 0.0
ISN 0470      5420 CONTINUE
ISN 0471      C
ISN 0472      TORSIONAL ROTATION
ISN 0473      IF(XK3(4,4,IJ).NE.0.0.AND.XIQ(IJ).NE.0.0) GO TO 5317
ISN 0474      ROTX=0.0
ISN 0475      GO TO 5318
ISN 0476      5317 ROTX=SHEAR(MC(IJ))/XIQ(IJ)/XK3(4,4,IJ)
ISN 0477      C
ISN 0478      BEND. ROTATION ((K33/DEL)*MOM.)
ISN 0479      5318 IF(XK3(5,5,IJ).EQ.0.0.OR.Z1(IJ).EQ.0.0) GO TO 5430
ISN 0480      ROTY=4.*SYIELD*Y1(IJ)/(Z1(IJ)*XK3(5,5,IJ))
ISN 0481      GO TO 5440
ISN 0482      5430 ROTY = 0.0
ISN 0483      5440 IF(XK3(6,6,IJ).EQ.0.0.OR.Z2(IJ).EQ.0.0) GO TO 5450
ISN 0484      ROTZ=4.*SYIELD*Z2(IJ)/(Z2(IJ)*XK3(6,6,IJ))
ISN 0485      GO TO 5460
ISN 0486      5450 ROTZ = 0.0
ISN 0487      5460 CONTINUE
ISN 0488      5316 PRINT 5319, (IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),XDEFB,XDEFT,XDEFC,
ISN 0489      1 YDSF,ZDSF,YDMZ,ZDMY,ROTX,ROTY,ROTZ)
ISN 0490      5319 FORMAT(1X,5I3,1P10E11.3)
ISN 0491      2500 CONTINUE
ISN 0492      RETURN
END

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LEVEL 21.6 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.30.51

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECT=55,SIZE=0600K,

SOURCE=BCD,NOLIST,NOECK,LOAD,MAP,NOEDIT,ID,XREF

C DATA SET D2334IFRNT AT LEVEL 009 AS OF 06/25/79

C DATA SET D2332GIR AT LEVEL 002 AS OF 05/02/78

C DATA SET D2332VIR AT LEVEL 004 AS OF 01/26/78

C DATA SET D2332MIR AT LEVEL 008 AS OF 01/12/78

SUBROUTINE INPRNT

C IMPLICIT REAL*8 (A-H,O-Z)

REAL*8 KUN

REAL*8 LBAR,MJ,KE,CASEIN,CASOUT,HINDT

REAL*4 KR(2700),SLOPE,XKS,XKI,XKR,LDPI(180),LDPI(180)

INTEGER*4 PY(150),PZ(150),PYJ(150),PZJ(150),RUNIN,RUNOUT

INTEGER*4 TITLE(40),BLANK,STOP

INTEGER*4 DIR

INTEGER*2 IJVM(150),IJFM(150),IJVM(150),IJFM(150)

INTEGER*2 HQ(180),NQ(180)

INTEGER*2 CHUG,INBUFF,IIIN,II(40),KK(40),INBUFF(80)

INTEGER*2 IQ(180),JQ(180),LQ(180),NPQ(180),NLSFLG,IJPR

INTEGER*2 NI,NM,IBS,IG,JG

INTEGER*2 NPLT,NPFCT,IPFCT,ITPL,NHPTS,MNUM,ISCALE

INTEGER*2 NTOL1,NTOL2,NTOL3

INTEGER*2 IJSAVE(180)

INTEGER*2 NKMVEC(150)

INTEGER*2 MM(40),MG(150),NG(150),INP(50),MNP(50)

DIMENSION G(150),XP(8),YP(8),ZP(8),VMAX2(6,150),FMAX2(6,150)

DIMENSION VMAX3(6,150),FMAX3(6,150)

DIMENSION XK3(6,6,150)

DIMENSION IJPR(14),VMAXT(6),FMAXT(6)

DIMENSION MASSHO(50),DIR(50),NPTS(50)

DIMENSION IPHDP(80)

DIMENSION XNPDP(50),YNPDP(50),ZNPDP(50)

COMMON/IBALL/ IBUFI(20)

COMMON/DEIN/ XNBAR,XPBAR,YNBAR,YFBAR,ZNBAR,ZPBAR,VLENZ(5,3),

1 FMAX(900),HEXT(80),HEY(80),HEZ(80),ALIFT(80),VMAX(900),VMAXN(900),

2 FMAXN(900),XKS(2700),XKI(2700),XKR(2700),NLSFLG(900),CHUG(180),

3 HVP

COMMON/DEINPR/ AA(150),E(150),YY(150),ZZ(150),XIQ(150),

1 XLBI(150),ZI(150),Z2(150),MC(150),XJ(150),SF26(150),SF35(150),

2 SF26J(150),SF35J(150),PY,PZ,PYJ,PZJ,NSC,NPIN

COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),EEI(20),GG(20),

1 FINT(6,150),VOL(5),VZERO(5),KMATR(6,4),NVCH,INBUFF(5,8)

COMMON/DOIN/ CBAR(150)

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ISN 0032	COMMON/GEIR/ PLM26(150), PLM35(150), PLM26J(150), PLM35J(150)	00000410
ISN 0033	COMMON/CFIR/ SIFL(40), SAFL(40), SBFL(40), SFFL(40), XKEFL(40)	00000420
ISN 0034	COMMON/INAC/ ACCEL(300), TIMI(300), INDEX(50,2), JAY(50,2), KOUNT	00000430
ISN 0035	COMMON/INCF/ SA(40), SB(40), SF(40), SI(40), XMU(40), XKE(40),	00000440
ISN 0036	1 XHAXI(40), FSPOI(40), FSPOI(40), EFLEX(40), CDAMP(40), PLOMT	00000450
	COMMON/PPLTS/ XSCALE(10), YSCALE(10), NPLT, NPFC, IPFCT, ITPL(10),	00000460
	* NPTS(10), MNUM(50,10), ISCALE(10)	00000470
ISN 0037	COMMON/INDEAC/ NACC	00000480
ISN 0038	COMMON/INIC/ XDP(80), ZDP(80), PHIDP(80), PSIDP(80),	00000490
	1 THEDP(80), PPR, QPR, RPR, XGIN, ZGIN, PHIPR, PSIPR, THEPR,	00000500
	2 XGDOT, YGDOT, ZGDOT	00000510
ISN 0039	COMMON/INIDCP/ YDP(80)	00000520
ISN 0040	COMMON/INPR/ NORI, NSP	00000530
ISN 0041	COMMON/INCFIC/ BETA	00000540
ISN 0042	COMMON/IRDE/ PFIL	00000550
ISN 0043	COMMON/MACFIN/ THAX, IPRINT	00000560
ISN 0044	COMMON/MCFII/ SYMFLS	00000570
ISN 0045	COMMON/COMNEW/ DAMPC, RUNMOD, RUNMOD	00000580
ISN 0046	COMMON/NP0012/ HG, NG, INP, MNP	00000590
ISN 0047	COMMON/NP0112/ II, KK, MM	00000600
ISN 0048	COMMON/NP0212/ HQ, NG, IJVM, IJFM, IJVMN, IJFMN	00000610
ISN 0049	COMMON/NP0014/ NNP	00000620
ISN 0050	COMMON/NP02R8/ XNPDP, YNPDP, ZNPDP	00000630
ISN 0051	COMMON/OLEO/EOLEO(20), FAO(20), FAI(20), EXPOLE(20), YMAX(20),	00000640
	1 YOLEO(20), BOLEO(20), BROLEO(20), XKEXT(20), XKCOMP(20), FCOUL(20),	00000650
	2 ALPHAP, IGOLEO(20), JGOLEO(20), MGOLEO(20), NGOLEO(20), NOLEO	00000660
	COMMON/CORALL/ C(6,150), P(80), R(80), V(80), W(80), X(81),	00000670
	1 Y(81), Z(81), AI(9), AJ(9), SC(40), XC(6), XK(5400), XI(80),	00000680
	2 YI(80), ZI(80), XZI(80), YZI(80), AIJ(9), BIJ(720),	00000690
	3 DRII(150), OAI(720), VEE(900), MGT(80), PHI(80), THETA(80), PSI(80),	00000700
	4 POUT(80), QOUT(80), ROUT(80), UOUT(80), VOUT(80), WOUT(80), XOUT(80),	00000710
	5 YOUT(80), ZOUT(80), PHIDOT(80), THEDOT(80), PSIDOT(80), TIME, DELTAT,	00000720
	6 XACC(80), YACC(80), ZACC(80), AIDOT(9),	00000730
	7 PHIIJ(150), THEIJ(150), PSIIJ(150), SUMOF(6,150), TITLE,	00000740
	8 XLBAR(40), FSPBAR(40), VEEDOT(3,3), DX(81), DY(81), DZ(81),	00000750
	9 DPIN(81), DQIN(81), DRIN(81), SEIJ(150), DEIJ(150), CEIK(40),	00000760
	A CEIKF(40),	00000770
	B SBARI(40), KUNI(40), MAXNM, MAXIGS, MAXTBL,	00000780
	C NI, NB, I, J, IG(150), JG(150),	00000790
	D NI(900), NI(40), IJPR(150)	00000800
ISN 0053	COMMON/ININPR/ NSF, NTF, NDE, NSPD, NED, NS, NRP, NIMP	00000810
ISN 0054	COMMON/COMTR8/ G	00000820
ISN 0055	COMMON/UB/ DB(150), IJUB(150), NUB	00000830
ISN 0056	COMMON/STUFF/ NEMI(80), NEWIJ(150), NMOLD, NBOLD	00000840
ISN 0057	COMMON/COMTR4/ KR , LDP , LDP1	00000850
ISN 0058	COMMON/COMMI4/ND, NVBHN, NFBHN, NHI, NKM, NLB,	00000860
	1 NPH , NMTL , NPTS , NVBM , IJPR , IPHDP, NFBM	00000870
ISN 0059	COMMON/COMMI2/ IQ , JQ , LQ , NPQ , INBUF ,	00000880
	1 NKMEC, IJSAVE	00000890
ISN 0060	COMMON/INOUT/ FCUT, NTOL1, NTOL2, NTOL3	00000900
ISN 0061	COMMON/TPIC/ NIC	00000910
ISN 0062	COMMON /RESTR/ CASEIN, RUNIN, MSECIN, CASOUT, RUNOUT, MSCOUT(5)	00000920
ISN 0063	COMMON /VARINT/ MINDT, DT2, TPRINT, EL, EU, RATHIN, RATHAX, IPC, IVAR	00000930


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ISN 0064      EQUIVALENCE (XK(1),XK3(1,1,1))
ISN 0065      EQUIVALENCE (VMA(1),VMA2(1),FMAX(1),FMAX2(1))
ISN 0066      EQUIVALENCE (VMA(1),VMA2(1),FMAX(1),FMAX2(1))
ISN 0067      EQUIVALENCE (VMA(1),VMA2(1),FMAX(1),FMAX2(1))
ISN 0068      EQUIVALENCE (MASSND(1),INDEX(1,1))
ISN 0069      EQUIVALENCE (DIR(1),INDEX(1,2))
ISN 0070      SQRT(X) = DSQRT(X)
ISN 0071      ABS(X) = DABS(X)
                PI = 3.141592653500
C
C      CARD 0001,0002
C
ISN 0072      PRINT 5500, TITLE
ISN 0073      5500 FORMAT(1H1,20A4,/,1X,20A4)
C
C      CARD 0003
C
ISN 0074      PRINT 5504
ISN 0075      5504 FORMAT(/,1X, 'PROGRAM SIZE DATA',/)
C
C      CARD 0004
C
ISN 0076      PRINT 5507,NM,NP,NB,NLB,NHI,MVP,NVCH,NDRI,NMTL,NACC,NVBM,
1 NVBM,NFBM,NFBM,NPH,ND,NKM,NP
ISN 0077      5507 FORMAT(1X, 'NUMBER OF:',/,33X, 'NON-',45X, 'NON-',5X, 'NON-',/,33X,
1 'ZERO',43X, 'STANDARD',1X, 'STANDARD',1X, 'NON-',4X, 'NON-',14X,
2 'NO',/,27X, 'KR',4X, 'HE OR',4X, 'MASS',3X, 'VOLUME',3X, 'ORI',5X,
3 'HTL',3X, 'ACCEL',3X, 'MAX',5X, 'MAX',3X, 'ZERO',2X,
4 'STANDARD STIFFNESS NODE',/,1X, 'MASS',2X, 'SPRINGS',
5 2X, 'BEAMS',2X, 'TABLES',3X, 'IXY',4X, 'PENETR',1X,
6 'CHANGE',1X, 'ELEMENTS',1X, 'TYPES',3X, 'TABLES',2X, 'DEFL',4X,
7 'FORCE',2X, 'SHIP',2X, 'DAMPING',2X, 'MATRICES',2X, 'PTS',/,
8 82X, 'NVB',6X, 'NFB',/,3X, 'NM',
9 6X, 'NSP',5X, 'NB',5X, 'NLB',5X, 'NHI',5X, 'MVP',5X, 'NVCH',4X,
A 'NDRI',3X, 'NMTL',5X, 'NACC',3X, 'I',3X, 'I',3X, 'I',3X, 'I',3X, 'I',3X,
B 'NPH',6X, 'ND',7X, 'NKM',5X, 'NMP',/,
C 1X,14,218,17,18,18,18,18,17,19,15,3(14),17,219,18)
ISN 0078      PRINT 5961,NSC,NIC,NTOL1,NTOL2,NTOL3
ISN 0079      5961 FORMAT(/,2X, 'NSC=',15,5X, 'NIC=',15,5X, 'NTOL1=',15,5X,
1 5X, 'NTOL2=',15,5X, 'NTOL3=',15,5X,/,
PRINT 5962,NOLEO,ALPHAP
ISN 0080      PRINT 5962,NOLEO,ALPHAP
ISN 0081      5962 FORMAT(/,2X, 'NO.OF OLEO STRUTS=',15,5X, 'ALPHA=',PIE10.3)
ISN 0082      PRINT 1000,CASEIN,CASOUT,PURIN,RUNOUT,MSECIN,MSECOUT
ISN 0083      1000 FORMAT(/,2X, 'PROGRAM DATA MANAGEMENT CONTROL DATA',
1 //10X, 'RESTART:',T20, 'TITLE - ',A8,
2 T50, 'SAVE:',T56, 'TITLE - ',A8,
3 /T20, 'CASE - ',I4,I56, 'CASE - ',I4,
4 /T20, 'TIME - ',I4,I56, 'TIMES - ',I514)
ISN 0084      PRINT 1008,IVAR,EL,EU,RATHIN,RATHMAX
ISN 0085      1008 FORMAT(/,2X, 'VARIABLE INTEGRATION CONTROL DATA',
1 //5X, 'VAR. INT. FLAG = ',I1,
2 2X, 'EL = ',F6.3,2X, 'EU = ',F6.3,
3 2X, 'LOWER RATIO = ',F5.2,2X, 'UPPER RATIO = ',F5.2)
ISN 0086      PRINT 5501

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ISN 0087 5501 FORMAT(//,1X,'PROGRAM CONTROL DATA',//,
1 3X,'PRINT INTERVAL',11X,'INTEGRATION',9X,'MAX.',10X,
2 'PLOW FORCE',9X,'FILTER CUTOFF',7X,'CASE TYPE',/,
3 1X,'INTEGRATION INTERVAL',9X,'INTERVAL',11X,'TIME',
4 9X,'STARTING TIME',9X,'FREQUENCY',9X,'INDICATOR',//,
5 8X,'DP/DI',20X,'DT',14X,'THAX',13X,'PLOWT',15X,'FCUT',14X,
6 'RUNMOD')
ISN 0088 PRINT 5503, IPRINT,DELTA,TMAX,PLOWT,FCUT,RUNMOD
ISN 0089 5503 FORMAT(9X,14,18X,F8.6,9X,F8.12X,F7.5,10X,F7.3,12X,F7.3)
ISN 0090 IF(FCUT.EQ.0.) GO TO 5509
ISN 0092 PFIL = 1./(2.*PI*FCUT)
ISN 0093 GO TO 5511
ISN 0094 5509 PFIL = 0.
C
C CARD 0005,006,007
C
ISN 0095 5511 PRINT 3000,NSF,NTF,NDE,NSPD,NED,NS,NRP,NIMP
ISN 0096 3000 FORMAT(//,1X,'TIME HISTORY PRINT CONTROL CARDS',//,
1 2X,'STRAIN',3X,'TOTAL',4X,'BEAM',6X,'EXT.SPRING',
2 2X,'ENERGY',2X,'STRESS',2X,'ACCEL',2X,'IMPULSE',/2X,'FORCES',
3 2X,'FORCES',1X,'DEFLECTIONS',5X,'DATA',6X,'DATA',
4 4X,'DATA',3X,'DATA',3X,'DATA',/4X,12,18,19,112,111,18,17,18)
IF(NPLT.EQ.0) GO TO 5519
ISN 0097 5513 PRINT 3002,NPLT,NPFT
ISN 0099 3002 FORMAT(//,1X,'NO.OF MASS POSITION PLOTS EACH TIME=',15,10X,
ISN 0100 * 'PLOT PRINT FACTOR =',15)
PRINT 3003
ISN 0101 3003 FORMAT(//,1X,'PLANE I.D.',5X,'NO.OF POINTS')
ISN 0102 PRINT 3004,(ITPL(J),NMPTS(J),J=1,NPLT)
ISN 0103 3004 FORMAT(3X,15,8X,15)
ISN 0104 GO TO 5510
ISN 0105 5519 PRINT 3001
ISN 0106 3001 FORMAT(//,1X,'NO.MASS POSITION PLOTS')
ISN 0107 5510 PRINT 4000
ISN 0108 4000 FORMAT(//,1X,'VEHICLE INITIAL CONDITIONS',//,
ISN 0109 1 1X,'VEHICLE TRANSLATIONAL VELOCITIES IN GROUND AXES (IN/SEC)',/
2 1X,'VEHICLE ROTATIONAL VELOCITIES IN VEHICLE AXES (RAD/SEC)',/
3 1X,'EULER ANGLES OF VEHICLE RELATIVE TO GROUND (RADIAN)',//
4 9X,'XGDOT',13X,'YGDOT',13X,'ZGDOT',/11X,'P',16X,'Q',16X,
5 'R',/10X,'PHI',13X,'THETA',13X,'PSI',/)
PRINT 5502, XGDOT,YGDOT,ZGDOT
ISN 0110 PRINT 5502, PPR,QPR,RPR
ISN 0111 PRINT 5502, PHIPR,THEPR,PSIPR
ISN 0112 5502 FORMAT(35X,1PE13.5)
ISN 0113 4003 PRINT 4003
ISN 0114 4003 FORMAT(//,1X,'GENERALIZED SURFACE DATA',/)
ISN 0115 PRINT 3999,BETA,XGIN,ZGIN
ISN 0116 3999 FORMAT(1X,'BETA =',F5.1,' DEGREES',/1X,'XGIN =',F5.1,/
ISN 0117 1 1X,'ZGIN =',F5.1)
C
C BEAM AND MASS NUMBERING CORRESPONDENCE (LEFT/RIGHT) DATA
C
C IF(RUNMOD.LT.2) GO TO 1010
ISN 0118

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ISN 0120      NMAX = MAXO(NHOLD,NBOLD)
ISN 0121      PRINT 1050
ISN 0122      1050 FORMAT(/,1X,'CORRESPONDING MASS AND BEAM NUMBERS FOR',
ISN 0123      1 ' LEFT AND RIGHT SIDES OF AIRPLANE')
ISN 0124      PRINT 1051
ISN 0125      1051 FORMAT(3X,'MASSES',23X,'BEAMS',11X,'LEFT RIGHT',12X,'LEFT',
ISN 0126      1 14X,'RIGHT',3X,'I',5X,'I',9X,'IJ I J M N IJ',
ISN 0127      2 'I J M N')
ISN 0128      DO 1020 I=1,NMAX
ISN 0129      IF(I.GT.NHOLD) GO TO 1030
ISN 0130      IF(I.GT.NBOLD) GO TO 1040
ISN 0131      INEW = NEWI(I)
ISN 0132      IJNEW = NEWIJ(I)
ISN 0133      IF(IJNEW.NE.0) GO TO 1042
ISN 0134      IGT = 0
ISN 0135      JGT = 0
ISN 0136      MGT = 0
ISN 0137      NGT = 0
ISN 0138      GO TO 1044
ISN 0139      1042 IGT = IG(IJNEW)
ISN 0140      JGT = JG(IJNEW)
ISN 0141      MGT = MG(IJNEW)
ISN 0142      NGT = NG(IJNEW)
ISN 0143      1044 PRINT 1052,I,INEW,I,IG(I),JG(I),MG(I),NG(I),IJNEW,IGT,JGT,MGT,NGT
ISN 0144      GO TO 1020
ISN 0145      1030 IJNEW = NEWIJ(I)
ISN 0146      IF(IJNEW.NE.0) GO TO 1046
ISN 0147      IGT = 0
ISN 0148      JGT = 0
ISN 0149      MGT = 0
ISN 0150      NGT = 0
ISN 0151      GO TO 1048
ISN 0152      1046 IGT = IG(IJNEW)
ISN 0153      JGT = JG(IJNEW)
ISN 0154      MGT = MG(IJNEW)
ISN 0155      NGT = NG(IJNEW)
ISN 0156      1048 PRINT 1053,I,IG(I),JG(I),MG(I),NG(I),IJNEW,IGT,JGT,MGT,NGT
ISN 0157      GO TO 1020
ISN 0158      1040 PRINT 1052,I,NEWI(I)
ISN 0159      1020 CONTINUE
ISN 0160      1052 FORMAT(2X,I2,4X,I2,5X,2(3X,5I3))
ISN 0161      1053 FORMAT(15X,2(3X,5I3))
ISN 0162      1010 PRINT 5498
ISN 0163      5498 FORMAT(/,1X,'MASS DATA')
ISN 0164      PRINT 5499
ISN 0165      5499 FORMAT(/,9X,'WEIGHTS',11X,'MASS COORDINATES F.S.,B.L.,M.L.',10X,
ISN 0166      1 'MASS MOMENTS OF INERTIA (LB-IN-SEC**2)',/)
ISN 0167      PRINT 5505
ISN 0168      5505 FORMAT(2X,'I',8X,'M',14X,3HX',12X,3HY',12X,3HZ',12X,'IX',
ISN 0169      1 13X,'IY',13X,'IZ',10X,'I')
ISN 0170      C
ISN 0171      C
ISN 0172      C
ISN 0173      CARDS 0100

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C      ISN 0202      DO 5160 IKM=1,NSP
      ISN 0203      I = II(IKM)
      ISN 0204      K = KK(IKM)
      ISN 0205      M = MM(IKM)
      ISN 0206      XKUN=FSPDI(IKM)/SI(IKM)
      ISN 0207      SRT=2.*SQRT(XKUN*NGT(I)/386.4)*CDAMP(IKM)
      ISN 0208      SRT=2.*CRIT.DAMPING*SQRT(K*M)
      ISN 0209      PRINT 5516,I,K,M,SI(IKM),SA(IKM),SBI(IKM),SF(IKM),FSPDI(IKM),
      ISN 0210      1 FSPDI(IKM),CDAMP(IKM),SRT
      ISN 0211      5516 FORMAT(1H,3I3,1P8E15.5)
      ISN 0212      CDAMP(IKM)=SRT
      ISN 0213      5160 CONTINUE
      ISN 0214      C
      ISN 0215      C      CARDS 0500
      ISN 0216      C
      ISN 0217      C      MAT.PROP.VALUES
      ISN 0218      C      MC=1(6130 STEEL),2(6150H STEEL),3(STAINLESS 3000 SERIES),
      ISN 0219      C      4(AL.2024-T3),5(AL.6061-T3),6(CAST AL.B195-T4)
      ISN 0220      C      7(LOW MOD.MAT.),8(JUNK),9,10(SPINE FOR DRI)
      ISN 0221      C
      ISN 0222      EE(1)=30.E06
      ISN 0223      EE(2)=30.E06
      ISN 0224      EE(3)=28.E06
      ISN 0225      EE(4)=10.5E06
      ISN 0226      EE(5)=10.0E06
      ISN 0227      EE(6)=EE(5)
      ISN 0228      EE(7)=1.0E06
      ISN 0229      EE(8)=1.0E06
      ISN 0230      EE(9)=1.0E06
      ISN 0231      EE(10)=1.0E06
      ISN 0232      GG(1)=11.0E06
      ISN 0233      GG(2)=GG(1)
      ISN 0234      GG(3)=12.5E06
      ISN 0235      GG(4)=4.0E06
      ISN 0236      GG(5)=3.8E06
      ISN 0237      GG(6)=3.8E06
      ISN 0238      GG(7)=.30E06
      ISN 0239      GG(8)=0.
      ISN 0240      GG(9)=.30E06
      ISN 0241      GG(10)=.30E06
      ISN 0242      STENS(1)=75000.
      ISN 0243      STENS(2)=205000.
      ISN 0244      STENS(3)=70000.
      ISN 0245      STENS(4)=47000.
      ISN 0246      STENS(5)=35000.
      ISN 0247      STENS(6)=16000.
      ISN 0248      STENS(7)=16000.
      ISN 0249      STENS(8)=16000.
      ISN 0250      STENS(9)=16000.
      ISN 0251      STENS(10)=16000.
      ISN 0252      SCOMP(1)=75000.
      ISN 0253      SCOMP(2)=205000.

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00003590 SCOMP(3)=46000.
00003600 SCOMP(4)=39000.
00003610 SCOMP(5)=34000.
00003620 SCOMP(6)=16000.
00003630 SCOMP(7)=16000.
00003640 SCOMP(8)=16000.
00003650 SCOMP(9)=16000.
00003660 SCOMP(10)=16000.
00003670 SHEAR(1)=37500.
00003680 SHEAR(2)=80000.
00003690 SHEAR(3)=36000.
00003700 SHEAR(4)=22000.
00003710 SHEAR(5)=17000.
00003720 SHEAR(6)=17000.
00003730 SHEAR(7)=17000.
00003740 SHEAR(8)=17000.
00003750 SHEAR(9)=17000.
00003760 SHEAR(10)=17000.
00003770 IF(NKMEC(IJ),NE.0) GO TO 5306
00003780 DO 5305 L=1,6
00003790 DO 5305 K=1,6
00003800 XK3(L,K,IJ) = 0.
00003810
00003820
00003830
00003840
00003850
00003860
00003870
00003880
00003890
00003900
00003910
00003920
00003930
00003940
00003950
00003960
00003970
00003980
00003990
00004000
00004010
00004020
00004030
00004040
00004050
00004060
00004070
00004080
00004090
00004100
00004110

ISN 0244 ISN 0245 ISN 0246 ISN 0247 ISN 0248 ISN 0249 ISN 0250 ISN 0251 ISN 0252 ISN 0253 ISN 0254 ISN 0255 ISN 0256 ISN 0257 ISN 0258 ISN 0259 ISN 0260 ISN 0261 ISN 0262 ISN 0263 ISN 0265 ISN 0266 ISN 0267 ISN 0268 ISN 0269

ISN 0270 ISN 0271 ISN 0272 ISN 0273 ISN 0274

ISN 0275 ISN 0276 ISN 0277 ISN 0278 ISN 0280 ISN 0281 ISN 0282 ISN 0283

IF(M.EQ.0) GO TO 5220
IF NOT,AT LEAST ONE BEAM END CONNECTS TO A NODE POINT RATHER THAN A MASS POINT.
FIRST CHECK END I.
IF(M.EQ.0) GO TO 5220
DO 5230 JJ=1,NMP
IF(I.EQ.INP(JJ).AND.M.EQ.MNP(JJ)) GO TO 5240
5230 CONTINUE
5240 XDP1 = XNPDPI(JJ)

ISN 0285 ISN 0287 ISN 0288 ISN 0290 ISN 0291 ISN 0292
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ISN 0292      YDPI = YNDP(JJ)
ISN 0293      ZDPI = ZNDP(JJ)
ISN 0294      DO 5220 IF(N.EQ.0) GO TO 5210
ISN 0296      DO 5260 JJ=1,NPJ
ISN 0297      IF(J.EQ.INP(JJ).AND.N.EQ.MNP(JJ)) GO TO 5270
ISN 0299      5260 CONTINUE
ISN 0300      5270 XDPJ = YNDP(JJ)
ISN 0301      YDPJ = YNDP(JJ)
ISN 0302      ZDPJ = ZNDP(JJ)
ISN 0303      5210 IF(J.NE.0) GO TO 5299
C
C      FOR A SYMMETRICAL MODEL, DATA FOR POINT J DOES NOT EXIST.
C
      XLB(IJ) = 2.*ABS(YDPI)
      GO TO 5054
ISN 0305      5299 DELXDP = XDPJ-XDPI
ISN 0306      DELYDP = YDPJ-YDPI
ISN 0307      DELZDP = ZDPJ-ZDPI
ISN 0308      XLB(IJ) = SQRT(DELXDP*DELXDP+DELYDP*DELYDP+DELZDP*DELZDP)
ISN 0309      5054 CONTINUE
ISN 0310      PRINT 5301
ISN 0311      5301 FORMAT(/,IX,'MATERIAL PROPERTIES')
ISN 0312      PRINT 5309
ISN 0313      5309 FORMAT(/,2X,'MATERIAL',5X,'MODULUS OF',10X,
ISN 0314      1 'MODULUS OF',10X,'TENSION',10X,'COMPRESS.',11X,
ISN 0315      2 'SHEAR',/4X,'NO.',8X,'ELASTICITY',
ISN 0316      3 11X,'RIGIDITY',11X,'STRESS',13X,'STRESS',11X,'STRESS',/)
ISN 0317      1 SHEAR(IJ),IJ=1,10)
ISN 0318      5310 FORMAT(4X,I2,7X,IPEL2.4,8X,E12.4,9X,OPF8.0,10X,F8.0,10X,F8.0)
ISN 0319      IF(NMTL.EQ.0) GO TO 200
ISN 0320      DO 2 LL=1,NMTL
ISN 0321      IJ = IBUF1(LL)
ISN 0322      PRINT 5310,IJ,EE(IJ),GG(IJ),STENS(IJ),SCOMP(IJ),SHEAR(IJ)
ISN 0323      2 CONTINUE
C      COMPUTE STIFFNESS MATRIX
ISN 0324      200 DO 5307 IJ=1,NB
ISN 0325      IF(NKMYEC(IJ).NE.0) GO TO 5307
ISN 0326      E(IJ)=EE(MC(IJ))
ISN 0327      G(IJ)=GG(MC(IJ))
ISN 0328      EOL = E(IJ)/XLB(IJ)
ISN 0329      EOL2 = EOL/XLB(IJ)
ISN 0330      EOL3 = EOL2/XLB(IJ)
ISN 0331      C
C      FOR MAN AND DRI TYPE ELEMENTS (TYPES 9 AND 10), CALCULATE AREA
C      AND DAMPING. THESE OVERRIDE ANY INPUT VALUES.
C
      IF(MC(IJ).EQ.9) GO TO 30
      IF(MC(IJ).EQ.10) GO TO 40
      GO TO 100
C
C      MAN ELEMENT.
C
ISN 0332
ISN 0333
ISN 0334
ISN 0335
ISN 0336

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ISN 0337 30 AAI(IJ) = 10.2276E-6*XLB(IJ)*MGT(JG(IJ))
ISN 0338 CBAR(IJ) = 0.3*SQRT(1. + MGT(JG(IJ))/MGT(IG(IJ)))
ISN 0339 GO TO 100

C
C DRI ELEMENT.
C
ISN 0340 40 AAI(IJ) = 6.5456E-6*XLB(IJ)*MGT(JG(IJ))
ISN 0341 CBAR(IJ) = 0.22*SQRT(1. + MGT(JG(IJ))/MGT(IG(IJ)))
ISN 0342 IJPR(IJ) = 1
ISN 0343 100 XK3(1,IJ) = EOL*AAI(IJ)
ISN 0344 XK3(2,IJ) = EOL*12.*ZZ(IJ)
ISN 0345 XK3(3,IJ) = EOL*12.*YY(IJ)
ISN 0346 XK3(4,IJ) = 6(IJ)*XJ(IJ)/XLB(IJ)
ISN 0347 XK3(5,IJ) = EOL*4.*YY(IJ)
ISN 0348 XK3(6,IJ) = EOL*4.*ZZ(IJ)
ISN 0349 XK3(2,6,IJ) = EOL2*(-6.*ZZ(IJ))
ISN 0350 XK3(5,3,IJ) = EOL2*6.*YY(IJ)
ISN 0351 XK3(3,5,IJ) = EOL2*6.*YY(IJ)
ISN 0352 XK3(6,2,IJ) = EOL2*(-6.*ZZ(IJ))
ISN 0353 5307 CONTINUE

C
C CARDS 0601 AND UP
C
ISN 0354 5308 PRINT 5308
ISN 0355 5308 FORMAT(/,IX,'INTERNAL BEAM DATA')
ISN 0356 5309 PRINT 5302
ISN 0357 5302 FORMAT(/,55X,'DISTANCES FROM NEUTRAL',30X,'M',/,55X,
1 'AXIS TO EXTREME FIBRES TORSION',13X,'DAMPING T',/,7X,'BEAM',
2 8X,'AREA',9X,'MOMENTS OF INERTIA',7X,'ZBIJ AXIS YBIJ AXIS ',
3 'PARAMETER LENGTH',5X,'RATIO L P-CODES BEAM',/
4 109X,'Y Z Y Z')
5309 PRINT 5303
ISN 0358 5303 FORMAT(2X,'IJ I J M N A',8X,'IYY',7X,'IZZ',
ISN 0359 1 8X,'JX',8X,'ZI',8X,'Z2',8X,'XIQ',6X,'XLB',7X,'CBAR ',
2 'PC I I J I J I J M N')
ISN 0360 5304,(IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),AA(IJ),YY(IJ),
1 ZZ(IJ),XJ(IJ),ZI(IJ),Z2(IJ),XIQ(IJ),XLB(IJ),CBAR(IJ),
2 MC(IJ),PY(IJ),PZ(IJ),PJ(IJ),PJ(IJ),IJ,IG(IJ),JG(IJ),
3 MG(IJ),NG(IJ),IJ=1,NB)
ISN 0361 5304 FORMAT(1X,5I3,1P9E10.3,5I2,5I3)
C
C UNSYMMETRICAL BEAM CARDS.
C
ISN 0362 IF(NUB.EQ.0) GO TO 4050
ISN 0363 PRINT 4022
ISN 0364 4022 FORMAT(/,IX,'UNSYMMETRICAL BEAM DATA')
ISN 0365 PRINT 4024
ISN 0366 4024 FORMAT(/,20X,'TENSION-',/,18X,'COMPRESSION',/,6X,
1 'BEAM',11X,'FLAG',5X,'DEADBAND')
ISN 0367 PRINT 4026
ISN 0368 4026 FORMAT(/,2X,'IJ I J M N',5X,'IUB',8X,'DB')
ISN 0369 DO 4028 IJ=1,NB
ISN 0370 IF(IJUB(IJ).EQ.0) GO TO 4028
ISN 0371

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ISN 0373 PRINT 4030,IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),IJOB(IJ),DB(IJ)
ISN 0374 4030 FORMAT(1X,5I3,18,X,1P1E10.3)
ISN 0375 4028 CONTINUE
C
C PINNED-END BEAMS AND PLASTIC HINGES
C
ISN 0376 4050 IF(INPIN.EQ.0) GO TO 4020
ISN 0377 PRINT 4052
ISN 0378 4052 FORMAT(//,1X,'PLASTIC HINGE AND END-FIXITY DATA')
ISN 0379 PRINT 4053
ISN 0380 4053 FORMAT(1X,6X,'BEAM',7X,'P-CODES',13X,'SHAPE FACTORS',25X,'PLASTIC',
ISN 0381 1 1X,'HINGE MOMENTS')
ISN 0382 PRINT 4054
ISN 0383 4054 FORMAT(1X,2X,'IJ I J M N IYZJYZ',4X,'SF35',4X,'SF26',4X,
ISN 0384 1 'SF35J',3X,'SF26J',3X,'PLM35',7X,'PLM26',7X,'PLM35J',6X,'PLM26J')
ISN 0385 4055 FORMAT(1X,5I3,1X,4I2,3X,4(F6.3,2X),4(1P1E10.3,2X))
ISN 0386 DO 4056 IJ=1,NB
IF(PY(IJ).EQ.0 .AND. PZ(IJ).EQ.0 .AND. PYJ(IJ).EQ.0 .AND.
1 PZJ(IJ).EQ.0) GO TO 4056
PLM26(IJ)=SF26(IJ)*STENS(MC(IJ))*ZZ(IJ)/Z2(IJ)
PLM35(IJ)=SF35(IJ)*STENS(MC(IJ))*YY(IJ)/Z1(IJ)
PLM26(IJ)=SF26(IJ)*STENS(MC(IJ))*ZZ(IJ)/Z2(IJ)
PLM35(IJ)=SF35(IJ)*STENS(MC(IJ))*YY(IJ)/Z1(IJ)
I=IG(IJ)
J=JG(IJ)
M=MG(IJ)
N=NG(IJ)
PRINT 4055,IJ,I,J,M,N,PY(IJ),PZ(IJ),PYJ(IJ),PZJ(IJ),SF35(IJ),
1 SF26(IJ),SF35J(IJ),SF26J(IJ),PLM35(IJ),PLM26(IJ),PLM35J(IJ),
2 PLM26J(IJ)
4056 CONTINUE
C
C CARDS 0700
C
ISN 0397 4020 IF(NOLEQ.EQ.0) GO TO 4021
PRINT 4031
ISN 0398 4031 FORMAT(//,1X,'OLEO STRUT BEAM DATA')
ISN 0400 PRINT 4032
ISN 0401 4032 FORMAT(20X,'BEAM AIR CURVE PARAMETERS')
ISN 0402 PRINT 4033
ISN 0403 4033 FORMAT(1X,1J I J M N',7X,'EOLEO',7X,'FAO',7X,'FAA',5X,
ISN 0404 1 'EXPOLE',5X,'YMAX')
ISN 0405 DO 4042 J=1,NLEO
DO 4041 IJ=1,NB
IF(IGOLEO(IJ).EQ.IG(IJ).AND. JGOLEO(IJ).EQ.JG(IJ).AND. MGOLEO(IJ).EQ.MG(IJ).AND. NGOLEO(IJ).EQ.NG(IJ)) GO TO 4045
1 .EQ.MG(IJ).AND. NGOLEO(IJ).EQ.NG(IJ),NG(IJ),EOLEO(IJ),FAO(IJ),
4041 CONTINUE
4045 PRINT 4034,IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),EOLEO(IJ),FAO(IJ),
1 FAA(IJ),EXPOLE(IJ),YMAX(IJ)
4034 FORMAT(1X,5I3,5X,1P5E10.3)
4042 CONTINUE
PRINT 4035
4035 FORMAT(1X,20X,'BEAM DAMPING CONSTANTS,COULOMB FRICTION AND LINEAR

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ISN 0459 5087 PRINT 5086,NP
ISN 0460 5088 FORMAT(IX // '9. NUMBER OF LINEAR DEFLECTION POINTS NOT',
* ' ACCEPTABLE VALUE = ',I2)
ISN 0461 STOP
ISN 0462 5083 KR(ICH+3) = 0.
ISN 0463 KR(ICH+4) = 0.
ISN 0464 XKR(ICH+4) = 10.*LDP(I)
ISN 0465 XKR(ICH+5) = 20.*LDP(I)
ISN 0466 GO TO 5082
ISN 0467 5084 KR(ICH+3) = -.25
ISN 0468 KR(ICH+4) = -.25
ISN 0469 XKR(ICH+4) = 4.*LDP(I)
ISN 0470 XKR(ICH+5) = 4.001*LDP(I)
ISN 0471 GO TO 5082
ISN 0472 5085 KR(ICH+3) = -.5
ISN 0473 KR(ICH+4) = -.5
ISN 0474 XKR(ICH+4) = 3.*LDP(I)
ISN 0475 XKR(ICH+5) = 3.001*LDP(I)
ISN 0476 XKR(ICH+7) = 20.*LDP(I)
ISN 0477 GO TO 5082
ISN 0478 5086 KR(ICH+3) = -1.
ISN 0479 KR(ICH+4) = -1.
ISN 0480 XKR(ICH+4) = 2.*LDP(I)
ISN 0481 XKR(ICH+5) = 2.001*LDP(I)
ISN 0482 XKR(ICH+7) = 15.*LDP(I)
ISN 0483 XKR(ICH+8) = 20.*LDP(I)
ISN 0484 GO TO 5082
ISN 0485 5091 KR(ICH+3) = -1.
ISN 0486 KR(ICH+4) = -1.
ISN 0487 KR(ICH+7) = 1.
ISN 0488 KR(ICH+8) = 1.
ISN 0489 KR(ICH+9) = 1.
ISN 0490 XKR(ICH+4) = 2.*LDP(I)
ISN 0491 XKR(ICH+5) = 2.001*LDP(I)
ISN 0492 XKR(ICH+6) = LDP(I)
ISN 0493 XKR(ICH+7) = 1.001*LDP(I)
ISN 0494 XKR(ICH+8) = 20.*LDP(I)
ISN 0495 XKR(ICH+9) = 30.*LDP(I)
ISN 0496 GO TO 5082
C
C CARDS 0800
C
5082 PRINT 5960,IQ(I),JQ(I),MQ(I),NQ(I),LQ(I)
5960 FORMAT(1H0,'KR TABLE FOR I,J,M,N,L = ',5I5)
5970 PRINT5970, (J,XKR(ICH+J),KR(ICH+J)),J=1,NP)
5970 FORMAT(1H ,I3,1P2E15.5)
C*****COMPUTE SLOPES AND INTERCEPTS
NPH1 = NP-1
DO 5080 J = 1,NPH1
SLOPE = (KR(ICH+J)-KR(ICH+J+1))/(XKR(ICH+J)-XKR(ICH+J+1))
XKS(ICH+J) = SLOPE
5080 XKI(ICH+J) = KR(ICH+J)-SLOPE*XKR(ICH+J)
C*****MOVE ENDPOINTS 'MAY OUT
00006240
00006250
00006260
00006270
00006280
00006290
00006300
00006310
00006320
00006330
00006340
00006350
00006360
00006370
00006380
00006390
00006400
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00006580
00006590
00006600
00006610
00006620
00006630
00006640
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00006660
00006670
00006680
00006690
00006700
00006710
00006720
00006730
00006740
00006750
00006760

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ISN 0506      XKR(ICH+1) = -1.E35
ISN 0507      XKR(ICH+NP) = 1.E35
ISN 0508
5070 CONTINUE
C
C CARDS 1000 DELETED 6/4/77
C
C CARD 1100
C
5540 IF(NVP.EQ.0) GO TO 5065
PRINT 4016
4016 FORMAT(//,1X,'VOLUME PENETRATION DATA',/)
PRINT 5538,NVP
5538 FORMAT(1X,'MASS USED TO IDENTIFY CONTROL VOLUME = ',I3)
PRINT 4017
4017 FORMAT(1X,'DISTANCE FROM MASS MEASURED ALONG POSITIVE (P) AND NEGATIVE (N) AXES')
PRINT 5530
5530 FORMAT(7X,'XN',14X,'XP',14X,'YN',14X,'YP',14X,'ZN',14X,'ZP')
PRINT 5522,XNBAR,XPBAR,YNBAR,YPBAR,ZNBAR,ZPBAR
5522 FORMAT(1X,1P6E15.5)
C
C CARDS 1101 AND UP
C
5065 IF(NDRI.EQ.0) GO TO 5056
PRINT 5531
5531 FORMAT(//,1X,'DRI ELEMENTS',//,2X,'I',2X,'J')
JDRI = 2*NDRI
PRINT 5532,(IJPR(J),J=1,JDRI)
5532 FORMAT(2I3)
C
C CARDS 1200
C
5056 IF(NVCH.EQ.0) GO TO 6000
PRINT 5601
5601 FORMAT(//,1X,'VOLUME CHANGE DATA',/)
FLIPP = 0.
DO 5620 I=1,NVCH
PRINT 5607
5607 FORMAT(9X,'MASS',/,1X,'POINT',2X,'NUMBER',14X,
1 'MASS COORDINATES',/,11X,'I',8X,3HX'',12X,3HY'',12X,3HZ'')
DO 5621 K=1,8
J = INBUFF(I,K)
IF(J.NE.0) GO TO 5623
J = INBUFF(I,K-1)
YDP(J) = -YDP(J)
FLIPP = 1.
5623 XP(K) = XDP(J)
YP(K) = YDP(J)
ZP(K) = ZDP(J)
IF(FLIPP.NE.1.) GO TO 5621
YDP(J) = -YDP(J)
FLIPP = 0.
5621 PRINT 5622,K,J,XP(K),YP(K),ZP(K)
ISN 0509
ISN 0510
ISN 0511
ISN 0512
ISN 0513
ISN 0514
ISN 0515
ISN 0516
ISN 0517
ISN 0518
ISN 0519
ISN 0520
ISN 0521
ISN 0522
ISN 0523
ISN 0524
ISN 0525
ISN 0526
ISN 0527
ISN 0528
ISN 0529
ISN 0530
ISN 0531
ISN 0532
ISN 0533
ISN 0534
ISN 0535
ISN 0536
ISN 0537
ISN 0538
ISN 0540
ISN 0541
ISN 0542
ISN 0543
ISN 0544
ISN 0545
ISN 0546
ISN 0548
ISN 0549
ISN 0550
0006770
0006780
0006790
0006800
0006810
0006820
0006830
0006840
0006850
0006860
0006870
0006880
0006890
0006900
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0006920
0006930
0006940
0006950
0006960
0006970
0006980
0006990
0007000
0007010
0007020
0007030
0007040
0007050
0007060
0007070
0007080
0007090
0007100
0007110
0007120
0007130
0007140
0007150
0007160
0007170
0007180
0007190
0007200
0007210
0007220
0007230
0007240
0007250
0007260
0007270
0007280
0007290

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ISN 0551      5622 FORMAT(IX,I3,I8,1P3E15.5)
ISN 0552      AVG1 = (XP(1)+XP(2)+XP(5)+XP(6))* .25
ISN 0553      AVG2 = (XP(3)+XP(4)+XP(7)+XP(8))* .25
ISN 0554      DLX = -AVG1+AVG2
ISN 0555      AVG2 = (YP(2)+YP(4)+YP(6)+YP(8))* .25
ISN 0556      AVG1 = (YP(1)+YP(5)+YP(3)+YP(7))* .25
ISN 0557      DLY = AVG1-AVG2
ISN 0558      AVG1 = (ZP(1)+ZP(2)+ZP(3)+ZP(4))* .25
ISN 0559      AVG2 = (ZP(5)+ZP(6)+ZP(7)+ZP(8))* .25
ISN 0560      DLZ = AVG1-AVG2
ISN 0561      PRINT 5604
ISN 0562      5604 FORMAT(/,16X,'VOLUME STOE LENGTHS',13X,'INITIAL VOLUME',/,
1 8X,'DELX',11X,'DELY',11X,'DELY',11X,'DELY',11X,'VZERO')
ISN 0563      VZERO(I) = DLX+DLY*DLZ
ISN 0564      PRINT 5605,DLX,DLY,DLZ,VZERO(I)
ISN 0565      5605 FORMAT(IX,1P4E15.5,/)
ISN 0566      VOLNZ(I,1) = DLX
ISN 0567      VOLNZ(I,2) = DLY
ISN 0568      VOLNZ(I,3) = DLZ
ISN 0569      5620 CONTINUE
C
C      CARDS 1300
C
ISN 0570      6000 IF(NVBH.EQ.0) GO TO 5178
ISN 0572      PRINT 5525
ISN 0573      5525 FORMAT(/,1X,'NON-STANDARD MAXIMUM DEFLECTIONS',/,
1 36X,'MAXIMUM DEFLECTIONS',/,4X,'BEAM',31X,'VMAX(I,J,L) L=',/,
2 2X,'I',2X,'J',2X,'L',2X,'M',2X,'N',
3 5X,'1',11X,'2',11X,'3',11X,'4',
4 11X,'5',11X,'6',/)
DO 5170 JI=1,NVBH
ISN 0574      I = IG(IJVM(JI))
ISN 0575      J = JG(IJVM(JI))
ISN 0576      M = MG(IJVM(JI))
ISN 0577      N = NG(IJVM(JI))
ISN 0578      DO 5171 IJ=1,NB
ISN 0579      IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.
ISN 0580      1 M.EQ.MG(IJ).AND.N.EQ.NG(IJ)) GO TO 5172
5171 CONTINUE
ISN 0582      5172 PRINT 5190,IJ,I,J,M,N,(VMAX2(L,IJ),L=1,6)
ISN 0583      5190 FORMAT(IX,5I3,1P6E12.4)
ISN 0584      5170 CONTINUE
ISN 0585      5178 IF(NVBH.EQ.0) GO TO 5191
ISN 0586      PRINT 5536
ISN 0588      5536 FORMAT(/,1X,'NON-STANDARD MAXIMUM NEGATIVE DEFLECTION',/,
ISN 0589      1 36X,'MAXIMUM DEFLECTIONS',/,4X,'BEAM',31X,'VMAXN(I,J,L) L=',/,
2 2X,'I',2X,'J',2X,'L',2X,'M',2X,'N',
3 5X,'1',11X,'2',11X,'3',11X,'4',11X,'5',11X,'6',/)
DO 5192 JI=1,NVBH
ISN 0590      I = IG(IJVMN(JI))
ISN 0591      J = JG(IJVMN(JI))
ISN 0592      M = MG(IJVMN(JI))
ISN 0593      N = NG(IJVMN(JI))
ISN 0594

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ISN 0595      DO 5193 IJ=1,NB
ISN 0596      IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ)).AND.
ISN 0598      1 M.EQ.MG(IJ).AND.N.EQ.NG(IJ)) GO TO 5194
ISN 0599      5193 CONTINUE
ISN 0600      5194 PRINT 5190,IJ,I,J,M,N,(VMAX3(L,IJ),L=1,6)
ISN 0601      5192 CONTINUE
ISN 0602      5191 IF(NFBM.EQ.0) GO TO 5199
ISN 0603      PRINT 5526
ISN 0604      5526 FORMAT(/,1X,'NON-STANDARD MAXIMUM FORCES',/,36X,'MAXIMUM',
ISN 0605      16X,'FORCES',/,4X,'BEAM',31X,'FMAX(I,J,L) L=',/
ISN 0606      22X,'I',2X,'J',2X,'M',2X,'N',5X,'1',11X,'2',11X,'3',
ISN 0607      31X,'4',11X,'5',11X,'6',/)
ISN 0608      DO 5180 JI=1,NFBM
ISN 0609      1 I = IG(IJFM(JI))
ISN 0610      J = JG(IJFM(JI))
ISN 0611      M = MG(IJFM(JI))
ISN 0612      N = NG(IJFM(JI))
ISN 0613      DO 5181 IJ=1,NB
ISN 0614      IF (I.EQ.IG(IJ).AND.J.EQ.JG(IJ)).AND.M.EQ.
ISN 0615      1MG(IJ).AND.N.EQ.NG(IJ)) GO TO 5182
ISN 0616      5181 CONTINUE
ISN 0617      5182 PRINT 5190,IJ,I,J,M,N,(FMAX2(L,IJ),L=1,6)
ISN 0618      5180 CONTINUE
ISN 0619      5199 IF(NFBM.EQ.0) GO TO 6001
ISN 0620      PRINT 5537
ISN 0621      5537 FORMAT(/,1X,'NON-STANDARD MAXIMUM NEGATIVE FORCES',/,
ISN 0622      1 36X,'MAXIMUM',6X,'FORCES',/,4X,'BEAM',31X,'FMAXN(I,J,L) L=',/
ISN 0623      2 2X,'I',2X,'J',2X,'M',2X,'N',5X,'1',11X,'2',11X,'3',
ISN 0624      3 11X,'4',11X,'5',11X,'6',/)
ISN 0625      DO 5195 JI=1,NFBM
ISN 0626      1 I=IG(IJFMN(JI))
ISN 0627      J=JG(IJFMN(JI))
ISN 0628      M=MG(IJFMN(JI))
ISN 0629      N=NG(IJFMN(JI))
ISN 0630      DO 5197 IJ=1,NB
ISN 0631      IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ)).AND.M.EQ.MG(IJ).AND.
ISN 0632      1 N.EQ.NG(IJ)) GO TO 5196
ISN 0633      5197 CONTINUE
ISN 0634      5196 PRINT 5190,IJ,I,J,M,N,(FMAX3(L,IJ),L=1,6)
ISN 0635      5195 CONTINUE
ISN 0636      C
ISN 0637      C
ISN 0638      C
ISN 0639      6001 IF(NHI.EQ.0) GO TO 6002
ISN 0640      PRINT 4006
ISN 0641      4006 FORMAT(/,1X,'MASSES HAVING NONZERO ANGULAR MOMENTA (HE)',/,
ISN 0642      1 1X,'CROSS PRODUCTS OF INERTIA (IXY,IYZ,IXZ)',/,
ISN 0643      2 1X,'OR LIFT CONSTANTS (LC)',/)
ISN 0644      PRINT 5512
ISN 0645      5512 FORMAT(5X,'I',6X,'LC',10X,'HEX',9X,'HEY',9X,'HEZ',9X,'IXY',9X,
ISN 0646      1 'IYZ',9X,'IXZ')
ISN 0647      DO 5120 I = 1,NHI
ISN 0648      PRINT 5508,INBUF(I),ALIFT(INBUF(I)),HEX(INBUF(I)),HEY(INBUF(I)),

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ISN 0639      INEZ(INBUF(I)),XYI(INBUF(I)),YZI(INBUF(I)),XZI(INBUF(I))
ISN 0640      5506 FORMAT(IX,IS,IP7E12.4)
                5120 CONTINUE
C
C      CARDS 1500
C
ISN 0641      6002 IF(NPH.EQ.0) GO TO 6003
ISN 0643      DO 5550 J=1,NPH
ISN 0644      PRINT 5570
ISN 0645      5570 FORMAT(IX,'NONZERO PHIDP,THEDP,PSIDP',/,9X,'I',3X,'PHIDP',10X,
                1,'THEDP',10X,'PSIDP')
ISN 0646      I = IPHOP(J)
ISN 0647      PRINT 5555,I,PHIDP(I),THEDP(I),PSIDP(I)
ISN 0648      5555 FORMAT(IX,II0,IP3E15.5)
ISN 0649      5550 CONTINUE
C
C      CARDS 1600
C
ISN 0650      PRINT 5571
ISN 0651      5571 FORMAT(IX,'BEAM EULER ANGLES',/,IX,'IJ',2X,'I',2X,'J',3X,
                1,'PHIJ',10X,'THEIJ',10X,'PSIJI')
ISN 0652      DO 5552 J=1,NB
ISN 0653      PRINT 5557,J,IG(J),JG(J),PHIJ(J),THEIJ(J),PSIJI(J)
ISN 0654      5557 FORMAT(II3,IP3E15.5)
ISN 0655      5552 CONTINUE
C
C      CARDS 1700,1800
C
ISN 0656      6003 IF(NACC.EQ.0) GO TO 6005
ISN 0658      PRINT 7001
ISN 0659      7001 FORMAT(//,IX,'ACCELERATION INPUT TABLE DATA')
ISN 0660      PRINT 7006
ISN 0661      7006 FORMAT(//,IX,'MASS LOCATION DIRECTION NO. PTS.')
ISN 0662      DO 7010 I=1,NACC
ISN 0663      PRINT 7009,MASSNO(I),DIR(I),NPTS(I)
ISN 0664      7009 FORMAT(IX,I2,12X,I2,9X,I2)
ISN 0665      7010 CONTINUE
ISN 0666      PRINT 7007
ISN 0667      7007 FORMAT(//,IX,'PT',7X,'TIME',11X,'ACCEL')
ISN 0668      L=0
ISN 0669      DO 7002 I=1,NACC
ISN 0670      K=NPTS(I)
ISN 0671      DO 7002 J=1,K
ISN 0672      L=L+1
ISN 0673      PRINT 7008,L,TIM(L),ACCEL(L)
ISN 0674      7008 FORMAT(IX,I2,2(5X,1PE10.3))
ISN 0675      7002 CONTINUE
C
C      CARDS 2100
C
ISN 0676      6005 PRINT 5524
ISN 0677      5524 FORMAT(//,IX,'I,J,M,N',/,1X,'K-MATRIX FOR INTERNAL BEAM IJ')
ISN 0678      DO 5528 IJ=1,NB

```


PAGE 018

00008890
00008900
00008910
00008920
00008930
00008940
00008950

PRINT 5529,IG(IJ),JG(IJ),MG(IJ),NG(IJ)
5529 FORMAT(IX,4I3)
PRINT 5533,((YK3(L,K,IJ),L=1,6),K=1,6)
5533 FORMAT(IX,1P6E15.5)
5528 CONTINUE
RETURN
END

ISN 0679
ISN 0680
ISN 0681
ISN 0682
ISN 0683
ISN 0684
ISN 0685

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,

SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,IO,XREF

C DATA SET D2334INPUT AT LEVEL 012 AS OF 06/25/79

DATA SET D2332VIU AT LEVEL 001 AS OF 01/17/78

DATA SET D2332V10 AT LEVEL 001 AS OF 01/17/78
DATA SET D2332NIU AT LEVEL 002 AS OF 11/09/77

C	DATA SET D2332NIU	AT LEVEL 002 AS OF 11/09/77
C	DATA SET D2332NIU	AT LEVEL 001 AS OF 11/02/77

DATA SET D2332NIO AT LEVEL 001 AS OF 11/02/77
DATA SET D2332VINPU AT LEVEL 004 AS OF 10/04/77

DATA SET D2332VINPO AT LEVEL 004 AS OF 10/04/77
DATA SET D2332QIU AT LEVEL 001 AS OF 07/26/77

SUBROUTINE INPUT

```
IMPLICIT REAL*8 (A-H,O-Z)
```

REAL*8 KUN,CASEIN,CASOUT,MINDT

REAL*8 LBAR,MU,KE

```
REAL*8 LBAR,NU,KE
REAL*4 KR(2700),SLOPE,XKS,XKI,XKR,LDP(180),LDP1(180)
```

```
REAL*4 KK(200),SLOPE,AKS,AKI,AKR,CDF(180),CDFI(180),
INTEGER*4 PY(150),PZ(150),PYJ(150),PZJ(150),PTEMP(4)
```

```
INTEGER*4 F(150),FZ(150),F13(150),FZ3(150)
INTEGER*4 TITLE(40),BLANK,STOP,RUNIN,RUNOUT
```

```

INTEGER*4 I11
INTEGER*4 DIR

```

```
INTEGER*4 DIR
INTEGER*2 CHUG,INBUFF,II(40),KK(40),INBUFF(80)
```

```
INTEGER*2 CRUG,INBOFF,II(40),KK(40),INBOF(80)
INTEGER*2 T-JVM(150),T-JFM(150),T-JVMN(150),T-JFMN(150)
```

```
INTEGER*2 IJFH(150), IJFH(150)
INTEGER*2 MQ(180), MQ(180)
```

```
INTEGER*2 HQ(180),NQ(180)
INTEGER*2 IQ(180),JQ(180),IQ(180),NPQ(180),NISF(6,1,IPR
```

```
INTEGER*2 IQ(I80),JQ(I80),
INTEGER*2 NI,NN,IAS,IG,JG
```

```
INTEGER*2 NI,NN,IBS,IG,JG
INTEGER*2 NIOI1,NIOI2,NIOI3
```

```

INTEGER#2 NTOL1,NTOL2,NTOL3
INTEGER#2 NBIT,NBEFCT,IBEFCT,ITPI,NMPTS,MMIM,ISCALE

```

```
INTEGER*2 NPL1,NPFC1,I
INTEGER*2 Y1SAVE(180)
```

```

INTEGER*2 IJSAVE(180)
INTEGER*2 NKHVEC(150)

```

```
INTEGER*2 NKHVEC(150)
INTEGER*2 MH(40) MC(150) NC(150) INP(50) MNR(50)
```

```
INTEGER*2 PH(40),PG(150),NG(150),INP(50),MNP(50)
INTEGER*2 NMED,NMFE,NMSE,NMDE,NMSE,NMDE,NMSE,NMDE
```

```

      INTEGER*2 NHEP,NNEP,NBFP,NBDP,NSEP,NDRP,NSTP,NENP,
      * IMASS(EQ,10),INODE(EQ,8),IDME(EQ,4),IDHD(EQ,4)

```

```

* JHASS(50,10),JNODE(50,8),JBMF(50,4),JBMD(50,
* JBMS(50,4),JSPB(50,4),JENF(50,3),JDPRT(10,

```

* JBMS(50,6), JSPPR{50,4}, JENG(50,3), JDRI(101),
* NNEW NNEW NNEW NNEW NNEW NNEW NNEW NNEW NNEW

* NMEW, NNEW, NBFW, NBOW, NSEW, NDRW, NSTW
DIMENSION C(10), IMA(256), YEA, EMAY(4), YEO)

```

DIMENSION G(150),VMAX2(6,150),FMAX2(6,150)

```

DIMENSION FMAX3(6,150),

DIMENSION XK3(6,6,150)

```

DIMENSION IJPRT(14),VMAXT(6),FMAXT(6)

```

DIMENSION MASSNO(50)

DIMENSION IPHDP(80)

DIMENSION XNPDP(50), YNPDP

COMMON/IBALL/ IBUFI(20)

COMMON/PPLTS/ XSCALE(10),YSCALE(10),NPLT,NPFCT,

```

*      NMPTS(10),MNUM(50,10),ISCALE(10)

```

COMMON/DEIN/ XNBAR,XPBAR,YNBAR,YPBAR,ZNBAR,ZPBAR,VOLENZ(5,3),

ISN 0031	2 FMAXN(900),XKSI(2700),XKRI(2700),XKR(2700),NLSFLG(900),CHUG(180),	00000410
	3 MVP	00000420
	COMMON/DEINPR/ AA(150),E(150),YY(150),ZZ(150),XI(150),	00000430
	1 XLBI(150),ZI(150),Z2(150),MC(150),XJ(150),SF26(150),SF35(150),	00000440
	2 SF26J(150),SF35J(150),PY,PZ,PYJ,PZJ,NSC,NPIN	00000450
ISN 0032	COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),EEI(20),GG(20),	00000460
	1 FINT(6,150),VOL(5),VZERO(5),KMATR(6,4),NVCH,INBUFF(5,8)	00000470
	COMMON/DOIN/ CBAR(150)	00000480
ISN 0033	COMMON/INAC/ACCEL(300),TIM(300),INDEX(50,2),JAY(50,2),KOUNT	00000490
ISN 0034	COMMON/INCF/ SA(40),SB(40),SF(40),SI(40),XTUI(40),XKE(40),	00000500
ISN 0035	1 XMAX(40),FSPOF(40),FSPOI(40),GFLEX(40),CDAMP(40),PLOWT	00000510
	COMMON/INDEAC/ NACC	00000520
ISN 0036	COMMON/INIC/ XOP(80),ZDP(80),PHIDP(80),PSIDPI(80),	00000530
ISN 0037	1 THEIDI(80),PPR,QPR,RPR,XGIN,ZGIN,PHIPR,PSIPR,THEPR,	00000540
	2 XGDOT,YGDOT,ZGDOT	00000550
	COMMON/INIDCP/ YDI(80)	00000560
ISN 0038	COMMON/INPR/ NDIR,NSP	00000570
ISN 0039	COMMON/INCFIC/ BETA	00000580
ISN 0040	COMMON/INCFIN/ THAX,IPRINT	00000590
ISN 0041	COMMON/MCFIII/ SYMFLG	00000600
ISN 0042	COMMON/COMNEW/ DAMPC,RUNMOD,RUNMOD	00000610
ISN 0043	COMMON/INP012/ MG,NG,INP,MNP	00000620
ISN 0044	COMMON/INP012/ II,KK,MH	00000630
ISN 0045	COMMON/INP0212/ MQ,NQ,IJVM,IJFM,IJVM,IJFM	00000640
ISN 0046	COMMON/INP0212/ NNP	00000650
ISN 0047	COMMON/INP0212/ XNPDP,YNPDP,ZNPDP	00000660
ISN 0048	COMMON/OLEO/EOLEO(20),FAOI(20),FAAI(20),EXPOL(20),YMAX(20),	00000670
ISN 0049	1 YOLEO(20),BOLEO(20),BROLEO(20),XKEXT(20),XKCOMP(20),FCOUL(20),	00000680
	2 ALPHAP,IGOLEO(20),JGOLEO(20),MGOLEO(20),NGOLEO(20),NOLEO	00000690
	COMMON/COMALL/ C(6,150),PI(80),Q(80),R(80),UI(80),V(80),WI(80),XI(81),	00000700
	1 YI(81),ZI(81),AI(9),AJ(9),XC(6),XK(15400),XI(80),	00000710
	2 YI(80),ZI(80),XII(80),XZI(80),YZI(80),YI(9),BIJ(720),	00000720
	3 DRII(150),OAI(720),VEE(900),MGT(80),PHI(80),THETA(80),PSI(80),	00000730
	4 PDOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),	00000740
	5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELIAT,	00000750
	6 XACC(80),YACC(80),ZACC(80),AIDOT(9),	00000760
	7 PHIIJ(150),THEIJ(150),PSIIJ(150),SURDF(6,150),TITLE,	00000770
	8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),	00000780
	9 DPIN(81),DQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),	00000790
	A CEIK(40),	00000800
	B SBAR(40),KUN(40),MAXNM,MAXIGS,MAXTBL,	00000810
	C MI,NB,I,J,IG(150),JG(150),	00000820
	D NI(900),NI(40),IJPR(150)	00000830
	COMMON/TPIC/ NIC	00000840
ISN 0051	COMMON/ININPR/ NSF,NTF,NDE,NSPD,NED,NS,NRP,NIMP	00000850
ISN 0052	COMMON/UB/ DB(150),IJUB(150),NUB	00000860
ISN 0053	COMMON/COMTR8/ G	00000870
ISN 0054	COMMON/COMTR4/ KR ,LDP ,LDPI	00000880
ISN 0055	COMMON/COMTR4/ ND,NVBPM,NFBPM,NHI,NKM,NLB,	00000890
ISN 0056	COMMON/COMTR4/ NPH ,NMTL ,NPTS ,NVBM ,IJPRT ,IPHOP,NFBM	00000900
	COMMON/COMTR2/ IQ ,Jq ,NPQ ,INBUF ,	00000910
ISN 0057	COMMON/COMTR2/ Iq ,Jq ,NPQ ,INBUF ,	00000920
	COMMON/INOUT/ FCUT,NTOLL,NTOL2,NTOL3	00000930

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ISN 0059      COMMON/OTPLT/ NMEP, NNEP, NBFP, NBDF, NSEP, NDRP, NSTP, NENP,
*              JHASS, JNODE, JBHF, JBMD, JBMS, JSRR, JENG, JDRI,
*              NTEM, NNEW, NBFM, NBDW, NSEW, NDRM, NSTM, NENM, NPRINT
ISN 0060      COMMON /RESTR/ CASEIN, RUNIN, MSECIN, CASOUT, RUNOUT, MSCOUT(5)
ISN 0061      COMMON /VARINT/ HINDT, DT2, TPRINT, EL, EU, RATHIN, RATHAX, IPC, IVAR
ISN 0062      EQUIVALENCE (XK(1), XK3(1,1,1))
ISN 0063      EQUIVALENCE (VMAX(1), VMAX2(1)), (FMAX(1), FMAX2(1))
ISN 0064      EQUIVALENCE (VMAXN(1), VMAX3(1)), (FMAXN(1), FMAX3(1))
ISN 0065      EQUIVALENCE (MASSNO(1), INDEX(1,1))
ISN 0066      EQUIVALENCE (DIR(1), INDEX(1,2))
ISN 0067      DATA STOP/'END '/
ISN 0068      DATA BLANK/' '/
ISN 0069      SQRT(X) = DSQRT(X)
ISN 0070      ABS(X) = DABS(X)

C
C
C      INITIALIZATION
C
DO 1 I=1,150
  NRVSEC(I) = 0
  SF26(I)=0.
  SF35(I)=0.
  SF26J(I)=0.
  SF35J(I)=0.
1 CONTINUE
DO 5130 I = 1, MAXNM
  ALIFT(I) = 0.0
  HEX(I) = 0.0
  HEY(I) = 0.0
  HEZ(I) = 0.0
  XYI(I) = 0.0
  YZI(I) = 0.0
  XZI(I) = 0.0
  PHIDPI(I) = 0.0
  THEDPI(I) = 0.0
  PSIDPI(I) = 0.0
5130 CONTINUE
MXIGS6 = 6*MAXIGS
DO 5010 I = 1, MXIGS6
5010 NL9FLG(I) = 0
C
C      CARD 0001.0002
C
READ 5100, (TITLE(I), I=1,20)
5100 FORMAT(20A4)
IF (TITLE(1).EQ.STOP) RETURN
READ 5100, (TITLE(I), I=21,40)
TITLE(19) = BLANK
TITLE(20) = BLANK
TITLE(39) = BLANK
TITLE(40) = BLANK
C
C      CARD 0003
C

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ISN 0102      C      READ 5100,DUMMY      00001470
ISN 0103      C      CARD 0004           00001480
ISN 0104      C      READ 5200,NM,NSP,NB,NLB,MNP,NFIN,NUB,NORI,NOLEO,NACC,MVP,NVCH, 00001490
ISN 0105      C      1 NMTL,ND           00001500
ISN 0106      C      READ 5200,NVBM,NFBM,NVBM,NFBM,NKM,NHI,NPH,NTOLL,NTOL2,NTOL3, 00001510
ISN 0107      C      1 NSC,NIC           00001520
ISN 0108      C      5200 FORMAT(14I5,2I1) 00001530
ISN 0109      C      NSC EQ.OR LESS 0 THEN NO STRESS CALC. 00001540
ISN 0110      C      NIC EQ.OR LESS 0 THEN NO PREL. LOADS/DEFLS IN SUBROUTINE IC 00001550
ISN 0111      C      CARDS 0005, 0006    00001560
ISN 0112      C      READ 5203,CASEIN,RUNIN,MSECIN 00001570
ISN 0113      C      READ 5203,CASOUT,RUNOUT,MSCOUT 00001580
ISN 0114      C      5203 FORMAT(A8,2X,6I10) 00001590
ISN 0115      C      CARD 0007           00001600
ISN 0116      C      READ 5201,IPRINT,DELTAT,TMAX,PLOMT,FCUT,RUNMOD 00001610
ISN 0117      C      MINT = 0.1 * DELTAT 00001620
ISN 0118      C      TPRINT = IPRINT * DELTAT 00001630
ISN 0119      C      READ 5201,IVAR,EL,EU,RATHIN,RATHAX 00001640
ISN 0120      C      5201 FORMAT(I10,5E10.0) 00001650
ISN 0121      C      CARDS 0008, 0009    00001660
ISN 0122      C      READ 5200,NSF,NTF,NDE,NSPD,NED,NS,NRP,NIMP 00001670
ISN 0123      C      IF(NTOL1.NE.0) GO TO 5570 00001680
ISN 0124      C      NTOL1=1 00001690
ISN 0125      C      5570 IF(NTOL2.NE. 0) GO TO 5571 00001700
ISN 0126      C      NTOL2=10 00001710
ISN 0127      C      5571 IF(NTOL3.NE.0) GO TO 5572 00001720
ISN 0128      C      NTOL3=30 00001730
ISN 0129      C      NTOL1=ALLOWABLE ENERGY GROWTH TOLERANCE IN PER CENT(%) 00001740
ISN 0130      C      NTOL2=ALLOWABLE INDIVIDUAL NEGATIVE ENERGY IN PER CENT(%) 00001750
ISN 0131      C      NTOL3=ALLOWABLE MASS DEVIATION TOLERANCE IN PER CENT(%) 00001760
ISN 0132      C      NIMP=MASS IMPULSE PRINT 2/1/79 00001770
ISN 0133      C      5572 READ 5200,NMEP,NNEP,NBFP,NBDP,NSTP,NSEP,NENP,NDRP,NPLT,NPFCT 00001780
ISN 0134      C      IPFCT = -1 00001790
ISN 0135      C      NSF=STRAIN FORCE,NTF=TOTAL FORCE,NDE=BEAM DEF.L.,NSPD=EXT. SPRING 00001800
ISN 0136      C      DATA,NED=MASS&BEAM ENERGY PRINT,NS=STRESS PRINT,NRP= 00001810
ISN 0137      C      TRANS.ACCEL(UNFILTERED&FILTERED)ONLY 00001820
ISN 0138      C      NSF,NTF,NDE,NSPD,NED,NS, EQ. OR LESS THAN 0 NO PRINT 00001830
ISN 0139      C      NRP EQ. OR LESS THAN 0 ONLY TRANS.ACCELS PRINT,>0 ALL MASS RESPONSE 00001840
ISN 0140      C      NUB=NO.OF UNSYMMETRICAL BEAMS 00001850
ISN 0141      C      NMEP,NNEP,NBFP,NBDP,NSTP,NSEP,NENP,NDRP,NPLT,NPFCT 00001860
ISN 0142      C      00001870
ISN 0143      C      00001880
ISN 0144      C      00001890
ISN 0145      C      00001900
ISN 0146      C      00001910
ISN 0147      C      00001920
ISN 0148      C      00001930
ISN 0149      C      00001940
ISN 0150      C      00001950
ISN 0151      C      00001960
ISN 0152      C      00001970
ISN 0153      C      00001980
ISN 0154      C      00001990

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C MASSPOINTS,NODE POINTS,BEAM FORCES,BEAM DEFLECTIONS,STRESSES,
C EXT.SPRINGS,ORI'S,RESPECTIVELY
C NPLT=NO.MASS POSITION PLOTS AT SELECTED INTERVALS
C NENP=TIME HISTORY PLOT OF STRAIN & DAMPING ENERGY
C
  IF(NSC.GT.0) GO TO 5210
  NS=0
  5210 CONTINUE
  IF(DELTA.T.LE.0.) GO TO 5000
  IF(NM.LE.0) GO TO 5000
  C
  C CARD 0010
  C
  C READ 5300,XGDOT,YGDOT,ZGDOT
  C
  C CARD 0011
  C
  C READ 5300,PPR,QPR,RPR
  C
  C CARD 0012
  C
  C READ 5300,PHIPR,THEPR,PSIPR,XGIN,ZGIN,BETA
  C
  C 5300 FORMAT(6E10.0)
  C
  C CARDS 0100
  C
  C READ 5301,(WGT(I),XDP(I),YDP(I),ZDP(I),XI(I),YI(I),ZI(I),I=1,NM)
  C 5301 FORMAT(7E10.0)
  C
  C CARDS 0200
  C
  C IF(NNP.EQ.0) GO TO 5534
  C READ 4001,(NMP(I),IMP(I),XNPDPI(I),YNPDPI(I),ZNPDPI(I),I=1,NNP)
  C 4001 FORMAT(2I5,3E10.0)
  C
  C CLEAR EXTERNAL SPRING FLAGS (AND THE ASSOCIATED DATA ALTHOUGH THIS
  C SHOULD NOT BE NECESSARY BECAUSE WE ONLY USE IT IF THE FLAG IS 1.
  C HOWEVER, THEY MUST BE CLEARED FOR THE SEARCH WHICH PRINTS THE INPUT.)
  C
  C 5534 IF(NSP.EQ.0) GO TO 5535
  C DO 5132 IKM=1,NSP
  C   XLBAR(IKM) = 0.
  C   XPU(IKM) = 0.
  C   XVE(IKM) = 0.
  C   SI(IKM) = 0.
  C   SA(IKM) = 0.
  C   SB(IKM) = 0.
  C   SF(IKM) = 0.
  C   FSPDI(IKM) = 0.
  C   FSPDF(IKM) = 0.
  C   CDAMP(IKM)=0.
  C 5132 CONTINUE
  C
  ISN 0126
  ISN 0128
  ISN 0129
  ISN 0130
  ISN 0132
  ISN 0134
  ISN 0135
  ISN 0136
  ISN 0137
  ISN 0138
  ISN 0139
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  00002400
  00002410
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  00002440
  00002450
  00002460
  00002470
  00002480
  00002490
  00002500
  00002510
  00002520

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C      CARDS 0300
C
ISN 0158      READ 5810, (MM(J), II(J), KK(J), XLBAR(J), XPMU(J), XKE(J), XMAX(J),
ISN 0159      1 GFLX(J), J=1, NSP)
C      5810 FORMAT(I2, I3, I5, 5E10.0)
C
C      CARDS 0400
C
ISN 0160      DO 5160 IKM=1, NSP
ISN 0161      READ 5301, SI(IKM), SA(IKM), SB(IKM), SF(IKM), FSPOI(IKM), FSPOF(IKM),
ISN 0162      1 CDAMP(IKM)
C      5160 CONTINUE
C      E=MODULUS OF ELASTICITY, A=AREA, G=MODULUS OF RIGIDITY
C      XJ=POLAR MOMENT OF INERTIA, YY=MOMENT OF INERTIA ABOUT THE Y AXIS
C      ZZ=MOMENT OF INERTIA ABOUT THE Z AXIS, XLB=MEMBER LENGTH
C      YY IS USED WITH (3,5) TERMS (Z, THETA)
C      ZZ IS USED WITH (2,6) TERMS (Y, PSI)
C
C      CARDS 0500
C
ISN 0163      5535 READ 5306, (MG(IJ), IG(IJ), NG(IJ), JG(IJ), AA(IJ), XJ(IJ), YY(IJ),
ISN 0164      1 ZZ(IJ), XI(IJ), ZI(IJ), Z2(IJ), MC(IJ), IJ=1, NB)
ISN 0165      5306 FORMAT(2(I2, I3), 5E10.0, 2F5.0, I2)
ISN 0166      DO 6101 IJ=1, NB
ISN 0167      IF(XJ(IJ), NE.0.0) GO TO 6102
ISN 0168      XJ(IJ)=YY(IJ)+ZZ(IJ)
ISN 0169      6102 PY(IJ) = 0
ISN 0170      PZ(IJ) = 0
ISN 0171      PY(IJ) = 0
ISN 0172      PZ(IJ) = 0
ISN 0173      6101 CONTINUE
C
C      CARDS 0600
C
ISN 0174      IF(NMTL.EQ.0) GO TO 2
ISN 0175      DO 4 LL=1, NMTL
ISN 0176      READ 3, K, EE(K), GG(K), STENS(K), SCOMP(K), SHEAR(K)
ISN 0177      IBUFI(LL) = K
ISN 0178      4 CONTINUE
ISN 0179      3 FORMAT(I5, 5X, 5E10.0)
ISN 0180
C
C      CARDS 0700
C
ISN 0181      2 IF(NPIN.EQ.0) GO TO 6112
ISN 0182      DO 6120 JI=1, NPIN
ISN 0183      READ 6122, M, I, N, J, (PTEMP(K), K=1, 4), (PTEMPH(K), K=1, 4)
ISN 0184      6122 FORMAT(2(I2, I3), 4I5, 4E10.0)
ISN 0185      DO 6124 IJ=1, NB
ISN 0186      IF(I.EQ.IG(IJ), AND. J.EQ. JG(IJ), AND. M.EQ. MG(IJ), AND. N.EQ. NG(IJ))
ISN 0187      1 GO TO 6126
ISN 0188      6124 CONTINUE
ISN 0189      6126 PY(IJ) = PTEMP(1)
ISN 0190      PZ(IJ) = PTEMP(2)
ISN 0191

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ISN 0192      PYJ(IJ) = PTEMP(3)
ISN 0193      PZJ(IJ) = PTEMP(4)
ISN 0194      SF35(IJ)=PTEMP(1)
ISN 0195      SF26(IJ)=PTEMP(2)
ISN 0196      SF35J(IJ)=PTEMP(3)
ISN 0197      SF26J(IJ)=PTEMP(4)
ISN 0198      6120 CONTINUE
C
C      CARDS 0900
C
ISN 0199      6112 DO 6111 IJ=1,NB
ISN 0200      IJUB(IJ)=0
ISN 0201      6111 DB(IJ)=0.
ISN 0202      IF(NB.EQ.0) GO TO 6110
ISN 0204      DO 6114 JI=1,NB
ISN 0205      READ 6116,M,I,N,J,IJTEMP,DBTEMP
ISN 0206      6116 FORMAT(12,13,15,E10.0)
ISN 0207      DO 6116 IJ=1,NB
ISN 0208      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
1 GO TO 6119
ISN 0210      6118 CONTINUE
ISN 0211      6119 IJUB(IJ)=IJTEMP
ISN 0212      DB(IJ)=DBTEMP
ISN 0213      6114 CONTINUE
C
C      CARD 0900
C
ISN 0214      6110 IF(NOLEQ.EQ.0) GO TO 6210
ISN 0216      READ 5301,ALPHAP
ISN 0217      READ 5306,(MGOLEO(IJ),IGOLEO(IJ),NGOLEO(IJ),JGOLEO(IJ),
1 EOLEO(IJ),FAO(IJ),EXPOLE(IJ),YHAX(IJ),IJ=1,NOLEO)
ISN 0218      READ 5306,(MGOLEO(IJ),IGOLEO(IJ),NGOLEO(IJ),JGOLEO(IJ),
1 BOLEO(IJ),BROLEO(IJ),XKEXT(IJ),XKCOMP(IJ),FCOUL(IJ),IJ=1,NOLEO)
ISN 0219      6210 READ 5600,DAMPC
ISN 0220      5600 FORMAT(E10.0)
C
C      DAMPC=DAMPING COEFF. FOR ALL BEAMS
C      NO STANDARD DAMPC VALUE AS OF 3/79 VALUE MUST BE INPUT
C      IF NO.NE.0 SET DESIRED CBAR TO VALUE READ IN
C
ISN 0221      CDUM=DAMPC
ISN 0222      DO 5549 IJ=1,NB
ISN 0223      5549 CBAR(IJ) = CDUM
C
C      CARDS 0901 AND UP
C
ISN 0224      IF(ND.EQ.0) GO TO 5543
ISN 0226      DO 5544 JI=1,ND
ISN 0227      READ 5547,M,I,N,J,CDUM
ISN 0228      5547 FORMAT(12,13,15,E10.0)
ISN 0229      DO 5544 IJ=1,NB
ISN 0230      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
1 CBAR(IJ) = CDUM

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ISN 0232      5544 CONTINUE
C
C      CARDS 1000
C
ISN 0233      5543 IF(NLB.EQ.0) GO TO 5541
ISN 0235      MXTBL1 = MAXTBL+1
ISN 0236      IF(NLB.GT.MXTBL1) GO TO 5921
C*****KR TABLE INPUT
C IN DERIV. TO SEE IF THERE IS A TABLE FOR A PARTICULAR IJL, WE LOOK
C AT NLSFLG(IJL) AND IF IT IS NON-ZERO, IT WILL BE THE TABLE NUMBER
C FOR THAT IJL. WE STILL USE SLOPES AND INTERCEPTS FOR THE
C INTERPOLATION BUT WE MUST FIND WHICH INTERVAL IN X WE'RE IN.
C THIS IS DONE BY KEEPING, FOR EACH TABLE, A POINTER TO THE LOWER X OF
C THE INTERVAL WE WERE IN AT THE LAST INTEGRATION STEP
C (INTEGER*2 CHUG(80)) ON THE GROUNDS THAT WE'RE PROBABLY
C STILL IN THAT INTERVAL. IF WE'RE NOT IN THAT INTERVAL, WE CHECK
C ONE BY ONE IN THE APPROPRIATE DIRECTION UNTIL WE FIND THE RIGHT
C INTERVAL AND WE SAVE THAT IN CHUG AND DO THE INTERPOLATION.
C XI) AND X(NPQ) FOR EACH TABLE ARE REPLACED BY VERY LARGE (E35)
C NEGATIVE AND POSITIVE NUMBERS SO THAT WE NEED NEVER CHECK FOR BEING
C OUT OF THE TABLE AND ALSO SO WE DON'T EVEN HAVE TO KNOW HOW MANY
C POINTS IN THE TABLE. (IF AN ARGUMENT EXCEEDS 1.E35 WE'LL BOMB
C SOONER OR LATER). THIS ALLOWS VERY RAPID TABLE SEARCH AND
C INTERPOLATION.
C*****INPUT KR TABLE SPECS
C DO TO NUMBER OF TABLES INPUT
DO 5090 I = 1,NLB
  READ 5900,MQ(I),IQ(I),NQ(I),JQ(I),LQ(I),NPQ(I),LDP(I),LDP1(I)
  5900 FORMAT(2(I2,I3),2I5,2E10.0)
C*****HUNT FOR I,J PAIR SO WE CAN STORE NONLINEAR BEAM I IN NLSFLG
DO 5030 J = 1,NB
  IF(IQ(I).EQ.IG(J).AND.JQ(I).EQ.JG(J).AND.MQ(I).EQ.MG(J)
    1 .AND.NQ(I).EQ.NG(J)) GO TO 5040
5030 CONTINUE
C*****NO SUCH I,J PAIR, ABORT
PRINT 5910,IQ(I),JQ(I),MQ(I),NQ(I)
STOP
5910 FORMAT(1H1,'5. NON-EXISTENT I,J PAIR IN KR TABLE SPECS',4I5)
C*****FOUND IT
5040 NLSFLG(6*(J-1)+LQ(I)) = I
I$AVE(I) = J
5090 CONTINUE
GO TO 5540
C*****TOO MANY KR TABLES, ABORT
5921 PRINT 5920
STOP
5920 FORMAT(1H1,'6. TOO MANY KR TABLES')
C
C      CARDS 1100
C
ISN 0255      5540 K = -14
ISN 0256      DO 5070 I = 1,NLB
ISN 0257      NP = NPQ(I)

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A-B1


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ISN 0258      K = K+15
ISN 0259      CHUG(I) = K
ISN 0260      ICH = CHUG(I)-1
ISN 0261      IF(INP.LT.10) GO TO 5070
C
C
C      IF NP.GE.10,ME READ KR TABLE DIRECTLY
C
ISN 0263      READ 5950,((XKR(ICH+J),KR(ICH+J),J=1,NP)
ISN 0264      5950 FORMAT(2E10.0)
ISN 0265      5070 CONTINUE
C
C      CARD 1200
C
ISN 0266      5541 IF(MVP.EQ.0) GO TO 5065
ISN 0268      READ 5300,XNBAR,XPBAR,YNBAR,YPBAR,ZNBAR,ZPBAR
C
C      CARDS 1201 AND UP
C
ISN 0269      5065 DO 5580 IJ=1,NB
ISN 0270      IJPR(IJ) = 0
ISN 0271      5580 CONTINUE
ISN 0272      IF(NORI.EQ.0) GO TO 5056
ISN 0273      FNORI = NORI
ISN 0274      LNRI = FNORI/7+.9
ISN 0275      DO 5560 JI=1,LNRI
ISN 0276      READ 5561,((IJPRT(J),J=1,14)
ISN 0277      5561 FORMAT(14I5)
ISN 0278      DO 5560 IJ=1,7
ISN 0279      DO 5560 IJ=1,NB
ISN 0280      IF(IJPRT(2*I-1).EQ.IG(IJ).AND.IJPRT(2*I).EQ.JG(IJ)) IJPR(IJ) = 1
ISN 0281      5560 CONTINUE
ISN 0283      C
C      CARDS 1210
C
ISN 0284      5056 IF(INVCH.EQ.0) GO TO 6000
ISN 0286      DO 5611 I=1,NVCH
ISN 0287      READ 5602,((INBUFF(I,J),J=1,8)
ISN 0288      5602 FORMAT(8I5)
ISN 0289      5611 CONTINUE
C
C      CARDS 1300, 1400
C
C*****STANDARD VMAX = 100
ISN 0290      6000 DO 5180 I = 1,MXIG56
ISN 0291      5180 VMAX(I) = 100.0
ISN 0292      IF(INVBM.EQ.0) GO TO 5185
ISN 0294      DO 5170 JI=1,NVBM
ISN 0295      READ 5820,M,I,N,J,(VMAXT(K),K=1,6)
ISN 0296      5820 FORMAT(2(I2,I3),6E10.0)
ISN 0297      DO 5171 IJ=1,NB
ISN 0298      IF(I.EQ.IG(IJ).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).
ISN 0300      1 AND.N.EQ.NG(IJ)) GO TO 5172
ISN 0300      5171 CONTINUE

```

```

ISN 0301      5172 IJVM(JI) = IJ
ISN 0302      DO 5173 L=1,6
ISN 0303      VMAX2(L,IJ)=VMAXT(L)
ISN 0304      5173 CONTINUE
ISN 0305      5170 CONTINUE
ISN 0306      5185 DO 5190 I=1,MXIGS6
ISN 0307      5190 VMAXN(I)=100.0
ISN 0308      IF(NVBMN.EQ.0) GO TO 5178
ISN 0309      DO 5186 JI=1,NVBMN
ISN 0310      READ 5820,M,I,N,J,(VMAXT(K),K=1,6)
ISN 0311      DO 5187 IJ=1,NB
ISN 0312      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
ISN 0313      1 GO TO 5188
ISN 0315      5187 CONTINUE
ISN 0316      5188 IJVM(JI)=IJ
ISN 0317      DO 5189 L=1,6
ISN 0318      VMAX3(L,IJ)=VMAXT(L)
ISN 0319      5189 CONTINUE
ISN 0320      5186 CONTINUE
ISN 0321      C STANDARD FMAX=1.E10
ISN 0322      5178 DO 5177 I=1,MXIGS6
ISN 0323      5177 FMAX(I)=1.E10
ISN 0324      IF(NFBM.EQ.0) GO TO 6100
ISN 0325      DO 5181 JI=1,NFBM
ISN 0326      READ 5820,M,I,N,J,(FMAXT(K),K=1,6)
ISN 0327      DO 5182 IJ=1,NB
ISN 0328      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).
ISN 0329      1AND.N.EQ.NG(IJ)) GO TO 5183
ISN 0330      5182 CONTINUE
ISN 0331      5183 IJFM(JI) = IJ
ISN 0332      DO 5184 L=1,6
ISN 0333      FMAX2(L,IJ)=FMAXT(L)
ISN 0334      5184 CONTINUE
ISN 0335      5181 CONTINUE
ISN 0336      6100 DO 6201 I=1,MXIGS6
ISN 0337      6201 FMAXN(I)=1.E10
ISN 0338      IF(NFBMN.EQ.0) GO TO 6001
ISN 0339      DO 6202 JI=1,NFBMN
ISN 0340      READ 5820,M,I,N,J,(FMAXT(K),K=1,6)
ISN 0341      DO 6103 IJ=1,NB
ISN 0342      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
ISN 0343      1 GO TO 6104
ISN 0344      6103 CONTINUE
ISN 0345      6104 IJFMN(JI)=IJ
ISN 0346      DO 6105 L=1,6
ISN 0347      FMAX3(L,IJ)=FMAXT(L)
ISN 0348      6105 CONTINUE
ISN 0349      6202 CONTINUE
ISN 0350      C
ISN 0351      C CARDS 1500
ISN 0352      C
ISN 0353      6001 IF(NMI.EQ.0) GO TO 6002
ISN 0354      DO 5120 I = 1,NMI

```

```

ISN 0354      READ 5000,INBUF(I),ALIFT(INBUF(I)),HEX(INBUF(I)),HEY(INBUF(I)),
ISN 0355      1HEZ(INBUF(I)),XYI(INBUF(I)),YZI(INBUF(I)),XZI(INBUF(I)),
ISN 0356      5000 FORMAT(I5,E5.0,6E10.0)
C             5120 CONTINUE
C             C
C             CARDS 1600
C
ISN 0357      6002 IF(NPH.EQ.0) GO TO 6003
ISN 0359      DO 5550 J=1,NPH
ISN 0360      READ 5551,IPHDP(J),T1,T2,T3
ISN 0361      I=IPHDP(J)
ISN 0362      PHIDP(I)=T1
ISN 0363      THEDP(I)=T2
ISN 0364      PSIDP(I)=T3
ISN 0365      5551 FORMAT(I5,5X,3E10.0)
ISN 0366      5550 CONTINUE
C             C
C             CARDS 1700
C
ISN 0367      6003 IF(NACC.EQ.0) GO TO 6005
ISN 0369      IF(NACC.GT.50) GO TO 7003
ISN 0371      KOUNT = 0
ISN 0372      DO 7010 I=1,NACC
ISN 0373      READ 7000,MASSNO(I),DIR(I),NPTS(I)
ISN 0374      7000 FORMAT(3I5)
ISN 0375      JAY(I,1) = I
ISN 0376      JAY(I,2) = NPTS(I)
ISN 0377      KOUNT = KOUNT+NPTS(I)
ISN 0378      IF(KOUNT.GT.300) GO TO 7003
ISN 0380      7010 CONTINUE
C             C
C             CARDS 1800
C
ISN 0381      L=0
ISN 0382      DO 7002 I=1,NACC
ISN 0383      K=NPTS(I)
ISN 0384      DO 7002 J=1,K
ISN 0385      L=L+1
ISN 0386      READ 7004,TIM(L),ACCEL(L)
ISN 0387      7004 FORMAT(2E10.0)
ISN 0388      7002 CONTINUE
ISN 0389      GO TO 6005
ISN 0390      7003 PRINT 7005,NACC,KOUNT
ISN 0391      7005 FORMAT(IX,'7. ERROR IN ACCEL TIME DATA INPUT' / IX,
C             *
C             'NUMACL,KOUNT = ',Z15)
C             C
C             CARDS 2000
C
ISN 0392      6005 IF(NKM.EQ.0) GO TO 5000
ISN 0394      DO 5521 I=1,NKM
ISN 0395      READ 5520,M,I,N,J
ISN 0396      5520 FORMAT(2(I2,I3))
ISN 0397      DO 5523 I2=1,NB

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ISN 0396      IF(I.EQ.IG(I2).AND.J.EQ.JG(I2).AND.M.EQ.MG(I2).AND.N.EQ.NG(I2))
ISN 0400      1 IJ=I2
ISN 0401      5523 CONTINUE
ISN 0402      NKHVEC(IJ) = 1
ISN 0403      READ 5300,((XK3(L,K,IJ),L=1,6),K=1,6)
ISN 0404      5521 CONTINUE
              5000 CONTINUE
C
C      NPLT=NO. OF PLOTS EACH TIME(MAX. OF 10)
C      ITPL=DESCRIBES PLANE 1=XY,2=XZ,3=YZ
C      NMPTS=NO. OF POINTS FOR A PLOT CURRENTLY=NO.MASS POINTS
C      MNUM=MASS NUMBERS TO BE PLOTTED
C
ISN 0405      IF(NPLT.EQ.0) GO TO 100
ISN 0407      DO 200 IP=1,NPLT
ISN 0408      READ 5400,ITPL(IP),NMPTS(IP),ISCALE(IP),XSCALE(IP),YSCALE(IP)
ISN 0409      NPT = NMPTS(IP)
ISN 0410      READ 5410, (MNUM(JP,IP), JP=1, NPT)
ISN 0411      5400 FORMAT(15,5X,2E10.5)
ISN 0412      5410 FORMAT(14I5)
ISN 0413      200 CONTINUE
ISN 0414      100 CONTINUE
ISN 0415      IF(NNEP.EQ.0) GO TO 8000
ISN 0417      DO 8010 I=1, NNEP
ISN 0418      READ 5200, (JMASS(I,J), J=1, 10)
ISN 0419      8010 CONTINUE
ISN 0420      8000 IF(NNEP.EQ.0) GO TO 8020
ISN 0422      DO 8030 I=1, NNEP
ISN 0423      READ 5200, (JNODE(I,J), J=1, 8)
ISN 0424      8030 CONTINUE
ISN 0425      8020 IF(NBFP.EQ.0) GO TO 8040
ISN 0427      DO 8050 I=1, NBFP
ISN 0428      READ 5200, (JBHF(I,J), J=1, 4)
ISN 0429      8050 CONTINUE
ISN 0430      8040 IF(NBDP.EQ.0) GO TO 8060
ISN 0432      DO 8070 I=1, NBDP
ISN 0433      READ 5200, (JBHD(I,J), J=1, 4)
ISN 0434      8070 CONTINUE
ISN 0435      8060 IF(NSTP.EQ.0) GO TO 8080
ISN 0437      DO 8090 I=1, NSTP
ISN 0438      READ 5200, (JBHS(I,J), J=1, 6)
ISN 0439      8090 CONTINUE
ISN 0440      8080 IF(NSEP.EQ.0) GO TO 8100
ISN 0442      DO 8110 I=1, NSEP
ISN 0443      READ 5200, (JSPR(I,J), J=1, 4)
ISN 0444      8110 CONTINUE
ISN 0445      8100 IF(NENP.EQ.0) GO TO 8101
ISN 0447      DO 8102 I=1, NENP
ISN 0448      READ 5200, (JENG(I,J), J=1, 3)
ISN 0449      8102 CONTINUE
ISN 0450      8101 IF(NDRP.EQ.0) GO TO 8120
ISN 0452      DO 8130 I=1, NDRP
ISN 0453      READ 5200, (JDRI(I)

```

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00005720
00005730
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00006200
00006210
00006220
00006230

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00006240
00006250
00006260

8130 CONTINUE
8120 RETURN
END

ISN 0454
ISN 0455
ISN 0456

LEVEL 21.8 (JUN 74)

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```

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NODEIT,ID,XREF
C      DATA SET D2334INTERP AT LEVEL 003 AS OF 06/25/79
SUBROUTINE INTERP(IREF,TT,YOUT)
IMPLICIT REAL*8 (A-H,O-Z)
COMMON/INAC/ACCEL(300),TIM(300),INDEX(50,2),JAY(50,2)
XNUM=ACCEL(IREF+1)-ACCEL(IREF)
XDEN=TIM(IREF+1)-TIM(IREF)
SLOPE=XNUM/XDEN
YOUT=ACCEL(IREF)+SLOPE*(TT-TIM(IREF))
6400  FORMAT(5E15.6)
      RETURN
      END
ISN 0002
ISN 0003
ISN 0004
ISN 0005
ISN 0006
ISN 0007
ISN 0008
ISN 0009
ISN 0010
ISN 0011

```

```

ISN 0002 SUBROUTINE INTERP(TT,YOUT)
ISN 0003 IMPLICIT REAL*8 (A-H,O-Z)
ISN 0004 COMMON/INAC/ACCEL(300),TIM(300),INDEX(50,2),JAY(50,2)
ISN 0005 XNUM=ACCEL(IREF+1)-ACCEL(IREF)
ISN 0006 XDEN=TIM(IREF+1)-TIM(IREF)
ISN 0007 SLOPE=XNUM/XDEN
ISN 0008 YOUT=ACCEL(IREF)+SLOPE*(TT-TIM(IREF))
ISN 0009 6400 FORMAT(5E15.6)
ISN 0010 RETURN
ISN 0011 END
00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100

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LEVEL 21.6 (JUN 74)

OS/360 FORTRAN H

DATE 79.177/14.31.18

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*

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      COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
                        SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
      C DATA SET D2334MAHUL AT LEVEL 001 AS OF 03/24/76
      C SUBROUTINE MATMUL(A,B,C)
      C IMPLICIT REAL*8 (A-H,O-Z)
      C DIMENSION A(3,3),B(3,3),C(3,3)
      C A*B TO C
      DO 10 I = 1,3
      DO 10 J = 1,3
      SUM = 0.0
      DO 20 K = 1,3
      20 SUM = SUM+A(I,K)*B(K,J)
      10 C(I,J) = SUM
      RETURN
      END

```

```

ISN 0002
ISN 0003
ISN 0004
ISN 0005
ISN 0006
ISN 0007
ISN 0008
ISN 0009
ISN 0010
ISN 0011
ISN 0012
00000010
00000020
00000030
00000040
00000050
00000060
00000070
00000080
00000090
00000100
00000110
00000120

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LEVEL 21.8 (JUN 74)

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[illegible]

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ISN 0075 YFIRST = YAXIS(I)
ISN 0076 YLAST = YAXIS(9)
C
ISN 0077 IF(YLAST .LE. 0.0) WRITE(6,7030)((XAXIS(I), I=1, 11)
C
C LOCATE FIRST VERTICAL SCALE MARK
C MARK LOCATES '-' IN VERTICAL SCALE
C
ISN 0079 MARK = 0
ISN 0080 L0 = (-YFIRST * 48.0 / DY) + 1.5
ISN 0081 IF(L0 .GT. 49) L0 = 49
ISN 0082 J = 1
ISN 0083 N = 1
ISN 0084 NL = 50
ISN 0085
C
C START LINE LOOP
C
C 100 CONTINUE
C
C IDENTIFY CURRENT PRINT LINE NUMBER
C
C NL = 50 - N
C
C SET UP I1 AND I2 FOR NORMAL PRINT LINE
C
C I1 = 1
C I2 = 3
ISN 0088 IF(NL .EQ. 1 .AND. YLAST .GT. 0.0) GO TO 110
ISN 0089 IF(NL .NE. L0) GO TO 125
ISN 0092
C
C SET UP I1 AND I2 FOR ZERO AXIS PRINT LINE
C
C 110 CONTINUE
C I1 = 4
C I2 = 5
ISN 0094
ISN 0095
ISN 0096
ISN 0097 DO 150 I=5, 104
ISN 0098 S(I) = G(I1)
ISN 0099
ISN 0100 150 CONTINUE
ISN 0101 S(2) = G(9)
ISN 0102 S(3) = G(8)
ISN 0103 S(4) = G(12)
C
C PUT HORIZONTAL SCALE MARKS IN 'S' ARRAY
C
C IF(NL .EQ. 1 .AND. YLAST .GT. 0.0) GO TO 115
C IF(NL .NE. L0) GO TO 160
ISN 0104
ISN 0105
ISN 0106 115 CONTINUE
ISN 0107 DO 155 I1=14, 104, 10
ISN 0108 155 S(I1) = G(5)
ISN 0109
ISN 0110 160 CONTINUE
ISN 0111
C
C START DIMINISHING LOOP ON DEPENDENT ARRAY LINE I.D.

```



```

ISN 0112      C      KT = 0
ISN 0113      DO 250 I2=J, NMPTS
ISN 0114      JJ = I2
ISN 0115      K = NMPTS - I2 + 1
ISN 0116      IF(Y(K) .GT. YAXIS(9)) GO TO 250
ISN 0117      L = ((Y(K) - YFIRST) * 48.0 / DY) + 1.5
ISN 0118      IF(L - NL) 260,200,250
ISN 0119      200 CONTINUE
ISN 0120
ISN 0121      C      CALCULATE LOCATION IN 'S' ARRAY FOR DATA POINT I.D.
ISN 0122      I1 = ((X(K) - X1) * 100.0 / DX) + 4.5
ISN 0123      IF(X(K) .GT. XAXIS(11)) GO TO 250
ISN 0124      S(I1) = G(2)
ISN 0125      KT = KT + 1
ISN 0126      MN(KT,1) = I1
ISN 0127      MN(KT,2) = K
ISN 0128      250 CONTINUE
ISN 0129      J = NMPTS
ISN 0130      GO TO 275
ISN 0131      260 J = JJ
ISN 0132      275 N = N + 1
ISN 0133      C
ISN 0134      IF(KT .EQ. 0) GO TO 190
ISN 0135      DO 140 I=4, 104
ISN 0136      IF(S(I) .NE. G(2)) GO TO 140
ISN 0137      DO 170 II=1, KT
ISN 0138      I1 = MN(II,1)
ISN 0139      K = MN(II,2)
ISN 0140      IF(I .EQ. II) GO TO 180
ISN 0141      170 CONTINUE
ISN 0142      GO TO 140
ISN 0143      180 CONTINUE
ISN 0144      IF(M(K) .LT. 10) GO TO 20
ISN 0145      IX = M(K) / 10
ISN 0146      IY = M(K) - (IX * 10)
ISN 0147      IF(IY .EQ. 0) IY = 10
ISN 0148      IF(II .GE. 103) GO TO 30
ISN 0149      IF(S(II+1) .EQ. G(2) .OR. S(II+2) .EQ. G(2)) GO TO 30
ISN 0150      S(II+1) = NN(IX)
ISN 0151      S(II+2) = NN(IY)
ISN 0152      GO TO 140
ISN 0153      30 IF(II .LE. 5) GO TO 140
ISN 0154      IF(S(II-1) .EQ. G(2) .OR. S(II-2) .EQ. G(2)) GO TO 140
ISN 0155      S(II-1) = NN(IY)
ISN 0156      S(II-2) = NN(IX)
ISN 0157      GO TO 140
ISN 0158      20 IF(II .GE. 104) GO TO 40
ISN 0159      IF(S(II+1) .EQ. G(2)) GO TO 40
ISN 0160      S(II+1) = NN(M(K))
ISN 0161      GO TO 140
ISN 0162      40 IF(II .LE. 4) GO TO 140
ISN 0163
ISN 0164
ISN 0165
ISN 0166
ISN 0167
ISN 0168
ISN 0169
ISN 0170
ISN 0171
ISN 0172

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ISN 0174      IF(S(11)-1) .EQ. 6(2)) GO TO 140
ISN 0176      S(11-1) = NN(M(K))
ISN 0177      140 CONTINUE
ISN 0178      190 CONTINUE
C
C      TEST FOR SCALE MARK LOCATION
C
ISN 0179      IF(MARK .NE. 0) GO TO 350
C
C      PLACE VERTICAL SCALE MARK IN 'S' ARRAY
C
ISN 0181      IF(S(4) .NE. 6(2)) S(4) = 6(5)
ISN 0183      S(2) = 6(7)
C
C      IAXIS = IAXIS - 1
C      WRITE(6,S) YAXIS(IAXIS)
ISN 0184
ISN 0185      RESET MARK INDEX
C
C      MARK = 6
C      GO TO 340
ISN 0186
ISN 0187      350 CONTINUE
ISN 0188
C      GENERATE ONE LINE OF PLOTTING
C
ISN 0189      WRITE(6,S)
C      DECREMENT MARK INDEX
C
ISN 0190      340 MARK = MARK - 1
C
C      TEST FOR LAST LINE TO DETERMINE IF PLOT IS COMPLETED
C
ISN 0191      IF(NL .GT. 1) GO TO 100
C
C      END OF PLOT. PRINT MAXIMUMS, MINIMUMS, AND SCALES
C
ISN 0193      IF(YLAST .LE. 0.0) GO TO 130
ISN 0195      PRINT 7030, (XAXIS(I), I=1, 11)
ISN 0196      130 CONTINUE
ISN 0197      RETURN
C
C      FORMATS
C
ISN 0198      7000 FORMAT(1X)
ISN 0199      7030 FORMAT(8X,11(1X,E9.3))
ISN 0200      END

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00000410
00000420
00000430
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00000460
00000470
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00000570
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00000620
00000630
00000640
00000650
00000660
00000670
00000680
00000690
00000700
00000710
00000720
00000730
00000735
00000740
00000750
00000760
00000770
00000780
00000790
00000800
00000810
00000820
00000830
00000840
00000850
00000860
00000870
00000880
00000890
00000900
00000910
00000920

MSW=3
60 DO 90 I=1,NP
   IF(A(I)-PP(MSW)) 70,75,75
70 IF(A(I)-PP(MSW)) 80,90,90
80 PP(MSW)=A(I)
   GO TO 90
75 PP(MSW)=A(I)
90 CONTINUE

*-----*
* REFERENCE AND SCALE FACTOR ARE CALCULATED *
*-----*
IF(MSW-(M-1)/20,40,92
92 CONTINUE
   XM=0.0
   XMI=PP(1)
   DO 96 I=1,3
     IF(PP(I)-XM) 93,94,94
94 XM=PP(I)
93 IF(PP(I)-XMI) 95,95,96
95 XMI=PP(I)
96 CONTINUE
   A(2)=PP(2)
   A(3)=PP(2)
   PP(2)=PP(3)
   PP(2)=PP(3)
   PP(3)=A(2)
   PP(3)=A(3)
   NRA=104-(M-1)*10
   RA=NRA
   SF=(XM-XMI)/RA
   SFT=10.*SF
   IF(SF.EQ. 0.0) SF=1.0
   IF(ABS(XM-XMI).LT.1.E-6)GO TO 97
   REF= ABS(XMI/(XM-XMI))*RA*1.5
   GO TO 98
97 REF=1.5
98 NR=REF
   IF(M-2)/100,105,110
100 PRINT 912, SFT
   GO TO 120
105 PRINT 911, SFT
   GO TO 120
110 PRINT 910, SFT
120 PRINT 920
   DO 200 I=1,NP
     PLOT(NR)=PRD
     L=Y(I)/SF*REF
     PLOT(I)=STAR
     IF(M.EQ.1)GO TO 130
     K=Y2(I)/SF*REF
     PLOT(K)=EQ
   END DO
200 CONTINUE

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COMPILE OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,

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SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,IO,XREF

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```

DATA SET D2334PREPL AT LEVEL 004 AS OF 06/25/79

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DATA SET D2332VPP AT LEVEL 001 AS OF 01/17/78

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```

DATA SET D2332VPPREP AT LEVEL 006 AS OF 10/07/77

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```

SUBROUTINE PREPL(TPRINT,NM,NMP,NB,NSP,NDR1,MSECIN)

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```

IN SUBROUTINE PREPL, OUTPUT DATA FROM KRASH ARE SHUFFLED AND
PROCESSED FOR SUBSEQUENT USE IN SUBROUTINE PLOTT.

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```

INTEGER*2 NMEP,NNEP,NBFP,NBDP,NSEP,NDRP,NSTP,NENP,

```

```

JMASS(50,10),JNODE(50,8),JBHF(50,4),JBHD(50,4),

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JBMS(50,6),JSPP(50,4),JENG(50,3),JDRI(10),

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```

NMEW,NNEW,NBFW,NBDW,NSEW,NDRW,NSTW,NENW,NPRINT

```

```

REAL*8 TPRINT,THAX

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```

DIMENSION WORK(900)

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DIMENSION AM(31,27),TM(31),IM(31)

```

```

DIMENSION AN(41,18),TN(41),IN(41),INM(41)

```

```

DIMENSION AB(51,8),TB(51),IBG(51),JBG(51),MBG(51),

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```

NBG(51),IB(51)

```

```

DIMENSION AT(51,10),TT(51),ITG(51),JTG(51),MTG(51),

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NTG(51),IT(51)

```

```

DIMENSION AS(41,6),TS(41),ISH(41),ISN(41)

```

```

DIMENSION AE(51,4),TE(51),IEG(51),JEG(51),MEG(51),NEG(51),IE(51)

```

```

DIMENSION AD(101),TD(101),IDM(101)

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```

DIMENSION AV(201,3),TV(201)

```

```

COMMON/MACFIN/ THAX,IPRINT

```

```

COMMON/OTPLT/ NMEP,NNEP,NBFP,NBDP,NSEP,NDRP,NSTP,NENP,

```

```

JMASS,JNODE,JBMF,JBHD,JBMS,JSPR,JENG,JDRI,

```

```

NMEW,NNEW,NBFW,NBDW,NSEW,NDRW,NSTW,NENW,NPRINT

```

```

EQUIVALENCE (WORK(1),AM(1,1)),(WORK(838),TM(1)),

```

```

(WORK(869),IM(1))

```

```

EQUIVALENCE (WORK(1),AN(1,1)),(WORK(738),TN(1)),

```

```

(WORK(779),IN(1)),(WORK(820),INM(1))

```

```

EQUIVALENCE (WORK(1),AB(1,1)),(WORK(409),TB(1)),

```

```

(WORK(460),IBG(1)),(WORK(511),JBG(1)),

```

```

(WORK(562),MBG(1)),(WORK(613),NBG(1)),

```

```

(WORK(664),IB(1))

```

```

EQUIVALENCE (WORK(1),AT(1,1)),(WORK(511),TT(1)),

```

```

(WORK(562),ITG(1)),(WORK(613),JTG(1)),

```

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00000020

00000030

00000040

00000050

00000060

00000070

00000080

00000090

00000100

00000110

00000120

00000130

00000140

00000150

00000160

00000170

00000180

00000190

00000200

00000210

00000220

00000230

00000240

00000250

00000260

00000270

00000280

00000290

00000300

00000310

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00000340

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00000360

00000370

00000380

00000390

00000400

```

*      (WORK(664),MTG(1)),(WORK(715),NTG(1)),
*      (WORK(766),IT(1))
*      EQUIVALENCE (WORK(1),AS(1,1)),(WORK(247),TS(1)),
*      (WORK(288),ISH(1)),(WORK(329),ISN(1))
*      EQUIVALENCE (WORK(1),AE(1,1)),(WORK(205),TE(1)),
*      (WORK(256),JEG(1)),(WORK(307),JEG(1)),
*      (WORK(358),MEG(1)),(WORK(409),NEG(1)),
*      (WORK(460),IE(1))
*      EQUIVALENCE (WORK(1),AD(1)),(WORK(102),TD(1)),
*      (WORK(203),IDM(1))
*      EQUIVALENCE (WORK(1),AV(1,1)),(WORK(604),TV(1))

C      TREST = MSECIN * 0.001
      NDT = ((THAX - TREST) / TPRINT) + 1.00001

C      PLOT MASS POINT DATA IF REQUESTED

C      REMIND 12
      IF(NHEP .LE. 0) GO TO 70
      PRINT 7000, NHEP
      7000 FORMAT (1H1,5X,15,2X,'MASS PLOT FLAG SUMMARY')
      DO 7010 I=1, NHEP
      7010 PRINT 7020, (JMASS(I,J), J=1, 10)
      7020 FORMAT (10X,10I8)
      7010 CONTINUE
      REMIND 1
      L = 1
      ICNT = 0
      NCNT = 0
      DO 10 I=1, NHEP
      10 IFIND = 0
      IF(NHEW .EQ. 0) GO TO 15
      DO 20 J=1, NDT
      20 J=1, NDT
      DO 30 K=1, NHEW
      30 READ(1) (TH(K),IM(K),AM(L,M),DUMY, M=1, 27))
      IF(IM(L) .NE. JMASS(I,1)) GO TO 30
      IFIND = 1
      L = L + 1
      ICNT = ICNT + 1
      30 CONTINUE
      20 CONTINUE
      IF(IFIND .EQ. 1) GO TO 35
      15 PRINT 6023, JMASS(I,1)
      6023 FORMAT(1H1,5X,'18. UNABLE TO FIND DATA FOR MASS',I5,
      *      ' PLOTS FOR THIS MASS WILL BE SUPPRESSED.')
      35 IF((ICNT+NDT).LE.30) GO TO 50
      NCNT = 1
      DO 40 K=1, ICNT
      40 WRITE(12) (TH(K),IM(K),AM(K,M), M=1, 27))
      CONTINUE
      ICNT = 0
      L = 1
      50 CONTINUE

```

ISN 0020

ISN 0021

ISN 0022

ISN 0023

ISN 0024

ISN 0025

ISN 0026

ISN 0027

ISN 0029

ISN 0030

ISN 0031

ISN 0032

ISN 0033

ISN 0034

ISN 0035

ISN 0036

ISN 0037

ISN 0038

ISN 0039

ISN 0040

ISN 0041

ISN 0043

ISN 0044

ISN 0045

ISN 0046

ISN 0048

ISN 0049

ISN 0050

ISN 0051

ISN 0052

ISN 0053

ISN 0055

ISN 0056

ISN 0057

ISN 0059

ISN 0060

ISN 0061

ISN 0062

ISN 0063

ISN 0064

ISN 0065

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ISN 0066      REMIND 1
ISN 0067      10 CONTINUE
ISN 0068      IF(ICNT.EQ.30.OR.NCNT.EQ.0) GO TO 65
ISN 0070      DO 60 K=1, ICNT
ISN 0071      WRITE(12) (TH(K),IM(K),(AM(K,M), M=1, 27))
ISN 0072      60 CONTINUE
ISN 0073      65 CONTINUE
ISN 0074      IF(NCNT.NE.0) REMIND 12
ISN 0076      IFIND = 0
ISN 0077      IC = 0
ISN 0078      DO 85 I=1, NMEP
ISN 0079      IF(IFIND.EQ.1) GO TO 2010
ISN 0081      IC = IC + 1
ISN 0082      IF(NCNT.EQ.0) GO TO 2000
ISN 0084      IF(IC.GT.NMEP) GO TO 81
ISN 0086      ICNT = 1
ISN 0087      DO 90 J=1, NDT
ISN 0088      READ(12) (TM(J),IM(J),(AM(J,K), K=1, 27))
ISN 0089      90 CONTINUE
ISN 0090      GO TO 2010
ISN 0091      2000 ICNT = IC * NDT + 1 - NDT
ISN 0092      2010 CONTINUE
ISN 0093      IF(IM(ICNT).EQ.JMASS(I,1)) GO TO 45
ISN 0095      IFIND = 1
ISN 0096      GO TO 80
ISN 0097      45 IFIND = 0
ISN 0098      IF(JMASS(I,2).EQ.0) GO TO 100
ISN 0100      PRINT 6000, IM(ICNT)
ISN 0101      6000 FORMAT(1H1,5X,'MASS ',I3,3X,'DISPLACEMENTS(IN)' //
* 1X,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
ISN 0102      CALL PLOTT(3,NDT,TM(ICNT),AM(ICNT,1),AM(ICNT,2),AM(ICNT,3))
ISN 0103      100 CONTINUE
ISN 0104      IF(JMASS(I,3).EQ.0) GO TO 110
ISN 0106      PRINT 6001, IM(ICNT)
ISN 0107      6001 FORMAT(1H1,5X,'MASS ',I3,3X,'EULER ANGLES(RADIAN)' //
* 1X,'TIME(SEC)',3X,'PHI',6X,'THETA',6X,'PSI')
ISN 0108      CALL PLOTT(3,NDT,TM(ICNT),AM(ICNT,16),AM(ICNT,17),AM(ICNT,18))
ISN 0109      110 CONTINUE
ISN 0110      IF(JMASS(I,4).EQ.0) GO TO 120
ISN 0112      PRINT 6002, IM(ICNT)
ISN 0113      6002 FORMAT(1H1,5X,'MASS ',I3,3X,'VELOCITY(IN/SEC) - GROUND AXES' //
* 1X,'TIME(SEC)',2X,'XDOT',6X,'YDOT',6X,'ZDOT')
ISN 0114      CALL PLOTT(3,NDT,TM(ICNT),AM(ICNT,4),AM(ICNT,5),AM(ICNT,6))
ISN 0115      120 CONTINUE
ISN 0116      IF(JMASS(I,5).EQ.0) GO TO 130
ISN 0118      PRINT 6003, IM(ICNT)
ISN 0119      6003 FORMAT(1H1,5X,'MASS ',I3,3X,'VELOCITY(IN/SEC) - MASS AXES' //
* 1X,'TIME(SEC)',4X,'U',9X,'V',9X,'W')
ISN 0120      CALL PLOTT(3,NDT,TM(ICNT),AM(ICNT,7),AM(ICNT,8),AM(ICNT,9))
ISN 0121      130 CONTINUE
ISN 0122      IF(JMASS(I,6).EQ.0) GO TO 140
ISN 0124      PRINT 6004, IM(ICNT)
ISN 0125      6004 FORMAT(1H1,5X,'MASS ',I3,3X,'ROTATIONAL VELOCITY(RAD/SEC)' //

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00001990

* 1X,'TIME(SEC)',6X,'P',6X,'Q',6X,'R')
  CALL PLOTT(3,NDT,TH,AM(ICNT,19),AM(ICNT,20),AM(ICNT,21))
140 CONTINUE
  IF(JMASS(I,7) .EQ. 0) GO TO 150
  PRINT 6005, IM(ICNT)
6005 FORMAT(1H1,5X,'MASS ',I3,3X,'UNFILTERED ACCELERATION(G''S)'
  * // 1X,'TIME(SEC)',2X,'XACC',6X,'YACC',6X,'ZACC')
  CALL PLOTT(3,NDT,TH(ICNT),AM(ICNT,10),AM(ICNT,11),AM(ICNT,12))
150 CONTINUE
  IF(JMASS(I,8) .EQ. 0) GO TO 160
  PRINT 6006, IM(ICNT)
6006 FORMAT(1H1,5X,'MASS ',I3,3X,'FILTERED ACCELERATION(G''S)'
  * // 1X,'TIME(SEC)',2X,'XACCF',5X,'YACCF',5X,'ZACCF')
  CALL PLOTT(3,NDT,TH(ICNT),AM(ICNT,13),AM(ICNT,14),AM(ICNT,15))
160 CONTINUE
  IF(JMASS(I,9) .EQ. 0) GO TO 80
  PRINT 6007, IM(ICNT)
6007 FORMAT(1H1,5X,'MASS ',I3,3X,'ROTATIONAL ACCELERATION(RAD/SEC**2)'
  * // 1X,'TIME(SEC)',2X,'PDOT',6X,'QDOT',6X,'RDOT')
  CALL PLOTT(3,NDT,TH(ICNT),AM(ICNT,22),AM(ICNT,23),AM(ICNT,24))
80 CONTINUE
  IF(JMASS(I,10) .EQ. 0) GO TO 85
  PRINT 6038, IM(ICNT)
6038 FORMAT(1H1,5X,'MASS ',I3,3X,'MASS IMPULSES'//1X,'TIME(SEC)',
  1 2X,'XIMP',6X,'YIMP',6X,'ZIMP')
  CALL PLOTT(3,NDT,TH(ICNT),AM(ICNT,25),AM(ICNT,26),AM(ICNT,27))
85 CONTINUE
  81 IF(ICNT .NE. 0) REMIND 12
70 CONTINUE

C
C PLOT NODE POINT DATA IF REQUESTED
C
  IF(NNEP .LE. 0) GO TO 170
  PRINT 7030, NNEP
7030 FORMAT(1H1,5X,I5,2X,'NODE PLOT FLAG SUMMARY')
  DO 7040 I=1, NNEP
  PRINT 7050,(JNODE(I,J),J=1,8)
7050 FORMAT(10X,8I8)
7040 CONTINUE
  REMIND 2
  L = 1
  ICNT = 0
  NCNT = 0
  DO 160 I=1, NNEP
  IFIND = 0
  IF(NNEP .EQ. 0) GO TO 185
  DO 190 J=1, NDT
  DO 200 K=1, NNEW
  READ(2) (TH( L),DUPPY,IM(I, L),IN( L), (AM( L,M),DUPPY,M=1,18))
  IF(IN( L) .NE. JNODE(I,1) .OR. IN(I, L) .NE. JNODE(I,2)) GO TO 200
  IFIND = 1
  L = L + 1
  ICNT = ICNT + 1
  ISN 0126
  ISN 0127
  ISN 0128
  ISN 0130
  ISN 0131
  ISN 0132
  ISN 0133
  ISN 0134
  ISN 0136
  ISN 0137
  ISN 0138
  ISN 0139
  ISN 0140
  ISN 0142
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  ISN 0144
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  ISN 0146
  ISN 0148
  ISN 0149
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  ISN 0176
  ISN 0177
  ISN 0178
  ISN 0179

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ISN 0179      200 CONTINUE
ISN 0180      190 CONTINUE
ISN 0181      IF(IFIND .EQ. 1) GO TO 195
ISN 0183      185 PRINT 6024, JNODE(I,2), JNODE(I,1)
ISN 0184      6024 FORMAT(1H,5X,'19. UNABLE TO FIND DATA FOR MASS',I5,
*   NODE',I5,'. PLOTS FOR THIS NODE WILL BE SUPPRESSED.')
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ISN 0185      195 IF(1CNT + NDT) .LE. 40) GO TO 210
ISN 0187      NCNT = 1
ISN 0188      DO 220 K=1, 1CNT
ISN 0189      WRITE(12) (TN(K), INH(K), IN(K), (AN(K,M), M=1,18))
ISN 0190      220 CONTINUE
ISN 0191      1CNT = 0
ISN 0192      L = 1
ISN 0193      210 CONTINUE
ISN 0194      REMIND 2
ISN 0195      180 CONTINUE
ISN 0196      IF(1CNT .EQ. 40 .OR. NCNT .EQ. 0) GO TO 230
ISN 0198      DO 240 K=1, 1CNT
ISN 0199      WRITE(12) (TN(K), INH(K), IN(K), (AN(K,M), M=1,18))
ISN 0200      240 CONTINUE
ISN 0201      230 CONTINUE
ISN 0202      IF(1CNT .NE. 0) REMIND 12
ISN 0204      IFIND = 0
ISN 0205      IC = 0
ISN 0206      DO 255 I=1, NNEP
ISN 0207      IF(IFIND .EQ. 1) GO TO 2030
ISN 0209      IC = IC + 1
ISN 0210      IF(1CNT .EQ. 0) GO TO 2020
ISN 0212      IF(IC .GT. NNEP) GO TO 251
ISN 0214      1CNT = 1
ISN 0215      DO 260 J=1, NDT
ISN 0216      READ(12) (TN(J), INH(J), INI(J), (ANI(J,K), K=1,18))
ISN 0217      260 CONTINUE
ISN 0218      GO TO 2030
ISN 0219      2020 1CNT = IC * NDT + 1 - NDT
ISN 0220      2030 CONTINUE
ISN 0221      IF(INI(1CNT) .EQ. JNODE(I,2) .AND. IN(1CNT) .EQ. JNODE(I,1))
*   GO TO 265
ISN 0223      IFIND = 1
ISN 0224      GO TO 250
ISN 0225      265 IFIND = 0
ISN 0226      IF(JNODE(I,3) .EQ. 0) GO TO 270
ISN 0228      PRINT 6008, INH(1CNT), IN(1CNT)
ISN 0229      6008 FORMAT(1H,5X,'MASS',I3,3X,'NODE',I3,3X,'DISPLACEMENTS(IN)'
*   1X,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
ISN 0230      CALL PLOT(13, NDT, TN(1CNT), ANI(1CNT,1), ANI(1CNT,2), ANI(1CNT,3))
ISN 0231      270 CONTINUE
ISN 0232      IF(JNODE(I,4) .EQ. 0) GO TO 280
ISN 0233      PRINT 6009, INH(1CNT), IN(1CNT)
ISN 0234      6009 FORMAT(1H,5X,'MASS',I3,3X,'NODE',I3,3X,'VELOCITY(IN/SEC) - GROU'
*   NDT AXES' // 1X,'TIME(SEC)',2X,'XDOT',6X,'YDOT',6X,'ZDOT')
ISN 0236      CALL PLOT(13, NDT, TN(1CNT), ANI(1CNT,4), ANI(1CNT,5), ANI(1CNT,6))
ISN 0237      280 CONTINUE

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IF(JNODE(I,5) .EQ. 0) GO TO 290
PRINT 6010, INH(ICNT),IN(ICNT)
6010 FORMAT(1H1,5X,'HASS ',I3,3X,'NODE ',I3,3X,'VELOCITY(IN/SEC) - MASS00002550
* AXES' // 1X,'TIME(SEC)',4X,'U',9X,'V',9X,'W')
CALL PLOTT(3,NOT,TN(ICNT),AN(ICNT,7),AN(ICNT,8),AN(ICNT,9))
290 CONTINUE
IF(JNODE(I,6) .EQ. 0) GO TO 300
PRINT 6011, INH(ICNT),IN(ICNT)
6011 FORMAT(1H1,5X,'HASS ',I3,3X,'NODE ',I3,3X,'UNFILTERED ACCELERATION00002610
*(6)'S) // 1X,'TIME(SEC)',2X,'XACC',6X,'YACC',6X,'ZACC')
CALL PLOTT(3,NOT,TN(ICNT),AN(ICNT,10),AN(ICNT,11),AN(ICNT,12))
300 CONTINUE
IF(JNODE(I,7) .EQ. 0) GO TO 250
PRINT 6012, INH(ICNT),IN(ICNT)
6012 FORMAT(1H1,5X,'HASS ',I3,3X,'NODE ',I3,3X,'FILTERED ACCELERATION(600002670
*')S) // 1X,'TIME(SEC)',2X,'XACCF',5X,'YACCF',5X,'ZACCF')
CALL PLOTT(3,NOT,TN(ICNT),AN(ICNT,13),AN(ICNT,14),AN(ICNT,15))
250 CONTINUE
IF(JNODE(I,8) .EQ. 0) GO TO 255
PRINT 6039, INH(ICNT),IN(ICNT)
6039 FORMAT(1H1,5X,'HASS ',I3,3X,'NODE ',I3,3X,'NODE IMPULSES(6-SEC)'
1 // 1X,'TIME(SEC)',2X,'XIMPNP',5X,'YIMPNP',5X,'ZIMPNP')
CALL PLOTT(3,NOT,TN(ICNT),AN(ICNT,16),AN(ICNT,17),AN(ICNT,18))
255 CONTINUE
251 IF(ICNT .NE. 0) REMIND 12
170 CONTINUE
C
C
C
PLOT BEAM ELEMENT FORCE DATA IF REQUIRED
IF(NBFF .LE. 0) GO TO 320
PRINT 7060, NBFF
7060 FORMAT(1H1,5X,I5,2X,'BEAM FORCE PLOT FLAG SUMMARY')
DO 7070 I=1, NBFF
PRINT 7080, (JBHF(I,J), J=1, 4)
7080 FORMAT(10X,4I8)
7070 CONTINUE
REWIND 3
L = 1
ICNT = 0
NCNT = 0
DO 330 I=1, NBFF
IFIND = 0
IF(NBFW .EQ. 0) GO TO 335
DO 340 J=1, NOT
DO 350 K=1, NBFW
READ(3) (TB(L),DUPY,IB(L),JBG(L),MBG(L),NBG(L),
* (AB(L,M), DUMY, M=1, 8))
IF(IB(L) .NE. JBHF(I,1)) GO TO 350
IFIND = 1
L = L + 1
ICNT = ICNT + 1
350 CONTINUE
340 CONTINUE

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ISN 0291      IF(IFIND .EQ. 1) GO TO 345
ISN 0293      335 PRINT 6025, JBMF(I,1)
ISN 0294      6025 FORMAT(1H1,5X,'2C. UNABLE TO FIND DATA FOR BEAM',I5,
*           ' . FORCE PLOTS FOR THIS BEAM WILL BE SUPPRESSED.')
ISN 0295      345 IF(ICNT + NDT) .LE. 50) GO TO 360
ISN 0297      NCNT = 1
ISN 0298      DO 370 K=1, ICNT
ISN 0299      WRITE(12) (TB(K),IB(K),JBG(K),MBG(K),NBG(K),(AB(K,M),
*           M=1, 8))
ISN 0300      370 CONTINUE
ISN 0301      ICNT = 0
ISN 0302      L = 1
ISN 0303      360 CONTINUE
ISN 0304      REMIND 3
ISN 0305      330 CONTINUE
ISN 0306      IF(ICNT .EQ. 50 .OR. NCNT .EQ. 0) GO TO 380
ISN 0308      DO 390 K=1, ICNT
ISN 0309      WRITE(12) (TB(K),IB(K),JBG(K),MBG(K),NBG(K),(AB(K,M),
*           M=1, 8))
ISN 0310      390 CONTINUE
ISN 0311      380 CONTINUE
ISN 0312      IF(ICNT .NE. 0) REMIND 12
ISN 0314      IFIND = 0
ISN 0315      IC = 0
ISN 0316      DO 400 I=1, NBFP
ISN 0317      IF(IFIND .EQ. 1) GO TO 2050
ISN 0319      IC = IC + 1
ISN 0320      IF(ICNT .EQ. 0) GO TO 2040
ISN 0322      IF(IC .GT. NBFW) GO TO 401
ISN 0324      ICNT = 1
ISN 0325      DO 410 J=1, NDT
ISN 0326      READ(12) (TB(J),IB(J),JBG(J),MBG(J),NBG(J),(AB(J,M),
*           M=1, 8))
ISN 0327      410 CONTINUE
ISN 0328      GO TO 2050
ISN 0329      2040 ICNT = IC * NDT + 1 - NDT
ISN 0330      2050 CONTINUE
ISN 0331      IF(IB(ICNT) .EQ. JBMF(I,1)) GO TO 415
ISN 0333      IFIND = 1
ISN 0334      GO TO 400
ISN 0335      415 IFIND = 0
ISN 0336      IF(JBMF(I,2) .EQ. 0) GO TO 420
ISN 0338      PRINT 6013, IB(ICNT),IBG(ICNT),MBG(ICNT),JBG(ICNT),NBG(ICNT)
ISN 0339      6013 FORMAT(1H1,5X,'BEAM ',I3,3X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
*           I2,5X,'AXIAL AND SHEAR FORCES(LB)' // 1X,'TIME(SEC)',3X,
*           'FX',8X,'FY',8X,'FZ')
ISN 0340      *
ISN 0341      CALL PLOTT(3,NDT,TB(ICNT),AB(ICNT,1),AB(ICNT,2),AB(ICNT,3))
ISN 0342      420 CONTINUE
ISN 0343      IF(JBMF(I,3) .EQ. 0) GO TO 430
ISN 0344      PRINT 6014, IB(ICNT),IBG(ICNT),MBG(ICNT),JBG(ICNT),NBG(ICNT)
ISN 0345      6014 FORMAT(1H1,5X,'BEAM ',I3,3X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
*           I2,5X,'MOMENTS AT I,M(IN-LB)' // 1X,'TIME(SEC)',
*           3X,'MX',8X,'MY',8X,'MZ')

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ISN 0399      DO 510 K=1, ICNT
ISN 0400      WRITE(12) (TB(K),IB(K),JBG(K),JBG(K),MBG(K),MBG(K),
*              (AB(K,M), M=1, 8))
ISN 0401      510 CONTINUE
ISN 0402      500 CONTINUE
ISN 0403      IFINCENT .NE. 0) REMIND 12
ISN 0404      IFIND = 0
ISN 0405      IC = 0
ISN 0406      DO 520 I=1, MBDP
ISN 0407      IF(I) GO TO 2070
ISN 0408      IC = IC + 1
ISN 0409      IFINCENT .EQ. 0) GO TO 2060
ISN 0410      IF(IC .GT. NBOW) GO TO 521
ISN 0411      ICNT = 1
ISN 0412      DO 530 J=1, NDT
ISN 0413      READ(12) (TB(J),IB(J),JBG(J),JBG(J),MBG(J),MBG(J),
*              (AB(J,M), M=1, 8))
ISN 0414      530 CONTINUE
ISN 0415      GO TO 2070
ISN 0416      2060 ICNT = IC * NDT + 1 - NDT
ISN 0417      2070 CONTINUE
ISN 0418      IF(I) GO TO 540
ISN 0419      PRINT 6016, IB(ICNT),IBG(ICNT),MBG(ICNT),JBG(ICNT),JBG(ICNT),
ISN 0420      FORMAT(1H1,5X,'BEAM ',I3,3X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
ISN 0421      * 12,5X,'RELATIVE DEFLECTIONS*J-I*(IN)' // 1X,'TIME(SEC)',
ISN 0422      * 4X,'X',9X,'Y',9X,'Z')
ISN 0423      CALL PLOTT(3,NDT,TB(ICNT),AB(ICNT,1),AB(ICNT,2),AB(ICNT,3))
ISN 0424      540 CONTINUE
ISN 0425      IF(J) GO TO 550
ISN 0426      PRINT 6017, IB(ICNT),IBG(ICNT),MBG(ICNT),JBG(ICNT),JBG(ICNT),
ISN 0427      FORMAT(1H1,5X,'BEAM ',I3,3X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
ISN 0428      * 12,5X,'RELATIVE ROTATIONS*J-I*(DEGREE)' // 1X,'TIME(SEC)',
ISN 0429      * 3X,'PHI',6X,'THETA',6X,'PSI')
ISN 0430      CALL PLOTT(3,NDT,TB(ICNT),AB(ICNT,4),AB(ICNT,5),AB(ICNT,6))
ISN 0431      550 CONTINUE
ISN 0432      IF(J) GO TO 560
ISN 0433      PRINT 6018, IB(ICNT),IBG(ICNT),MBG(ICNT),JBG(ICNT),JBG(ICNT),
ISN 0434      FORMAT(1H1,5X,'BEAM ',I3,3X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
ISN 0435      * 12,5X,'RELATIVE ROTATIONS*J-I*(DEGREE)' // 1X,'TIME(SEC)',
ISN 0436      * 3X,'PHI',6X,'THETA',6X,'PSI')
ISN 0437      CALL PLOTT(3,NDT,TB(ICNT),AB(ICNT,7),AB(ICNT,8))
ISN 0438      560 CONTINUE
ISN 0439      IF(I) GO TO 570
ISN 0440      PRINT 6019, IB(ICNT),IBG(ICNT),MBG(ICNT),JBG(ICNT),JBG(ICNT),
ISN 0441      FORMAT(1H1,5X,'BEAM ',I3,3X,'I,M =',I4,',',I2,5X,'J,N =',I4,',',
ISN 0442      * 12,5X,'RELATIVE ROTATIONS*J-I*(DEGREE)' // 1X,'TIME(SEC)',
ISN 0443      * 3X,'PHI',6X,'THETA',6X,'PSI')
ISN 0444      CALL PLOTT(3,NDT,TB(ICNT),AB(ICNT,9),AB(ICNT,10),AB(ICNT,11))
ISN 0445      570 CONTINUE
ISN 0446      521 IFINCENT .NE. 0) REMIND 12
ISN 0447      440 CONTINUE
ISN 0448      C PLOT BEAM STRESS DATA IF REQUIRED
ISN 0449      C IF(INSTP .LE. 0) GO TO 850
ISN 0450      C PRINT 7110, NSTP

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ISN 0451 7110 FORMAT (I1,5X,I5,2X,'BEAM STRESS PLOT FLAG SUMMARY')
ISN 0452 DO 7120 I=1, NSTP
ISN 0453 PRINT 7130, (JBMS(I,J), J=1, 6)
ISN 0454 7130 FORMAT (10X,618)
ISN 0455 7120 CONTINUE
ISN 0456 L = 1
ISN 0457 REMIND 13
ISN 0458 L = 1
ISN 0459 ICNT = 0
ISN 0460 NCNT = 0
ISN 0461 DO 860 I=1, NSTP
ISN 0462 IFIND = 0
ISN 0463 IF(NSTM.EQ.0) GO TO 865
ISN 0464 DO 870 J=1, NDT
ISN 0465 DO 880 K=1, NSTW
ISN 0466 READ(13) (TT(L),DUMMY,IT(L),ITG(L),JTG(L),MTG(L),NTG(L),
* (AT(L,M),DUMMY,M=1,10))
IF(IT(L).NE. JBMS(I,1)) GO TO 880
IFIND = 1
L = L + 1
ICNT = ICNT + 1
860 CONTINUE
870 CONTINUE
IF(IFIND.EQ.1) GO TO 875
865 PRINT 6029, JBMS(I,1)
6029 FORMAT(I1,5X,'22. UNABLE TO FIND DATA FOR BEAM',I5,
* ' . STRESS PLOTS FOR THIS BEAM WILL BE SUPPRESSED.')
875 IF((ICNT + NDT) .LE. 50) GO TO 890
NCNT = 1
DO 900 K=1, ICNT
WRITE(12) (TT(K),IT(K),ITG(K),JTG(K),MTG(K),NTG(K),
* (AT(K,M),M=1,10))
900 CONTINUE
ICNT = 0
L = 1
890 CONTINUE
REIND 13
860 CONTINUE
IF(ICNT.EQ.50.OR. NCNT.EQ.0) GO TO 910
DO 920 K=1, ICNT
WRITE(12) (TT(K),IT(K),ITG(K),JTG(K),MTG(K),NTG(K),
* (AT(K,M),M=1,10))
920 CONTINUE
910 CONTINUE
IF(NCNT.NE.0) REMIND 12
IFIND = 0
IC = 0
DO 930 I=1, NSTP
IF(IFIND.EQ.1) GO TO 2090
IC = IC + 1
IF(NCNT.EQ.0) GO TO 2080
IF(IC.GT. NSTW) GO TO 931
ICNT = 1
DO 940 J=1, NDT
ISN 0467 00004650
ISN 0468 00004660
ISN 0469 00004670
ISN 0470 00004680
ISN 0471 00004690
ISN 0472 00004700
ISN 0473 00004710
ISN 0474 00004720
ISN 0475 00004730
ISN 0476 00004740
ISN 0477 00004750
ISN 0478 00004760
ISN 0479 00004770
ISN 0480 00004780
ISN 0481 00004790
ISN 0482 00004800
ISN 0483 00004810
ISN 0484 00004820
ISN 0485 00004830
ISN 0486 00004840
ISN 0487 00004850
ISN 0488 00004860
ISN 0489 00004870
ISN 0490 00004880
ISN 0491 00004890
ISN 0492 00004900
ISN 0493 00004910
ISN 0494 00004920
ISN 0495 00004930
ISN 0496 00004940
ISN 0497 00004950
ISN 0498 00004960
ISN 0499 00004970
ISN 0500 00004980
ISN 0501 00004990
ISN 0502 00005000
ISN 0503 00005010
ISN 0504 00005020
ISN 0505 00005030
ISN 0506 00005040
ISN 0507 00005050
ISN 0508 00005060
ISN 0509 00005070
ISN 0510 00005080
ISN 0511 00005090
ISN 0512 00005100
ISN 0513 00005110
ISN 0514 00005120
ISN 0515 00005130
ISN 0516 00005140
ISN 0517 00005150
ISN 0518 00005160
ISN 0519 00005170

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ISN 0509      READ(12) (TT(J),IT(J),ITG(J),JTG(J),MTG(J),NTG(J),
*              (AT(J,M),M=1,10))
ISN 0510      940 CONTINUE
ISN 0511      GO TO 2090
ISN 0512      2080 ICNT = IC * NDT + 1 - NDT
ISN 0513      2090 CONTINUE
ISN 0514      IF(IT(ICNT) .EQ. JBMS(I,1)) GO TO 945
ISN 0515      IFIND = 1
ISN 0516      GO TO 930
ISN 0517      945 IFIND = 0
ISN 0518      IF(JBMS(I,2) .EQ. 0) GO TO 950
ISN 0519      PRINT 6070, IT(ICNT),ITG(ICNT),MTG(ICNT),JTG(ICNT),NTG(ICNT)
ISN 0520      6070 FORMAT(1H1,5X,'BEAM',I3,3X,'I,M =',I4,',',I2,5X,
*              'J,N =',I4,',',I2,5X,'STRESS RATIO (MAXIMUM SHEAR STRESS THEORY) A0005310
ISN 0521      *T TOP AND BOTTOM OF BEAM' // 1X,'TIME(SEC)',3X,'TOP',6X,'BOTTOM')
ISN 0522      CALL PLOTT(2,NDT,TT(ICNT),AT(ICNT,1),AT(ICNT,2),TT(ICNT))
*
ISN 0523      950 CONTINUE
ISN 0524      IF(JBMS(I,3) .EQ. 0) GO TO 960
ISN 0525      PRINT 6080, IT(ICNT),ITG(ICNT),MTG(ICNT),JTG(ICNT),NTG(ICNT)
ISN 0526      6080 FORMAT(1H1,5X,'BEAM',I3,3X,'I,M =',I4,',',I2,5X,
*              'J,N =',I4,',',I2,5X,'STRESS RATIO (MAXIMUM SHEAR STRESS THEORY) A0005330
ISN 0527      *T LEFT AND RIGHT EDGE OF BEAM' // 1X,'TIME(SEC)',3X,'LEFT',5X,
ISN 0528      *'RIGHT')
*
ISN 0529      CALL PLOTT(2,NDT,TT(ICNT),AT(ICNT,3),AT(ICNT,4),TT(ICNT))
ISN 0530      960 CONTINUE
ISN 0531      IF(JBMS(I,4) .EQ. 0) GO TO 970
ISN 0532      PRINT 6090, IT(ICNT),ITG(ICNT),MTG(ICNT),JTG(ICNT),NTG(ICNT)
ISN 0533      6090 FORMAT(1H1,5X,'BEAM',I3,3X,'I,M =',I4,',',I2,5X,
*              'J,N =',I4,',',I2,5X,'STRESS RATIO (THEORY OF CONST. ENERGY OF DIS0005460
ISN 0534      *T) AT TOP AND BOTTOM OF BEAM' // 1X,'TIME(SEC)',
*              3X,'TOP',6X,'BOTTOM')
*
ISN 0535      CALL PLOTT(2,NDT,TT(ICNT),AT(ICNT,5),AT(ICNT,6),TT(ICNT))
ISN 0536      970 CONTINUE
ISN 0537      IF(JBMS(I,5) .EQ. 0) GO TO 980
ISN 0538      PRINT 6100, IT(ICNT),ITG(ICNT),MTG(ICNT),JTG(ICNT),NTG(ICNT)
ISN 0539      6100 FORMAT(1H1,5X,'BEAM',I3,3X,'I,M =',I4,',',I2,5X,
*              'J,N =',I4,',',I2,5X,'STRESS RATIO (THEORY OF CONST. ENERGY OF DIS0005550
ISN 0540      *T) AT LEFT AND RIGHT EDGE OF BEAM' // 1X,'TIME(SEC)',
*              3X,'LEFT',5X,'RIGHT')
*
ISN 0541      CALL PLOTT(2,NDT,TT(ICNT),AT(ICNT,7),AT(ICNT,8),TT(ICNT))
ISN 0542      980 IF(JBMS(I,6) .EQ. 0) GO TO 930
ISN 0543      PRINT 6110, IT(ICNT),ITG(ICNT),MTG(ICNT),JTG(ICNT),NTG(ICNT)
ISN 0544      6110 FORMAT(1H1,5X,'BEAM',I3,3X,'I,M =',I4,',',I2,5X,
*              'J,N =',I4,',',I2,5X,'AXIAL STRESS AND BUCKLING LOAD RATIOS' //
ISN 0545      *1X,'TIME(SEC)',2X,'AXIAL',4X,'BUCKLING' / 11X,
*              *'STRESS',5X,'LOAD')
*
ISN 0546      CALL PLOTT(2,NDT,TT(ICNT),AT(ICNT,9),AT(ICNT,10),TT(ICNT))
ISN 0547      930 CONTINUE
ISN 0548      931 IF(ICNT .NE. 0) REMIND 12
ISN 0550      850 CONTINUE

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C
C PLOT EXTERNAL SPRING DATA IF REQUIRED
C


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ISN 0551 IF(NSEP .EQ. 0) GO TO 580
ISN 0553 PRINT 7140, NSEP
ISN 0554 7140 FORMAT (I11,5X,I5,2X,'EXTERNAL SPRING PLOT FLAG SUMMARY')
ISN 0555 DO 7150 I=1, NSEP
ISN 0556 PRINT 7080, (JSR(I,J), J=1, 4)
ISN 0557 7150 CONTINUE
ISN 0558 REMIND 8
ISN 0559 L = 1
ISN 0560 NCNT = 0
ISN 0561 NCNT = 0
ISN 0562 DO 545 I=1, 40
ISN 0563 DO 545 J=1, 6
ISN 0564 AS(I,J) = 0.0
ISN 0565 545 CONTINUE
ISN 0566 DO 555 I=1, NSEP
ISN 0567 IFIND = 0
ISN 0568 IF(NSEP .EQ. 0) GO TO 556
ISN 0570 DO 560 J=1, NOT
ISN 0571 DO 570 K=1, NSEW
ISN 0572 READ(8) (TSD,DUMMY,JSH,JSK,JSN,ADUM1,DUMMY,ADUM2,DUMMY)
ISN 0573 IF(JSN .NE. JSR(I,1)) .OR. JSN .NE. JSR(I,2)) GO TO 570
ISN 0575 IFIND = 1
ISN 0576 TS(L) = TSD
ISN 0577 ISH(L) = JSN
ISN 0578 ISN(L) = JSN
ISN 0579 AS(L,JSK) = ADUM1
ISN 0580 AS(L,JSK+3) = ADUM2
ISN 0581 570 CONTINUE
ISN 0582 L = L + 1
ISN 0583 ICNT = ICNT + 1
ISN 0584 540 CONTINUE
ISN 0585 IF(IFIND .EQ. 1) GO TO 565
ISN 0587 556 PRINT 6027, JSR(I,1),JSR(I,2)
ISN 0588 6027 FORMAT(I11,5X,'23. UNABLE TO FIND DATA FOR SPRING',I5,
* ' NODE',I5,'. PLOTS FOR THIS SPRING WILL BE SUPPRESSED.')
ISN 0589 565 IF((ICNT + NOT) .LE. 40) GO TO 590
ISN 0591 NCNT = 1
ISN 0592 DO 600 K=1, ICNT
ISN 0593 WRITE(12) (TS(K),ISH(K),ISN(K),(AS(K,M), M=1, 6))
ISN 0594 600 CONTINUE
ISN 0595 ICNT = 0
ISN 0596 L = 1
ISN 0597 590 CONTINUE
ISN 0598 REMIND 8
ISN 0599 555 CONTINUE
ISN 0600 IF(ICNT .EQ. 40 .OR. NCNT .EQ. 0) GO TO 610
ISN 0602 DO 620 K=1, ICNT
ISN 0603 WRITE(12) (TS(K),ISH(K),ISN(K),(AS(K,M), M=1, 6))
ISN 0604 620 CONTINUE
ISN 0605 610 CONTINUE
ISN 0606 IF(NCNT .NE. 0) REMIND 12
ISN 0608 IFIND = 0
ISN 0609 IC = 0

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ISN 0610      DO 630 I=1, NSEP
ISN 0611      IF(IFIND.EQ. 1) GO TO 2110
ISN 0613      IC = IC + 1
ISN 0614      IF(NCNT.EQ. 0) GO TO 2100
ISN 0616      IF(IC.GT. NSEM) GO TO 631
ISN 0618      ICNT = 1
ISN 0619      DO 640 J=1, NDT
ISN 0620      READ(12) (TS(J),ISM(J),ISN(J),(AS(J,M), M=1, 6))
ISN 0621      GO TO 2110
ISN 0622      640 CONTINUE
ISN 0623      2100 ICNT = IC * NDT + 1 - NDT
ISN 0624      2110 CONTINUE
ISN 0625      IF(ISM(ICNT).EQ. JSPP(I,1).AND. ISN(ICNT).EQ. JSPP(I,2))
*      GO TO 645
ISN 0627      IFIND = 1
ISN 0628      GO TO 630
ISN 0629      645 IFIND = 0
ISN 0630      IF(JSPP(I,3).EQ. 0) GO TO 650
ISN 0632      PRINT 6019, ISM(ICNT),ISN(ICNT)
ISN 0633      6019 FORMAT(1H1,5X,'EXTERNAL SPRING I,M =',I4,',',I2,5X,
*      'COMPRESSION(IN)' // 1X,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
ISN 0634      CALL PLOTT(3,NDT,TS(ICNT),AS(ICNT,1),AS(ICNT,2),AS(ICNT,3))
ISN 0635      650 CONTINUE
ISN 0636      IF(JSPP(I,4).EQ. 0) GO TO 630
ISN 0638      PRINT 6020, ISM(ICNT),ISN(ICNT)
ISN 0639      6020 FORMAT(1H1,5X,'EXTERNAL SPRING I,M =',I4,',',I2,5X,
*      'AXIAL LOAD(LB)' // 1X,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
ISN 0640      CALL PLOTT(3,NDT,TS(ICNT),AS(ICNT,4),AS(ICNT,5),AS(ICNT,6))
ISN 0641      630 CONTINUE
ISN 0642      631 IF(NCNT.NE. 0) REWIND 12
ISN 0644      580 CONTINUE
C
C      PLOT STRAIN&DAMPING ENERGY
C
ISN 0645      IF(NENP.EQ.0) GO TO 581
ISN 0647      PRINT 7161,NENP
ISN 0648      7161 FORMAT(1H1,5X,I5,2X,'STRAIN AND DAMPING PLOT FLAG SUMMARY')
ISN 0649      DO 7162 I=1,NENP
ISN 0650      PRINT 7080,(JENG(I,J),J=1,3)
ISN 0652      7081 FORMAT(10X,3I8)
ISN 0653      7162 CONTINUE
ISN 0654      REWIND 11
ISN 0655      L=1
ISN 0656      NCNT=0
ISN 0657      DO 331 I=1,NENP
ISN 0658      IFIND=0
ISN 0659      IF(NENM.EQ.0) GO TO 336
ISN 0661      DO 341 J=1,NDT
ISN 0662      DO 351 K=1,NENM
ISN 0663      READ(11) (TE(L),DUMMY,IE(L),IEG(L),MEG(L),JEG(L),NEG(L),
1      (AE(L,M),DUMMY,M=1,4))
ISN 0664      IF(IE(L).NE. JENG(I,1)) GO TO 351

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ISN 0666      IFIND=1
ISN 0667      L=L+1
ISN 0668      ICNT=ICNT+1
ISN 0669      351 CONTINUE
ISN 0670      341 CONTINUE
ISN 0671      336 PRINT 6040,JENG(I,1)
ISN 0672      6040 FORMAT(1H1,5X,'26.UNABLE TO FIND DATA FOR BEAM',I5,'.ENERGY PLOTS
ISN 0673      1 FOR THIS BEAM WILL BE SUPPRESSED.')
ISN 0674      346 IF((ICNT+NDT).LE.50) GO TO 361
ISN 0675      NCNT=1
ISN 0676      DO 371 K=1,ICNT
ISN 0677      WRITE(12) (TE(K),IE(K),JEG(K),NEG(K),JEG(K),NEG(K),
ISN 0678      1 (AE(L,M),M=1,4))
ISN 0679      371 CONTINUE
ISN 0680      ICNT=0
ISN 0681      L=1
ISN 0682      361 CONTINUE
ISN 0683      REMIND 11
ISN 0684      331 CONTINUE
ISN 0685      IF(ICNT.EQ.50.OR.NCNT.EQ.0) GO TO 361
ISN 0686      DO 391 K=1,ICNT
ISN 0687      WRITE(12) (TE(K),IE(K),JEG(K),NEG(K),JEG(K),NEG(K),
ISN 0688      1 (AE(L,M),M=1,4))
ISN 0689      391 CONTINUE
ISN 0690      381 CONTINUE
ISN 0691      IF(NCNT.NE.0) REMIND 12
ISN 0692      IFIND=0
ISN 0693      IC=0
ISN 0694      DO 402 I=1,NENP
ISN 0695      IF(IFIND.EQ.1) GO TO 2051
ISN 0696      IC=IC+1
ISN 0697      IF(NCNT.EQ.0) GO TO 2041
ISN 0698      IF(IC.GT.NENM) GO TO 403
ISN 0699      ICNT=1
ISN 0700      DO 411 J=1,NDT
ISN 0701      READ(12) (TE(J),IE(J),JEG(J),NEG(J),JEG(J),NEG(J),
ISN 0702      1 (AE(J,M),M=1,4))
ISN 0703      411 CONTINUE
ISN 0704      GO TO 2051
ISN 0705      2041 ICNT=IC+NDT+1-NDT
ISN 0706      2051 CONTINUE
ISN 0707      IF(IE(ICNT).EQ.JENG(I,1)) GO TO 416
ISN 0708      IFIND=1
ISN 0709      GO TO 402
ISN 0710      416 IFIND=0
ISN 0711      IF(JENG(I,2).EQ.0) GO TO 421
ISN 0712      PRINT 6050,IE(ICNT),JEG(ICNT),NEG(ICNT),JEG(ICNT),NEG(ICNT)
ISN 0713      6050 FORMAT(1H1,5X,'BEAM',I3,3X,'I,M=',I4,'.I2,5X,'J,N=',I4,'.I2,
ISN 0714      1 5X,'STRAIN ENERGY AND PERCENT',I3,3X,'SE',I4,
ISN 0715      2 'X')
ISN 0716      CALL PLOTT(2,NDT,TE(ICNT),AE(ICNT,1),AE(ICNT,2))
ISN 0717      421 CONTINUE
ISN 0718
ISN 0719
ISN 0720
ISN 0721

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ISN 0722 IF(JEMG(I,3),EQ,0) GO TO 431
ISN 0724 PRINT 6051,IE(ICNT),IEG(ICNT),NEG(ICNT),JEG(ICNT),NEG(ICNT)
ISN 0725 6051 FORMAT(IH1,5X,'BEAM',I3,3X,'I,M=',I4,' ',I2,5X,'J,N=',I4,
1 ' ',I2,5X,'DAMPING ENERGY AND PERCENT'// 1X,'TIME(SEC)',3X,
2 'DE',8X,'%')
ISN 0726 CALL PLOT(I2,NDT,TE(ICNT),AE(ICNT,3),AE(ICNT,4))
ISN 0727 431 CONTINUE
ISN 0728 402 CONTINUE
ISN 0729 403 IF(NCNT.NE.0) REMIND 12
ISN 0731 581 CONTINUE
C
C PLOT DRI MASS DATA IF REQUIRED
C
ISN 0732 IF(NDRP .EQ. 0) GO TO 660
ISN 0734 PRINT 7160, NDRP
ISN 0735 7160 FORMAT (IH1,5X,I5,2X,'DRI PLOT FLAG SUMMARY')
ISN 0736 DO 7170 I=1, NDRP
ISN 0737 PRINT 7180, (JORI(I))
ISN 0738 7180 FORMAT (10X,I8)
ISN 0739 7170 CONTINUE
ISN 0740 REMIND 9
ISN 0741 L = 1
ISN 0742 ICNT = 0
ISN 0743 NCNT = 0
ISN 0744 DO 670 I=1, NDRP
ISN 0745 IFIND = 0
ISN 0746 IF(NDRW .EQ. 0) GO TO 675
ISN 0748 DO 680 J=1, NDT
ISN 0749 DO 690 K=1, NDRW
ISN 0750 READ(9) (TD(L),DUMY,IDM(L),AD(L),DUMY)
ISN 0751 IF(IDM(L) .NE. JORI(I)) GO TO 690
ISN 0752 IFIND = 1
ISN 0753 L = L + 1
ISN 0754 ICNT = ICNT + 1
ISN 0755 690 CONTINUE
ISN 0756 680 CONTINUE
ISN 0757 IF(IFIND .EQ. 1) GO TO 685
ISN 0758 675 PRINT 6028, JORI(I)
ISN 0760 6028 FORMAT(IH1,5X,'24. UNABLE TO FIND DATA FOR DRI MASS',I5,
ISN 0761 * ' . PLOTS FOR THIS DRI MASS WILL BE SUPPRESSED.')
ISN 0762 685 IF((ICNT + NDT) .LE. 100) GO TO 700
ISN 0764 NCNT = 1
ISN 0765 DO 710 K=1, ICNT
ISN 0766 WRITE(12) (TD(K),IDM(K),AD(K))
ISN 0767 710 CONTINUE
ISN 0768 ICNT = 0
ISN 0769 L = 1
ISN 0770 700 CONTINUE
ISN 0771 REMIND 9
ISN 0772 670 CONTINUE
ISN 0773 IF(ICNT .EQ. 100 .OR. NCNT .EQ. 0) GO TO 720
ISN 0775 DO 730 K=1, ICNT
ISN 0776 WRITE(12) (TD(K),IDM(K),AD(K))

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ISN 0777 730 CONTINUE
ISN 0778 720 CONTINUE
ISN 0779 IF(INCNT .NE. 0) REMIND 12
ISN 0780 IFIND = 0
ISN 0781 IC = 0
ISN 0782 DO 740 I=1, NDRP
ISN 0783 IF(IFIND .EQ. 1) GO TO 2130
ISN 0784 IC = IC + 1
ISN 0785 IF(INCNT .EQ. 0) GO TO 2120
ISN 0786 IF(IC .GT. NDRM) GO TO 741
ISN 0787 ICNT = 1
ISN 0788 DO 750 J=1, NOT
ISN 0789 READ(12) (TD(J),IDM(J),AD(J))
ISN 0790 750 CONTINUE
ISN 0791 GO TO 2130
ISN 0792 2120 ICNT = IC * NOT + 1 - NOT
ISN 0793 2130 CONTINUE
ISN 0794 IF(IDM(ICNT) .EQ. JDR(I)) GO TO 755
ISN 0795 IFIND = 1
ISN 0796 GO TO 740
ISN 0797 755 IFIND = 0
ISN 0798 IF(JDR(I) .EQ. 0) GO TO 740
ISN 0799 PRINT 6021, IDM(ICNT)
ISN 0800 6021 FORMAT(1H1,5X,'DRI MASS ',I3 // IX,'TIME(SEC)',3X,'DRI')
ISN 0801 CALL PLOTT(1,NOT,TD(ICNT),AD(ICNT),TD(ICNT))
ISN 0802 740 CONTINUE
ISN 0803 741 IF(INCNT .NE. 0) REMIND 12
ISN 0804 660 CONTINUE
ISN 0805 C
ISN 0806 C
ISN 0807 C
ISN 0808 PLOT VEHICLE C.G. DATA
ISN 0809 REMIND 10
ISN 0810 DO 760 I=1, NOT
ISN 0811 READ(10,ERR=999) (TV(I),DUMMY,(AV(I,M),DUMMY, M=1, 3))
ISN 0812 760 CONTINUE
ISN 0813 ICNT = 1
ISN 0814 PRINT 6022
ISN 0815 6022 FORMAT(1H1,5X,'VEHICLE C.G. VELOCITY(IN/SEC)' //
ISN 0816 * IX,'TIME(SEC)',4X,'X',9X,'Y',9X,'Z')
ISN 0817 * CALL PLOTT(3,NOT,TV(ICNT),AV(1,1),AV(1,2),AV(1,3))
ISN 0818 800 CONTINUE
ISN 0819 RETURN
ISN 0820 999 CONTINUE
ISN 0821 PRINT 1000,I,NOT
ISN 0822 PRINT 1003
ISN 0823 DO 998 I1=1,I
ISN 0824 998 PRINT 1001,TV(I1),(AV(I1,M),M=1,3)
ISN 0825 RETURN
ISN 0826 1000 FORMAT(/// '25. ***ERROR PLOT***' / 10X,'I = ',I4,5X,
ISN 0827 * 'NOT = ',I4)
ISN 0828 1001 FORMAT(1X,1P4E15.5)
ISN 0829 1003 FORMAT(/// 10X,'TVI ',7X,'AV(1,1)',7X,'AV(1,2)',7X,'AV(1,3)')
ISN 0830 END
ISN 0831

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,1D,XREF
C DATA SET D2334PRINT AT LEVEL 022 AS OF 06/25/79
C DATA SET D2332XPR AT LEVEL 012 AS OF 05/22/78
C DATA SET D2332FPR AT LEVEL 006 AS OF 02/08/78
SUBROUTINE PRINT
C

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ISN 0002 C IMPLICIT REAL*8 (A-H,O-Z)
ISN 0003 REAL*8 KUN,KEI,KETOTL,MINDT
ISN 0004 REAL*4 ENGSMT(6,200),ETIME(200)
ISN 0005 REAL*4 XKS,XKI,XKR,CLTEST
ISN 0006 INTEGER*4 PY(150),PZ(150),PJ(150),PZJ(150)
ISN 0007 INTEGER*4 TITLE(40)
ISN 0008 INTEGER*2 NTOL1,NTOL2,NTOL3
ISN 0009 INTEGER*2 NLSFLG,CHUG,NL,NW,IG,JG,IEER,IESE,IEPE,IEDE,IEPDE
ISN 0010 INTEGER*2 IECE,IEPCE,IEFE,IEPFE,IEDEV,IETOT
ISN 0011 INTEGER*2 IJPR,INBUFF,II(40),KK(40)
ISN 0012 INTEGER*2 NPLT,NPFCT,IPFCT,ITPL,NMPTS,MNUM,ISCALE
ISN 0013 INTEGER*2 MH(40),MG(150),NG(150),INP(50),MNP(50)
ISN 0014 INTEGER*2 NMIEP,NMIEP,NBFP,NBOP,NSEP,NDRP,NSTP,NENP,
ISN 0015 * JMASS(50,10),JNODE(50,8),JBMF(50,4),JBMD(50,4),
* JBMS(50,6),JSPP(50,4),JENG(50,3),JDRI(10),
* NMIEW,NMIEW,NBFW,NBDM,NSEM,NDRW,NSTM,NENW,NPRINT
DIMENSION XNP(50),YNP(50),ZNP(50),XDNP(50),YDNP(50),ZDNP(50)
DIMENSION VEE2(6,150),TEMP(7),DEV(200)
DIMENSION IPLN(15)
DIMENSION A(50),B(50)
COMMON/PPLTS/ XSCALE(10),YSCALE(10),NPLT,NPFCT,IPFCT,ITPL(10),
* NMPTS(10),MNUM(50,10),ISCALE(10)
COMMON/CFPR/ FSPRNG(40,8),DELG(40)
COMMON/DEPR/ XDOTAP,YDOTAP,ZDOTAP,DLVOL(5,3),FRD(150,4),
1 FRS(150,4),SUMDFIT(6,150),FINIT(6,150),VEEN(2,150)
COMMON/DEIC/ WTOT,CLTEST(150)
COMMON/DEIN/ XNBAR,XFBAR,YNBAR,YFBAR,ZNBAR,ZFBAR,VOLENZ(5,3),
1 FHAXI(900),HEX(80),HEY(80),HEZI(80),ALIFT(80),VHAXI(900),VHAXNI(900),
2 FHAXNI(900),XKI(2700),XKR(2700),NLSFLG(900),CHUG(180),
3 HVP
COMMON/DEINPR/ AA(150),E(150),YY(150),ZZ(150),XIQ(150),
1 XLBI(150),ZLI(150),ZLI(150),MC(150),XJ(150),SF26(150),SF35(150),
2 SF26J(150),SF35J(150),PJ,PZ,PY,PZJ,NSC,NPIN
COMMON/DEHA/ DEVHAX
COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),FE(20),GG(20),

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1 FINT(6,150),VOL(5),VZERO(5),KMATR(6,4),NVCH,INBUFF(5,8)
COMMON/ENERGY/ XPC(80),XETOT(80),XETOT(80),XSE(80),XDE(80),
1 XCE(80),XFE(80),KEI(80),PEI(80),XETOTL,KETOTL,
2 PETOTL,SETOTL,DETOTL,CETOTL,FETOTL
COMMON/INIDCP/ YDI(80)
COMMON/INPR/ NDRI,NSP
COMMON/MAPR/ ETOTL,ENGSMY,INGSCY
COMMON/MAPRI/ DEV,ETIME,IEER,IESE,IEPSE,IEDE,IEPDE,IECE,IEPCE,
1 IEFE,IEFFE,IEDEV,IEYOT
COMMON/MCFIII/ SYMFLG
COMMON/MP0012/ MG,NG,INP,MP
COMMON/MP0112/ II,KK,MM
COMMON/MP0014/ NNP
COMMON/MP01R8/ XNP,YNP,UNP,VNP,MNP,XDNP,ZDNP,
1 XACNP,YACNP,ZACNP,SBUCKR(150),PCR(150)
COMMON/INOUT/ FCUT,NTOL1,NTOL2,NTOL3
COMMON/PRNA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50),
1 ZACNPF(50),XIMP(80),YIMP(80),ZIMP(80),XIMPNP(50),YIMPNP(50),
2 ZIMPNP(50),XIMPOL(80),YIMPOL(80),ZIMPOL(80),XIMPPL(50),
3 YIMPPL(50),ZIMPPL(50)
COMMON/COMALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),
1 Y(81),Z(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),
2 YI(80),ZI(80),XZI(80),XZI(80),YI(9),BIJ(720),
3 DRI(150),OAI(720),VEE(900),MGT(80),PHI(80),THETA(80),PSI(80),
4 PDOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),
5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
6 XACC(80),YACC(80),ZACC(80),AIDOT(9),
7 PHIJJ(150),THEIJ(150),PSIJ(150),SUMDF(6,150),TITLE,
8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9 DPIN(81),DQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),
A CEIKF(40),
B SBAR(40),KUN(40),MAXNH,MAXIGS,MAXTBL,
C NM,NB,I,J,IG(150),JG(150),
D NI(900),NN(40),IJPR(150)
COMMON/ININPR/ NSF,NTE,NDE,NSPD,NSPO,NSD,NSP,NRP,NIMP
COMMON/OTPLT/ NNEP,NNEP,NBFP,NSEP,NSEP,NDRP,NSIP,NENP,
* JHSS,JNODE,JBHF,JBMD,JBMS,JSPR,JENG,JORI,
* NHEM,NHEM,NBFW,NBDM,NSEW,NDRM,NSTM,NENM,NPRINT
COMMON /MAX/ IRUPSH(150),IPENSM(80),VEEBAR(900),ZINIT(80),
1 DPHIJ(150),FUB(150)
COMMON /VARINT/ MINDT,DT2,TPRINT,EL,EU,RATMIN,RATHMAX,IPC,IVAR
EQUIVALENCE (VEE(1),VEE2(1,1))
DATA IPLN /
* X(+AFT) - Y(+RIGHT) X(+AFT) - Z(+UP) Y(+RIGHT) - Z(+UP) , /
I LINES = 60
IPL = 6
IF (NPR .LE. 0) IPL = 2
ITTL = 9
C FORCE NEW PAGE
NPR = 1000
DO 3099 I = 1,NM
IF (I LINES-NPR-IPL) 3010,3020,3020,3020
3010 PRINT 3100,TITLE

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ISN 0029

ISN 0030

ISN 0031

ISN 0032

ISN 0033

ISN 0034

ISN 0035

ISN 0036

ISN 0037

ISN 0038

ISN 0039

ISN 0040

ISN 0041

ISN 0042

ISN 0043

ISN 0044

ISN 0045

ISN 0046

ISN 0047

ISN 0048

ISN 0049

ISN 0050

ISN 0052

ISN 0053

ISN 0054

ISN 0055

ISN 0056

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ISN 0057 3100 FORMAT(1H,20A4 / 1X,20A4 / )
ISN 0058 PRINT 3200,TIME,IPC
ISN 0059 3200 FORMAT(1H ,6H TIME =,F9.6,5X,'NUMBER OF INTEGRATION INTERVALS =',
1 I4,/)
ISN 0060 IF(INRP .GT. 0) PRINT 3201
ISN 0062 IF(INRP .LE. 0) PRINT 3214
ISN 0064 3201 FORMAT(1X,'MASS DISPLACEMENTS,VELOCITIES,AND ACCELERATIONS' / )
ISN 0065 3214 FORMAT(1X,'NO MASS RESPONSE DATA REQUESTED EXCEPT TRANSLATIONAL
*ACCELERATIONS' / )
ISN 0066 IF(INRP .LE. 0) GO TO 3018
ISN 0068 PRINT 3300
ISN 0069 PRINT 400
ISN 0070 PRINT 500
ISN 0071 PRINT 600
ISN 0072 3018 PRINT 900
ISN 0073 3300 FORMAT(1H ,18X,1HX,14X,1HY,14X,1HZ,13X,3HPHI,11X,5H THETA,
1 11X,3HPSI)
ISN 0074 400 FORMAT(1H ,17X,4HXDOT,11X,4HYDOT,11X,4HZDOT,10X,6HPHIDOT,
1 8X,8H THETADOT,8X,6HPSIDOT)
ISN 0075 500 FORMAT(1H ,18X,1HU,14X,1HV,14X,1HW,14X,1HP,14X,1HQ,14X,1HR)
ISN 0076 600 FORMAT(1H ,17X,4HUDDOT,11X,4HYDDOT,11X,4HZDDOT,11X,4HPDDOT,11X,
1 4HQDDOT,11X,4HRDDOT)
ISN 0077 900 FORMAT (1H ,16X,6HXACCEL,9X,6HYACCEL,9X,6HZACCEL,
1 9X,6HXACFIL,9X,6HYACFIL,9X,6HZACFIL / )
ISN 0078 NPR = ITTL
ISN 0079 3020 NPR = NPR+IPL
ISN 0080 IF(INRP .LE. 0) GO TO 788
ISN 0082 PRINT 700, I,X(I),Y(I),Z(I),PHI(I),THETA(I),PSI(I)
ISN 0083 PRINT 800, XDOT(I),YDOT(I),ZDOT(I),PHIDOT(I),THETDOT(I),PSIDOT(I)
ISN 0084 PRINT 800, U(I),V(I),W(I),P(I),Q(I),R(I)
ISN 0085 PRINT 800, UDOT(I),VDOT(I),WDOT(I),PDOT(I),QDOT(I),RODOT(I)
ISN 0086 IF(FCUT.EQ.0.) GO TO 1000
ISN 0088 PRINT 800,XACC(I),YACC(I),ZACC(I),XACF(I),YACF(I),ZACF(I)
ISN 0089 GO TO 1010
ISN 0090 1000 PRINT 800, XACC(I),YACC(I),ZACC(I)
ISN 0091 GO TO 1010
ISN 0092 788 IF(FCUT.EQ.0.) GO TO 1001
ISN 0094 PRINT 700,I,XACC(I),YACC(I),ZACC(I),XACF(I),YACF(I),ZACF(I)
ISN 0095 GO TO 1010
ISN 0096 1001 PRINT 700,I, XACC(I),YACC(I),ZACC(I)
ISN 0097 1010 PRINT 800
C
C WRITE MASS POINT DATA ON UNIT 1 FOR SUBSEQUENT USE IN PREPLT
C
ISN 0098 IF(INMEP .EQ. 0) GO TO 7000
ISN 0100 DO 7020 IA=1, NMEP
ISN 0101 IF(1 .NE. JMASS(IA,1)) GO TO 7020
ISN 0103 WRITE(1) TIME,I,X(I),Y(I),Z(I),XDOT(I),YDOT(I),ZDOT(I),U(I),V(I),
* W(I),XACC(I),YACC(I),ZACC(I),XACF(I),YACF(I),ZACF(I),
* PHI(I),THETA(I),PSI(I),P(I),Q(I),R(I),PDOT(I),QDOT(I),
* RODOT(I),XIMP(I),YIMP(I),ZIMP(I)
IF(INPRINT .EQ. 0) NMIEW = NMIEW + 1
GO TO 7000
ISN 0104
ISN 0106

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ISN 0107 7020 CONTINUE
ISN 0108 7000 CONTINUE
C
C PRINT NODE POINT DATA IF THERE IS ANY.
C
IF(NNP.EQ.0) GO TO 3099
DO 4000 JJ=1,NNP
IF(I.NE.INP(JJ)) GO TO 4000
IF(NRP.LE.0) GO TO 2000
NPR = NPR+5
PRINT 701,MNP(JJ),XNP(JJ),YNP(JJ),ZNP(JJ)
PRINT 800,XDNP(JJ),YDNP(JJ),ZDNP(JJ)
PRINT 800,UNP(JJ),VNP(JJ),WNP(JJ)
IF(FCUT.EQ.0.) GO TO 1020
PRINT 800,XACNP(JJ),YACNP(JJ),ZACNP(JJ),
1 XACNP(JJ),YACNP(JJ),ZACNP(JJ)
GO TO 1030
1020 PRINT 800,XACNP(JJ),YACNP(JJ),ZACNP(JJ)
GO TO 1030
2000 NPR = NPR + 2
IF(FCUT.EQ.0.0) GO TO 2001
PRINT 701,MNP(JJ),XACNP(JJ),YACNP(JJ),ZACNP(JJ),
1 XACNP(JJ),YACNP(JJ),ZACNP(JJ)
GO TO 1030
2001 PRINT 701,MNP(JJ),XACNP(JJ),YACNP(JJ),ZACNP(JJ)
1030 PRINT 800
C
C WRITE NODE POINT DATA ON UNIT 2 FOR SUBSEQUENT USE IN PREPLT
C
IF(NNEP.EQ.0) GO TO 7001
IMNP = MNP(JJ)
DO 7030 IA=1, NNEP
IF(I.NE.JNODE(IA,2).OR. IMNP.NE. JNODE(IA,1)) GO TO 7030
WRITE(2) TIME,I,IMNP,XNP(JJ),YNP(JJ),ZNP(JJ),XDNP(JJ),
* YDNP(JJ),ZDNP(JJ),UNP(JJ),VNP(JJ),WNP(JJ),XACNP(JJ),
* YACNP(JJ),ZACNP(JJ),XACNP(JJ),YACNP(JJ),ZACNP(JJ),
* XIMPNP(JJ),YIMPNP(JJ),ZIMPNP(JJ)
IF(NPRINT.EQ.0) NNEW = NNEW + 1
GO TO 7001
7030 CONTINUE
7001 CONTINUE
4000 CONTINUE
701 FORMAT(4X,'NODE',I2,IP6E15.5)
700 FORMAT(11H,5HMASS,I2,2X,IP6E15.5)
800 FORMAT(11H,9X,IP6E15.5)
3099 CONTINUE
IF(NIMP.GT.0) PRINT 3215
IF(NIMP.LE.0) PRINT 3216
3215 FORMAT(1X,'MASS IMPULSES(G-SEC)-BASED ON FILTERED ACCELS'//
1 16X,8HYIMPULSE,7X,8HYIMPULSE,7X,8HZIMPULSE/)
3216 FORMAT (//1X,'NO MASS IMPULSE DATA REQUESTED'//
1 16X,8HYIMPULSE,7X,8HYIMPULSE,7X,8HZIMPULSE/)
DO 3097 I=1,NM

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ISN 0159 PRINT 700,I,XIMP(I),YIMP(I),ZIMP(I)
ISN 0160 IF(INP.EQ.0) GO TO 3096
ISN 0162 DO 30% JJ=1,NNP
ISN 0163 IF(I.NE.INP(JJ)) GO TO 3096
ISN 0165 NPR=NPR+2
ISN 0166 PRINT 701,MNP(JJ),XIMP(JJ),YIMP(JJ),ZIMP(JJ)
ISN 0167 3096 CONTINUE
ISN 0168 3097 CONTINUE
ISN 0169 3098 CONTINUE
ISN 0170 PRINT 3202
ISN 0171 3202 FORMAT(1X,'BEAM FORCES' /)
ISN 0172 C NSF=OR< 0 NO STRAIN FORCE PRINT
ISN 0173 IF(NSF=0) 3208,3208,3223
ISN 0174 3223 PRINT 3203
ISN 0175 3203 FORMAT(1X,'STRAIN FORCES' /)
ISN 0176 PRINT 830
ISN 0177 830 FORMAT(4X,'I',3X,'J',3X,'M',3X,'N',7X,'FX',11X,'FY',11X,'FZ',11X,
      1 'MX',11X,'MY',10X,'MZ',10X,'MZX',10X,'MZY')
      1 PRINT 810,(IG(IJ),JG(IJ),MG(IJ),NG(IJ)),(SUMDF(K,IJ),K=1,4),
      1 SUMDF(5,IJ),SUMDF(6,IJ),SUMDF(6,IJ),I,J=1,NB)
      1 SUMDF(5,IJ),SUMDF(6,IJ),SUMDF(6,IJ),I,J=1,NB)
C
C 1 NSF=OR<0 NO TOTAL FORCE PRINT
C GO TO 3250
ISN 0178 3208 PRINT 850
ISN 0179 850 FORMAT(/ 1X,'NO STRAIN FORCE PRINT')
ISN 0180 3250 IF(INF=0)3209,3209,3224
ISN 0181 3224 PRINT 3204
ISN 0182 3204 FORMAT(/ 1X,'TOTAL FORCES (STRAIN+DAMPING)' /)
ISN 0183 PRINT 830
ISN 0184 830 PRINT 810,(IG(IJ),JG(IJ),MG(IJ),NG(IJ)),(FINT(K,IJ),K=1,4),
ISN 0185 1 FINT(5,IJ),FINT(5,IJ),FINT(6,IJ),FINT(6,IJ),I,J=1,NB)
      1 GO TO 3251
ISN 0186 3209 PRINT 851
ISN 0187 851 FORMAT(/ 1X,'NO TOTAL FORCE PRINT')
ISN 0188 3251 CONTINUE
ISN 0189 C
C
C WRITE BEAM FORCE DATA ON UNIT 3 FOR SUBSEQUENT USE IN PREPLT
C
C IF(NBFP.EQ.0) GO TO 7002
ISN 0190 DO 7006 IJ=1, NB
ISN 0192 DO 7040 IA=1, NBFP
ISN 0193 IF(IJ.NE.JBHF(IA,1)) GO TO 7040
ISN 0194 IIG = IG(IJ)
ISN 0196 IJG = JG(IJ)
ISN 0197 IMG = MG(IJ)
ISN 0198 ING = NG(IJ)
ISN 0199 WRITE(3) TIME,IJ,IIG,IJG,IMG,ING,(FINT(K,IJ),K=1,4),FINT(5,IJ),
ISN 0200 * FINT(5,IJ),FINT(6,IJ),FINT(6,IJ)
      1 IF(INP.EQ.0) NBFW = NBFW + 1
      1 GO TO 7006
ISN 0201 7040 CONTINUE
ISN 0203 7006 CONTINUE
ISN 0204 7002 CONTINUE
ISN 0205 IF(INDE - 0) 3210,3210,3225
ISN 0207

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C       NDE=OR<0 NO DEFL.PRINT
3225 PRINT 3205
3205 FORMAT(/ / 1X, 'BEAM RELATIVE DEFLECTIONS AND ROTATIONS AND',
      1      ' BEAM EULER ANGLES (INCHES AND DEGREES)')
      PRINT 3301
3301 FORMAT(/ 5X, 'BEAM', 16X, 'DEFLECTIONS (J-I)', 23X, 'ROTATIONS (J-I)',
      1      16X, 'ROTATIONS (J+I)', 7X, 'EULER ANGLES')
      PRINT 3302
3302 FORMAT(/ 3X, 'I', 2X, 'J', 2X, 'M', 2X, 'N', 7X, 'X', 12X, 'Y', 12X, 'Z',
      1      11X, 'PHI', 9X, 'THETA', 9X, 'PSI', 9X, 'THETA', 9X, 'PSI', 7X,
      2      'THETA', 3X, 'PSI')
      DO 3303 IJ=1,NB
      RADEG = 180./3.1415926535
      DO 3304 K=1,3
      TEMPIK = RADEG*VEE2(K+3,IJ)
      IF(K.GT.2) GO TO 3304
      TEMPIK+3 = RADEG*VEEN(K,IJ)
      CONTINUE
      TEMPI6 = RADEG*THEI(IJ)
      TEMPI7 = RADEG*PSII(IJ)
      PRINT 3305,IG(IJ),JG(IJ),MG(IJ),NG(IJ),(VEE2(K,IJ),K=1,3),
      1      (TEMP(K),K=1,7)
      3305 FORMAT(1X,4I3,1P8E13.4,1X,OP2F7.1)
      3303 CONTINUE
      810 FORMAT (1X,4I4,1P8E13.4)
      GO TO 3252
3210 PRINT 852
      852 FORMAT(/ 1X, 'NO BEAM DEFL.PRINT')
      3252 CONTINUE
C
C       WRITE BEAM DEFLECTION DATA ON UNIT 4 FOR SUBSEQUENT USE IN PREPLT
C
      IF(NBOP.EQ.0) GO TO 7003
      GRADEG = 180.0 / 3.1415926535
      DO 7008 IJ=1, NB
      DO 7050 IA=1, NBOP
      IF(IJ.NE.JBND(IA,1)) GO TO 7050
      DO 7010 K=1, 3
      TEMPIK = RADEG * VEE2(K+3,IJ)
      IF(K.GT.2) GO TO 7010
      TEMPIK+3 = RADEG * VEEN(K,IJ)
      CONTINUE
      7010 TEMPI6 = RADEG * THEI(IJ)
      TEMPI7 = RADEG * PSII(IJ)
      IIG = IG(IJ)
      IJG = JG(IJ)
      IMG = MG(IJ)
      ING = NG(IJ)
      WRITE(4) TIME,IJ,IIG,IJG,IMG,ING,(VEE2(K,IJ),K=1,3),
      *      (TEMP(K),K=1,5)
      IF(NPRINT.EQ.0) NBDM = NBDM + 1
      GO TO 7008
      7050 CONTINUE

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ISN 0256 7008 CONTINUE
ISN 0257 7003 CONTINUE
ISN 0258 IF(NSPD - 0) 3211,3211,3226
C NSPD=OR<0 NO EXT SPRING PRINT
ISN 0259 3226 PRINT 3206
ISN 0260 3206 FORMAT(/ / 1X,'EXTERNAL SPRINGS' /
1 57X,'GROUND CONTACT POINT LOADS',13X,'GROUND CONTACT POINT LOADS',
2 / 59X,'IN GROUND OR SLOPE AXES',21X,'IN MASS AXES' /
3 41X,'SPRING' / 1X,'MASS SPRING SPRING',8X,'GROUND',4X,
4 'COMPRESSION',2X,'X(+ AFT OR',4X,'Y(+ LEFT) Z(+ UP OR NOR-',6X,
5 'X',13X,'Y',12X,'Z' / 3X,'I K M COMPRESSION',3X,
6 'DEFLECTION',5X,
7 'LOAD',6X,'DOWN SLOPE',13X,'MAL TO SLOPE',2X,'(+ FORWARD)',
8 3X,'(+ RIGHT)',5X,'(+ DOWN)' /)
GO TO 3228
ISN 0261 3211 PRINT 853
ISN 0262 853 FORMAT(/ 1X,'NO EXTERNAL SPRING PRINT')
ISN 0263 GO TO 3227
ISN 0264 3228 DO 3040 IKM=1,NSP
ISN 0265 SCNET = SC(IKM)-DELG(IKM)
ISN 0266 PRINT 820,II(IKM),KK(IKM),MM(IKM),SCNET,DELG(IKM),
ISN 0267 1 (FSPRG(IKM,J),J=1,7)
ISN 0268 820 FORMAT(1X,3I3,1P9E13.5)
ISN 0269 3040 CONTINUE
ISN 0270 3227 CONTINUE
C
C WRITE EXTERNAL SPRING DATA ON UNIT 8 FOR SUBSEQUENT USE IN PREPLT
C
ISN 0271 IF(NSPD .EQ. 0) GO TO 7004
ISN 0272 DO 7060 IA=1, NSEP
ISN 0273 DO 7009 IKM=1, NSP
ISN 0274 IF(II(IKM) .NE. JSPP(IA,1) .OR. MM(IKM) .NE. JSPP(IA,2))
ISN 0275 * GO TO 7009
ISN 0276 * III = II(IKM)
ISN 0277 IKK = KK(IKM)
ISN 0278 IMM = MM(IKM)
ISN 0279 WRITE(8) TIME,III,IKK,IMM,SC(IKM),FSPRG(IKM,1)
ISN 0280 IF(NPRINT .EQ. 0) NSEW = NSEW + 1
ISN 0281 7009 CONTINUE
ISN 0282 7060 CONTINUE
ISN 0283 7004 CONTINUE
ISN 0284 IF(INDRI .EQ. 0) GO TO 3076
ISN 0285 PRINT 3207
ISN 0286 3207 FORMAT(/ 1X,'DRI RESULTS: MASS NO. AND DRI VALUE')
ISN 0287 PRINT 821
ISN 0288 821 FORMAT(1X // 1X,'MASS',7X,'DRI')
ISN 0289 DO 3070 I = 1,NB
ISN 0290 IF(IJPR(I).EQ.0) GO TO 3070
ISN 0291 3065 PRINT 822, JG(I),DRI(I)
ISN 0292 C
ISN 0293 C WRITE BEAM DRI DATA ON UNIT 9 FOR SUBSEQUENT USE IN PREPLT
ISN 0294 C
ISN 0295 IF(INDRP .EQ. 0) GO TO 7005
ISN 0296

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ISN 0298      IJG = JG(I)
ISN 0299      DO 7070 IA=1, NORP
ISN 0300      IF(IJG.NE. JDR(I,IA)) GO TO 7070
ISN 0301      WRITE(9) TIME,IJG,DRI(I)
ISN 0302      IF(NPRINT.EQ. 0) NORM = NORM + 1
ISN 0303      GO TO 7005
ISN 0304      7070 CONTINUE
ISN 0305      7005 CONTINUE
ISN 0306      3070 CONTINUE
ISN 0307      3076 PRINT 3075,XDOTAP,YDOTAP,ZDOTAP
ISN 0308      3075 FORMAT(/ 1X,'VEHICLE C.G. TRANSLATIONAL VELOCITIES, GROUND AXES, B00003690
ISN 0309      1X,'BASED ON SYSTEM LINEAR MOMENTUM' // 11X,'XDOT',10X,'YDOT',12X,'ZDOT00003700
ISN 0310      2' / 10X,'(+FWD)',7X,'(+RIGHT)',8X,'(+DOWN)', / 4X,1P3E15.5)
ISN 0311      C
ISN 0312      C
ISN 0313      C
ISN 0314      C
ISN 0315      C
ISN 0316      C
ISN 0317      C
ISN 0318      C
ISN 0319      C
ISN 0320      C
ISN 0321      C
ISN 0322      C
ISN 0323      C
ISN 0324      C
ISN 0325      C
ISN 0326      C
ISN 0327      C
ISN 0328      C
ISN 0329      C
ISN 0330      C
ISN 0331      C
ISN 0332      C
ISN 0333      C
ISN 0334      C
ISN 0335      C
ISN 0336      C
ISN 0337      C
ISN 0338      C
ISN 0339      C
ISN 0340      C
ISN 0341      C
ISN 0342      C
ISN 0343      C
ISN 0344      C

ISN 0311      WRITE(10) TIME,XDOTAP,YDOTAP,ZDOTAP
ISN 0312      IF(NVCH.LE. 0) GO TO 3074
ISN 0313      PRINT 3071
ISN 0314      3071 FORMAT(/ 1X,'VOLUME CHANGE DATA' // 48X,'VOLUME LENGTH CHANGES'
ISN 0315      1/ 1X,'VOL. NO.',5X,'VOL.',8X,'VOL./VZERO',8X,'DX',13X,'DY',13X,
ISN 0316      2'02' //)
ISN 0317      DO 3073 I=1,NVCH
ISN 0318      VOV = VOL(I)/VZERO(I)
ISN 0319      PRINT 3072,I,VOL(I),VOV,(DLVOL(I,J),J=1,3)
ISN 0320      3073 CONTINUE
ISN 0321      3072 FORMAT(1X,I6,1P5E15.5)
ISN 0322      822 FORMAT(1H,1X,I2,3X,1P5E15.5)
ISN 0323      3074 SUMPEI = 0.0
ISN 0324      SUMPEI = 0.0
ISN 0325      SUMPEI = 0.0
ISN 0326      SUMPEI = 0.0
ISN 0327      SUMPEI = 0.0
ISN 0328      DO 3400 I = 1,NM
ISN 0329      SUMPEI = SUMPEI+PEI(I)
ISN 0330      SUMPEI = SUMPEI+KEI(I)
ISN 0331      3400 CONTINUE
ISN 0332      DO 3406 IJ = 1,NB
ISN 0333      SUMSEI = SUMSEI+SEI(IJ)
ISN 0334      SUMDEI = SUMDEI+DEI(IJ)
ISN 0335      3406 WRITE BEAM STRAIN&DAMPING ENERGY DATA ON UNIT 11 FOR USE IN PREPLT00004020
ISN 0336      DO 7200 IJ=1,NB
ISN 0337      IF(TIME.EQ.0.) GO TO 9003
ISN 0338      PCSE=(SEI(IJ)/SUMSEI)*100.
ISN 0339      PCDE=(DEI(IJ)/SUMDEI)*100.
ISN 0340      GO TO 9004
ISN 0341      9003 SEI(IJ)=0.
ISN 0342      DEI(IJ)=0.
ISN 0343      PCSE=0.
ISN 0344      PCDE=0.

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ISN 0345 9004 DO 7201 IA=1,NENP
ISN 0346 IF(IJ.NE.JENG(IA,1)) GO TO 7201
ISN 0348 IIG=IG(IJ)
ISN 0349 IJG=JG(IJ)
ISN 0350 IJG=MG(IJ)
ISN 0351 IJG=NG(IJ)
ISN 0352 WRITE(11) TIME,IJ,IIG,IMG,IJG,ING,SEIJ(IJ),PCSE,DEIJ(IJ),PCDE
ISN 0353 IF(NPRINT.EQ.0) NENP=NENP+1
ISN 0355 GO TO 7200
ISN 0356 7201 CONTINUE
ISN 0357 7200 CONTINUE
ISN 0358 IF(NSP.EQ.0) GO TO 3409
ISN 0360 DO 3407 IKM=1,NSP
ISN 0361 SUMFEI = SUMFEI+CEIKF(IKM)
ISN 0362 SUMFCEI = SUMFCEI+CEIK(IKM)
ISN 0363 3407 SUMFCEI = SUMFEI+SUMFEI+SUMFCEI+SUMFCEI+SUMFEI
ISN 0364 3409 ETOT = SUMFEI+SUMFEI+SUMFEI+SUMFEI+SUMFEI+SUMFEI
ISN 0366 IF(TIME.EQ.0.0) ETOTOT = ETOT
ISN 0367 ETOTR=ETOT/ETOTOT
ISN 0368 XTOLL=NTOLL/100.
ISN 0370 IF((DABS(ETOTR)-1.).LE. XTOLL) GO TO 3770
ISN 0371 IEER=1
ISN 0372 IETOT=1
ISN 0373 3770 IF(INGSCCT.EQ.200) GO TO 3414
ISN 0374 INGSCCT = INGSCCT+1
ISN 0375 ETIME(INGSCCT) = TIME
ISN 0376 DEV(INGSCCT) = DEVMAX
ISN 0377 ENGSHY(1,INGSCCT) = SUMFEI
ISN 0378 ENGSHY(2,INGSCCT) = SUMFEI
ISN 0379 ENGSHY(3,INGSCCT) = SUMFEI
ISN 0380 ENGSHY(4,INGSCCT) = SUMFEI
ISN 0381 ENGSHY(5,INGSCCT) = SUMFEI
ISN 0382 ENGSHY(6,INGSCCT) = SUMFEI
ISN 0383 3414 CONTINUE
ISN 0384 PRINT 3405
ISN 0385 3405 FORMAT(// 1X,'ENERGY DISTRIBUTION' //)
ISN 0386 3401 PRINT 3401
ISN 0387 3401 FORMAT(1H0,6X,'TOTAL',7X,'KINETIC',6X,'POTENTIAL',7X,'STRAIN',7X,
1 'DAMPING',7X,'CRUSHING',6X,'FRICTION' / 6X,'ENERGY',
2 6(8X,'ENERGY') /)
ISN 0388 PRINT 3402, ETOT,SUMFEI,SUMFEI,SUMFEI,SUMFEI,SUMFEI,SUMFEI
ISN 0389 3402 FORMAT(1X,1P7E14.5)
ISN 0390 PCKE = SUMFEI/ETOT
ISN 0391 PCPE = SUMFEI/ETOT
ISN 0392 PCSE = SUMFEI/ETOT
ISN 0393 PCDE = SUMFEI/ETOT
ISN 0394 PCCE = SUMFEI/ETOT
ISN 0395 PCFE = SUMFEI/ETOT
ISN 0396 PRINT 3403, PCKE,PCPE,PCSE,PCDE,PCCE,PCFE
ISN 0397 3403 FORMAT(10 PERCENT OF',2P6F14.3/3X,'TOTAL ENERGY')
ISN 0398 IF(NED=0) 3601,3601,3229
C NED=<0. NO INDIVIDUAL ENERGY TERMS PRINTED
ISN 0399 3229 PRINT 3404
ISN 0400 3404 FORMAT(// 43X,'INTERNAL',38X,'EXTERNAL' /

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ISN 0401      1 45X,'BEAM',41X,'SPRING' / 7X,'KINETIC',9X,
ISN 0402      2 'POTENTIAL',25X,'STRAIN',11X,'DAMPING',17X,'CRUSHING',9X,
ISN 0403      3 'FRICTION' / 1X,'MASS',2X,'ENERGY',5X,'PCT',3X,'ENERGY',5X,
ISN 0404      4 'PCT',2X,'I',2X,'J',2X,'M',2X,'N',3X,'ENERGY',5X,'PCT',
ISN 0405      5 3X,'ENERGY',5X,'PCT',3X,'I',1X,'K',1X,'M',3X,'ENERGY',5X,'PCT',
ISN 0406      6 3X,'ENERGY',5X,'PCT' /
ISN 0407      3601 XTOL2=NTOL2/100.
ISN 0408      XTOL3=NTOL3
ISN 0409      MAXEN = MAX0(NM,NB,NSP)
ISN 0410      IF(TIME.EQ.0.0) MAXEN = NM
ISN 0411      DO 3410 IO = 1,MAXEN
ISN 0412      IOPTR = 0
ISN 0413      IF(10.GT.NM) GO TO 3411
ISN 0414      IOPTR = IOPTR+4
ISN 0415      IF(SUMKEI.NE.0.) GO TO 5000
ISN 0416      PCKE = 0.
ISN 0417      GO TO 5001
ISN 0418      5000 PCKE = KEI(IO)/SUMKEI
ISN 0419      5001 IF(SUMPEI.NE.0.) GO TO 5002
ISN 0420      PCPE = 0.
ISN 0421      GO TO 5003
ISN 0422      5002 PCPE = PEI(IO)/SUMPEI
ISN 0423      5003 IF(TIME.EQ.0.0) GO TO 3504
ISN 0424      3411 IF(10.GT.NB) GO TO 3412
ISN 0425      IOPTR = IOPTR+2
ISN 0426      IF (SUMSEI.EQ.0) GO TO 3415
ISN 0427      PCSE = SEI(IO)/SUMSEI
ISN 0428      IF(SUMSEI.GE.0.) GO TO 3700
ISN 0429      IESE=1
ISN 0430      IEER=1
ISN 0431      3700 IF(SEI(IO).GE.0. .OR. DABS(SEI(IO)).LE.DABS(SUMSEI*XTOL2))
ISN 0432      1 GO TO 3710
ISN 0433      IEPSE=1
ISN 0434      IEER=1
ISN 0435      3710 GO TO 3416
ISN 0436      3415 PCSE = 0.
ISN 0437      3416 IF (SUMDEI.EQ.0.) GO TO 3417
ISN 0438      PCDE = DEI(IO)/SUMDEI
ISN 0439      IF(SUMDEI.GE.0.) GO TO 3720
ISN 0440      IEDE=1
ISN 0441      IEER=1
ISN 0442      3720 IF(DEI(IO).GE.0. .OR. DABS(DEI(IO)).LE.DABS(SUMDEI*XTOL2))
ISN 0443      1 GO TO 3730
ISN 0444      IEPDE=1
ISN 0445      IEER=1
ISN 0446      3730 GO TO 3412
ISN 0447      3417 PCDE = 0.
ISN 0448      3412 IF(10.GT.NSP) GO TO 3418
ISN 0449      IOPTR = IOPTR+1
ISN 0450      I = I1(IO)
ISN 0451      K = KK(IO)
ISN 0452      M = MM(IO)
ISN 0453      CE = CEIK(IO)
ISN 0454      00004650
ISN 0455      00004660
ISN 0456      00004670
ISN 0457      00004680
ISN 0458      00004690
ISN 0459      00004700
ISN 0460      00004710
ISN 0461      00004720
ISN 0462      00004730
ISN 0463      00004740
ISN 0464      00004750
ISN 0465      00004760
ISN 0466      00004770
ISN 0467      00004780
ISN 0468      00004790
ISN 0469      00004800
ISN 0470      00004810
ISN 0471      00004820
ISN 0472      00004830
ISN 0473      00004840
ISN 0474      00004850
ISN 0475      00004860
ISN 0476      00004870
ISN 0477      00004880
ISN 0478      00004890
ISN 0479      00004900
ISN 0480      00004910
ISN 0481      00004920
ISN 0482      00004930
ISN 0483      00004940
ISN 0484      00004950
ISN 0485      00004960
ISN 0486      00004970
ISN 0487      00004980
ISN 0488      00004990
ISN 0489      00005000
ISN 0490      00005010
ISN 0491      00005020
ISN 0492      00005030
ISN 0493      00005040
ISN 0494      00005050
ISN 0495      00005060
ISN 0496      00005070
ISN 0497      00005080
ISN 0498      00005090
ISN 0499      00005100
ISN 0500      00005110
ISN 0501      00005120
ISN 0502      00005130
ISN 0503      00005140
ISN 0504      00005150
ISN 0505      00005160
ISN 0506      00005170

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ISN 0459 IF(SUMCEI.NE.0.) GC TO 5010
ISN 0461 PCCE = 0.
ISN 0462 GO TO 5011
ISN 0463 5010 PCCE = CE/SUMCEI
ISN 0464 IF(SUMCEI.GE.0.) GO TO 3740
ISN 0466 IECE=1
ISN 0467 IEER=1
ISN 0468 3740 IF(CEIKF(IO).GE.0. .OR. DABS(CEIKF(IO)).LE.DABS(SUMCEI*XTOL2))
      1 GO TO 5011
      IEPCE=1
ISN 0470 IEER=1
ISN 0471 5011 FE = CEIKF(IO)
ISN 0472 IF(SUMFEI.NE.0.) GO TO 5012
ISN 0473 PCFE = 0.
ISN 0475 GO TO 3418
ISN 0476 5012 PCFE = FE/SUMFEI
ISN 0477 IF(SUMFEI.GE.0.) GO TO 3750
ISN 0478 IEFE=1
ISN 0480 IEER=1
ISN 0481 3750 IF(CEIKF(IO).GE.0. .OR. DABS(CEIKF(IO)).LE.DABS(SUMFEI*XTOL2))
      1 GO TO 3418
      IEPFE=1
ISN 0484 IEER=1
ISN 0485 3418 IF(NED=0) 3410,3410,3413
ISN 0486 3413 GO TO (3501,3502,3503,3504,3505,3506,3507), IOPTR
ISN 0487 C*****ONLY CE
ISN 0488 3501 PRINT 3511,I,K,M,CE,PCCE,FE,PCFE
ISN 0489 3511 FORMAT(8X,I4,2I2,1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0490 GO TO 3410
ISN 0491 C*****SE AND DE
ISN 0492 3502 PRINT 3512,IO,IG(IO),JG(IO),MG(IO),NG(IO),SEIJ(IO),PCSE,DEIJ(IO),
      1 PCDE
ISN 0493 3512 FORMAT(39X,5I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0494 C*****SE, DE, CE
ISN 0495 3503 PRINT 3513,IO,IG(IO),JG(IO),MG(IO),NG(IO),
      1 SEIJ(IO),PCSE,DEIJ(IO),PCDE,I,K,M,CE,
      2 PCCE,FE,PCFE
ISN 0496 3513 FORMAT(39X,5I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1,I4,2I2,1PE11.3,
      1 2PF6.1,1PE11.3,2PF6.1)
ISN 0497 GO TO 3410
ISN 0498 C*****KE AND PE
ISN 0499 3504 PRINT 3514,IO,KEI(IO),PCKE,PEI(IO),PCPE
ISN 0500 3514 FORMAT(1X,I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0501 GO TO 3410
ISN 0502 C*****KE, PE, CE
ISN 0503 3505 PRINT 3515,IO,KEI(IO),PCKE,PEI(IO),PCPE,I,K,M,CE,PCCE,FE,PCFE
ISN 0504 3515 FORMAT(1X,I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1,50X,I4,2I2,
      1 1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0505 GO TO 3410
ISN 0506 C*****KE, PE, SE, DE
ISN 0507 3506 PRINT 3516,IO,KEI(IO),PCKE,PEI(IO),PCPE,IO,IG(IO),JG(IO),
      1 MG(IO),NG(IO),SEIJ(IO),

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ISN 0504      2 PCSE,DEL(I,IO),PCDE
ISN 0505      3516 FORMAT(1X,I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1,1X,5I3,
ISN 0506      1 1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0507      GO TO 3410
ISN 0508      C*****KE, PE, SE, DE, CE
ISN 0509      3507 PRINT 3517,IO,KEI(IO),PCKE,PEI(IO),PCPE,IO,IG(IO),JG(IO),
ISN 0510      1 NG(IO),NG(IO),SEIJ(IO),
ISN 0511      2 PCSE,DEL(I,IO),PCDE,I,K,M,CE,PCCE,FE,PCFE
ISN 0512      3517 FORMAT(1X,I3,1PE11.3,2PF6.1,1PE11.3,2PF6.1,1X,5I3,1PE11.3,2PF6.1,
ISN 0513      1 1PE11.3,2PF6.1,1X,2I2,1PE11.3,2PF6.1,1PE11.3,2PF6.1)
ISN 0514      3410 CONTINUE
ISN 0515      PRINT 8000
ISN 0516      8000 FORMAT(// 1X,'DEVIATION OF TOTAL ENERGY OF EACH MASS FROM ',
ISN 0517      1 '100 PERCENT')
ISN 0518      PRINT 8002
ISN 0519      8002 FORMAT(// 1X,'MASS',2X,'DEVIATION(PERCENT)' /)
ISN 0520      DO 8004 I=1,NM
ISN 0521      DEVIAT = XPC(I)-100.
ISN 0522      IF(ABS(DEVIAT).LE.XTOL3) GO TO 3760
ISN 0523      IEDEV=1
ISN 0524      IEER=1
ISN 0525      3760 IF(XPC(I).EQ.0) DEVIAT=0.
ISN 0526      PRINT 8006,I,DEVIAT
ISN 0527      8004 CONTINUE
ISN 0528      8006 FORMAT(1X,I3,4X,F12.6)
ISN 0529      IF(NEED-0) 3212,3212,3602
ISN 0530      3602 GO TO 3230
ISN 0531      3212 PRINT 854
ISN 0532      854 FORMAT (/ 1X,'NO ENERGY TERMS PRINTED')
ISN 0533      3230 IF(NS-0) 3213,3213,3231
ISN 0534      3231 PRINT 3510
ISN 0535      C NS EQ OR LESS THAN 0 NO STRESSES ARE PRINTED
ISN 0536      3510 FORMAT(// 1X,'ELEMENT STRESSES')
ISN 0537      PRINT 3519
ISN 0538      3519 FORMAT(// 39X,'RATIO OF CURRENT STRESS / FAILURE STRESS',31X,
ISN 0539      1 'RATIO OF CURRENT' / 8X,'BEAM',12X,'MAXIMUM SHEAR STRESS THEORY',00006060
ISN 0540      * 9X,'THEORY OF CONSTANT ENERGY OF DISTORTION',6X,'AXIAL/FAILURE',
ISN 0541      * 5X,'BUCK.' / 2X,'I',2X,'J',2X,'M',2X,'N',5X,'TOP',5X,
ISN 0542      * 'BOTTOM',6X,'LEFT',5X,'RIGHT',8X,'TOP',5X,'BOTTOM',8X,'LEFT',5X,
ISN 0543      * 'RIGHT',7X,'COMPR. TENSILE CR.BUCK.' / 104X,'STRESS STRESS'
ISN 0544      * ,6X,'LOAD' /)
ISN 0545      DO 3520 IJ=1,NB
ISN 0546      I = IG(IJ)
ISN 0547      J = JG(IJ)
ISN 0548      M = MG(IJ)
ISN 0549      N = NG(IJ)
ISN 0550      IF(SBUCKR(IJ).GT. 0.0) GO TO 3521
ISN 0551      BLOAD = DABS(SBUCKR(IJ))
ISN 0552      IF(AA(IJ).EQ. 0.0) GO TO 3525
ISN 0553      SAXL = BLOAD * PCR(IJ) / (AA(IJ) * SCOMP(MC(IJ)))
ISN 0554      GO TO 3526
ISN 0555      3525 SAXL = 0.0
ISN 0556      3526 PRINT 3518, IJ,I,J,M,N,(FRS(IJ,IS),IS=1,4),(FRD(IJ,IT),IT=1,4),

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ISN 0547      *
ISN 0548      SAXL,BLOAD
ISN 0549      3518 FORMAT(IX,5I3,IX,IP4E10.3,2X,4E10.3,2X,E10.3,10X,E10.3)
ISN 0550      GO TO 3520
ISN 0551      3521 CONTINUE
ISN 0552      BLOAD = 0.0
ISN 0553      IF(AA(IJ).EQ.0.0) GO TO 3522
ISN 0554      SAXL = SBUCKR(IJ) * PCR(IJ) / (STENS(MC(IJ)) * AA(IJ))
ISN 0555      GO TO 3523
ISN 0556      3522 SBUCK = 0.0
ISN 0557      3523 PRINT 3524, IJ,I,J,M,N,(FRS(IJ,IS),IS=1,4),(FRD(IJ,IT),IT=1,4),
ISN 0558      *
ISN 0559      3524 FORMAT(IX,5I3,IX,IP4E10.3,2X,4E10.3,12X,E10.3)
ISN 0560      3520 CONTINUE
ISN 0561      GO TO 3232
ISN 0562      3213 PRINT 855
ISN 0563      855 FORMAT(/ IX,'NO STRESS PRINT')
ISN 0564      C
ISN 0565      C
ISN 0566      C
ISN 0567      C
ISN 0568      C
ISN 0569      C
ISN 0570      C
ISN 0571      C
ISN 0572      C
ISN 0573      C
ISN 0574      C
ISN 0575      C
ISN 0576      C
ISN 0577      C
ISN 0578      C
ISN 0579      C
ISN 0580      C
ISN 0581      C
ISN 0582      C
ISN 0583      C
ISN 0584      C
ISN 0585      C
ISN 0586      C
ISN 0587      C
ISN 0588      C
ISN 0589      C
ISN 0590      C
ISN 0591      C
ISN 0592      C
ISN 0593      C
ISN 0594      C
ISN 0595      C
ISN 0596      C
ISN 0597      C
ISN 0598      C
ISN 0599      C
ISN 0600      C
ISN 0601      C

3232 IF(NSTP.EQ.0) GO TO 7100
DO 7110 IJ=1, NB
DO 7080 IA=1, NSTP
IF(IJ.NE.JBNS(IA,1)) GO TO 7080
I = IG(IJ)
J = JG(IJ)
M = MG(IJ)
N = NG(IJ)
BLOAD = SBUCKR(IJ)
IF(BLOAD.GT.0.0) BLOAD = 0.0
IF(AA(IJ).EQ.0.0) GO TO 3527
IF(SBUCKR(IJ).GT.0.0) GO TO 3528
SAXL = SBUCKR(IJ) * PCR(IJ) / (AA(IJ) * SCOMP(MC(IJ)))
GO TO 3529
3528 SAXL = SBUCKR(IJ) * PCR(IJ) / (AA(IJ) * STENS(MC(IJ)))
GO TO 3529
3527 SAXL = 0.0
3529 CONTINUE
*
WRITE(13) TIME,IJ,I,J,M,N,(FRS(IJ,IS),IS=1,4),
(FRD(IJ,IT),IT=1,4),SAXL,BLOAD
*
IF(NPRINT.EQ.0) NSTW = NSTW + 1
GO TO 7110
7080 CONTINUE
7110 CONTINUE
7100 CONTINUE
IF(NPLT.EQ.0) GO TO 100
IPFCT = IPFCT + 1
IF(IPFCT.EQ.0 .OR. IPFCT.EQ.NPFCT) GO TO 170
GO TO 100
170 CONTINUE
IPFCT = 0
DO 110 IP=1,NPLT
NJ=NPTS(IP)

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ISN 0602      DO 160 IJ=1,NJ
ISN 0603      DO 120 IM=1,NM
ISN 0604      IFIM.NE. MNUM(IJ,IP)) 60 TO 120
ISN 0606      J=ITPL(IP)
ISN 0607      GO TO (130,140,150),J
ISN 0608      130 A(IJ)=-X(IM)
ISN 0609      B(IJ)=Y(IM)
ISN 0610      IFIRST = 1
ISN 0611      ILAST = 5
ISN 0612      GO TO 160
ISN 0613      140 A(IJ)=-X(IM)
ISN 0614      B(IJ) = -Z(IM)
ISN 0615      IFIRST = 6
ISN 0616      ILAST = 10
ISN 0617      GO TO 160
ISN 0618      150 A(IJ)=Y(IM)
ISN 0619      B(IJ) = -Z(IM)
ISN 0620      IFIRST = 11
ISN 0621      ILAST = 15
ISN 0622      GO TO 160
ISN 0623      120 CONTINUE
ISN 0624      160 CONTINUE
ISN 0625      PRINT 7120, (IPLN(IJ), IJ=IFIRST, ILAST)
ISN 0626      7120 FORMAT(1H1,51X,'MASS POSITION PLOT PLANE ** ',5A4 / 20X,
* 'NOTE *** A MODIFIED RIGHT HAND GROUND COORDINATE',
* ' SYSTEM HAS BEEN USED FOR THIS PLOT ***' / )
ISN 0627      PRINT 7130
ISN 0628      7130 FORMAT(47X,'MASS HORIZ VERTICAL' ) /
* 1 4(8X,'NO AXIS ' ) / )
ISN 0629      PRINT 7140, (MNUM(IJ,IP),A(IJ),B(IJ),IJ=1,NJ)
ISN 0630      7140 FORMAT(4(8X,I2,F10.2,F10.2))
ISN 0631      PRINT 7150
ISN 0632      7150 FORMAT(1X)
ISN 0633      IFINJ.LE. 12) 60 TO 180
ISN 0635      PRINT 7120, IPLN(ITPL(IP))
ISN 0636      180 CALL PAPLOT(A,B,XSCALE(IP),YSCALE(IP),MNUM(1,IP),NMPTS(IP),
* ISCALE(IP))
ISN 0637      110 CONTINUE
ISN 0638      PRINT 7160
ISN 0639      7160 FORMAT(1H1,1X)
ISN 0640      100 CONTINUE
ISN 0641      RETURN
ISN 0642      END
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DATE 79.177/14.43.00

OS/360 FORTRAN H

LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.

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      COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
                        SOURCE=BCD,NOLIST,LOAD,MAP,NOEDIT,1D,XREF
      C DATA SET D2334RC AT LEVEL 003 AS OF 06/25/79
      C DATA SET D2332NRC AT LEVEL 004 AS OF 12/01/77
      C DATA SET D2332NRC AT LEVEL 002 AS OF 11/04/77
      C SUBROUTINE RC
      C
      C IMPLICIT REAL*8 (A-H,O-Z)
      C REAL*8 KUN
      C REAL*4 CLTEST
      C INTEGER*4 PY(150),PZ(150),PYJ(150),PZJ(150)
      C INTEGER*4 TITLE(40)
      C INTEGER*2 NI,NN
      C INTEGER*2 INBUFF
      C INTEGER*2 IJPR,IG,JG
      C INTEGER*2 MG(150),NG(150),INP(50),MNP(50)
      C DIMENSION AIDP(3,3)
      C DIMENSION XK3(6,6,150),YZMTNK(150)
      C DIMENSION RX(50),RY(50),XNDP(50),YNDP(50),ZNDP(50)
      C DIMENSION XNP(50),YNP(50),ZNP(50),XONP(50),YONP(50),ZONP(50)
      C DIMENSION UNP(50),VNP(50),WNP(50),XACNP(50),YACNP(50),ZACNP(50)
      C DIMENSION IMDRI(80)
      C COMMON/DEINPR/ AA(150),E(150),YY(150),ZZ(150),XIQ(150),
      1 XIB(150),ZL(150),Z2(150),MC(150),XJ(150),SF26(150),SF35(150),
      2 SF26J(150),SF35J(150),PY,PZ,PYJ,PZJ,NSC,NSC,NPIN
      C COMMON/CFIC/ SINBET,COSBET,ABETA(9)
      C COMMON/DINICP/ STENS(20),SCORP(20),SHEAR(20),EE(20),GG(20),
      1 FINI(6,150),VOL(5),VZERO(5),KHATRI(6,4),NVCH,INBUFF(5,6)
      C COMMON/INIC/ XDP(80),ZDP(80),PHIDP(80),PSIDP(80),
      1 THEDP(80),PPR,QPR,RPR,XGIN,ZGIN,PHIPR,PSIPR,THEPR,
      2 XGDOT,YGDOT,ZGDOT
      C COMMON/INDCP/ YDP(80)
      C COMMON/INCFIC/ BETA
      C COMMON/MCFIJI/ SYHFLG
      C COMMON/NP00I2/ MG,NG,INP,MNP
      C COMMON/NP00I4/ NNP
      C COMMON/NP00R8/ RX,RY,RZ
      C COMMON/NP01R8/ XNP,YNP,ZNP,XNP,MNP,XONP,YONP,ZONP,ZONP,
      1 XACNP,YACNP,ZACNP,SBUCKR(150),PCR(150)
      C COMMON/NP02R8/ XNPDP,YNPDP,ZNPDP
      C COMMON/DEIC/ MTOT,CLTEST(150)
      C COMMON/CORALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),
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1 Y(81),Z(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),
2 YI(80),ZI(80),XZI(80),YZI(80),YI(9),BIJ(720),
3 DRI(150),DAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80),
4 PDOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),
5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
6 XACC(80),YACC(80),ZACC(80),AIDOT(9),
7 PHIJ(150),THEIJ(150),PSIJJ(150),SUMDF(6,150),TITLE,
8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9 DPIN(81),DQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),
A CEIK(40),
B SBARI(40),KUN(40),MAXNM,MAXIGS,MAXTBL,
C NM,NB,I,J,I6(150),J6(150),
D NI(900),NN(40),IJPRI(150)
COTTON/IPIC/ NIC
EQUIVALENCE (XK(1),XK3(1,1,1))
SIN(X) = DSIN(X)
COS(X) = DCOS(X)
SQRT(X) = DSQRT(X)
ARSIN(X) = DARSIN(X)
ATAN2(Y,X) = DATAN2(Y,X)
AMINI(X,Y) = DMINI(X,Y)
WTOT = 0.0
PI = 3.1415926535897932400
PI2 = PI/2.
PIN = -PI
PI2N = -PI2
BETAR = BETAP/180.
SINBET = DSIN(BETAR)
COSBET = DCOS(BETAR)
ABETA(1) = COSBET
ABETA(2) = 0.
ABETA(3) = -SINBET
ABETA(4) = 0.
ABETA(5) = 1.
ABETA(6) = 0.
ABETA(7) = SINBET
ABETA(8) = 0.
ABETA(9) = COSBET
KHATR(1,1) = 3
KHATR(1,2) = 4
KHATR(1,3) = 7
KHATR(1,4) = 8
KHATR(2,1) = 1
KHATR(2,2) = 2
KHATR(2,3) = 5
KHATR(2,4) = 6
KHATR(3,1) = 1
KHATR(3,2) = 3
KHATR(3,3) = 5
KHATR(3,4) = 7
KHATR(4,1) = 2
KHATR(4,2) = 4
KHATR(4,3) = 6

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ISN 0072      KHATR(4,4) = 8
ISN 0073      KHATR(5,1) = 1
ISN 0074      KHATR(5,2) = 2
ISN 0075      KHATR(5,3) = 3
ISN 0076      KHATR(5,4) = 4
ISN 0077      KHATR(6,1) = 5
ISN 0078      KHATR(6,2) = 6
ISN 0079      KHATR(6,3) = 7
ISN 0080      KHATR(6,4) = 8
ISN 0081      PRINT 2001
ISN 0082      2001 FORMAT(1H1 / 1X, 'MODEL PARAMETERS')
ISN 0083      DO 2006 I=1,NM
ISN 0084      IMDRI(I) = 0
ISN 0085      2006 CONTINUE
ISN 0086      DO 2004 IJ=1,NB
ISN 0087      IF(IJPRI(IJ).NE.0) IMDRI(JG(IJ))=1
ISN 0088      2004 CONTINUE
ISN 0089      DO 2010 I = 1,NM
ISN 0090      IF(IMDRI(I).NE.0) GO TO 2010
ISN 0091      MTOT = MTOT+WG(I)
ISN 0092
ISN 0093      C
ISN 0094      C FOR SYMMETRICAL MODEL,ADD CONTRIBUTIONS FROM OTHER SIDE.
ISN 0095      C
ISN 0096      IF(SYMF6.NE.1.OR.YDP(I).EQ.0.) GO TO 2010
ISN 0097      MTOT = MTOT+WG(I)
ISN 0098      2010 CONTINUE
ISN 0099      PRINT 2011,MTOT
ISN 0100      2011 FORMAT(/ 1X, 'VEHICLE WT = ',1PE12.6)
ISN 0101      XGDP = 0.0
ISN 0102      YGDP = 0.0
ISN 0103      ZGDP = 0.0
ISN 0104      DO 2020 I = 1,NM
ISN 0105      IF(IMDRI(I).NE.0) GO TO 2020
ISN 0106      XGDP = XGDP+WG(I)*XDP(I)
ISN 0107      YGDP = YGDP+WG(I)*YDP(I)
ISN 0108      ZGDP = ZGDP+WG(I)*ZDP(I)
ISN 0109      IF(SYMF6.NE.1.OR.YDP(I).EQ.0.) GO TO 2020
ISN 0110      XGDP = XGDP+WG(I)*XDP(I)
ISN 0111      YGDP = YGDP+WG(I)*YDP(I)
ISN 0112      ZGDP = ZGDP+WG(I)*ZDP(I)
ISN 0113      2020 CONTINUE
ISN 0114      XGDP = XGDP/MTOT
ISN 0115      YGDP = YGDP/MTOT
ISN 0116      ZGDP = ZGDP/MTOT
ISN 0117      PRINT 2013
ISN 0118      2013 FORMAT(/ 1X, 'VEHICLE CG POSITION')
ISN 0119      PRINT 2012,XGDP,YGDP,ZGDP
ISN 0120      2012 FORMAT(1X,'X (FS) = ',1PE12.5 /
ISN 0121      1 1X,'Y (BL) = ',1PE12.5 /
ISN 0122      1 1X,'Z (WL) = ',1PE12.5)
ISN 0123
ISN 0124      C
ISN 0125      C CALCULATE VECTOR COMPONENTS FROM MASS I TO NODE POINT M
ISN 0126      C FOR ALL NNP NODE POINTS.
ISN 0127      C

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ISN 0122      IF(MNP.EQ.0) GO TO 2051
ISN 0124      DO 3000 JJ=1,MNP
ISN 0125      I = INP(JJ)
ISN 0126      T1 = XDP(I)-XNDP(JJ)
ISN 0127      T2 = YDP(I)-YNDP(JJ)
ISN 0128      T3 = ZDP(I)-ZNDP(JJ)

C
C   THESE ARE IN (-) AIRPLANE AXES.  CONVERT TO BODY AXES BY
C   MULTIPLYING BY AIDP TRANSPOSE.  THIS NORMALLY IS UNITY.
C
C   CALL EULER(AIDP,PHIDP(I),THEDP(I),PSIDP(I))
C   RX(JJ) = AIDP(1,1)*T1 + AIDP(2,1)*T2 + AIDP(3,1)*T3
C   RY(JJ) = AIDP(1,2)*T1 + AIDP(2,2)*T2 + AIDP(3,2)*T3
C   RZ(JJ) = AIDP(1,3)*T1 + AIDP(2,3)*T2 + AIDP(3,3)*T3
C
C   3000 CONTINUE
C   2051 CONTINUE
C   PRINT 2014
C   2014 FORMAT(/ IX,'VEHICLE INERTIAS (IN-LB-SEC**2)')
C   XIG = 0
C   YIG = 0
C   ZIG = 0
C
C   DO 2015 I=1,NM
C   IF(INDR(I).NE.0) GO TO 2015
C   XARM = XDP(I) - XGDP
C   YARM = YDP(I) - YGDP
C   ZARM = ZDP(I) - ZGDP
C   GOODY1 = MGT(I)*(YARM*YARM+ZARM*ZARM)/386.
C   GOODY2 = MGT(I)*(XARM*XARM+ZARM*ZARM)/386.
C   GOODY3 = MGT(I)*(XARM*XARM+YARM*YARM)/386.
C   XIG = XIG+XI(I)+GOODY1
C   YIG = YIG+YI(I)+GOODY2
C   ZIG = ZIG+ZI(I)+GOODY3
C   IF(SYHFL6.NE.1.OR.YDP(I).EQ.0.) GO TO 2015
C   XIG = XIG+XI(I)+GOODY1
C   YIG = YIG+YI(I)+GOODY2
C   ZIG = ZIG+ZI(I)+GOODY3
C   2015 CONTINUE
C   PRINT 2016,XIG,YIG,ZIG
C   2016 FORMAT(IX,'(XX) = ',1PE11.5 / IX,'(YY) = ',1PE11.5 / IX,
C   1,'(ZZ) = ',1PE11.5)
C   DO 2022 IJ=1,NB
C   I = IG(IJ)
C   J = JG(IJ)
C   M = MG(IJ)
C   N = NG(IJ)
C   IF(M.EQ.0) GO TO 5020
C   DO 5010 JI=1,MNP
C   IF(I.EQ.INP(JI).AND.M.EQ.MNP(JI)) GO TO 5020
C   5010 CONTINUE
C   5020 IF(N.EQ.0) GO TO 5030
C   DO 5040 JJ=1,MNP
C   IF(J.EQ.INP(JJ).AND.N.EQ.MNP(JJ)) GO TO 5030

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ISN 0176      5040 CONTINUE
C
C      THE FOLLOWING CODE GETS CLTEST(IJ), WHICH IS 1 IF BEAM IJ
C      LIES ENTIRELY IN THE CENTER PLANE OF THE AIRPLANE. THIS
C      IS USED IN DERIV FOR A NUMBER OF TESTS.
C
ISN 0177      5030 CLTEST(IJ) = 0.
ISN 0178      IF (SYMF LG.NE.1.) GO TO 2022
ISN 0180      IF (YDPI(I).NE.0.OR.YDPI(J).NE.0.) GO TO 2022
C
C      BOTH MASSES ON CENTERLINE.
C
ISN 0182      IF (N.EQ.0.AND.M.EQ.0) GO TO 5000
ISN 0184      IF (N.EQ.0) GO TO 5001
ISN 0186      IF (M.EQ.0) GO TO 5002
ISN 0188      IF (YNPOP(JI).EQ.0.AND.YNPOP(JJ).EQ.0.) GO TO 5000
ISN 0190      GO TO 2022
ISN 0191      5001 IF (YNPOP(JJ).EQ.0.) GO TO 5000
ISN 0193      GO TO 2022
ISN 0194      5002 IF (YNPOP(JI).EQ.0.) GO TO 5000
ISN 0196      GO TO 2022
ISN 0197      5000 CLTEST(IJ) = 1.
ISN 0198      2022 CONTINUE
ISN 0199      IF (NIC.LE.0) RETURN
C
C      COMPUTE PREL. UNCOUPLED LOADS AND DEFLECTIONS
C
C
C      PRINT 5011
ISN 0201      5011 FORMAT(/, '1X, 'BEAM LOADS')
ISN 0202      PRINT 5012
ISN 0203      5012 FORMAT(/, '6X, 'BEAM', 19X, 'AXIAL LOAD', 19X, 'SHEAR FORCE', 22X,
ISN 0204      *      'MOMENT', 20X, 'BEAM' / 2X, 'I J I J M N', 3X, 'BUCKLING',
*      4X, 'TENSION COMPRESSION LATERAL(Y) VERTICAL(Z)', 3X,
*      'ROLL(X)', 5X, 'PITCH(Y)', 5X, 'YAW(Z)', 3X, 'I J I J M N' /
DO 2400 IJ=1,NB
ISN 0205      IF (Y(IJ).LE. ZZ(IJ)) GO TO 5013
ISN 0206      YZMIN(IJ)=ZZ(IJ)
ISN 0208      GO TO 5014
ISN 0209      5013 YZMIN(IJ)=YY(IJ)
C
C      YZMIN = MIN. CROSS SECTION AREA INERTIA
C
C      5013 CALC. FORCES AND MOMENTS
C
C      AXIAL FORCES
ISN 0211      5014 PCRFYF=4.*PI*PI*E(IJ)*Y(IJ)/(XLB(IJ)**2)
ISN 0212      PCRFZ=4.*PI*PI*E(IJ)*Z(IJ)/(XLB(IJ)**2)
ISN 0213      PTENS=STENS(MC(IJ))*AA(IJ)
ISN 0214      PCOMP=SCOMP(MC(IJ))*AA(IJ)
C
C      SHEAR FORCES
ISN 0215      FY=.67*SHEAR(MC(IJ))*AA(IJ)
ISN 0216      FZ=FY
C
C      MOMENTS
ISN 0217      IF (XIQ(IJ).NE.0.) GO TO 400
ISN 0219      THOYX = 0.
ISN 0220      GO TO 410

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ISM 0221      400 THORX=SHEAR(MC(IJ))/XIG(IJ)
ISM 0222      410 YIELD = AMINI(ACOMP(MC(IJ)),STENS(MC(IJ)))
ISM 0223      IF(Z1(IJ).NE.0.) GO TO 420
ISM 0224      BENDMY = 0.
ISM 0225      GO TO 430
ISM 0226      420 BENDMY=SYIELD*YY(IJ)/Z1(IJ)
ISM 0227      430 IF(Z2(IJ).NE.0.) GO TO 440
ISM 0228      BENDMZ = 0.
ISM 0229      GO TO 450
ISM 0230      440 BENDMZ=SYIELD*ZZ(IJ)/Z2(IJ)
ISM 0231      GO TO 450
ISM 0232      C
ISM 0233      C CHECK BEAM END CONDITIONS.
ISM 0234      450 IF(PY(IJ).EQ.0.AND.PYJ(IJ).EQ.0) GO TO 100
ISM 0235      IF(PY(IJ).EQ.0.OR.PYJ(IJ).EQ.0) GO TO 110
ISM 0236      C PINNED-PINNED.
ISM 0237      PCRY = PCRFYF/4.
ISM 0238      BENDMY = 0.
ISM 0239      FZ = 0.
ISM 0240      GO TO 120
ISM 0241      C FIXED-PINNED.
ISM 0242      110 PCRY = PCRFYF/2.
ISM 0243      GO TO 120
ISM 0244      C FIXED-FIXED
ISM 0245      100 PCRY = PCRFYF
ISM 0246      120 IF(PZ(IJ).EQ.0.AND.PZJ(IJ).EQ.0) GO TO 200
ISM 0247      IF(PZ(IJ).EQ.0.OR.PZJ(IJ).EQ.0) GO TO 210
ISM 0248      C PINNED-PINNED.
ISM 0249      PCRZ = PCRFZF/4.
ISM 0250      BENDMZ = 0.
ISM 0251      FY = 0.
ISM 0252      GO TO 220
ISM 0253      C FIXED-PINNED.
ISM 0254      210 PCRZ = PCRFZF/2.
ISM 0255      GO TO 220
ISM 0256      C FIXED-FIXED
ISM 0257      200 PCRZ = PCRFZF
ISM 0258      220 PCR(IJ) = PCRZ
ISM 0259      IF(PCRY.LT.PCRZ) PCR(IJ)=PCRY
ISM 0260      5018 PRINT 5015,(IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),PCR(IJ),PTENS,
ISM 0261      1 PCOMP,FY,FZ,THOMX,BENDMY,BENDMZ,IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ))
ISM 0262      5015 FORMAT(1X,5I3,1P8E12.4,5I3)
ISM 0263      2400 CONTINUE
ISM 0264      5050 FORMAT(/,1X,'BEAM DEFLECTIONS')
ISM 0265      PRINT 5051
ISM 0266      5051 FORMAT(/,6X,'BEAM',17X,'DEFLECTION',25X,'TRANSLATION DUE TO',23X,
ISM 0267      * 'ROTATION ABOUT',/2X,'IJ I J M N',2X,'BUCKLING',4X,
ISM 0268      * 'TENSION COMPRESSION F(Y)',7X,'F(Z)',7X,'BMIZ)',6X,
ISM 0269      * 'BM(Y)',5X,'X-AXIS Y-AXIS Z-AXIS' / )
ISM 0270      C
ISM 0271      C CALC. DEFLECTIONS
ISM 0272      C
ISM 0273      C

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134 0265      C      AXIAL DEFLECTIONS
134 0266      DO 2500 IJ=1,NB
134 0267      SYIELD = ANINI(SCOMP(MC(IJ)),STENS(MC(IJ)))
134 0268      IF(XK3(1,1,IJ).EQ.0.0) GO TO 5330
134 0269      XDEFB=PCR(IJ)/XK3(1,1,IJ)
134 0270      XDEFT=STENS(MC(IJ))*AA(IJ)/XK3(1,1,IJ)
134 0271      XDEFC=SCOMP(MC(IJ))*AA(IJ)/XK3(1,1,IJ)
134 0272      GO TO 5340
134 0273      5330 XDEFB = 0.0
134 0274      XDEFT = 0.0
134 0275      XDEFC = 0.0
134 0276      5340 CONTINUE
134 0277      C      DUE TO SHEAR FORCES
134 0278      IF(XK3(2,2,IJ).EQ.0.0) GO TO 5350
134 0279      YDSF=.67*SHEAR(MC(IJ))*AA(IJ)/XK3(2,2,IJ)
134 0280      GO TO 5360
134 0281      5350 YDSF = 0.0
134 0282      5360 IF(XK3(3,3,IJ).EQ.0.0) GO TO 5370
134 0283      ZDSF=.67*SHEAR(MC(IJ))*AA(IJ)/XK3(3,3,IJ)
134 0284      GO TO 5380
134 0285      5370 ZDSF = 0.0
134 0286      5380 CONTINUE
134 0287      C      DEF. DUE TO BEND. FORCE ((K55/DEL)*FORCE)
134 0288      IF(XK3(2,2,IJ).EQ.0.0.OR.Z2(IJ).EQ.0.0) GO TO 5390
134 0289      YHOMZ=4.*SYIELD*Z2(IJ)/(Z2(IJ)*XLB(IJ)*XK3(2,2,IJ))
134 0290      GO TO 5400
134 0291      5390 YHOMZ = 0.0
134 0292      5400 IF(XK3(3,3,IJ).EQ.0.0.OR.Z1(IJ).EQ.0.0) GO TO 5410
134 0293      ZHOMY=4.*SYIELD*Y1(IJ)/(Z1(IJ)*XLB(IJ)*XK3(3,3,IJ))
134 0294      GO TO 5420
134 0295      5410 ZHOMY = 0.0
134 0296      5420 CONTINUE
134 0297      C      TORSIONAL ROTATION
134 0298      IF(XK3(4,4,IJ).NE.0.0.AND.XIQ(IJ).NE.0.0) GO TO 5317
134 0299      ROTX=0.0
134 0300      GO TO 5318
134 0301      5317 ROTX=SHEAR(MC(IJ))/XIQ(IJ)/XK3(4,4,IJ)
134 0302      GO TO 5318
134 0303      C      BEND. ROTATION ((K33/DEL)*MOM.)
134 0304      5318 IF(XK3(5,5,IJ).EQ.0.0.OR.Z1(IJ).EQ.0.0) GO TO 5430
134 0305      ROTY=4.*SYIELD*Y1(IJ)/(Z1(IJ)*XK3(5,5,IJ))
134 0306      GO TO 5440
134 0307      5430 ROTY = 0.0
134 0308      5440 IF(XK3(6,6,IJ).EQ.0.0.OR.Z2(IJ).EQ.0.0) GO TO 5450
134 0309      ROTZ=4.*SYIELD*Z2(IJ)/(Z2(IJ)*XK3(6,6,IJ))
134 0310      GO TO 5460
134 0311      5450 ROTZ = 0.0
134 0312      5460 CONTINUE
134 0313      5319 PRINT 5319, (IJ,IG(IJ),JG(IJ),MG(IJ),NG(IJ),XDEFB,XDEFT,XDEFC,
134 0314      1 YDSF,ZDSF,YHOMZ,ZHOMY,ROTX,ROTY,ROTZ)
134 0315      5319 FORMAT(1X,5I3,1P10E11.3)
134 0316      2500 CONTINUE
134 0317      RETURN
134 0318

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END

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LEVEL 21.8 (JUN 74) OS/360 FORTRAN H DATE 79.177/14.43.10

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COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
 SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
 DATA SET D2334RSIN AT LEVEL 006 AS OF 06/25/79
 DATA SET D2332VRI AT LEVEL 005 AS OF 01/27/78
 SUBROUTINE RSIN(IMODEL,ICASE,IMSEC)

13M 0002	C	IMPLICIT REAL*8(A-H,O-Z)	00000010
	C	REAL*8 KUN, MODEL, IMODEL, KEI, KETOTL	00000020
	C	REAL*4 XKS, XXI, XKR, ENGSMT	00000030
	C	INTEGER*4 TITLE(40),UNIT,CASE,HEADER(24),BPL(100,3)	00000040
	C	INTEGER*2 FL26I(150),FL26J(150),FL35I(150),FL35J(150)	00000050
13M 0003		COMMON/DEIN/ XKBAR,XPBAR,YNBAR,ZNBAR,ZPBAR,VOLENZ(5,3),	00000060
13M 0004		1 FHAXN(900),HEX(80),HEY(80),HEZ(80),ALIFT(80),VHAXN(900),VHAXNI(900),	00000070
13M 0005		2 FHAXNI(900),XKS(2700),XKR(2700),NLSFLG(900),CHUG(180),	00000080
13M 0006		3 HVP	00000090
13M 0007		COMMON/DEPR/ XDOTAP,YDOTAP,ZDOTAP,DLVOL(5,3),FRD(150,4),	00000100
13M 0008		1 FRD(150,4),SUMDI(6,150),FINTI(6,150),VEEN(2,150)	00000110
13M 0009		COMMON/ENERGY/ XPCT(80),XETOT(80),XETOTO(80),XSE(80),XDE(80),	00000120
		1 XCE(80),XFE(80),KEI(80),PEI(80),XETOTL,KETOTL,	00000130
		2 PETOTL,SETOTL,DETOTL,CETOTL,FETOTL	00000140
		COMMON/MADE/ KFL26(150),KFL35(150),FL26I,FL26J,FL35I,FL35J,	00000150
		1 TPL(100),BPL,KPL	00000160
		COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),EE(20),GG(20),	00000170
		1 FINT(6,150),VOL(5),VZERO(5),KMATR(6,4),NVCH,INBUFF(5,8)	00000180
		COMMON/INPR/ NDRI,NSP	00000190
		COMMON	00000200
		1 XNI(80),DPX(80),OPY(80),DPZ(80),DPL(80),DPH(80),DPN(80),PIN(80),	00000210
		2 QIN(80),RIN(80),XII(80),XIZ(80),XI3(80),XI4(80),XI5(80),XI6(80),	00000220
		5 DELI(80),POLDI(80),QOLD(80),ZOLD(80),UOLD(80),VOLD(80),	00000230
		6 WOLD(80),XOLD(80),YOLD(80),ZOLD(80),PINO(80),QINO(80),RINO(80),	00000240
		7 PHIOLD(80),THEOLD(80),PSIOLD(80),	00000250
		8 XACFD(80),YACFD(80),ZACFD(80),XAFOLD(80),YAFOLD(80),ZAFOLD(80),	00000260
		9 XNPF(80),YNPF(80),ZNPF(80),XANPFO(50),YANPFO(50),ZANPFO(50),	00000270
		A TKR(200),TPEN(80),DTHALF,	00000280
		B KPBEM(4,200),KRF(900),IPEN(80),KPEN,KRCONT	00000290
		COMMON/NP0014/ NRIP	00000300
		COMMON/NP01R8/ XNP(50),YNP(50),ZNP(50),UNP(50),VNP(50),WNP(50),	00000310
		1 XNPF(50),YNPF(50),ZNPF(50),XACNPF(50),YACNPF(50),ZACNPF(50),	00000320
		2 SBUCKR(150),PCR(150)	00000330
		COMMON/PRHA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50),	00000340
			00000350
			00000360
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			00000380
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13M 0016
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1  ZACNPF(50),XIMP(80),YIMP(80),ZIMP(80),XIMP(150),YIMP(150),ZIMP(150),
2  ZIMP(150),XIMP(150),YIMP(150),ZIMP(150),XIMP(150),YIMP(150),ZIMP(150),
3  YIMP(150),ZIMP(150)
COMMON/OLEO/OLEO(20),FAO(20),FAA(20),EXP(20),YMAX(20),
1  YOLEO(20),BOLEO(20),BROLEO(20),XEXT(20),XCOHP(20),FCOUL(20),
2  ALPHAP,IGOLED(20),JGOLED(20),NGOLEO(20),NGOLEO(20),NOLEO
COMMON/CORALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),
1  Y(81),Z(81),AI(9),AJ(9),SC(40),XC(6),XK(5400),XI(80),
2  YI(80),ZI(80),XII(80),XZI(80),YZI(80),AIJ(9),BIJ(720),
3  DRI(150),DAI(720),VEE(900),NGT(80),PHI(80),THETA(80),PSI(80),
4  POUT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),
5  YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
6  XACCI(80),YACCI(80),ZACCI(80),AIDOT(9),
7  PHIIJ(150),THEIJ(150),PSIIJ(150),SUMDF(6,150),TITLE,
8  XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9  DPIN(81),DQIN(81),DRIN(81),SEIJ(150),DEIJ(150),CEIK(40),
A  CEIK(40),
B  SBARI(40),KUN(40),MAXNM,MAXIGS,MAXTBL,
C  NM,NB,I,J,IG(150),JG(150),
D  NI(900),NN(40),IJPR(150)
COMMON/CFPR/FSRNG(40,8),DELG(40)
COMMON/MACF/IBS(40),FSPOP(40),SCPI(40),JBS(40),
1  KKSPI(5,200),EXSPI(5,200),TSP(200),STEMP1(40),STEMP2(40),
2  STEMP3(40),STEMP4(40),STEMP5(6,200),KKONT
COMMON/MAPR/ ETOTTO, ENGSMT(6,200), INGSCT
COMMON/CORII/4,ND,NVBHN,NFBHN,NH1,NKM,NLB,NPH,NHTL,NPTS(50),
1  NVBM,IJPR(14),IPHOP(80),NFBM
COMMON /MAX/ IRUPSW(150), IPENSH(80), VEEBAR(900), ZINIT(80),
1  DATA UNIT/21/
C  ...FIND DESIRED CASE...
C
10 CALL OPIN(HEADER,24,UNIT,IER)
IF (IER.NE.0) STOP
CALL DATIN(MODEL ,8HMODEL ,2,UNIT,IER)
CALL DATIN(CASE ,8HCASE ,1,UNIT,IER)
CALL DATIN(MSEC ,8HMSEC ,1,UNIT,IER)
IF ( (MODEL.EQ.IMODEL) .AND. (CASE.EQ.ICASE)
1  .AND. (MSEC.EQ.IMSEC) ) GO TO 20
CALL CLSIN(UNIT,IER)
IF (IER.NE.0) STOP
GO TO 10
C  ...RETRIEVE VARIABLES...
C
20 CALL DATIN(TIME ,8HTIME ,2,UNIT,IER)
C  ...INDICES...
C
CALL DATIN(KRCONT ,8HKRCONT ,1,UNIT,IER)
CALL DATIN(KPEN ,8HKPEN ,1,UNIT,IER)
CALL DATIN(KKONT ,8HKKONT ,1,UNIT,IER)
CALL DATIN(KPL ,8HKPL ,1,UNIT,IER)

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1304 0044  ...ARRAYS...
1304 0045  N12 = 2*N1
1304 0046  CALL DATIN(P ,8HP ,N12,UNIT,IER)
1304 0047  CALL DATIN(Q ,8HQ ,N12,UNIT,IER)
1304 0048  CALL DATIN(R ,8HR ,N12,UNIT,IER)
1304 0049  CALL DATIN(U ,8HU ,N12,UNIT,IER)
1304 0050  CALL DATIN(V ,8HV ,N12,UNIT,IER)
1304 0051  CALL DATIN(W ,8HW ,N12,UNIT,IER)
1304 0052  CALL DATIN(X ,8HX ,N12,UNIT,IER)
1304 0053  CALL DATIN(Y ,8HY ,N12,UNIT,IER)
1304 0054  CALL DATIN(Z ,8HZ ,N12,UNIT,IER)
1304 0055  CALL DATIN(PHI ,8PHI ,N12,UNIT,IER)
1304 0056  CALL DATIN(THETA ,8THETA ,N12,UNIT,IER)
1304 0057  CALL DATIN(PSI ,8PSI ,N12,UNIT,IER)
1304 0058  CALL DATIN(PDOT ,8PDOT ,N12,UNIT,IER)
1304 0059  CALL DATIN(QDOT ,8QDOT ,N12,UNIT,IER)
1304 0060  CALL DATIN(RDOT ,8RDOT ,N12,UNIT,IER)
1304 0061  CALL DATIN(UDOT ,8UDOT ,N12,UNIT,IER)
1304 0062  CALL DATIN(VDOT ,8VDOT ,N12,UNIT,IER)
1304 0063  CALL DATIN(WDOT ,8WDOT ,N12,UNIT,IER)
1304 0064  CALL DATIN(XDOT ,8XDOT ,N12,UNIT,IER)
1304 0065  CALL DATIN(YDOT ,8YDOT ,N12,UNIT,IER)
1304 0066  CALL DATIN(ZDOT ,8ZDOT ,N12,UNIT,IER)
1304 0067  CALL DATIN(PHIDOT ,8PHIDOT ,N12,UNIT,IER)
1304 0068  CALL DATIN(THEDOT ,8THEDOT ,N12,UNIT,IER)
1304 0069  CALL DATIN(PSIDOT ,8PSIDOT ,N12,UNIT,IER)
1304 0070  CALL DATIN(POLD ,8POLD ,N12,UNIT,IER)
1304 0071  CALL DATIN(ROLD ,8ROLD ,N12,UNIT,IER)
1304 0072  CALL DATIN(UOLD ,8UOLD ,N12,UNIT,IER)
1304 0073  CALL DATIN(VOLD ,8VOLD ,N12,UNIT,IER)
1304 0074  CALL DATIN(WOLD ,8WOLD ,N12,UNIT,IER)
1304 0075  CALL DATIN(XOLD ,8XOLD ,N12,UNIT,IER)
1304 0076  CALL DATIN(YOLD ,8YOLD ,N12,UNIT,IER)
1304 0077  CALL DATIN(ZOLD ,8ZOLD ,N12,UNIT,IER)
1304 0078  CALL DATIN(PHIOLD ,8PHIOLD ,N12,UNIT,IER)
1304 0079  CALL DATIN(THOLD ,8THOLD ,N12,UNIT,IER)
1304 0080  CALL DATIN(PSIOLD ,8PSIOLD ,N12,UNIT,IER)
1304 0081  CALL DATIN(PDX ,8PDX ,N12,UNIT,IER)
1304 0082  CALL DATIN(DY ,8DY ,N12,UNIT,IER)
1304 0083  CALL DATIN(DZ ,8DZ ,N12,UNIT,IER)
1304 0084  CALL DATIN(XACC ,8XACC ,N12,UNIT,IER)
1304 0085  CALL DATIN(YACC ,8YACC ,N12,UNIT,IER)
1304 0086  CALL DATIN(ZACC ,8ZACC ,N12,UNIT,IER)
1304 0087  CALL DATIN(XACF ,8XACF ,N12,UNIT,IER)
1304 0088  CALL DATIN(YACF ,8YACF ,N12,UNIT,IER)
1304 0089  CALL DATIN(ZACF ,8ZACF ,N12,UNIT,IER)
1304 0090  CALL DATIN(XACFD ,8XACFD ,N12,UNIT,IER)
1304 0091  CALL DATIN(YACFD ,8YACFD ,N12,UNIT,IER)
1304 0092  CALL DATIN(ZACFD ,8ZACFD ,N12,UNIT,IER)
1304 0093  CALL DATIN(XAFOLD ,8XAFOLD ,N12,UNIT,IER)

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1300 0074	CALL DATIN(YAFOLD,8HYAFOLD	,NM2,UNIT,IER)	00001470
1300 0075	CALL DATIN(ZAFOLD,8HZAFOLD	,NM2,UNIT,IER)	00001480
1300 0076	CALL DATIN(XIMP,8HXIMP	,NM2,UNIT,IER)	00001490
1300 0077	CALL DATIN(YIMP,8HYIMP	,NM2,UNIT,IER)	00001500
1300 0078	CALL DATIN(ZIMP,8HZIMP	,NM2,UNIT,IER)	00001510
1300 0079	CALL DATIN(XIMPOL,8HXIMPOL	,NM2,UNIT,IER)	00001520
1300 0100	CALL DATIN(YIMPOL,8HYIMPOL	,NM2,UNIT,IER)	00001530
1300 0101	CALL DATIN(ZIMPOL,8HZIMPOL	,NM2,UNIT,IER)	00001540
1300 0102	CALL DATIN(ZINIT,8HZINIT	,NM2,UNIT,IER)	00001550
1300 0103	CALL DATIN(PINO,8HPINO	,NM2,UNIT,IER)	00001560
1300 0104	CALL DATIN(QINO,8HQINO	,NM2,UNIT,IER)	00001570
1300 0105	CALL DATIN(RINO,8HRINO	,NM2,UNIT,IER)	00001580
1300 0106	CALL DATIN(OPIN,8HDPIN	,NM2,UNIT,IER)	00001590
1300 0107	CALL DATIN(DQIN,8HDQIN	,NM2,UNIT,IER)	00001600
1300 0108	CALL DATIN(ORIN,8HQRIN	,NM2,UNIT,IER)	00001610
1300 0109	CALL DATIN(PIN,8HPIN	,NM2,UNIT,IER)	00001620
1300 0110	CALL DATIN(QIN,8HQIN	,NM2,UNIT,IER)	00001630
1300 0111	CALL DATIN(KEI,8HKEI	,NM2,UNIT,IER)	00001640
1300 0112	CALL DATIN(PEI,8HPEI	,NM2,UNIT,IER)	00001650
1300 0113	CALL DATIN(XSE,8HXSE	,NM2,UNIT,IER)	00001660
1300 0114	CALL DATIN(XOE,8HXOE	,NM2,UNIT,IER)	00001670
1300 0115	CALL DATIN(XCE,8HXC	,NM2,UNIT,IER)	00001680
1300 0116	CALL DATIN(XFE,8HXFE	,NM2,UNIT,IER)	00001690
1300 0117	CALL DATIN(XETOT,8HXETOT	,NM2,UNIT,IER)	00001700
1300 0118	CALL DATIN(XPCT,8HXPCT	,NM2,UNIT,IER)	00001710
1300 0119	CALL DATIN(XETOTO,8HXETOTO	,NM2,UNIT,IER)	00001720
1300 0120	NM9 = 9*2*NM		00001730
1300 0121	CALL DATIN(BIJ,8HBIJ	,NM9,UNIT,IER)	00001740
1300 0122	CALL DATIN(IPENSW,8HIPENSW	,NM1,UNIT,IER)	00001750
1300 0123			00001760
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1300 0124	NMP2 = 2*NM	
1300 0125	CALL DATIN(XNP,8HXP	,NMP2,UNIT,IER)
1300 0126	CALL DATIN(YNP,8HYNP	,NMP2,UNIT,IER)
1300 0127	CALL DATIN(ZNP,8HZN	,NMP2,UNIT,IER)
1300 0128	CALL DATIN(XONP,8HXONP	,NMP2,UNIT,IER)
1300 0129	CALL DATIN(YONP,8HYONP	,NMP2,UNIT,IER)
1300 0130	CALL DATIN(ZONP,8HZONP	,NMP2,UNIT,IER)
1300 0131	CALL DATIN(XNP,8HXP	,NMP2,UNIT,IER)
1300 0132	CALL DATIN(YNP,8HYNP	,NMP2,UNIT,IER)
1300 0133	CALL DATIN(ZNP,8HZN	,NMP2,UNIT,IER)
1300 0134	CALL DATIN(XACNP,8HXACNP	,NMP2,UNIT,IER)
1300 0135	CALL DATIN(YACNP,8HYACNP	,NMP2,UNIT,IER)
1300 0136	CALL DATIN(ZACNP,8HZACNP	,NMP2,UNIT,IER)
1300 0137	CALL DATIN(XACNPF,8HXACNPF	,NMP2,UNIT,IER)
1300 0138	CALL DATIN(YACNPF,8HYACNPF	,NMP2,UNIT,IER)
1300 0139	CALL DATIN(ZACNPF,8HZACNPF	,NMP2,UNIT,IER)
1300 0140	CALL DATIN(XNPF,8HXNPF	,NMP2,UNIT,IER)
1300 0141	CALL DATIN(YNPF,8HYNPF	,NMP2,UNIT,IER)
1300 0142	CALL DATIN(ZNPF,8HZNPF	,NMP2,UNIT,IER)
1300 0143	CALL DATIN(XANPFO,8XANPFO	,NMP2,UNIT,IER)

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1300 0144 CALL DATINIYANPFO,8HYANPFO ,NNP2,UNIT,IER)
1300 0145 CALL DATINIZANPFO,8HZANPFO ,NNP2,UNIT,IER)
1300 0146 CALL DATINIXIMPUP,8HXIMPUP ,NNP2,UNIT,IER)
1300 0147 CALL DATINIYIMPUP,8HYIMPUP ,NNP2,UNIT,IER)
1300 0148 CALL DATINIZIMPUP,8HZIMPUP ,NNP2,UNIT,IER)
1300 0149 CALL DATINIXIMPPL,8HXIMPPL ,NNP2,UNIT,IER)
1300 0150 CALL DATINIYIMPPL,8HYIMPPL ,NNP2,UNIT,IER)
1300 0151 CALL DATINIZIMPPL,8HZIMPPL ,NNP2,UNIT,IER)

1300 0152 NB2 = 2*NB
1300 0153 CALL DATINIKFL35 ,8HKFL35 ,NB,UNIT,IER)
1300 0154 CALL DATINIKFL26 ,8HKFL26 ,NB,UNIT,IER)
1300 0155 CALL DATINIFL26J ,8HFL26J ,NB,UNIT,IER)
1300 0156 CALL DATINIFL26J ,8HFL26J ,NB,UNIT,IER)
1300 0157 CALL DATINIFL35I ,8HFL35I ,NB,UNIT,IER)
1300 0158 CALL DATINIFL35J ,8HFL35J ,NB,UNIT,IER)
1300 0159 CALL DATINISEIJ ,8HSEIJ ,NB,UNIT,IER)
1300 0160 CALL DATINIDEIJ ,8HDEIJ ,NB,UNIT,IER)
1300 0161 CALL DATINIRUPSM,8HIRUPSM ,NB,UNIT,IER)
1300 0162 CALL DATINOPHIJ,8DPHIJ ,NB,UNIT,IER)
1300 0163 CALL DATINPHIJ ,8PHIJ ,NB,UNIT,IER)
1300 0164 CALL DATINTHEIJ ,8HTHEIJ ,NB,UNIT,IER)
1300 0165 CALL DATINPSIJ ,8HPSIJ ,NB,UNIT,IER)
1300 0166 CALL DATINSBUCKR,8HSBUCKR ,NB,UNIT,IER)
1300 0167 CALL DATINDRI ,8HDRI ,NB,UNIT,IER)
1300 0168 CALL DATINFUB ,8HFUB ,NB,UNIT,IER)
1300 0169 NB4 = 2*2*NB
1300 0170 CALL DATINVEEN (1,1),8HVEEN ,NB4,UNIT,IER)
1300 0171 NB12 = 2*6*NB
1300 0172 CALL DATINSUMDF (1,1),8HSUMDF ,NB12,UNIT,IER)
1300 0173 CALL DATINFINT (1,1),8HFINT ,NB12,UNIT,IER)
1300 0174 CALL DATINSUMDFI(1,1),8HSUMDFI ,NB12,UNIT,IER)
1300 0175 CALL DATINFINTI (1,1),8HFINTI ,NB12,UNIT,IER)
1300 0176 NB10 = 2*9*NB
1300 0177 CALL DATINVEEBAR,8HVEEBAR ,NB10,UNIT,IER)
1300 0178 NB6 = 6*NB
1300 0179 NB3 = 3*NB
1300 0180 NB12 = 6*2*NB
1300 0181 CALL DATININI ,8HNI ,NB3,UNIT,IER)
1300 0182 CALL DATINIVEE ,8HVEE ,NB12,UNIT,IER)
1300 0183 CALL DATINIKFLAG,8HKFLAG ,NB6,UNIT,IER)
1300 0184 NOL2=2*NHOLEO
1300 0185 CALL DATINIOLEO ,8HYOLEO ,NOL2,UNIT,IER)
1300 0186 DO 100 K = 1,4
1300 0187 CALL DATIN(FRD (1,K),8HFRD ,NB2,UNIT,IER)
1300 0188 CALL DATIN(FRS (1,K),8HFRS ,NB2,UNIT,IER)
1300 0189 100 CONTINUE
1300 0190 NLI = NLB/2 + MOD(NLB,2)
1300 0191 CALL DATINICHUG ,8HCHUG ,NLI,UNIT,IER)

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      KR2 = 2*KRCONT
      CALL DATINI(TKR ,8HTRK ,KR2,UNIT,IER)
      KR4 = 4*KRCONT
      CALL DATINI(KRBEAM(1,1),8HKRBEAM ,KR4,UNIT,IER)
      CALL DATINI(IPEN ,8HIPEN ,KPEN,UNIT,IER)
      KPEN2 = 2*KPEN
      CALL DATINI(IPEN ,8HTPEN ,KPEN2,UNIT,IER)
      KPL2=2*KPL
      CALL DATINI(TPL ,8HTPL ,KPL2,UNIT,IER)
      DO 120 K=1,3
      CALL DATINI(BPL(1,K),8HBPL ,KPL,UNIT,IER)
120 CONTINUE

      KK2=2*KKONT
      CALL DATINI(TSP ,8HTSP ,KK2,UNIT,IER)
      KK5=5*KKONT
      CALL DATINI(KKSP(1,1),8HKKSP ,KK5,UNIT,IER)
      KK52=5*2*KKONT
      CALL DATINI(EXSP(1,1),8HEXSP ,KK52,UNIT,IER)
      NSP2 = 2*NSP
      NS2 = NSP/2 + MOD(NSP,2)
      CALL DATINI(DELG ,8HDELG ,NSP2,UNIT,IER)
      CALL DATINI(IRS ,8HIRS ,NS2,UNIT,IER)
      CALL DATINI(JBS ,8HJBS ,NS2,UNIT,IER)
      CALL DATINI(SBAR ,8HSBAR ,NSP2,UNIT,IER)
      CALL DATINI(FSFBAR,8HFSFBAR ,NSP2,UNIT,IER)
      CALL DATINI(FSOP ,8HFSOP ,NSP2,UNIT,IER)
      CALL DATINI(SCP ,8HSCP ,NSP2,UNIT,IER)
      CALL DATINI(STEMP1,8HSTEMP1 ,NSP2,UNIT,IER)
      CALL DATINI(STEMP2,8HSTEMP2 ,NSP2,UNIT,IER)
      CALL DATINI(STEMP3,8HSTEMP3 ,NSP2,UNIT,IER)
      CALL DATINI(STEMP4,8HSTEMP4 ,NSP2,UNIT,IER)
      CALL DATINI(STEMP5,8HSTEMP5 ,NSP2,UNIT,IER)
      CALL DATINI(KUN ,8HKN ,NS2,UNIT,IER)
      CALL DATINI(CEIK ,8HCEIK ,NSP2,UNIT,IER)
      CALL DATINI(CEIKF ,8HCEIKF ,NSP2,UNIT,IER)
      CALL DATINI(SC ,8HSC ,NSP2,UNIT,IER)
      CALL DATINI(KUN ,8HKUN ,NSP2,UNIT,IER)
      DO 200 K=1,8
      CALL DATINI(FSPRG(1,K),8HFSPRG ,NSP2,UNIT,IER)
200 CONTINUE
      NVCH2 = 2*NVCH
      CALL DATINI(VOL ,8HVOL ,NVCH2,UNIT,IER)
      DO 300 K = 1,3
      CALL DATINI(DVOL (1,K),8HDVOL ,NVCH2,UNIT,IER)
300 CONTINUE

      CALL DATINI(XDOTAP,8HXDOTAP ,2,UNIT,IER)

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AD-A055 898

LOCKHEED-CALIFORNIA CO BURBANK

F/G 1/2

GENERAL AVIATION AIRPLANE STRUCTURAL CRASHWORTHINESS USER'S MAN--ETC(U)

FEB 78 M A GAMON

DOT-FA75WA-3707

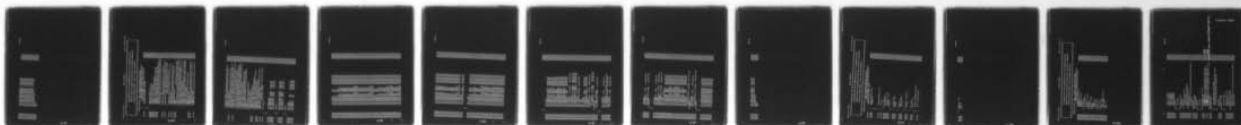
UNCLASSIFIED

LR-28307-VOL-1

FAA/RD-77/189-VOL-1

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CALL DATIN(YDOTAP,8HYDOTAP ,2,UNIT,IER)
CALL DATIN(ZDOTAP,8HZDOTAP ,2,UNIT,IER)
CALL DATIN(ETOTTO,8HETOTTO ,2,UNIT,IER)
CALL DATIN(XETOTL,8HXETOTL ,2,UNIT,IER)
CALL DATIN(KETOTL,8HKETOTL ,2,UNIT,IER)
CALL DATIN(PETOTL,8HPETOTL ,2,UNIT,IER)
CALL DATIN(SETOTL,8HSETOTL ,2,UNIT,IER)
CALL DATIN(DETOTL,8HDETOTL ,2,UNIT,IER)
CALL DATIN(CETOTL,8HCETOTL ,2,UNIT,IER)
CALL DATIN(FETOTL,8HFETOTL ,2,UNIT,IER)
CALL DATIN(INGSCT,8HINGSCT ,1,UNIT,IER)
CALL CLSIN(UNIT,IER)
RETURN
END

ISN 0238
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*****
*
* THIS DOCUMENT SHALL NOT BE REPRODUCED NOR SHALL THE INFORMATION CONTAINED
*
* THEREIN BE USED BY OR DISCLOSED TO OTHERS EXCEPT AS EXPRESSLY AUTHORIZED BY
*
* LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.
*
*****
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*
* COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
* SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,ID,XREF
* DATA SET D2334RSOUT AT LEVEL 006 AS OF 06/25/79
* DATA SET D2332VRO AT LEVEL 005 AS OF 01/27/78
* SUBROUTINE RSOUT(MODEL,CASE,MSEC)
*
*****
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IMPLICIT REAL*(A-H,O-Z)

REAL*8 KUN, MODEL, KEI, KETOTL

REAL*4 XKS, XKI, XKR, ENGSMT

INTEGER*4 TITLE(40),UNIT,CASE,BPL(100,3)

INTEGER*2 FL26I(150),FL26J(150),FL35I(150),FL35J(150)

COMMON/DEIN/ XNBAR,XPBAR,YNBAR,YPBAR,ZNBAR,ZPBAR,VOLENZ(5,3),

1 FHAXI(900),HEX(80),HEY(80),HEZI(80),ALIFT(80),VHAXI(900),VHAXN(900),

2 FHAXN(900),XKS(2700),XKI(2700),XKR(2700),NLSFLG(900),CHUG(180),

3 MYP

COMMON/DEPR/ XDOTAP,YDOTAP,ZDOTAP,DLVOL(5,3),FRDI(150,4),

1 FRS(150,4),SURDFI(6,150),FINTI(6,150),VEENI(2,150)

COMMON/ENERGY/ XPECT(80),XETOT(80),XETOTO(80),XSE(80),XDEI(80),

1 XCE(80),XFEI(80),KEI(80),PEI(80),XETOTL,KETOTL,

2 PETOTL,SETOTL,DETOTL,CETOTL,FETOTL

COMMON/MADE/ KFL26(150),KFL35(150),FL26I,FL26J,FL35I,FL35J,

1 TPL(100),BPL,KPL

COMMON/DINICP/ STENS(20),SCOMP(20),SHEAR(20),EE(20),GG(20),

1 FINTI(6,150),VOL(5),VZERO(5),KHATRI(6,4),NVCH,INBUFF(5,8)

COMMON/INPR/ NDRI,NSP

COMMON

1 XN(80),DPX(80),DPY(80),DPZ(80),DPL(80),DPH(80),DPN(80),PINI(80),

2 QIN(80),RINI(80),XII(80),XII(80),XII(80),XII(80),XII(80),XII(80),

5 DELI(80),POLDI(80),ROLDI(80),ROLDI(80),UOLDI(80),VOLDI(80),

6 WOLDI(80),XOLDI(80),YOLDI(80),ZOLDI(80),PINO(80),QINO(80),RINO(80),

7 PHIOLD(80),THEOLD(80),PSIOLD(80),

8 XACFI(80),YACFI(80),ZACFI(80),XAFOLD(80),YAFOLD(80),ZAFOLD(80),

9 XNPFDI(50),YNPFDI(50),ZNPFDI(50),XANPFOI(50),YANPFOI(50),ZANPFOI(50),

A TKR(200),TPEN(80),DTHALF,

B KRBEAM(4,200),KRFAG(900),IPENI(80),KPEN,KRCONT

COMMON/NP0014/ NNP

COMMON/NP01R8/ NNP

1 XDNPI(50),YDNPI(50),ZDNPI(50),XACNPI(50),YACNPI(50),ZACNPI(50),

2 SBUCKR(150),PCR(150)

COMMON/PRHA/ XACF(80),YACF(80),ZACF(80),XACNPF(50),YACNPF(50),

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1 ZACNPF(50),XIMP(80),YIMP(80),ZIMP(80),XIMP(50),YIMP(50),ZIMP(50),
2 ZIMP(50),XIMP(80),YIMP(80),ZIMP(80),XIMP(50),YIMP(50),ZIMP(50),
3 YIMP(50),ZIMP(50)
COMMON/OLED/OLED(20),FAO(20),FAA(20),EXPOLE(20),YMAX(20),
1 YOLED(20),BOLE(20),BOLE(20),XEXT(20),XCOMP(20),FCOUL(20),
2 ALPHAP,IGOLE(20),JGOLE(20),NGOLE(20),NGOLE(20),NGOLE
COMMON/COHALL/ C(6,150),P(80),Q(80),R(80),U(80),V(80),W(80),X(81),
1 Y(81),Z(81),AI(9),AJ(9),SC(40),XC(16),XK(5400),XI(80),
2 YI(80),ZI(80),XI(80),XZI(80),YZI(80),AIJ(9),BIJ(720),
3 DRII(150),OAI(720),VEE(900),WGT(80),PHI(80),THETA(80),PSI(80),
4 PDOT(80),QDOT(80),RDOT(80),UDOT(80),VDOT(80),WDOT(80),XDOT(80),
5 YDOT(80),ZDOT(80),PHIDOT(80),THEDOT(80),PSIDOT(80),TIME,DELTAT,
6 YACCI(80),YACCI(80),ZACCI(80),AIDOT(9),
7 PHIIJ(150),THEIJ(150),PSIIJ(150),SUMOF(6,150),TITLE,
8 XLBAR(40),FSPBAR(40),VEEDOT(3,3),DX(81),DY(81),DZ(81),
9 DPINI(81),DQIN(81),DRINI(81),SEIJ(150),DEIJ(150),CEIK(40),
A CEIKF(40),
B SBAR(40),KUNI(40),MAXNM,MAXIGS,MAXTBL,
C NM,NB,I,J,I6(150),J6(150),
D NI(900),NN(40),IJPR(150)
COMMON/CFPR/FSPRG(40,8),DELG(40)
COMMON/MACF/TBSI(40),FSPOP(40),SCPI(40),JBSI(40),
1 KKSPI(5,200),EXSP(5,200),TSP(200),STEMP1(40),STEMP2(40),
2 STEMP3(40),STEMP4(40),STEMP5(40),KKONT
COMMON/MAPR/ ETOTTO, ENGSY(6,200), INGSCT
COMMON/COMH14/ND,NVBH,NFBH,NFI,NKM,NLB,NPH,NMTL,NPTS(50),
1 NVBH,IJPR(14),IPHDP(80),NFBH
COMMON /MAX/ IRUPSI(150), IPENSW(80), VEEBAR(900), ZINIT(80),
1 DPHIIJ(150), FUB(150)
DATA UNIT/21/

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CALL OPNOUT(UNIT)
CALL DATOUT(MODEL ,8HMODEL ,2,UNIT,IER)
CALL DATOUT(CASE ,8HCASE ,1,UNIT,IER)
CALL DATOUT(INSEC ,8HINSEC ,1,UNIT,IER)
CALL DATOUT(TIME ,8HTIME ,2,UNIT,IER)

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...INDICES...
CALL DATOUT(KRCONT,8HKRCONT ,1,UNIT,IER)
CALL DATOUT(KPEN ,8HKPEN ,1,UNIT,IER)
CALL DATOUT(KKONT ,8HKKONT ,1,UNIT,IER)
CALL DATOUT(KPL ,8HKPL ,1,UNIT,IER)

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...ARRAYS...
NM2 = 2*NM
CALL DATOUT(P ,8HP ,NM2,UNIT,IER)
CALL DATOUT(Q ,8HQ ,NM2,UNIT,IER)
CALL DATOUT(R ,8HR ,NM2,UNIT,IER)
CALL DATOUT(U ,8HU ,NM2,UNIT,IER)

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ISN 0041	CALL DATOUT(V	,8HV	,NH2,UNIT,IER)	00000940
ISN 0042	CALL DATOUT(W	,8HW	,NH2,UNIT,IER)	00000950
ISN 0043	CALL DATOUT(X	,8HX	,NH2,UNIT,IER)	00000960
ISN 0044	CALL DATOUT(Y	,8HY	,NH2,UNIT,IER)	00000970
ISN 0045	CALL DATOUT(Z	,8HZ	,NH2,UNIT,IER)	00000980
ISN 0046	CALL DATOUT(PHI	,8PHI	,NH2,UNIT,IER)	00000990
ISN 0047	CALL DATOUT(THETA	,8THETA	,NH2,UNIT,IER)	00001000
ISN 0048	CALL DATOUT(PSI	,8PSI	,NH2,UNIT,IER)	00001010
ISN 0049	CALL DATOUT(PDOT	,8PDOT	,NH2,UNIT,IER)	00001020
ISN 0050	CALL DATOUT(QDOT	,8QDOT	,NH2,UNIT,IER)	00001030
ISN 0051	CALL DATOUT(RDOT	,8RDOT	,NH2,UNIT,IER)	00001040
ISN 0052	CALL DATOUT(UDOT	,8UDOT	,NH2,UNIT,IER)	00001050
ISN 0053	CALL DATOUT(VDOT	,8VDOT	,NH2,UNIT,IER)	00001060
ISN 0054	CALL DATOUT(WDOT	,8WDOT	,NH2,UNIT,IER)	00001070
ISN 0055	CALL DATOUT(XDOT	,8XDOT	,NH2,UNIT,IER)	00001080
ISN 0056	CALL DATOUT(YDOT	,8YDOT	,NH2,UNIT,IER)	00001090
ISN 0057	CALL DATOUT(ZDOT	,8ZDOT	,NH2,UNIT,IER)	00001100
ISN 0058	CALL DATOUT(PHIDOT	,8PHIDOT	,NH2,UNIT,IER)	00001110
ISN 0059	CALL DATOUT(THEDOT	,8THEDOT	,NH2,UNIT,IER)	00001120
ISN 0060	CALL DATOUT(PSIDOT	,8PSIDOT	,NH2,UNIT,IER)	00001130
ISN 0061	CALL DATOUT(POLD	,8POLD	,NH2,UNIT,IER)	00001140
ISN 0062	CALL DATOUT(GOLD	,8GOLD	,NH2,UNIT,IER)	00001150
ISN 0063	CALL DATOUT(ROLD	,8ROLD	,NH2,UNIT,IER)	00001160
ISN 0064	CALL DATOUT(UOLD	,8UOLD	,NH2,UNIT,IER)	00001170
ISN 0065	CALL DATOUT(VOLD	,8VOLD	,NH2,UNIT,IER)	00001180
ISN 0066	CALL DATOUT(WOLD	,8WOLD	,NH2,UNIT,IER)	00001190
ISN 0067	CALL DATOUT(XOLD	,8XOLD	,NH2,UNIT,IER)	00001200
ISN 0068	CALL DATOUT(YOLD	,8YOLD	,NH2,UNIT,IER)	00001210
ISN 0069	CALL DATOUT(ZOLD	,8ZOLD	,NH2,UNIT,IER)	00001220
ISN 0070	CALL DATOUT(PHIOLD	,8PHIOLD	,NH2,UNIT,IER)	00001230
ISN 0071	CALL DATOUT(THOLD	,8THOLD	,NH2,UNIT,IER)	00001240
ISN 0072	CALL DATOUT(PSIOLD	,8PSIOLD	,NH2,UNIT,IER)	00001250
ISN 0073	CALL DATOUT(DX	,8DX	,NH2,UNIT,IER)	00001260
ISN 0074	CALL DATOUT(DY	,8DY	,NH2,UNIT,IER)	00001270
ISN 0075	CALL DATOUT(DZ	,8DZ	,NH2,UNIT,IER)	00001280
ISN 0076	CALL DATOUT(XACC	,8XACC	,NH2,UNIT,IER)	00001290
ISN 0077	CALL DATOUT(YACC	,8YACC	,NH2,UNIT,IER)	00001300
ISN 0078	CALL DATOUT(ZACC	,8ZACC	,NH2,UNIT,IER)	00001310
ISN 0079	CALL DATOUT(XACF	,8XACF	,NH2,UNIT,IER)	00001320
ISN 0080	CALL DATOUT(YACF	,8YACF	,NH2,UNIT,IER)	00001330
ISN 0081	CALL DATOUT(ZACF	,8ZACF	,NH2,UNIT,IER)	00001340
ISN 0082	CALL DATOUT(XACFD	,8XACFD	,NH2,UNIT,IER)	00001350
ISN 0083	CALL DATOUT(YACFD	,8YACFD	,NH2,UNIT,IER)	00001360
ISN 0084	CALL DATOUT(ZACFD	,8ZACFD	,NH2,UNIT,IER)	00001370
ISN 0085	CALL DATOUT(XAFOLD	,8XAFOLD	,NH2,UNIT,IER)	00001380
ISN 0086	CALL DATOUT(YAFOLD	,8YAFOLD	,NH2,UNIT,IER)	00001390
ISN 0087	CALL DATOUT(ZAFOLD	,8ZAFOLD	,NH2,UNIT,IER)	00001400
ISN 0088	CALL DATOUT(XIMP	,8XIMP	,NH2,UNIT,IER)	00001410
ISN 0089	CALL DATOUT(YIMP	,8YIMP	,NH2,UNIT,IER)	00001420
ISN 0090	CALL DATOUT(ZIMP	,8ZIMP	,NH2,UNIT,IER)	00001430
ISN 0091	CALL DATOUT(XIMPOL	,8XIMPOL	,NH2,UNIT,IER)	00001440
ISN 0092	CALL DATOUT(YIMPOL	,8YIMPOL	,NH2,UNIT,IER)	00001450
ISN 0093	CALL DATOUT(ZIMPOL	,8ZIMPOL	,NH2,UNIT,IER)	00001460

ISN 0094	CALL DATOUT(ZINIT ,8HZINIT	,NH2,UNIT,IER)	00001470
ISN 0095	CALL DATOUT(PINO ,8HPINO	,NH2,UNIT,IER)	00001480
ISN 0096	CALL DATOUT(QINO ,8HQINO	,NH2,UNIT,IER)	00001490
ISN 0097	CALL DATOUT(RINO ,8HRINO	,NH2,UNIT,IER)	00001500
ISN 0098	CALL DATOUT(OPIN ,8HOPIN	,NH2,UNIT,IER)	00001510
ISN 0099	CALL DATOUT(OQIN ,8HQQIN	,NH2,UNIT,IER)	00001520
ISN 0100	CALL DATOUT(ORIN ,8HORIN	,NH2,UNIT,IER)	00001530
ISN 0101	CALL DATOUT(PIN ,8HPIN	,NH2,UNIT,IER)	00001540
ISN 0102	CALL DATOUT(QIN ,8HQIN	,NH2,UNIT,IER)	00001550
ISN 0103	CALL DATOUT(RIN ,8HRIN	,NH2,UNIT,IER)	00001560
ISN 0104	CALL DATOUT(KEI ,8HKEI	,NH2,UNIT,IER)	00001570
ISN 0105	CALL DATOUT(PEI ,8HPEI	,NH2,UNIT,IER)	00001580
ISN 0106	CALL DATOUT(XSE ,8HXSE	,NH2,UNIT,IER)	00001590
ISN 0107	CALL DATOUT(XDE ,8HXDE	,NH2,UNIT,IER)	00001600
ISN 0108	CALL DATOUT(XCE ,8HXCE	,NH2,UNIT,IER)	00001610
ISN 0109	CALL DATOUT(XFE ,8HXFE	,NH2,UNIT,IER)	00001620
ISN 0110	CALL DATOUT(XETOT ,8HXETOT	,NH2,UNIT,IER)	00001630
ISN 0111	CALL DATOUT(XPCT ,8HXPCT	,NH2,UNIT,IER)	00001640
ISN 0112	CALL DATOUT(XETOTO,8HXETOTO	,NH2,UNIT,IER)	00001650
ISN 0113	NH9 = 9*2*MM		00001660
ISN 0114	CALL DATOUT(BIJ ,8HBIJ	,NH9,UNIT,IER)	00001670
ISN 0115	CALL DATOUT(IPENSM,8HIPENSM	,NH1,UNIT,IER)	00001680
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ISN 0116	NH2 = 2*NH2		
ISN 0117	CALL DATOUT(XNP ,8HXNP	,NH2,UNIT,IER)	
ISN 0118	CALL DATOUT(YNP ,8HYNP	,NH2,UNIT,IER)	
ISN 0119	CALL DATOUT(ZNP ,8HZNP	,NH2,UNIT,IER)	
ISN 0120	CALL DATOUT(XDNP ,8HXDNP	,NH2,UNIT,IER)	
ISN 0121	CALL DATOUT(YDNP ,8HYDNP	,NH2,UNIT,IER)	
ISN 0122	CALL DATOUT(ZDNP ,8HZDNP	,NH2,UNIT,IER)	
ISN 0123	CALL DATOUT(UNP ,8HUNP	,NH2,UNIT,IER)	
ISN 0124	CALL DATOUT(VNP ,8HVNP	,NH2,UNIT,IER)	
ISN 0125	CALL DATOUT(WNP ,8HWNP	,NH2,UNIT,IER)	
ISN 0126	CALL DATOUT(XACNP,8HXACNP	,NH2,UNIT,IER)	
ISN 0127	CALL DATOUT(YACNP,8HYACNP	,NH2,UNIT,IER)	
ISN 0128	CALL DATOUT(ZACNP,8HZACNP	,NH2,UNIT,IER)	
ISN 0129	CALL DATOUT(XACNPF,8HXACNPF	,NH2,UNIT,IER)	
ISN 0130	CALL DATOUT(YACNPF,8HYACNPF	,NH2,UNIT,IER)	
ISN 0131	CALL DATOUT(ZACNPF,8HZACNPF	,NH2,UNIT,IER)	
ISN 0132	CALL DATOUT(XNPF ,8HXNPF	,NH2,UNIT,IER)	
ISN 0133	CALL DATOUT(YNPF ,8HYNPF	,NH2,UNIT,IER)	
ISN 0134	CALL DATOUT(ZNPF ,8HZNPF	,NH2,UNIT,IER)	
ISN 0135	CALL DATOUT(XANPFO,8HXANPFO	,NH2,UNIT,IER)	
ISN 0136	CALL DATOUT(YANPFO,8HYANPFO	,NH2,UNIT,IER)	
ISN 0137	CALL DATOUT(ZANPFO,8HZANPFO	,NH2,UNIT,IER)	
ISN 0138	CALL DATOUT(XIMPNP,8HXIMPNP	,NH2,UNIT,IER)	
ISN 0139	CALL DATOUT(YIMPNP,8HYIMPNP	,NH2,UNIT,IER)	
ISN 0140	CALL DATOUT(ZIMPNP,8HZIMPNP	,NH2,UNIT,IER)	
ISN 0141	CALL DATOUT(XIMPPL,8HXIMPPL	,NH2,UNIT,IER)	
ISN 0142	CALL DATOUT(YIMPPL,8HYIMPPL	,NH2,UNIT,IER)	
ISN 0143	CALL DATOUT(ZIMPPL,8HZIMPPL	,NH2,UNIT,IER)	

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NB2 = 2*NB
CALL DATOUT(KFL35 ,8HKFL35 ,NB,UNIT,IER)
CALL DATOUT(KFL26 ,8HKFL26 ,NB,UNIT,IER)
CALL DATOUT(KFL26I ,8HKFL26I ,NB,UNIT,IER)
CALL DATOUT(KFL26J ,8HKFL26J ,NB,UNIT,IER)
CALL DATOUT(KFL35I ,8HKFL35I ,NB,UNIT,IER)
CALL DATOUT(KFL35J ,8HKFL35J ,NB,UNIT,IER)
CALL DATOUT(SELJ ,8HSELJ ,NB,UNIT,IER)
CALL DATOUT(DELJ ,8HDELJ ,NB,UNIT,IER)
CALL DATOUT(IRUPSM ,8HIRUPSM ,NB,UNIT,IER)
CALL DATOUT(DPHIJ ,8HDPHIJ ,NB,UNIT,IER)
CALL DATOUT(PHIJ ,8HPHIJ ,NB,UNIT,IER)
CALL DATOUT(THIJ ,8HTHIJ ,NB,UNIT,IER)
CALL DATOUT(PSIJ ,8HPSIJ ,NB,UNIT,IER)
CALL DATOUT(SBUCKR ,8HSBUCKR ,NB,UNIT,IER)
CALL DATOUT(DRI ,8HDRI ,NB,UNIT,IER)
CALL DATOUT(FUB ,8HFUB ,NB,UNIT,IER)
NB4 = 2*2*NB
CALL DATOUT(VEEN (1,1),8HVEEN ,NB4,UNIT,IER)
NB12 = 2*6*NB
CALL DATOUT(SUMDF (1,1),8HSUMDF ,NB12,UNIT,IER)
CALL DATOUT(FINT (1,1),8HFINT ,NB12,UNIT,IER)
CALL DATOUT(SUMDFI(1,1),8HSUMDFI ,NB12,UNIT,IER)
CALL DATOUT(FINTI (1,1),8HFINTI ,NB12,UNIT,IER)
NB18 = 2*9*NB
CALL DATOUT(VEEBAR ,8HVEEBAR ,NB18,UNIT,IER)
NB3 = 3*NB
NB6 = 6*NB
NB12 = 6*2*NB
CALL DATOUT(NI ,8HNI ,NB3,UNIT,IER)
CALL DATOUT(VEE ,8HVEE ,NB12,UNIT,IER)
CALL DATOUT(KRFLAG ,8HKRFLAG ,NB6,UNIT,IER)
NOL2=2*NOL2
CALL DATOUT(YOLEO ,8HYOLEO ,NOL2,UNIT,IER)
DO 100 K = 1,4
CALL DATOUT(FRD (1,K),8HFRD ,NB2,UNIT,IER)
CALL DATOUT(FRS (1,K),8HFRS ,NB2,UNIT,IER)
100 CONTINUE
NLI = NLB/2 + MOD(NLB,2)
CALL DATOUT(CHUG ,8HCHUG ,NLI,UNIT,IER)

C C C
KR2 = 2*KRCONT
CALL DATOUT(TKR ,8HTKR ,KR2,UNIT,IER)
KR4 = 4*KRCONT
CALL DATOUT(KRBEAM(1,1),8HKRBEAM ,KR4,UNIT,IER)
CALL DATOUT(IPEN ,8HIPEN ,KPEN,UNIT,IER)
KPEN2 = 2*KPEN
CALL DATOUT(IPEN ,8HTPEN ,KPEN2,UNIT,IER)

```



```

ISM 0191 KPL2=2*KKPL
ISM 0192 CALL DATOUT(TPL ,&HTPL ,KPL2,UNIT,IER)
ISM 0193 DO 120 K=1,3
ISM 0194 CALL DATOUT(BPL(1,K),&HBPL ,KPL,UNIT,IER)
ISM 0195 120 CONTINUE
C
C
C
ISM 0196 KX2=2*KKONT
ISM 0197 CALL DATOUT(TSP ,&HTSP ,KK2,UNIT,IER)
ISM 0198 KX3=5*KKONT
ISM 0199 CALL DATOUT(KKSP(1,1),&HKKSP ,KK5,UNIT,IER)
ISM 0200 KX52=5*2*KKONT
ISM 0201 CALL DATOUT(EXSP(1,1),&HEXSP ,KK52,UNIT,IER)
ISM 0202 NSP2 = 2*NSP
ISM 0203 NSP2 = NSP/2 + MOD(NSP,2)
ISM 0204 CALL DATOUT(DELG ,&HDELG ,NSP2,UNIT,IER)
ISM 0205 CALL DATOUT(IFS ,&HIFS ,NS2,UNIT,IER)
ISM 0206 CALL DATOUT(JBS ,&HJBS ,NS2,UNIT,IER)
ISM 0207 CALL DATOUT(SBAR ,&HSBAR ,NSP2,UNIT,IER)
ISM 0208 CALL DATOUT(FSPBAR ,&HFSBAR ,NSP2,UNIT,IER)
ISM 0209 CALL DATOUT(FSPOP ,&HFSPOP ,NSP2,UNIT,IER)
ISM 0210 CALL DATOUT(SCP ,&HSCP ,NSP2,UNIT,IER)
ISM 0211 CALL DATOUT(STEMP1 ,&HSTEMP1 ,NSP2,UNIT,IER)
ISM 0212 CALL DATOUT(STEMP2 ,&HSTEMP2 ,NSP2,UNIT,IER)
ISM 0213 CALL DATOUT(STEMP3 ,&HSTEMP3 ,NSP2,UNIT,IER)
ISM 0214 CALL DATOUT(STEMP4 ,&HSTEMP4 ,NSP2,UNIT,IER)
ISM 0215 CALL DATOUT(STEMP5 ,&HSTEMP5 ,NSP2,UNIT,IER)
ISM 0216 CALL DATOUT(INN ,&HINN ,NS2,UNIT,IER)
ISM 0217 CALL DATOUT(CEIK ,&HCEIK ,NSP2,UNIT,IER)
ISM 0218 CALL DATOUT(CEIKF ,&HCEIKF ,NSP2,UNIT,IER)
ISM 0219 CALL DATOUT(SC ,&HSC ,NSP2,UNIT,IER)
ISM 0220 CALL DATOUT(KUN ,&HKUN ,NSP2,UNIT,IER)
ISM 0221 DO 200 K=1,8
ISM 0222 CALL DATOUT(FSPRING(1,K),&HFSRING ,NSP2,UNIT,IER)
ISM 0223 200 CONTINUE
ISM 0224 NVCH2 = 2*NVCH
ISM 0225 CALL DATOUT(VOL ,&HVOL ,NVCH2,UNIT,IER)
ISM 0226 DO 300 K = 1,3
ISM 0227 CALL DATOUT(OLVOL (1,K),&HOLVOL ,NVCH2,UNIT,IER)
ISM 0228 300 CONTINUE
C
C
C
ISM 0229 CALL DATOUT(XDOTAP ,&HXDOTAP ,2,UNIT,IER)
ISM 0230 CALL DATOUT(YDOTAP ,&HYDOTAP ,2,UNIT,IER)
ISM 0231 CALL DATOUT(ZDOTAP ,&HZDOTAP ,2,UNIT,IER)
ISM 0232 CALL DATOUT(ETOTTO ,&HETOTTO ,2,UNIT,IER)
ISM 0233 CALL DATOUT(XETOTL ,&HXETOTL ,2,UNIT,IER)
ISM 0234 CALL DATOUT(KETOTL ,&HKETOTL ,2,UNIT,IER)
ISM 0235 CALL DATOUT(PETOTL ,&HPETOTL ,2,UNIT,IER)
ISM 0236 CALL DATOUT(SETOTL ,&HSETOTL ,2,UNIT,IER)
ISM 0237 CALL DATOUT(DETOTL ,&HDETOTL ,2,UNIT,IER)

```


ISN 0238
ISN 0239
ISN 0240
ISN 0241
ISN 0242
ISN 0243

CALL DATOUT(CETOTL,8HCFOTL ,2,UNIT,IER)
CALL DATOUT(FETOTL,8HCFOTL ,2,UNIT,IER)
CALL DATOUT(LINGSCT,8HINGSCT ,1,UNIT,IER)
CALL CLSOUT(UNIT)
RETURN
END

00003060
00003070
00003080
00003090
00003100
00003110

LEVEL 21.8 (JUN 74)

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```

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINCENT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NOECC,LOAD,MAP,NOEDIT,1
C DATA SET D2334SHX AT LEVEL 002 AS OF 05/17/
SUBROUTINE SHELLEX(DARPAY,KEY,N)

```

IMPLICIT REAL*8(A-H,O-Z)
INTEGER*2 N

ISN 0006 IFIRST = 1

```
10 K = IFIRST - 1
DO 20 I=IFIRST, N
K = K + 1
IF(KEY(K)) 20,20,4
20 CONTINUE
```

```
DO 30 I=1, N
30 KEY(I) = -KEY(I)
RETURN
```

```
40 IFIRST = K
   TEMP = DARRAY(K)
   GO TO 60
```

```
DARRAY(K) = DARRAY(IK)
```

$$IK = KEY(K)$$

TK MUST BE COMPARED WITH IFIRST.

IF(IK - IFIRST) 50,70,50

000000010
000000015
000000020
000000025
000000030
000000040
000000050
000000060
000000070
000000080
000000090
000000100
000000110
000000120
000000130
000000140
000000150
000000160
000000170
000000180
000000190
000000200
000000210
000000220
000000230
000000240
000000250
000000260
000000270
000000280
000000290
000000300
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000000330
000000340
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000000370
000000380

PAGE 002

00000390
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C 70 DARRAY(K) = TEMP
GO TO 10
END

ISN 0023
ISN 0024
ISN 0025

A-201

LEVEL 21.6 (JUN 74)

OS/360 FORTRAN M

DATE 79.177/14.43.26

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* LOCKHEED-CALIFORNIA COMPANY, A UNIT OF LOCKHEED CORPORATION.
*

COMPILER OPTIONS - NAME= MAIN,OPT=02,LINECNT=55,SIZE=0600K,
SOURCE,BCD,NOLIST,NODECK,LOAD,MAP,NOEDIT,IO,XREF
C DATA SET D2334SHH AT LEVEL 002 AS OF 07/19/78

ISN 0002 SUBROUTINE SHELL(M,KEY,M,N)
ISN 0003 INTEGER*2 N
ISN 0004 DIMENSION KEY(1),M(1)
ISN 0005 IFIRST = 1
ISN 0006 10 K = IFIRST - 1
ISN 0007 DO 20 I=IFIRST, N
ISN 0008 K = K + 1
ISN 0009 IF(KEY(K)) 20,20,40
ISN 0010 20 CONTINUE
ISN 0011 DO 30 I=1, N
ISN 0012 30 KEY(I) = -KEY(I)
ISN 0013 RETURN
ISN 0014 40 IFIRST = K
ISN 0015 MTEMP = M(K)
ISN 0016 GO TO 60
ISN 0017 50 M(K) = M(IK)
ISN 0018 K = IK
ISN 0019 60 IK = KEY(K)
ISN 0020 KEY(K) = -IK
ISN 0021 IF(IK - IFIRST) 50,70,50
ISN 0022 70 M(K) = MTEMP
ISN 0023 GO TO 10
ISN 0024 END
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00000050
00000060
00000070
00000080
00000090
00000100
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00000210
00000220
00000230

A-202

Subroutine 'INPUT'

```

ISN 0192      PYJ(IJ) = PTEMP(3)
ISN 0193      PZJ(IJ) = PTEMP(4)
ISN 0194      SF35(IJ)=PTEMP(1)
ISN 0195      SF26(IJ)=PTEMP(2)
ISN 0196      SF35J(IJ)=PTEMP(3)
ISN 0197      SF26J(IJ)=PTEMP(4)
ISN 0198      6120 CONTINUE
C
C      CARDS 0600
C
ISN 0199      6112 DO 6111 IJ=1,NB
ISN 0200      IJUB(IJ)=0
ISN 0201      6111 DB(IJ)=0
ISN 0202      IF(NUB.EQ.0) GO TO 6110
ISN 0203      DO 6114 JI=1,NUB
ISN 0204      READ 6116,M,I,N,J,IJTEMP,DBTEMP
ISN 0205      6116 FORMAT(2(I2,I3),I5,E10.0)
ISN 0206      DO 6118 IJ=1,NB
ISN 0207      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
ISN 0208      I GO TO 6119
ISN 0210      6118 CONTINUE
ISN 0211      6119 IJUB(IJ)=IJTEMP
ISN 0212      DB(IJ)=DBTEMP
ISN 0213      6114 CONTINUE
C
C      CARD 0900
C
ISN 0214      6110 IF(NOLEO.EQ.0) GO TO 6210
ISN 0215      READ 5301,ALPHAP
ISN 0216      READ 5306,(NGOLEO(IJ),IGOLEO(IJ),NGOLEO(IJ),JGOLEO(IJ),
ISN 0217      1 EOLEO(IJ),FAO(IJ),EXPOLE(IJ),YMAX(IJ),IJ=1,NOLEO)
ISN 0218      READ 5308,(HGOLEO(IJ),IGOLEO(IJ),NGOLEO(IJ),JGOLEO(IJ),
ISN 0219      1 BOLEO(IJ),BROLEO(IJ),XKEXT(IJ),XKCOMPI(IJ),FCOUL(IJ),IJ=1,NOLEO)
ISN 0220      6210 READ 5600,DAHPC
ISN 0221      5600 FORMAT(E10.0)
C
C      DAHPC=DAHPING COEFF. FOR ALL BEAMS
C      NO STANDARD DAHPC VALUE AS OF 3/79 VALUE MUST BE INPUT
C      IF NO.NE.0 SET DESIRED CBAR TO VALUE READ IN
C
ISN 0221      CDAWI=DAHPC
ISN 0222      DO 5549 IJ=1,NB
ISN 0223      5549 CBAR(IJ) = CDUH
C
C      CARDS 0901 AND UP
C
ISN 0224      IF(ND.EQ.0) GO TO 5543
ISN 0225      DO 5544 JI=1,ND
ISN 0226      READ 5547,M,I,N,J,CDUH
ISN 0227      5547 FORMAT(2(I2,I3),E10.0)
ISN 0228      DO 5544 IJ=1,NB
ISN 0229      IF(I.EQ.IG(IJ)).AND.J.EQ.JG(IJ).AND.M.EQ.MG(IJ).AND.N.EQ.NG(IJ))
ISN 0230      1 CBAR(IJ) = CDUH

```

6211 FORMAT(2(I2,I3),E10.0)

6211

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